

Final
Treatability Study Report for the
Shallow Aquifer at the
Hadnot Point Industrial Area
Operable Unit
Camp Lejeune Marine Corps Base
Jacksonville, North Carolina



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Camp Lejeune Marine Corps kase Jacksonville, North Carolina

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Department of the Navy
Atlantic Division
Naval Facilities
Engineering Command
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Camp Lejeune Marine Corps Base Jacksonville, North Carolina



Prepared For:

Department of the Navy Atlantic Division Naval Facilities Engineering Command Norfolk, Virginia

Under the

**LANTDIV CLEAN Program** 

Comprehensive Long-Term Environmental Action Navy Reference: Contract N62470-89-D-4814

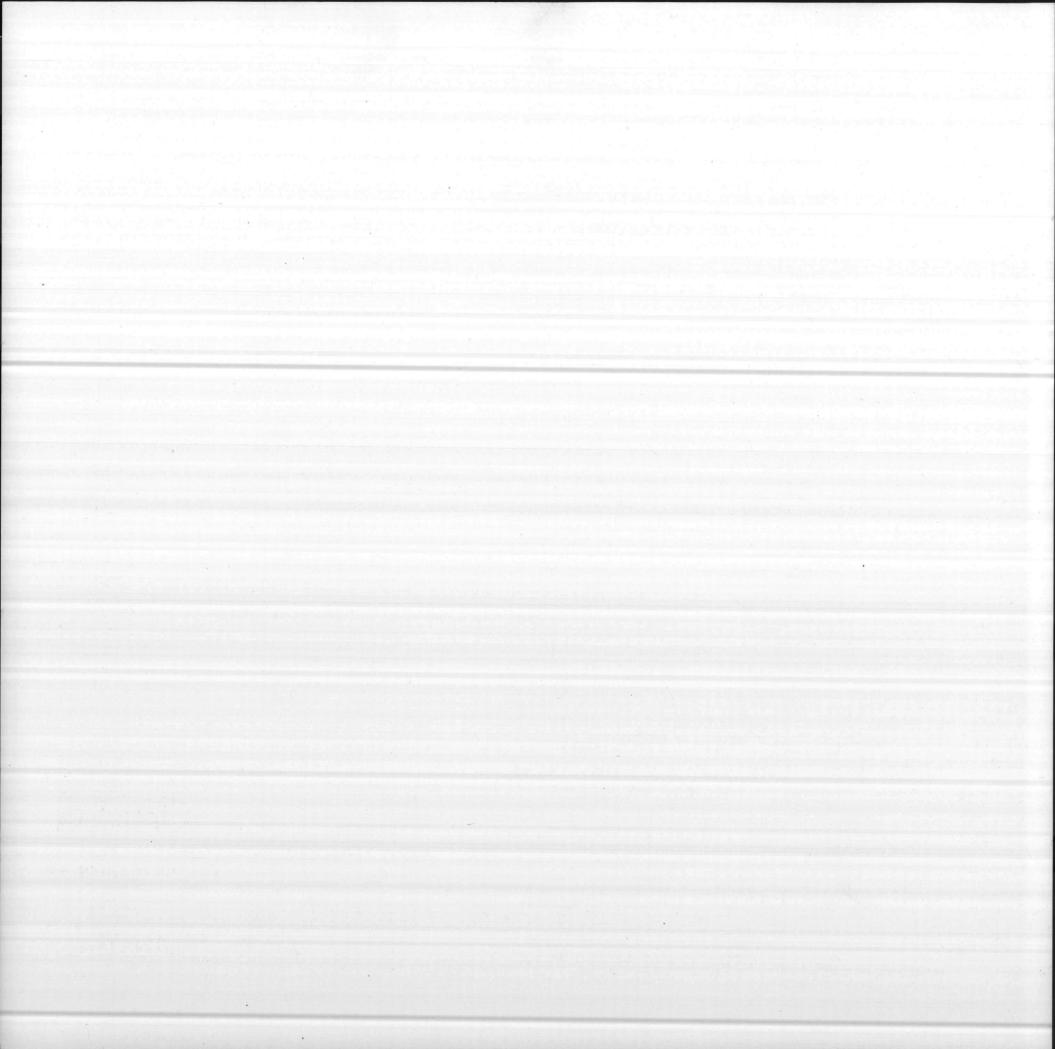
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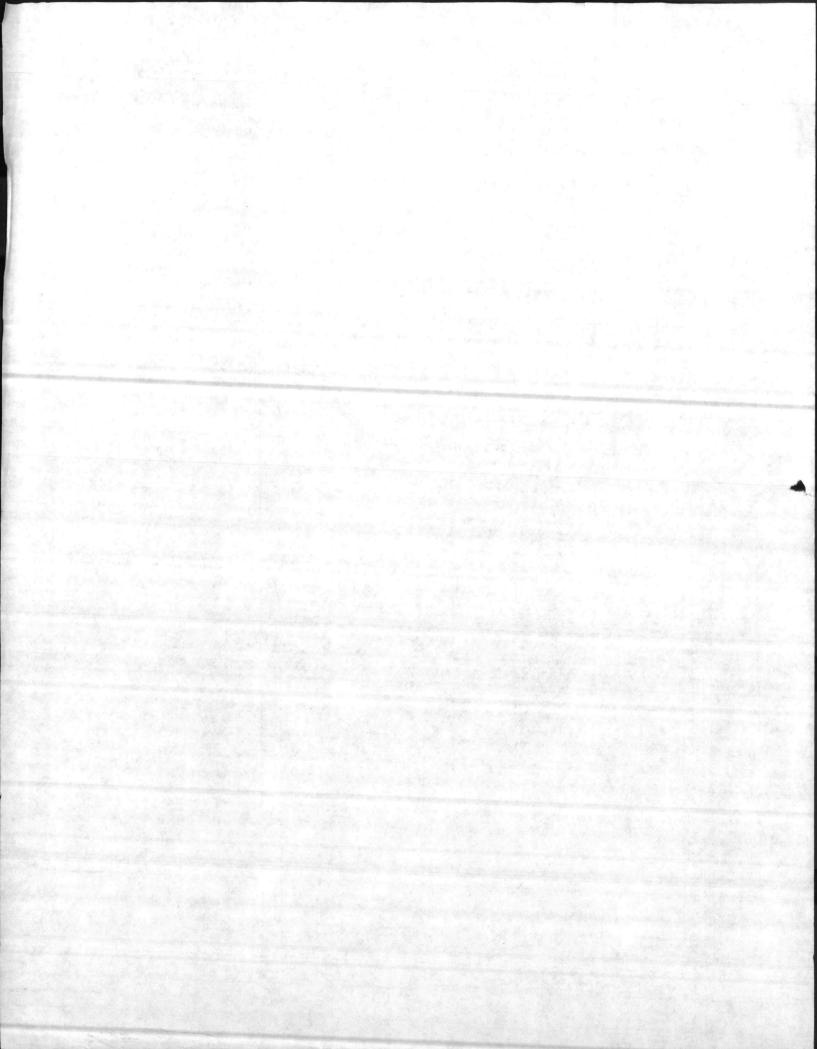


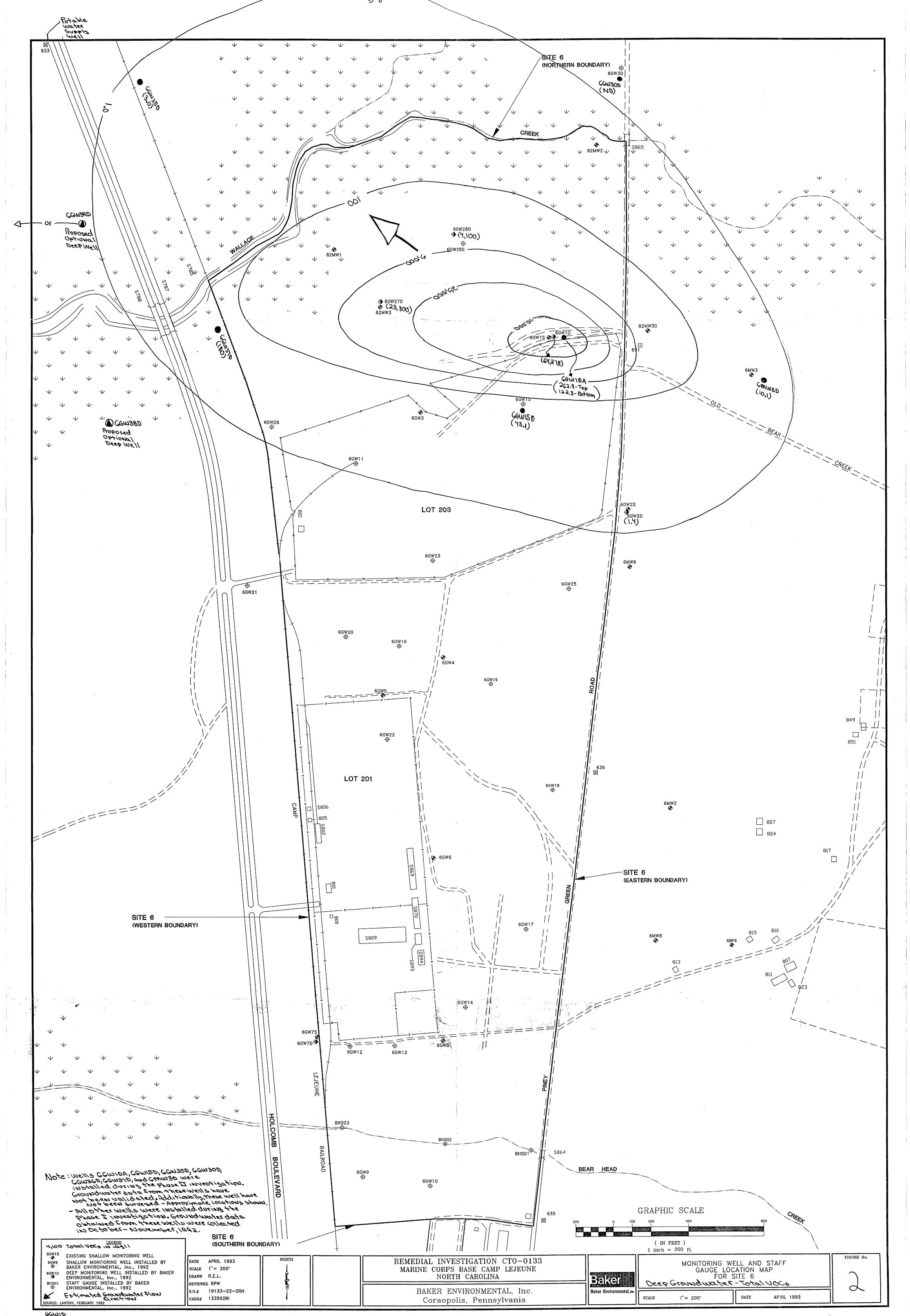






S.O. No. 19133-70-SRN FIGURE 3 Baker Subject: \_\_\_\_\_ Sheet No. \_\_\_\_\_ of \_\_\_\_ Drawing No. Computed by \_\_\_\_\_ Checked By \_\_\_\_ Cross-Sectional View of Contaminant Distribution beep mell GEWIS GGWID GGWIDA - 15.25' VOCs= 5.3 TO=25 102-1117 475, 42 = 200V TD=112.5 = 120-230 7 VOCs = 262.9 70=230' > VOC=122.3 230 CIAY 240 = Sugen





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# TREATABILITY STUDY FOR THE HADNOT POINT INDUSTRIAL AREA SHALLOW AQUIFER

MARINE CORPS BASE CAMP LEJEUNE JACKSONVILLE, NORTH CAROLINA

CONTRACT TASK ORDER 0017

Prepared For:

DEPARTMENT OF THE NAVY
ATLANTIC DIVISION
NAVAL FACILITIES
ENGINEERING COMMAND
Norfolk, Virginia

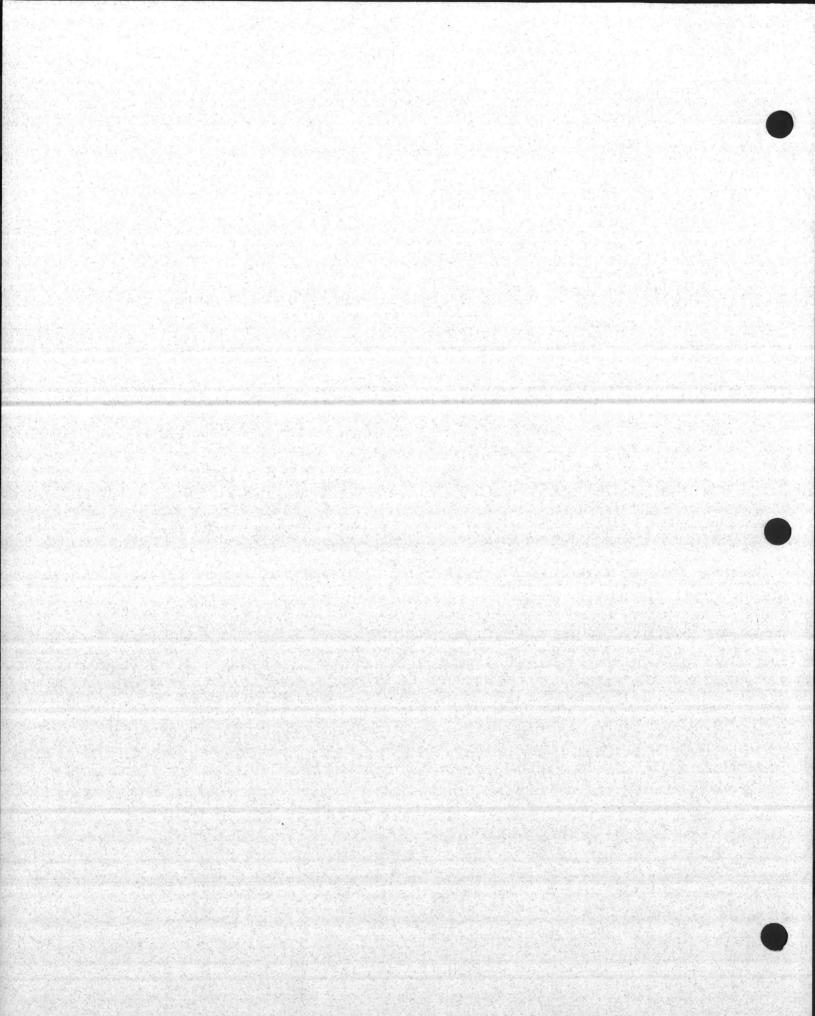
Under the:

LANTDIV CLEAN Program Contract N62470-89-D-4814

Prepared By:

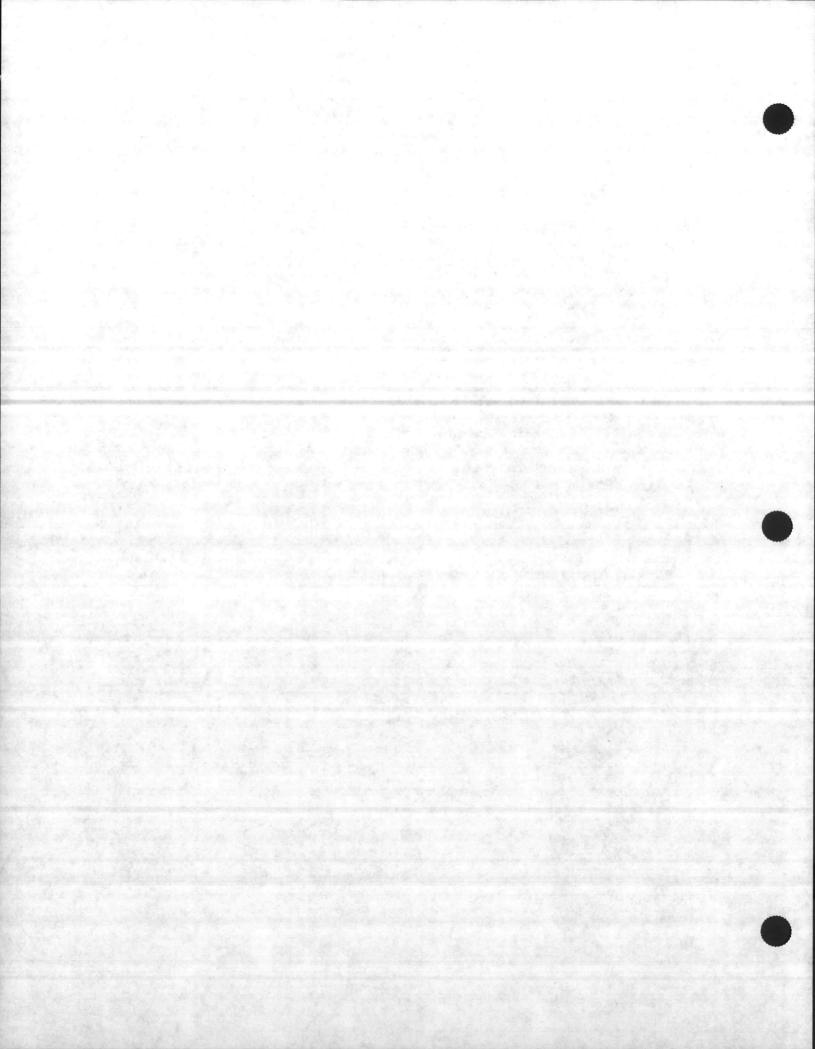
BAKER ENVIRONMENTAL, INC. Coraopolis, Pennsylvania

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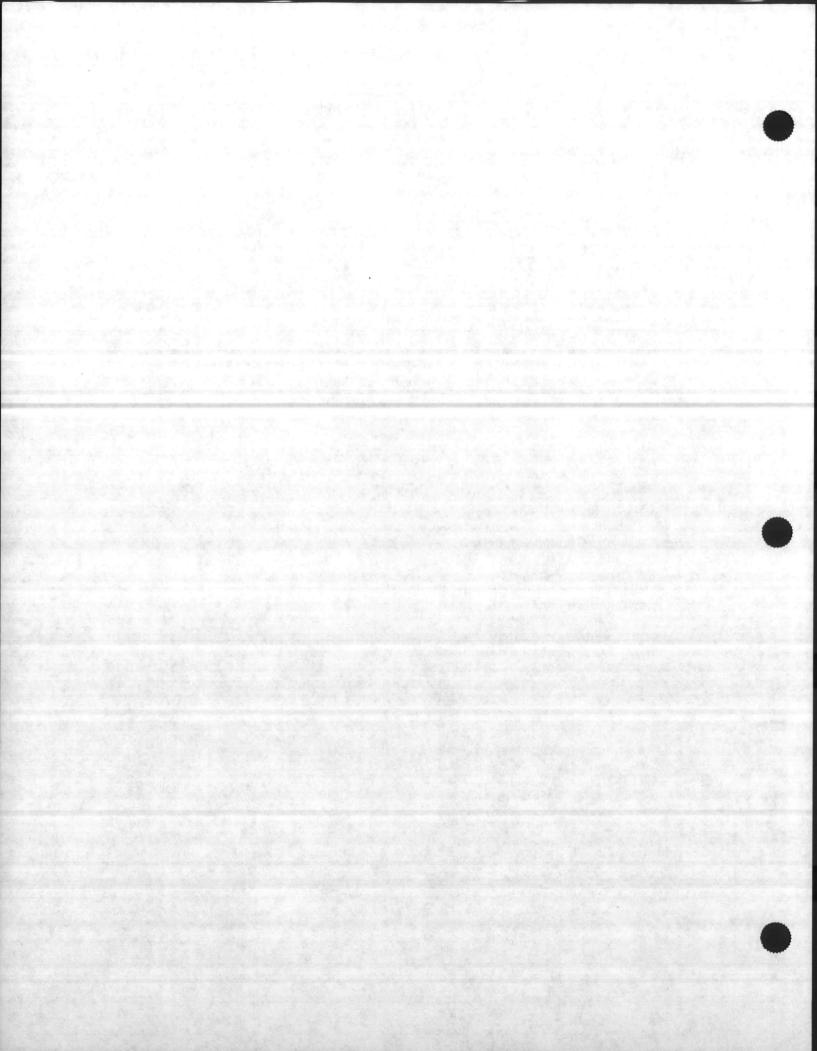
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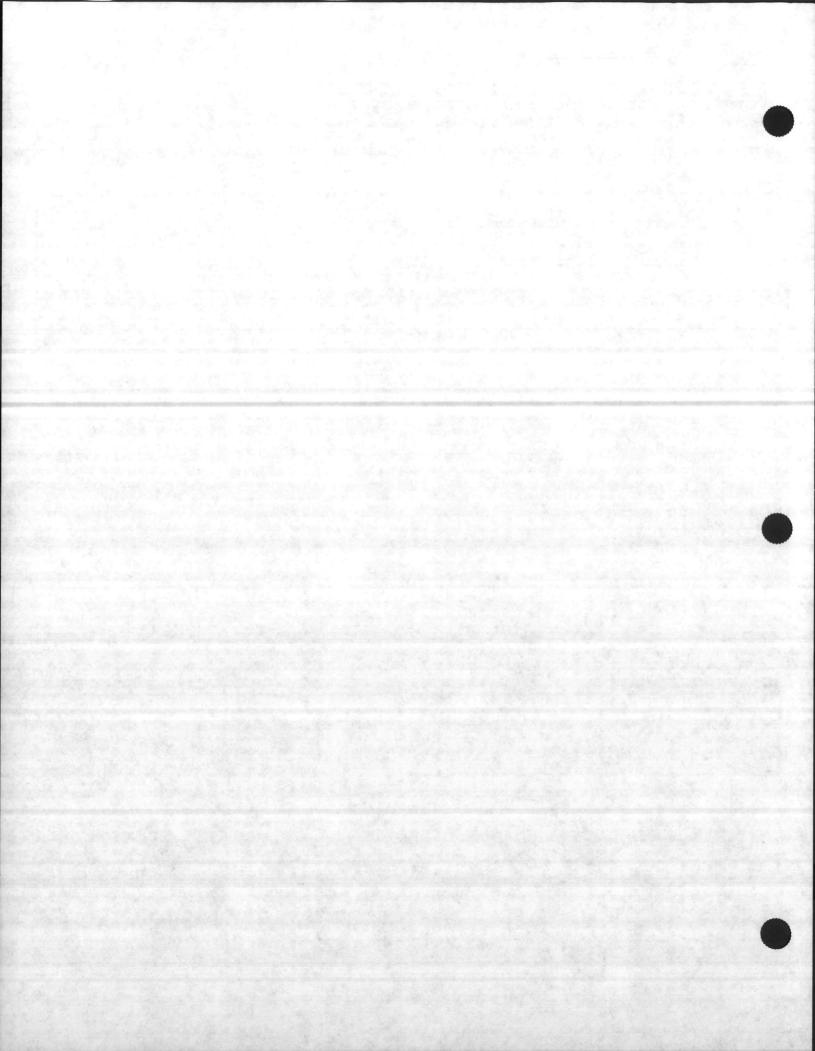
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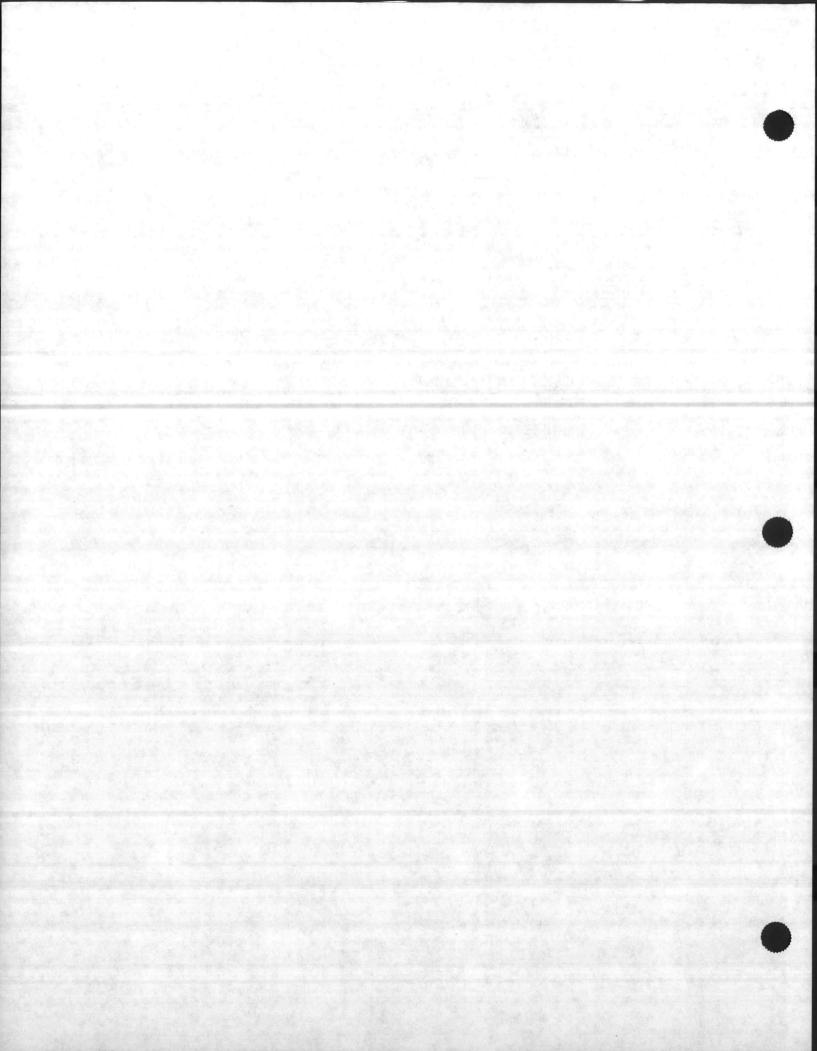
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#### 1.0 INTRODUCTION

The Atlantic Division Naval Facilities Engineering Command has directed Baker Environmental, Inc. (Baker) to conduct a treatability study for the shallow aquifer at the Hadnot Point Industrial Area (HPIA) Operable Unit Site at the Marine Corps Base Camp Lejeune (CLEJ) in Onslow County, North Carolina. This effort has been conducted in support of the remedial design for an Interim Remedial Action (IRA) for the shallow aquifer at Hadnot Point. This IRA has been documented in a Final Record of Decision (ROD) for this Site (Baker, September 17, 1992). The Navy/Marine Corps has obtained concurrence on this IRA from the State of North Carolina and the United States Environmental Protection Agency (USEPA) Region IV.

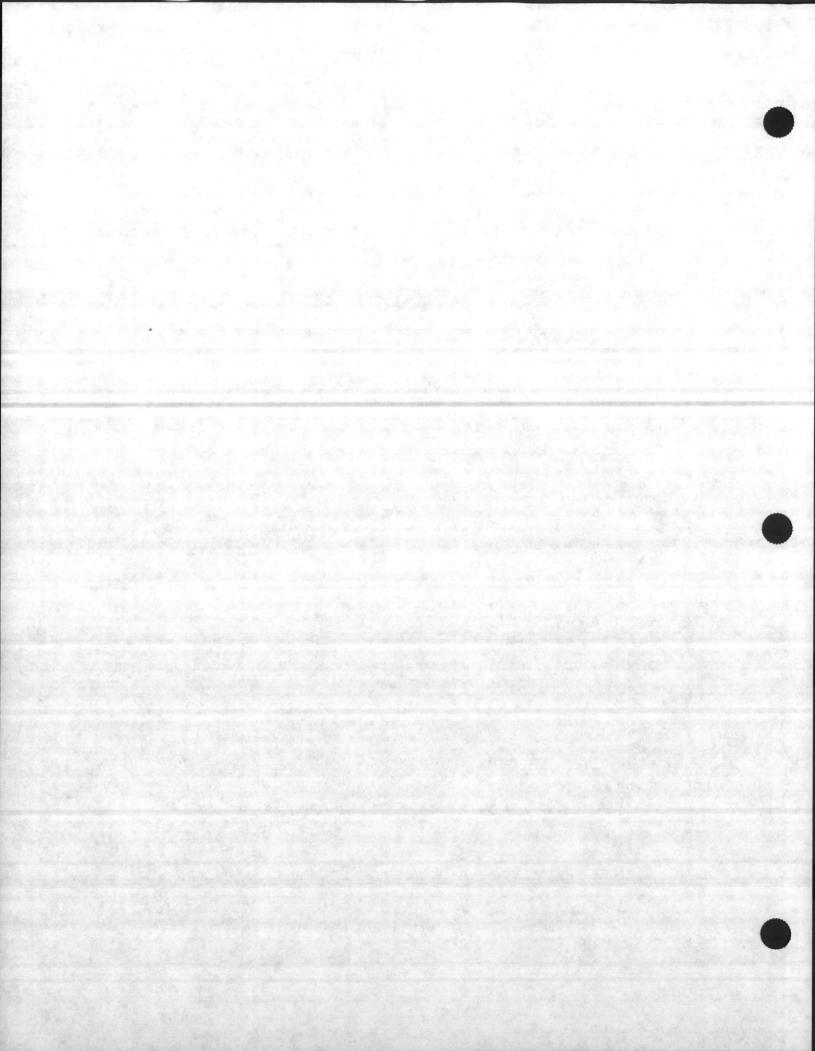
A detailed description of this Treatability Study, its objectives and management plan, was presented in the Remedial Design Project Plans for the Shallow Aquifer at the HPIA Operable Unit, submitted by Baker in January,1993. This report includes a summary of the Treatability Study project description and presents the results of the Treatability Study activities along with recommendations based on these results.

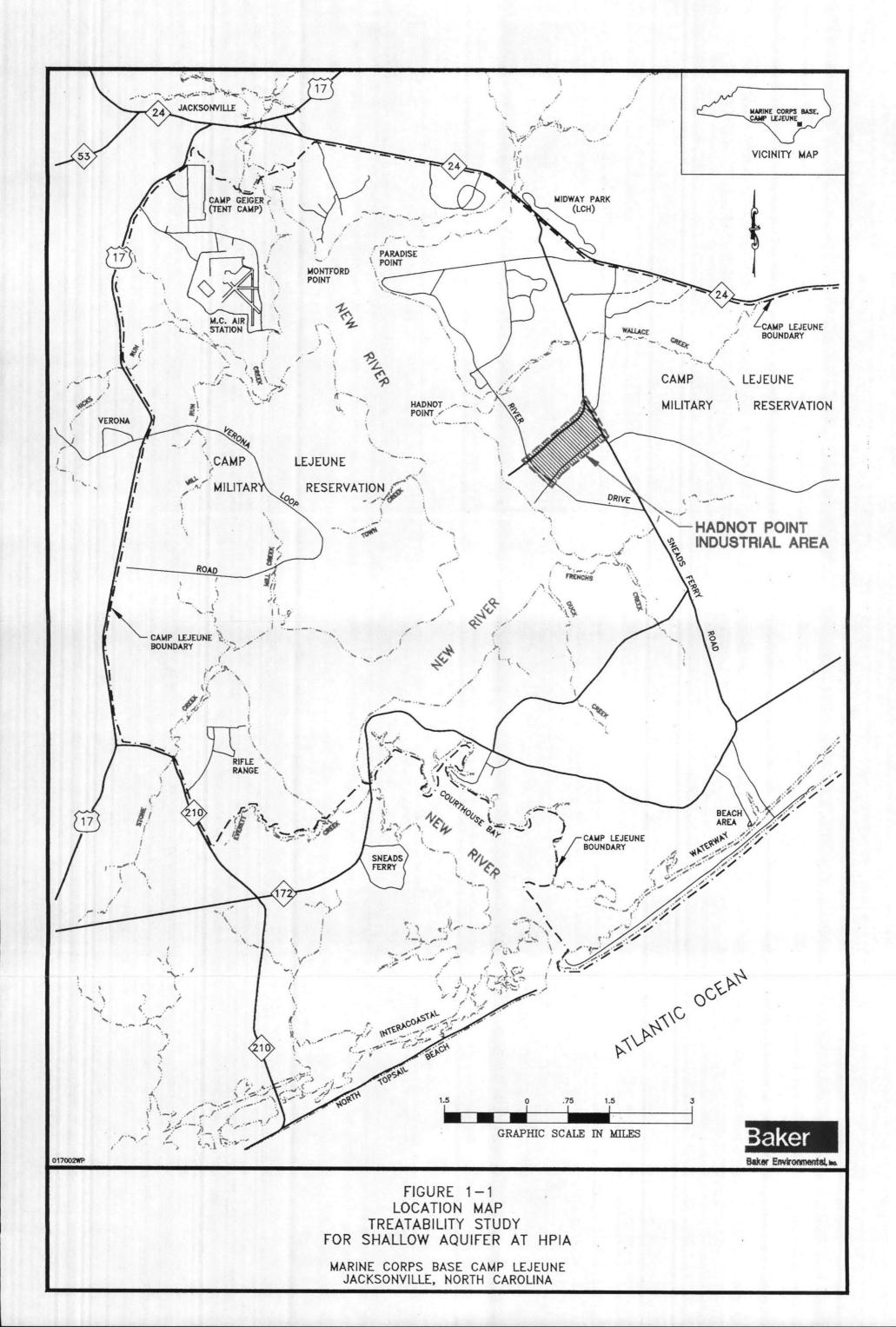
### 1.1 Site Description

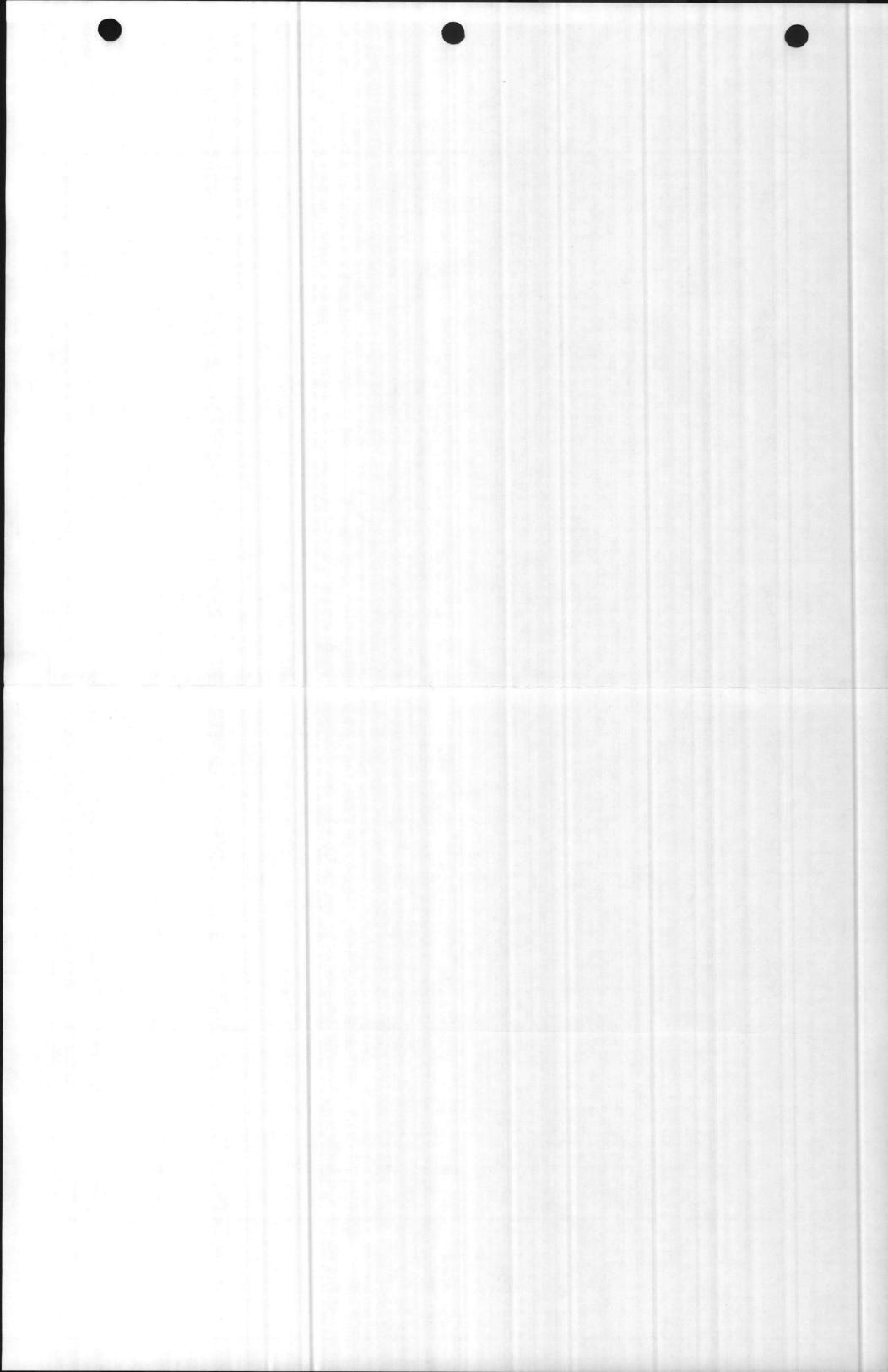
Camp Lejeune covers 170 square miles and is located just north of Jacksonville, North Carolina in Onslow County. The base is bounded to the southeast by the Atlantic Ocean, to the northeast by State Route 24 and to west by State Route 17 (Figure 1-1). This base is primarily a training facility and includes necessary support personnel and industrial support activities.

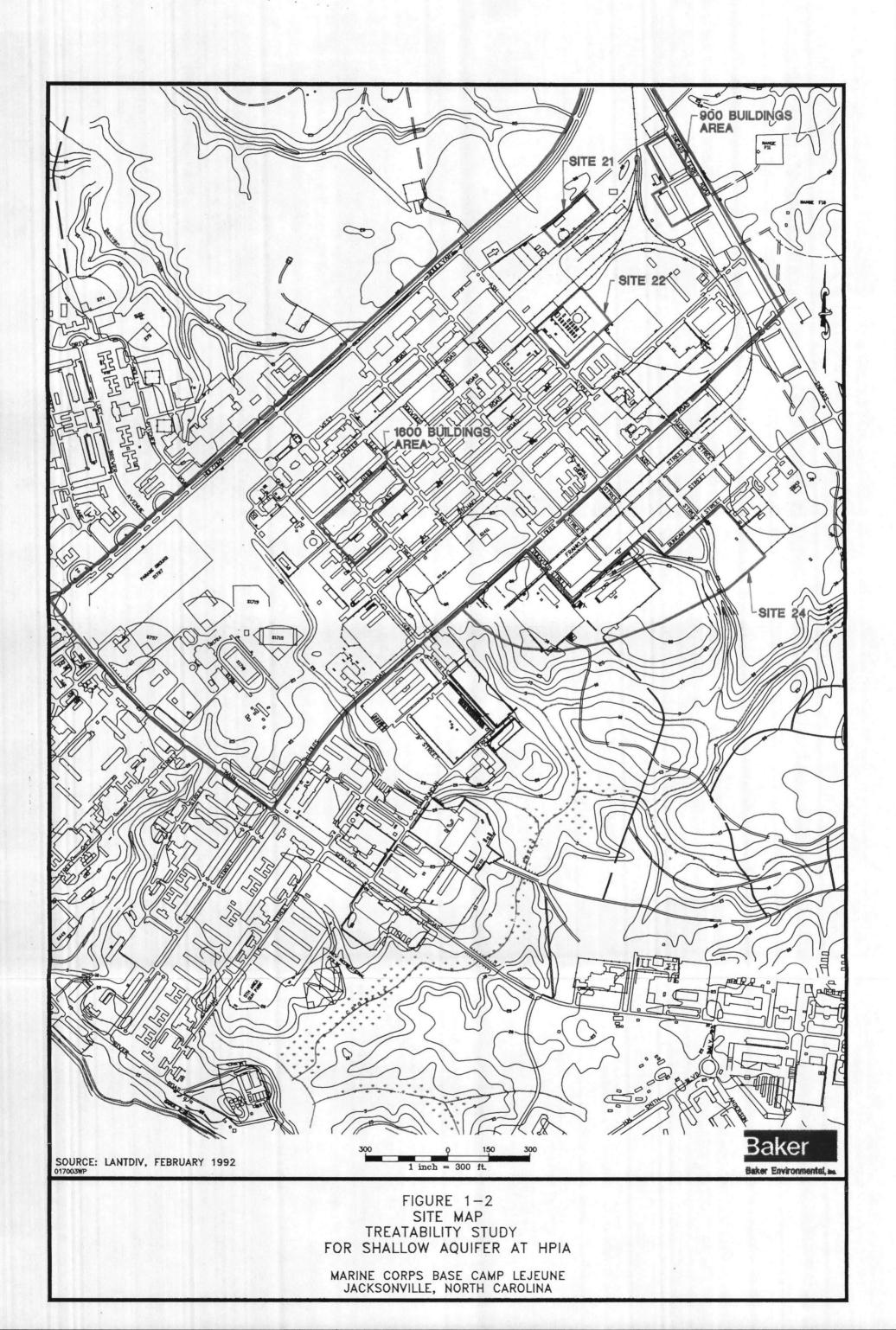
The HPIA was the first facility at MCB Camp Lejeune and was constructed in the 1940's. Currently, HPIA is comprised of approximately 75 buildings that include: maintenance shops, refueling facilities, warehouses, storage yards, rail facilities, a steam generation plant, a training facility, a fire station, dormitories, a snack bar, administrative offices, commissaries, and a dry-cleaning facility (Figure 1-2).

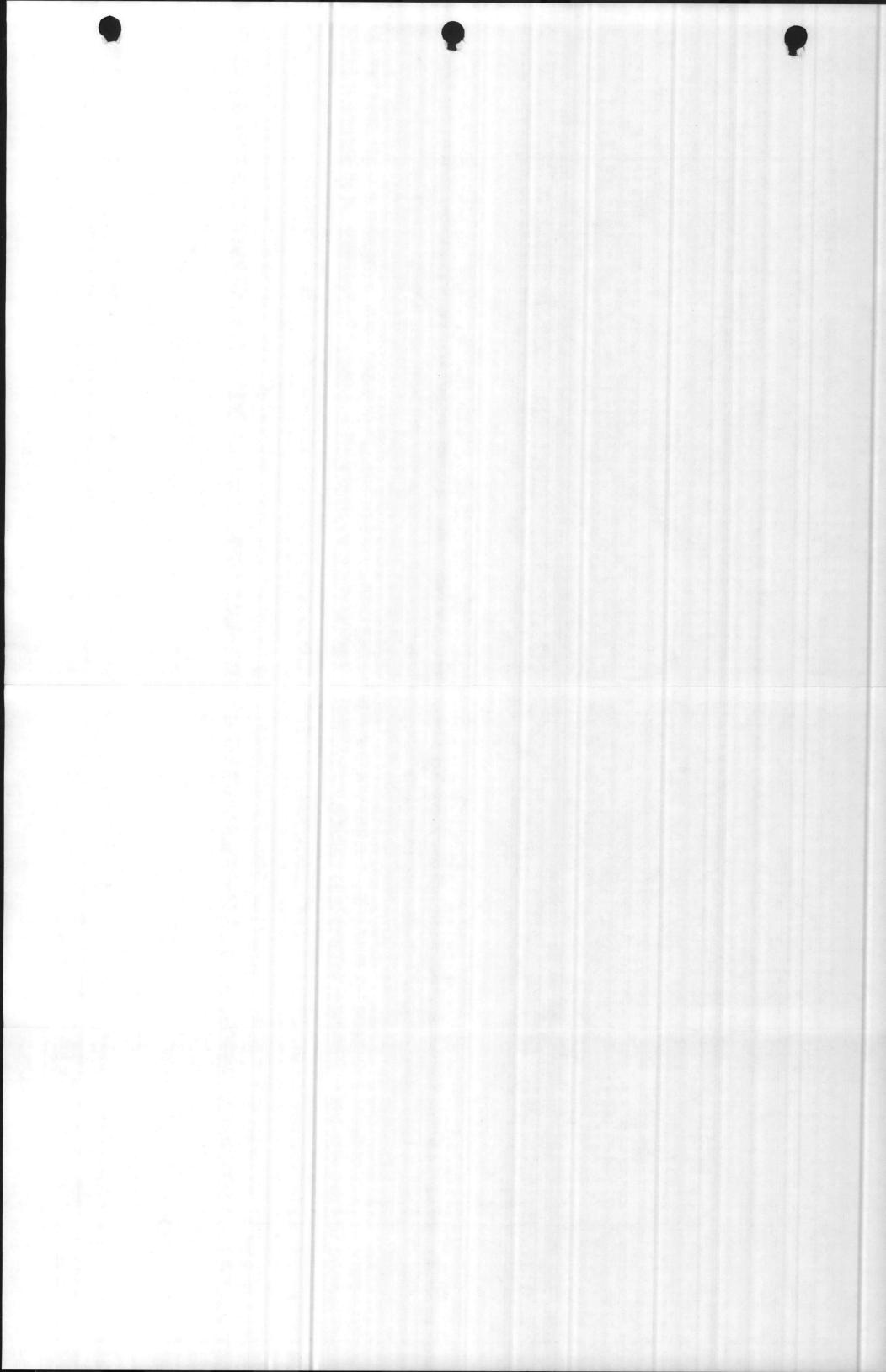
A former fuel tank farm (Site 22) is located within the HPIA Operable Unit boundaries. This site, which is not being administered under CERCLA regulations, is currently being remediated by a fuel recovery groundwater treatment system.











The specific location of the Aquifer and Pilot-Scale Treatability Tests are the 900 Series buildings located at the northeast end of HPIA on Sneads Ferry Road.

## 1.2 Waste Stream Description

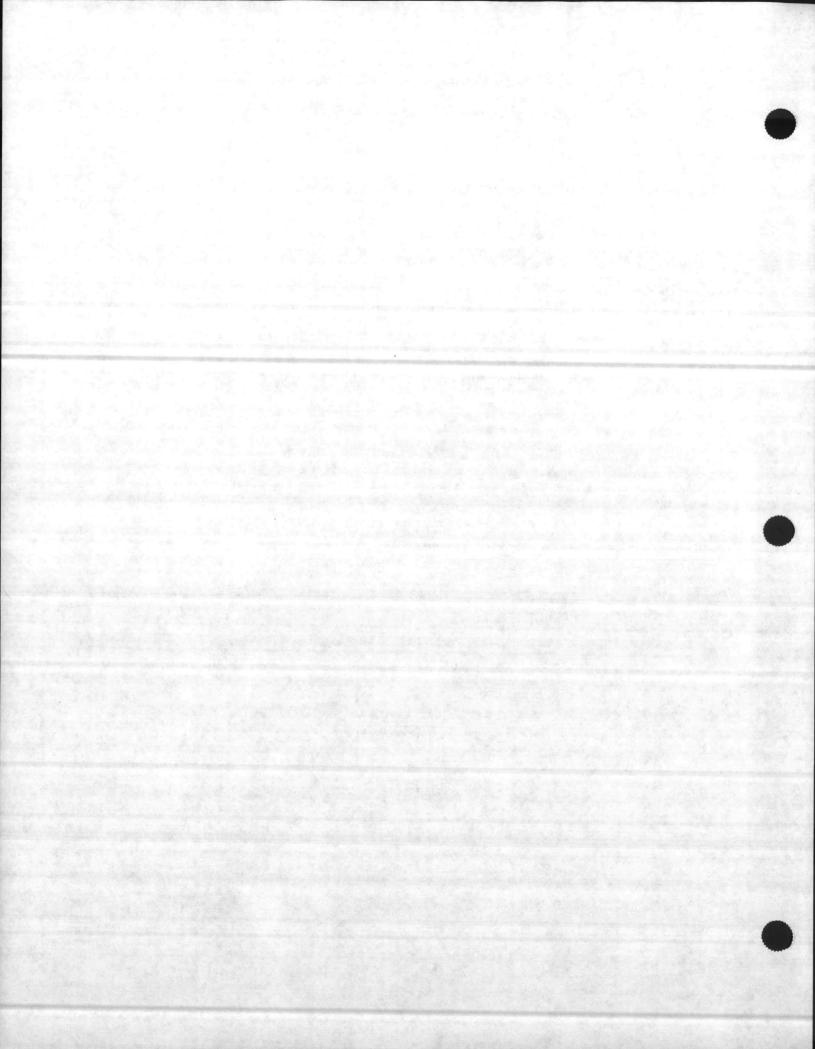
Previous studies indicate that the shallow groundwater is contaminated primarily with fuel related compounds, benzene, 1,2-dichloroethene (1,2-DCE), trichloroethene (TCE), solvents, and metals, such as antimony, arsenic, beryllium, chromium, iron, lead, manganese, mercury, and nickel. Several compounds were detected at concentrations exceeding the Federal and North Carolina drinking water standards for groundwater.

Prior to this Treatability Study, the most recent shallow groundwater data was collected in January 1991 by ESE. Based upon the results of the 1991 sampling, the following compounds were identified as potential contaminants of concern for the shallow aquifer at the HPIA: benzene; 1,2-DCE; TCE; antimony; arsenic; beryllium; chromium; iron; lead; manganese; mercury; and, nickel. Table 1-1 presents a summary of the 1991 shallow aquifer groundwater data with respect to the contaminants of concern. Oil and grease data are not included on Table 1-1 due to the fact that this analysis was not conducted on any of the 1991 samples. The maximum concentrations of benzene (7900 µg/L) were detected in a monitoring well immediately adjacent to the fuel tank farm (Site 22). Maximum concentrations of 1,2-DCE (42,000 µg/L) and TCE (14,000 µg/L) were detected in the northeast corner of the site (near the 900 series buildings) and in the southwestern portion of the site (near the 1600 series buildings), respectively. Metals concentrations were elevated throughout most of the site, especially near the fuel farm (lead).

Based on review of existing data, two major areas of contaminated groundwater (source areas) have been identified in the shallow aquifer at HPIA as shown on Figure 1-3. The first area or plume is located northeast of Cedar Street near the 900 series buildings. The other plume is located southwest of Cedar Street near the 1600 buildings.

## 1.3 Remedial Technology Description

A description of the liquid treatment processes that were evaluated in the bench-scale and pilot-scale tests are presented in this subsection.





# SUMMARY OF CONTAMINANTS OF CONCERN DETECTED IN THE SHALLOW GROUNDWATER AQUIFER, JANUARY 1991

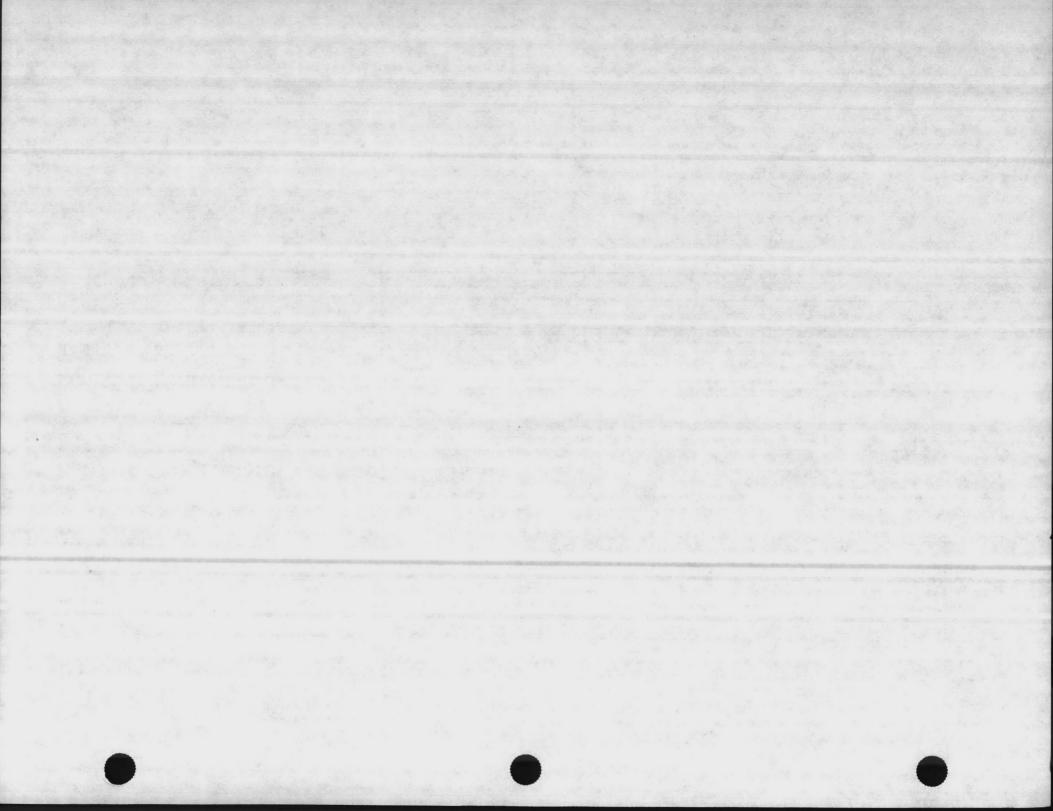
Potential Contaminants of Concern	HPGW1	HPGW2	HPGW3	HPGW4-1	HPGW5	HPGW6	HPGW7	HPGW8	HPGW9-1	HPGW10	HPGW11	HPGW12	HPGW13	HPGW14	HPGW15
VOC (µg/L)	Para de la constante de la con		THE PERSON				20 May 10 198			J-7078588	FA TELLER	German Print Print		100	
Benzene	5 <	5 <	5 <	5 <	5 <	5 <	5 <	5 <	5 <	5 <	5 <	5 <	5 <	5 <	5 <
1,2-Dichloroethene	73	10 <	10 <	5 <	5 <	5 <	5 <	5 <	1200	5 <	5 <	5 <	5 <	5 <	7
Trichloroethene	91	5 <	5 <	0.9 J	5 <	5 <	5 <	2 J	14000	5 <	5 <	5 <	5 <	5 <	4 J
Inorganics (µg/L) Chromium	87	64.3	16.7	187	3.6 B	1590	313	91.8	66.4	310	140	25.5	48.9	127	21.4
Iron	64100	34800	10400	100000	3100	265000	65700	40900	19800	119000	31800	5600	33500	87200	4800
Lead	16.6	29.4	11.4	66.6	13.6	60.7	112	54.1	128	186	45.2	15.7	9	66.5	16.6
Manganese	168	77	53.9	425	162	487	136	46.5	45	255	103	18.3	30.3	80	18.3
Antimony	13.3 <	15.6 B	46.5 B	21.9 B	13.3 <	13.3 <	22 <	22	17.6 B	22 <	22 <	22 <	13.3 <	13.3 <	22 <
Arsenic	8 B	24.1	15.6	15.5	1.5 <	31.5	18.3	28.4	3 B	39.9	9.1 B	1.8 <	47	45.6	1.8 <
Beryllium	6	1.7 BG	1.2 B	6.7	0.86 B	20	4.8 B	2.1	0.79 B	5.6	2.1 <	2.1 <	0.59 B	2.7 B	2.1 <
Mercury	0.1 <	0.1 <	0.1 <	0.1 <	0.1 <	1.4	0.25	0.13	0.1 <	0.82	0.1 B	0.1 <	0.1 <	0.26	0.1 <
Nickel	31.3 B	16.9 B	12.1 B	57	5.2 <	161	50.7	25.2	15.1 B	92.2	23.6 B	11 <	21.2 B	41.6	11 <

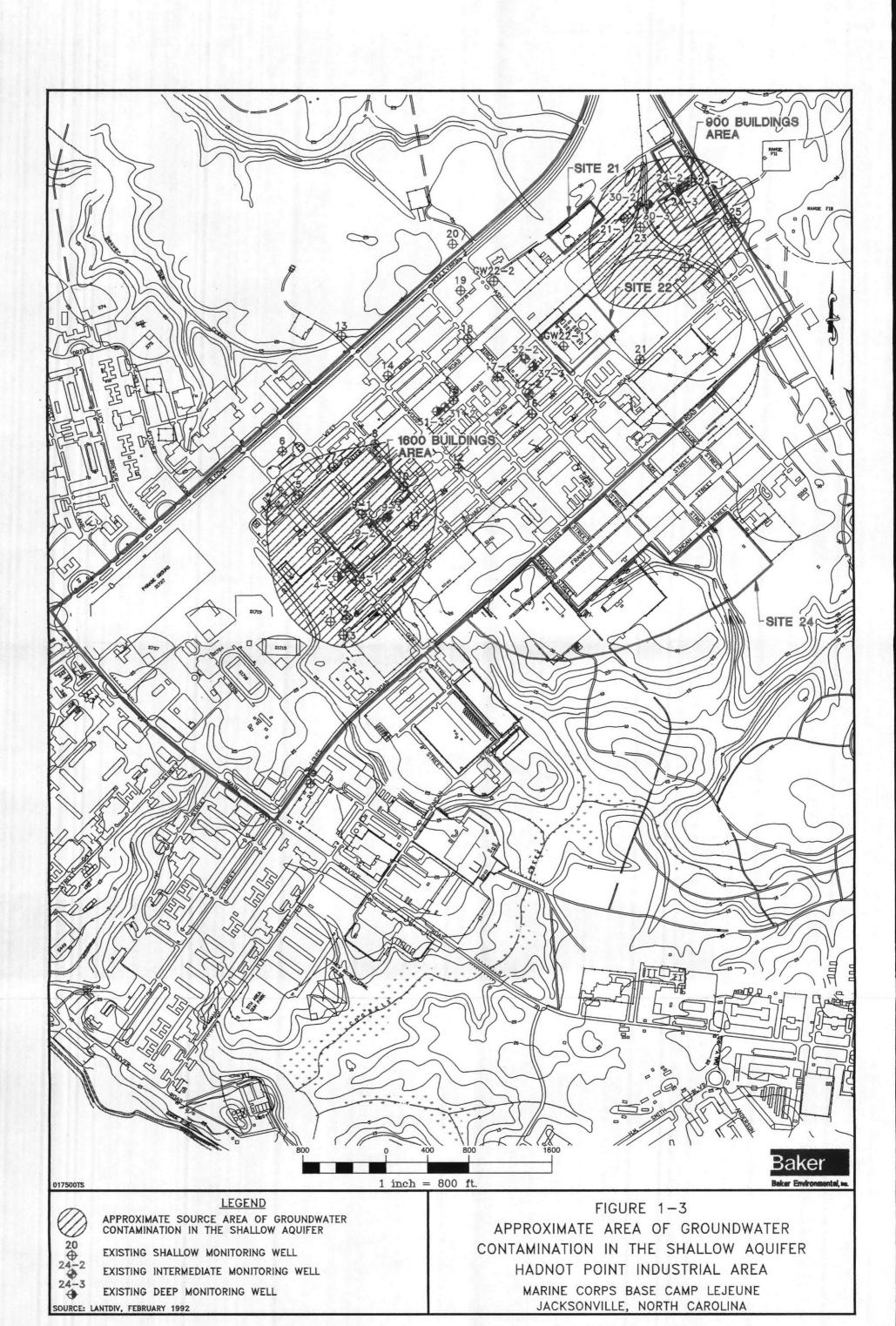
Potential Contaminants of Concern	HPGW16	HPGW17-1	HPGW18	HPGW19	HPGW20	HPGW21	HPGW22	HPGW23	HPGW24-1	HPGW25	HPGW26	HPGW29	22GW1	22GW2
VOC (µg/L)						BKT L		A PARTIES						
Benzene	5 <	5 <	N/A	5 <	5 <	5 <	5 <	24	3 J	5 <	5 <	5 <	7900	5 <
1,2-Dichloroethene	5 <	5 <	N/A	0.8 J	5 <	5 <	5 <	8900	42000 D	5 <	5 <	5 <	5 <	5 <
Trichloroethene	5 <	5 <	N/A	2 J	5 <	3 J	5 <	3700	180	5 <	5 <	5 <	5 J	5 <
Inorganics (µg/L)		A San I	and a		4	140,000				Y \$				
Chromium	209	37	N/A	13.8	424	45	79.8	76.3	26.3	205	13	179	457	26.3
Iron	47200	10500	N/A	36200	2E+05	56600	24400	23300	19200	46600	19000	76200	1E+05	16200
Lead	100	23.7	N/A	31.7	20	49.4	39.4	45	21.4	71.6	9	29.1	307	16.2
Manganese	98.3	31.3	N/A	79	217	136	94.1	68.8	54.8	118	10.6 B	236	284	763
Antimony	22 <	22 <	N/A	13.3	21.9B	13.3 <	24.6 B	24.6 <	22 <	13.3 <	13.3 <	13.3 <	20.9 B	13.3
Arsenic	17.3	1.8 <	N/A	5 B	49.4	12.1	7.2 B	6.6 B	4.2 B	13.2	1.5 <	25.6	50.3	11
Beryllium	5.3	2.1 <	N/A	2.3 B	9.5	3.7 B	0.6 B	1 B	2.1 <	2.8 B	0.5 <	8.7	5.8	0.5
Mercury	0.13 B	0.1 <	N/A	N/A	0.5	0.1 <	0.1 <	0.1 <	0.1 <	0.1 <	0.1 <	0.1 <	0.35	0.1
Nickel	41	11.9 B	N/A	7.3 B	168	30.8 B	23.2 B	33.2 B	14 <	39.2 B	5.2 <	93.5	186	17

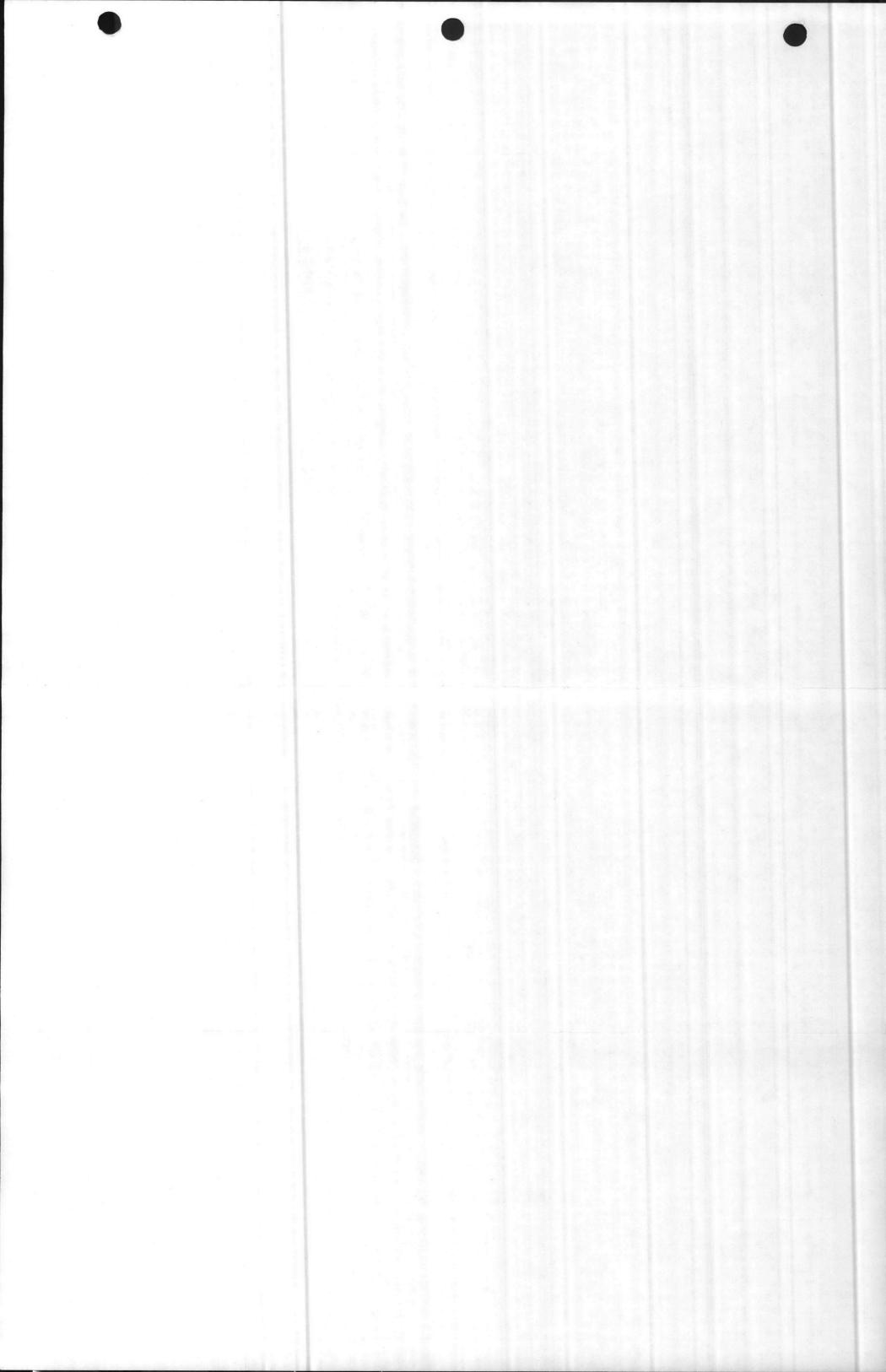
Notes: < = Compound was analyzed, but not detected at the listed detection limit J = Value is estimated

B = Reported value is < contract required detection limit (CRDL), but > instrument detection limit (IDL)
D = Compound identified in an analysis at a secondary dilution factor

N/A = Not Analyzed







#### 1.3.1 Bench-Scale

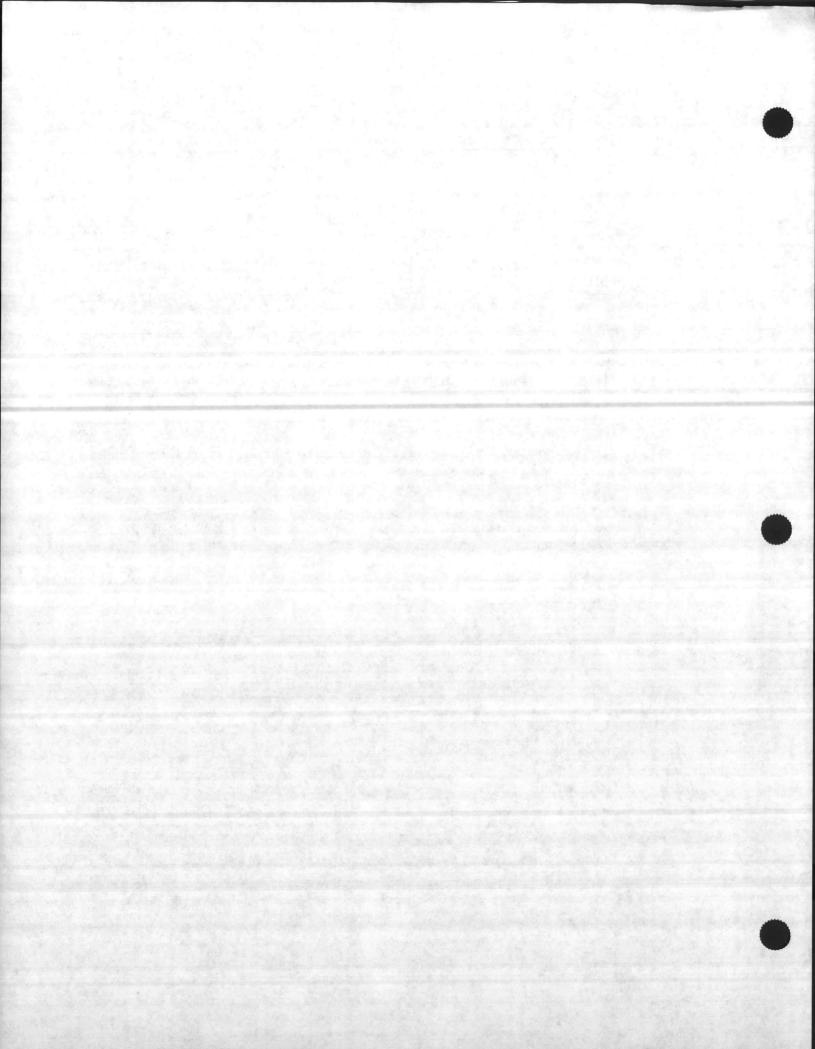
Bench-scale testing was designed to simulate the following processes:

- Oil/water separation was used as pretreatment to remove free oil and oily sludges through gravity separation.
- Metals Removal was used to remove inorganics from the groundwater. The metals removal processes included flocculation, precipitation, and sedimentation:
  - Flocculation is the process by which very small, unsettleable particles suspended in a liquid medium collide and agglomerate into larger heavier particles or flocs and settle out.
  - Precipitation is the process in which materials in solution are transferred into a solid phase for removal.
  - Sedimentation is the process used to remove suspended solids from aqueous waste streams by gravity separation.

#### 1.3.2 Pilot-Scale

Pilot-Scale testing consisted of the following processes:

- Air Stripping is a physical treatment process in which water and air are brought into contact with each other for the purpose of transferring volatile substances from solution in a liquid to solution in a gas.
- <u>Carbon Adsorption</u> is a physical process that binds organic molecules to the surface of the activated carbon particles. Activated carbon has an enormous surface area. One gram of commercially activated carbon is estimated to have a surface area of 1,000 to 1,400 square meters. The process involves contacting a waste stream with carbon, usually by flow through a series of packed bed reactors.



#### 2.0 GEOLOGIC CONDITIONS

The following subsections present summaries of the regional and site geology encountered in the HPIA.

## 2.1 Regional Geology

MCB Camp Lejeune is located in the Atlantic Coastal Plain physiographic province. The region is underlain by several thousand feet of unconsolidated deposits ranging in age from Lower Cretaceous to Holocene. These sediments consist of interbedded sands, clays, calcareous clays, shell beds, and gravel. Regionally, they comprise 10 aquifers and nine confining units which overlie a bedrock basement of Pre-Cambrian and Jurassic/Triassic age. Generally, these deposits dip and thicken gently eastward (i.e., seaward) with thicknesses ranging from 1,500 feet to 5,000 feet. The sediment complex at Jacksonville, North Carolina, is approximately 1,500 feet thick (U.S.G.S. W-RIR 894128). Table 2-1 presents a generalized stratigraphic column for this area.

## 2.2 Site Geologic Conditions

USGS studies at MCB Camp Lejeune indicate that the Base is underlain by seven sand and limestone aquifers separated by confining units of silt and clay. These include the water table (surficial), Castle Hayne, Beaufort, Peedee, Black Creek, and Upper and Lower Cape Fear aquifers. The combined thicknesses of these sediments is approximately 1,500 feet. Less permeable clay and silt beds function as confining or semi-confining units which separate the aquifers and impede the flow of groundwater between aquifers.

Lithologic information obtained during monitoring well, recovery well and piezometer installation at Hadnot Point Industrial Area (HPIA) indicate that the site is underlain by silty sand with extensive, but discontinuous, layers of silty clay and silty-sandy clay. Peat, wood fragments, and plant debris are present in a one or two foot layer in the southwest portion of the HPIA, suggesting a historical marsh environment. Peat was also encountered at a depth of 18 feet in the northwest portion of the site. Other geologic materials underlying the site include fill (up to four feet thick) adjacent to construction areas, and marl.

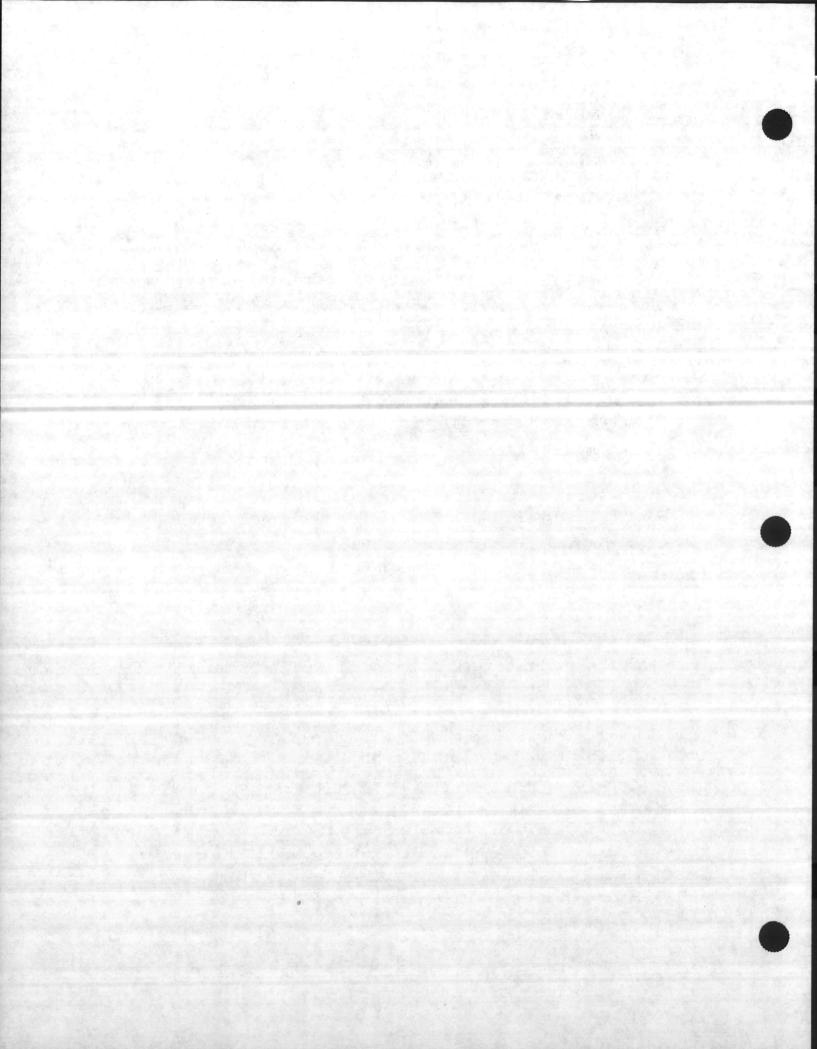


TABLE 2-1

GENERALIZED RELATION BETWEEN GEOLOGIC AND HYDROGEOLOGIC UNITS IN THE COASTAL PLAIN OF NORTH CAROLINA

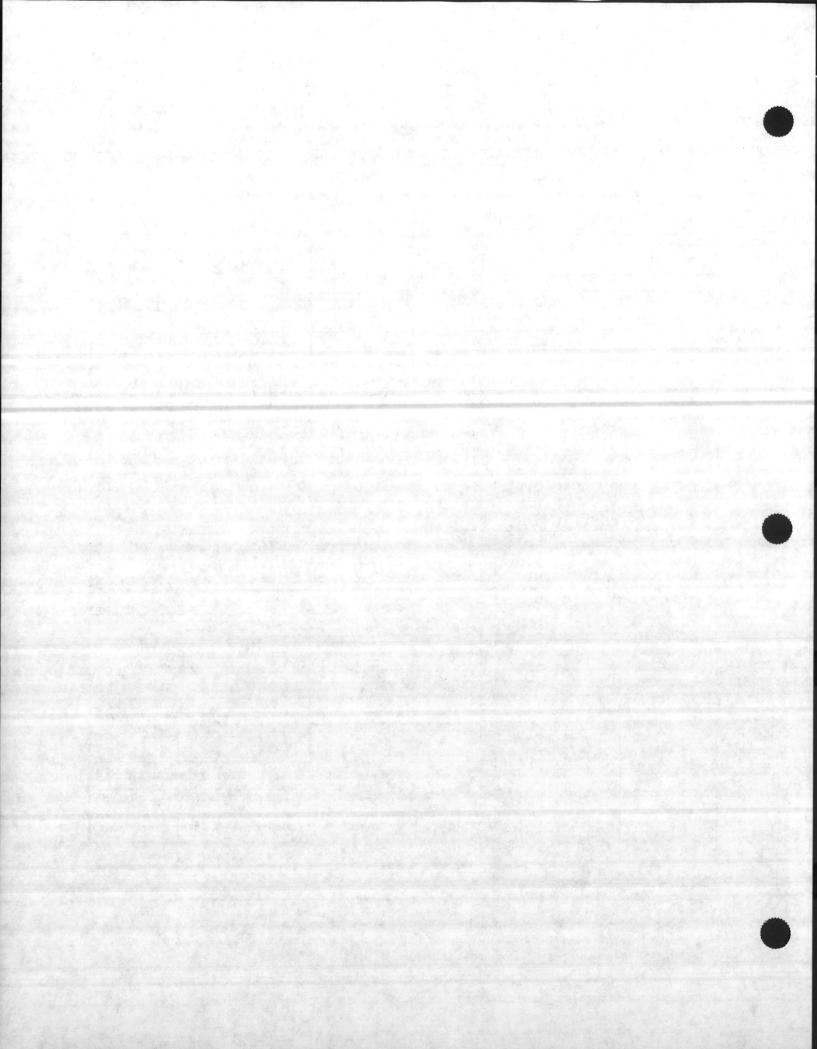
	Geologic Un	Hydrogeologic Units					
System	Series	Formation	Aquifer and Confining Uni				
Quaternary	Holocene Pleistocene	Undifferentiated	Surficial Aquifer				
	Pliocene	Yorktown Formation(1)	Yorktown Confining Unit				
		Eastover Formation <sup>(1)</sup>	Yorktown Aquifer				
	Miocene		Pungo River Confining Unit				
Tertiary		Pungo River Formation(1)	Pungo River Aquifer				
		Belgrade Formation(2)	Castle Hayne Confining Unit				
	Oligocene	River Bed Formation	Castle Hayne Aquifer				
	Eocene	Castle Hayne Formation					
			Beaufort Confining Unit				
	Paleocene	Beaufort Formation	Beaufort Aquifer				
			Peedee Confining Unit				
		Peedee Formation	Peedee Aquifer				
			Black Creek Confining Unit				
	Upper Cretaceous	Black Creek and Middendorf Formations	Black Creek Aquifer				
Cretaceous			Upper Cape Fear Confining Unit				
			Upper Cape Fear Aquifer				
		Cape Fear Formation	Lower Cape Fear Confining Unit				
		All the state of t	Lower Cape Fear Aquifer				
	Lower Cretaceous(1)	Unnamed Deposits(1)	Lower Cretaceous Confining Uni				
	27 27 27 27 27 27 27		Lower Cretaceous Aquifer				
Pre-Cretaceou	s Basement Rocks	water the same of the					

<sup>(1)</sup> Geologic and hydrologic units probably not present beneath Camp Lejeune.

Source: U.S.G.S., Water Resources Investigations Report 89-4096, "Assessment of Hydrologic and Hydrogeologic Data at Camp Lejeune Marine Corps Base, North Carolina," 1989.

<sup>(2)</sup> Constitutes part of the surficial aquifer and Castle Hayne Confining Unit beneath Camp Lejeune.

<sup>3)</sup> Estimated to be confined to deposits of Paleocene Age in the study area.



#### 3.0 HYDROGEOLOGY

The following subsections present summaries of the regional and site hydrogeologic conditions encountered in the HPIA.

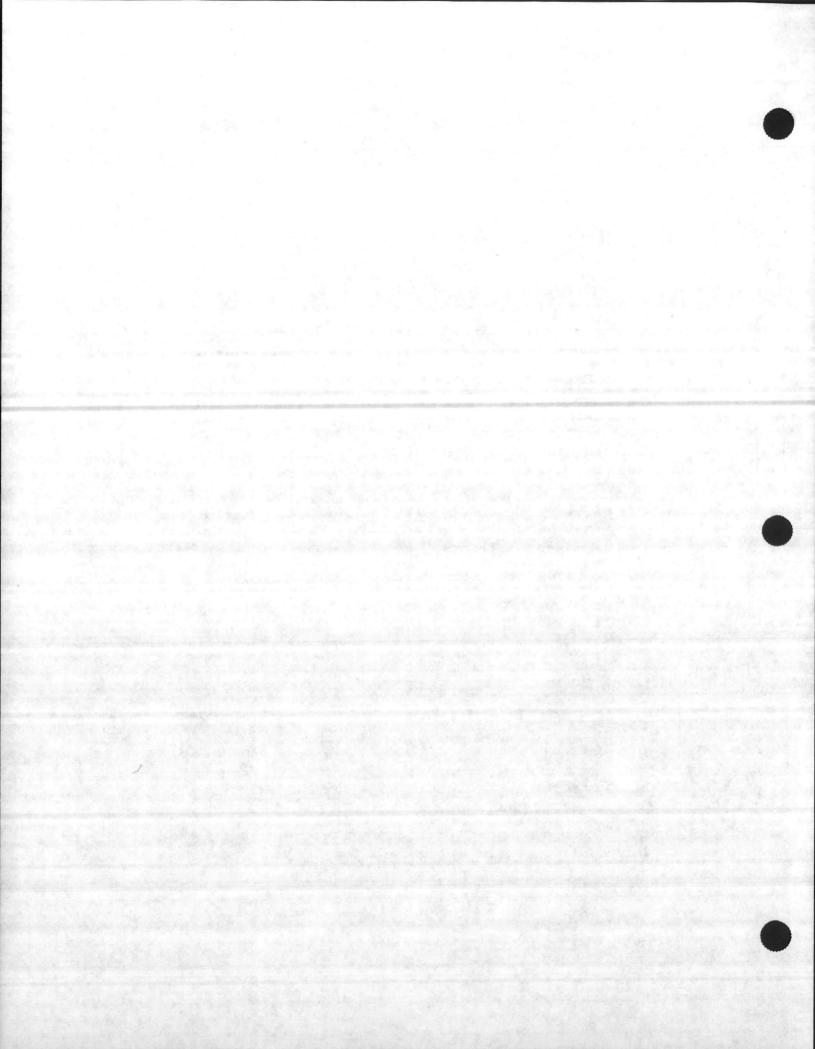
## 3.1 Regional Hydrogeology

The hydrogeologic framework of the Jacksonville, North Carolina area includes seven principal aquifers listed in superposition as follows: (1) the surficial water table; (2) the Castle Hayne; (3) Beaufort; (4) Peedee; (5) Black Creek; (6) Upper Cape Fear; and (7) Lower Cape Fear. Only the surficial and Castle Hayne Aquifers are of concern in this report. Aquifers below the Castle Hayne lie in a thick sequence of sand and clay. Although some of these aquifers are used for water supply elsewhere in the coastal plain, they contain saltwater in the Camp Lejeune area and are not used (U.S.G.S., W-RIR 89-4096).

The surficial aquifer is found in beds and lenses of sand and clay. These deposits range in thickness from 25 to 100 feet and overlie the sediments containing the Castle Hayne aquifer. The sand lenses are the major water-bearing strata and are very heterogeneous and discontinuous because of the complex marine/estuarine environments in which they were deposited. In some areas, the surficial aquifer is reported to contain water contaminated by waste disposal practices (Putnam, 1983).

The Castle Hayne Aquifer underlies the surficial aquifer. Most of the supply wells in the area tap this aquifer at depths ranging from 50 to 300 feet. This aquifer ranges in thickness from 250 to 400 feet but brackish water is normally encountered below 300 feet. The water-bearing zones are a series of sandstone, limestone and clay beds of the Oligocene River Bend Formation and the Middle Eocene Castle Hayne Formation.

The upper half of the Castle Hayne Aquifer is primarily sand; the lower half is sand and limestone. The top of the aquifer ranges from about 20 feet above sea level in the northern part of the area to about 40 feet below sea level in the southeastern part. The aquifer thickens toward the southeast from 175 feet at the Marine Corps Air Station to about 375 feet at the coast (U.S.G.S., W-RIR 89-4096).



Clay layers occur in both the Castle Hayne and the surficial aquifers. However, no continuous clay layer separates the surficial and the Castle Hayne. The clay layers appear to be more continuous in the northwestern part of the base (U.S.G.S., W-RIR 89-4096).

Confining sediment beds restrict the direct exchange of groundwater between the surficial and the Castle Hayne aquifers. However, some hydraulic connection between the two aquifers has been observed (Department of the Navy, 1990).

# 3.2 Site Hydrogeologic Conditions

The groundwater system at the HPIA consists of an unconfined shallow aquifer (i.e., surficial aquifer) and underlying semi-confined aquifers. The shallow aquifer is separated from the underlying aquifers by a discontinuous clay and sandy clay layer. Groundwater in this zone ranges in depths from 6 to 23 feet below ground surface, based on two rounds of water level measurements collected in January and February 1991 (ESE, 1991b). Seasonal water level fluctuations were reported to range from 1 to 4 feet.

In general, groundwater in the shallow aquifer flows to the southwest, towards the New River. Figure 3-1 presents a potentiometric surface map of the water table constructed from water level measurements taken from the shallow monitoring wells on February 20, 1991 by Environmental Science and Engineering, Inc.. The ESE report indicated some mounding of groundwater in the southern corner of HPIA. A surface drainage ditch, which was observed to be full of water, is located in this portion of the HPIA and may act as a recharge point (ESE, 1991b).

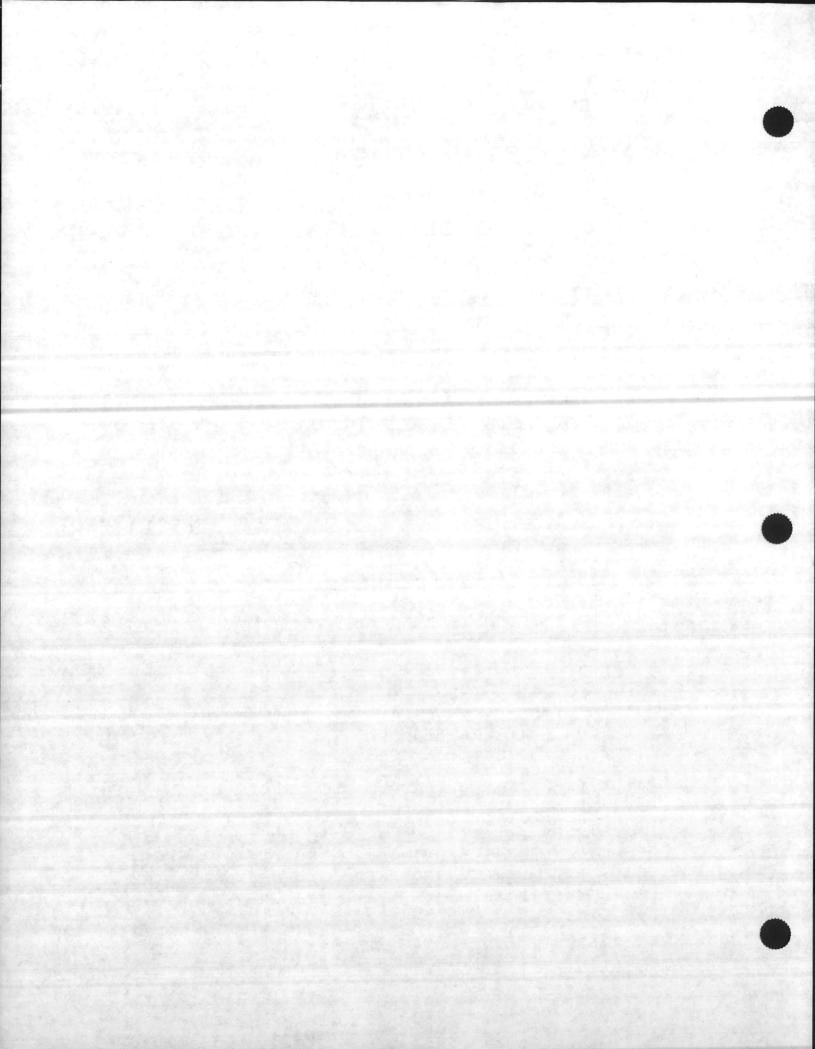
The following shallow aquifer characteristics were calculated by O'Brien & Gere based on the results of an 8-hour pump test conducted in 1988:

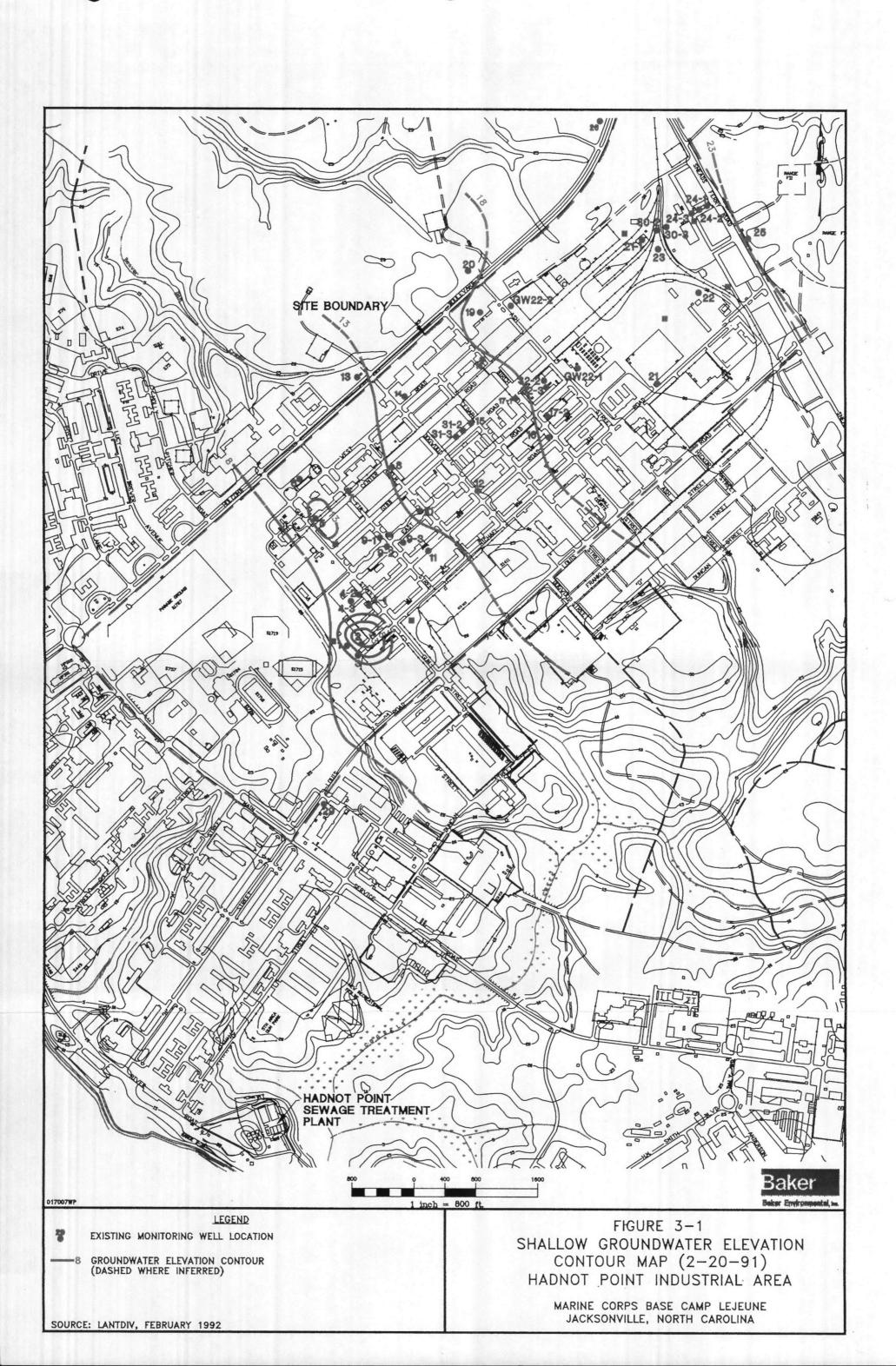
Transmissivity = 500 gpd/ft

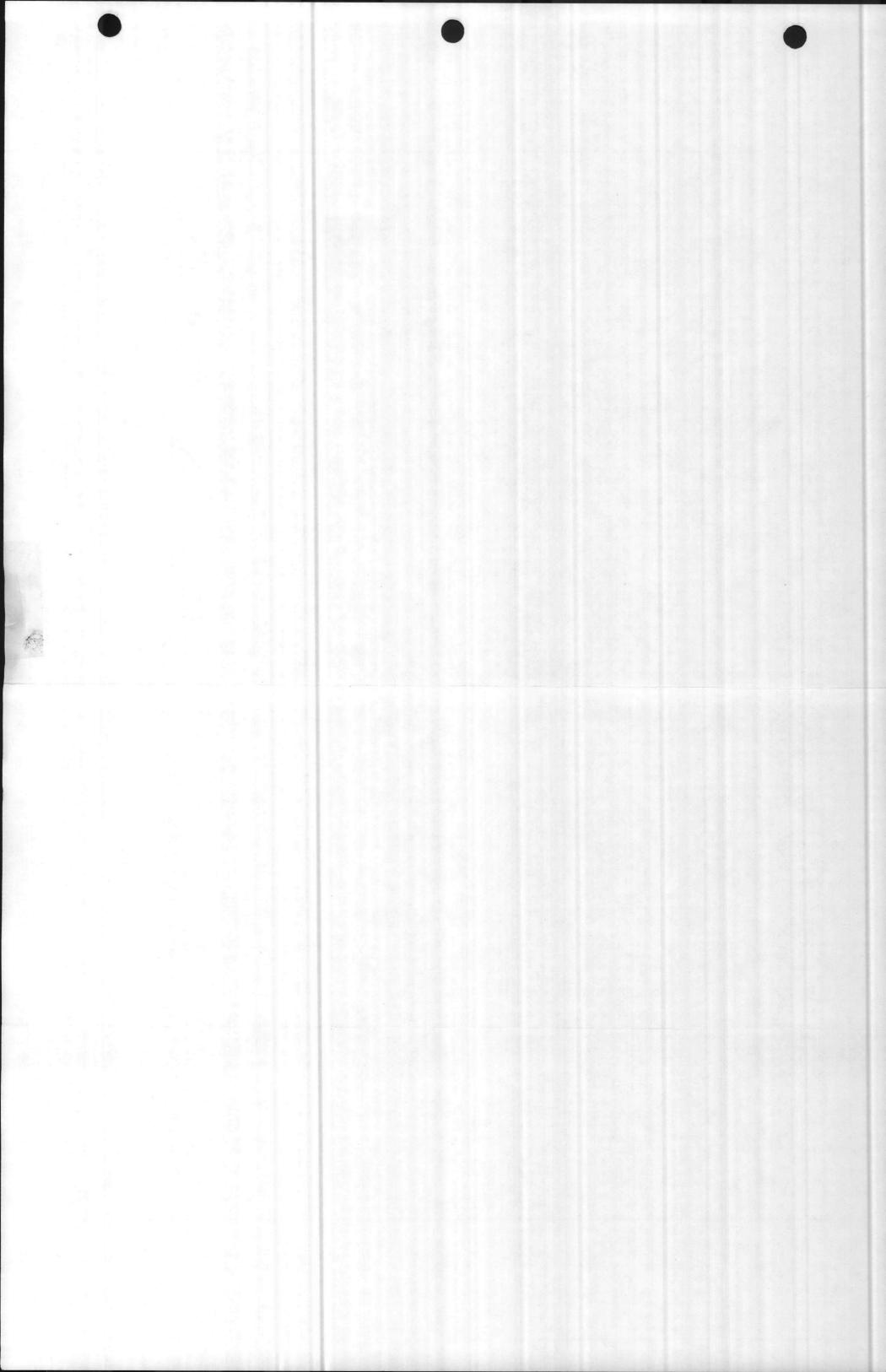
Well yield = 3 gpm

Saturated thickness = 19 - 22 feet

• Radius of influence = 300 - 400 feet







# 4.0 TREATABILITY STUDY ACTIVITIES APPROACH

# 4.1 Test Objectives

The Feasibility Study (FS) for the HPIA Operable Unit provided remedial screening of potential technologies for the treatment of the contaminants of concern. This treatability study will provide remedy selection testing to evaluate the remedial technologies' performance in meeting the site-specific clean-up goals for the HPIA Operable Unit. The cleanup goals include Federal and North Carolina Groundwater MCLs that are shown on Table 4-1. These goals have been defined by the USEPA Region IV and the North Carolina DEHNR. The treatability studies will provide data to support the design of pretreatment components (e.g., metals removal, oil separation) and the air stripping treatment unit. Additionally, the pilot study will provide data to evaluate whether other treatment components (i.e., carbon adsorption) are required as part of the treatment system in order to meet cleanup goals.

#### 4.2 Bench-Scale Treatability Studies

This section describes the experimental design and procedures, as well as equipment and materials used to perform bench-scale treatability testing on groundwater samples from the HPIA Operable Unit. A representative sample of groundwater (approximately 70 liters) was collected prior to the aquifer pump test to perform sample characterization and bench-scale treatability testing. Based on the sample characterization results, oil/water separation and gravity settling tests were conducted on the groundwater samples. Analytical results for the sample characterization and treatability tests are provided in Section 5.1, Bench-Scale Studies.

#### 4.2.1 Experimental Design and Procedures

The procedures used to collect the characterization samples, to conduct the oil/water separation, and gravity settling tests are discussed in the following subsections.

#### 4.2.1.1 Sample Characterization

A representative composite groundwater sample was obtained from groundwater pumping well HPIA-GW-24, located within the HPIA Operable Unit. A raw unfiltered aliquot of this

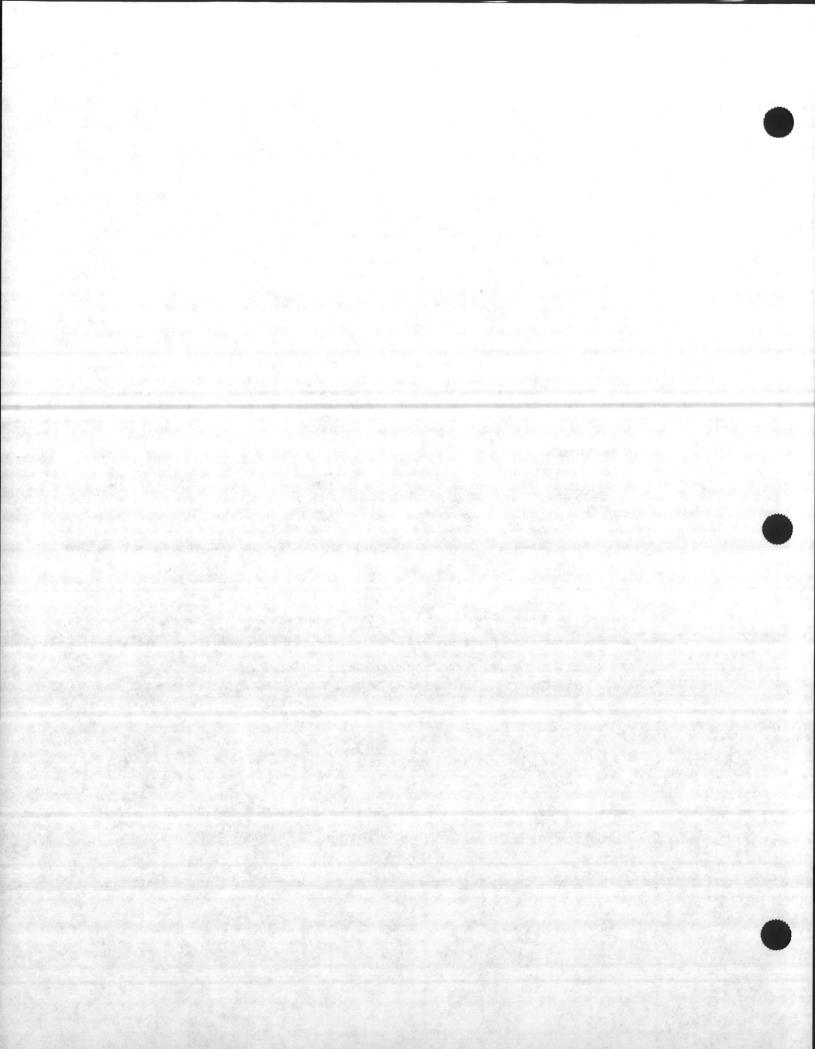
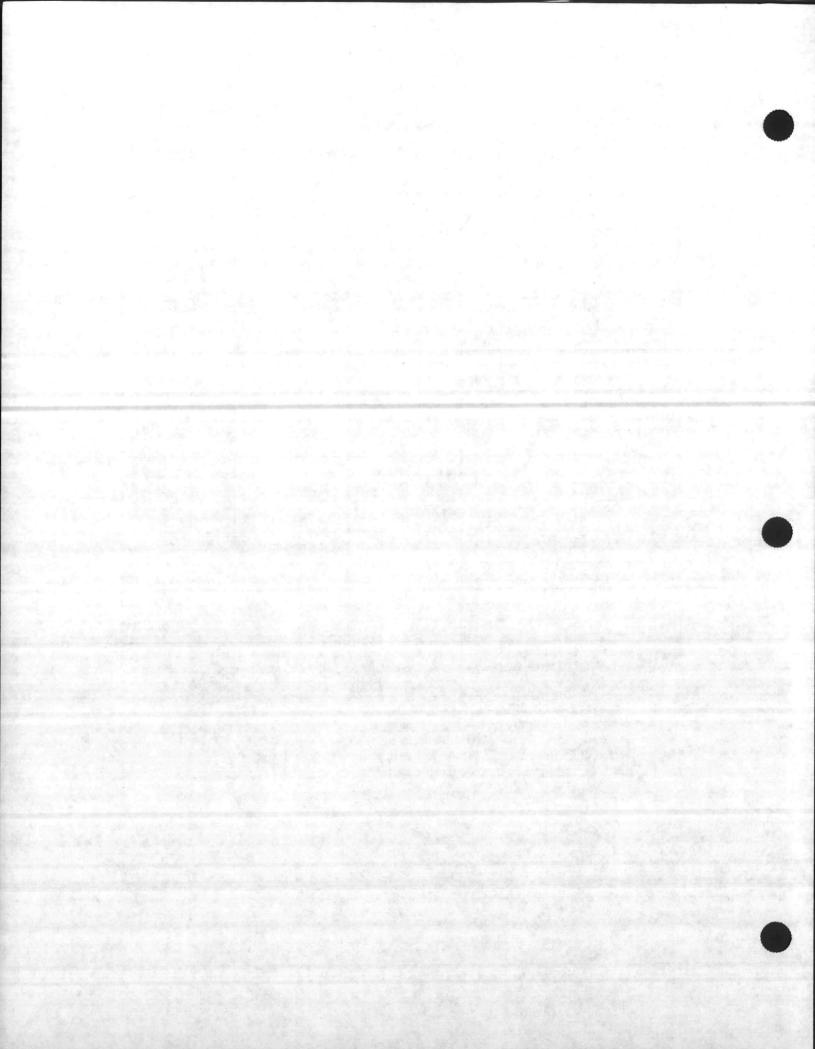


TABLE 4-1

# FEDERAL AND STATE CRITERIA FOR THE CONTAMINANTS OF CONCERN IDENTIFIED FOR THE SHALLOW AQUIFER

Contaminant of Concern	North Carolina* Water Quality Criteria for Groundwater (µg/L)	Federal Drinking Water MCLs (µg/L)	North Carolina* Water Criteria for Fresh Surface Water (µg/L) Class C Waters	North Carolina* Water Quality Criteria for Tidal Salt Waters (µg/L) Class SC Waters	
TCE	2.8	5	92.4 (4)	92.4 (4)	
1,2-DCE	-	70		-	
Benzene	1	5	71.4 (4)	71.4 (4)	
Antimony	-	6			
Arsenic	50	50	50 (1)	50(1)	
Beryllium	- 100 mil	4	.117(4) 6.5(1)	.117 (4)	
Chromium	50	100	50 (1)	20(1)	
Iron	300	-	1000 (5)	-	
Lead	50	15(3)	25 (1)	25 (1)	
Manganese	50	-	-	-	
Mercury	1.1	2	0.012 (1) .025 (1)		
Nickel	150	100	88 (1)		

- From NC Administrative Code 15A NCAC 2B.0200
- (1) Protection of Aquatic Life.
- (2) -- = No standard established.
- (3) MCL is action level for public water supply systems.
- (4) Protection of Human Health through consumption of fish/shell fish.
   (5) NC Action Level for discharge to fresh waters.



water was submitted for analysis of Target Analyte List (TAL) metals and selected engineering parameters. The purpose of the analysis was to determine a representative value for total inorganics and oil & grease content of groundwater from the HPIA Operable Unit. In addition, a groundwater aliquot was field filtered through a 0.45-micron filter using a vacuum pump. This sample was analyzed for TAL metals to provide information on concentrations of dissolved metals in HPIA groundwater. A summary of the analytical methods, sample preservation, and other pertinent details regarding the bench-scale analytical requirements is presented in Table 4-2.

Comparison of sample characterization data with anticipated discharge criteria and knowledge of general engineering practices will provide a reliable indication as to whether pretreatment for metals and/or solids removal is necessary. For instance, if dissolved metals concentrations are below anticipated discharge criteria, then physical treatment to remove suspended solids (gravity settling and/or filtration) would provide adequate pretreatment. If dissolved metals concentrations exceed anticipated discharge criteria, then some form of chemical treatment or advanced physical treatment (e.g. ultrafiltration) may be required.

# 4.2.1.2 Oil/Water Separation

Oil/water separation treatability testing was conducted on HPIA groundwater samples to assess the need for free phase oil and grease removal prior to organics removal (e.g., air stripping and/or carbon adsorption) and to provide information in sizing separation equipment and product storage. The treatability testing consisted of a single oil/water separation run. To set up the test run, groundwater (well mixed near room temperature) was poured into a large pyrex jar and allowed to sit quiescently over a one hour period. Samples for oil and grease analysis were extracted from below the discernible oil layer at various time intervals. A description of the detailed test procedures implemented in the treatability testing are outlined below:

#### TEST PROCEDURES FOR OIL/WATER SEPARATION TREATABILITY TESTING

- (1) Set up bench-scale oil/water separation apparatus as shown in Figure 4-1.
- (2) Retrieve groundwater samples from cold storage (approximately 4 degrees C) and place in a warm water bath. Allow temperature of samples to reach approximate room temperature.

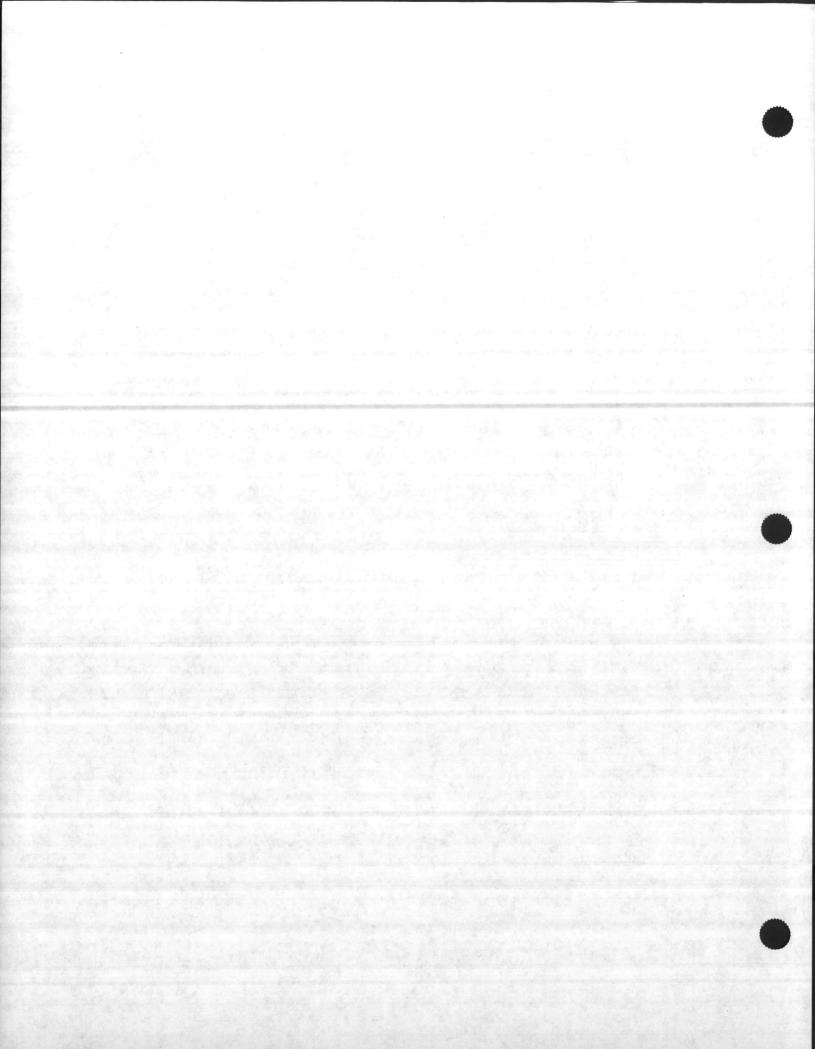
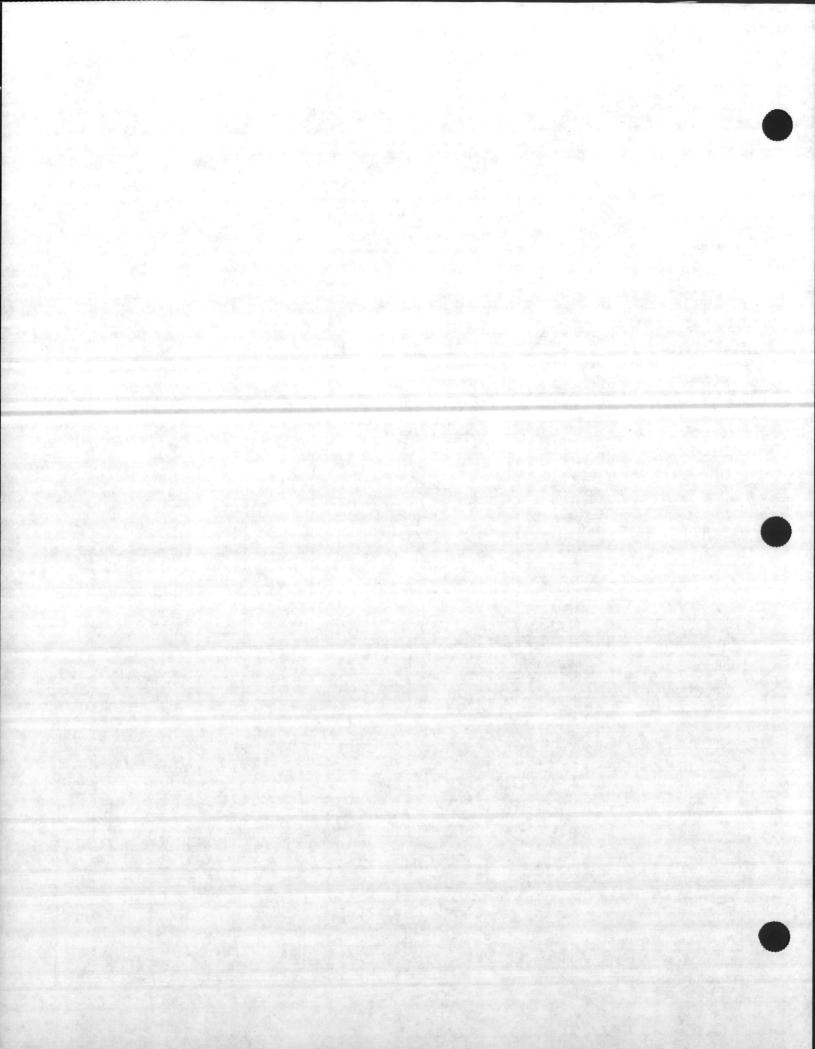
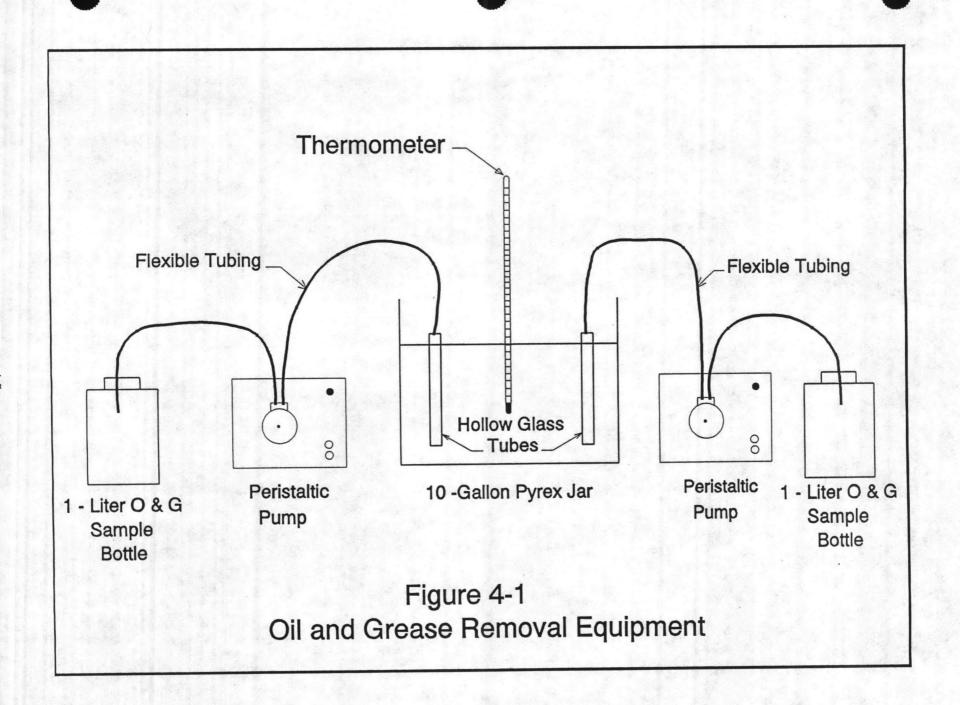
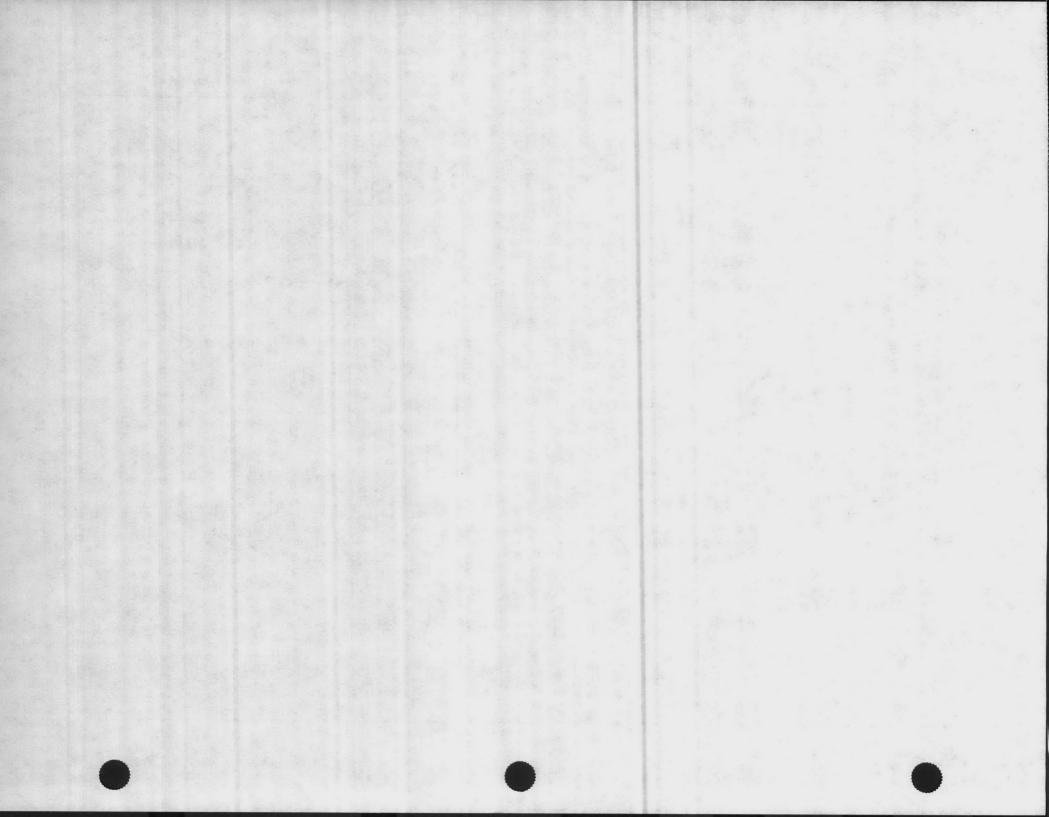


Table 4-2
Groundwater Characterization and Bench-Scale Treatability Testing Analytical Requirements Summary Table

Parameter	Method	Practical Quantitation Limit (ug/l)	Sample Volume Requirement	Container Type	Sample Preservation	Holding Time
Target Analyte List Metals						
		40				
Aluminum	EPA 200.7	40				
Antimony	EPA 204.2	2				
Arsenic	EPA 206.2	5	The Bullion of the			
Barium	EPA 200.7	2				
Beryllium	EPA 200.7	2	de terres de la companya de la comp			
Cadmium	EPA 213.2	1				
Calcium	EPA 200.7	5				
	EPA 215.1					
Chromium	EPA 218.2	5				
Cobalt	EPA 200.7	5				
Copper	EPA 200.7	7				
Iron	EPA 200.7	6				180 Days
Lead	EPA 239.2	5				
Magnesium	EPA 200.7	100	500 ml	Plastic	Cool to 4 C	Except
Manganese	EPA 200.7	1			HNO3 to pH < 2	Mercury at 28 Days
Mercury	EPA 245.1	0.2				
Nickel	EPA 200.7	20				
Potassium	EPA 200.7	200				
Selenium	EPA 270.2	2				
Silver	EPA 200.7	20				
Sodium	EPA 200.7	100				
Thallium	EPA 279.2	5				
Vanadium	EPA 200.7	7				
Zinc	EPA 200.7	50				
Engineering Parameters						
Ammonia	EPA 350.2	100	500 ml	Plastic	Cool to 4 C H2SO4 to pH < 2	28 Days
Bicarbonate	SM 403/406C	1000	500 ml	Plastic	None Required	14 Days
	SM 403/406C			Plastic	None Required	14 Days
Carbonate	EPA 325.2	1000		Plastic	None Required	28 Days
Chloride	EPA 130.2	1000		Plastic	HNO3 to pH < 2	180 Days
Hardness	EPA 353.2	1000	The second secon	Plastic	Cool to 4 C	28 Days
Nitrate/Nitrite	EFA 333.2		200		H2SO4 to pH < 2	
Oil and Grease	EPA 413.1	2000	1000 ml	Glass	Cool 4 C H2SO4 to pH < 2	28 Days
Total Dissolved Solids	EPA 160.1	1000	250 ml	Plastic	Cool to 4 C	7 Days
Total Suspended Solids	EPA 160.1	1000		Plastic	Cool to 4 C	7 Days



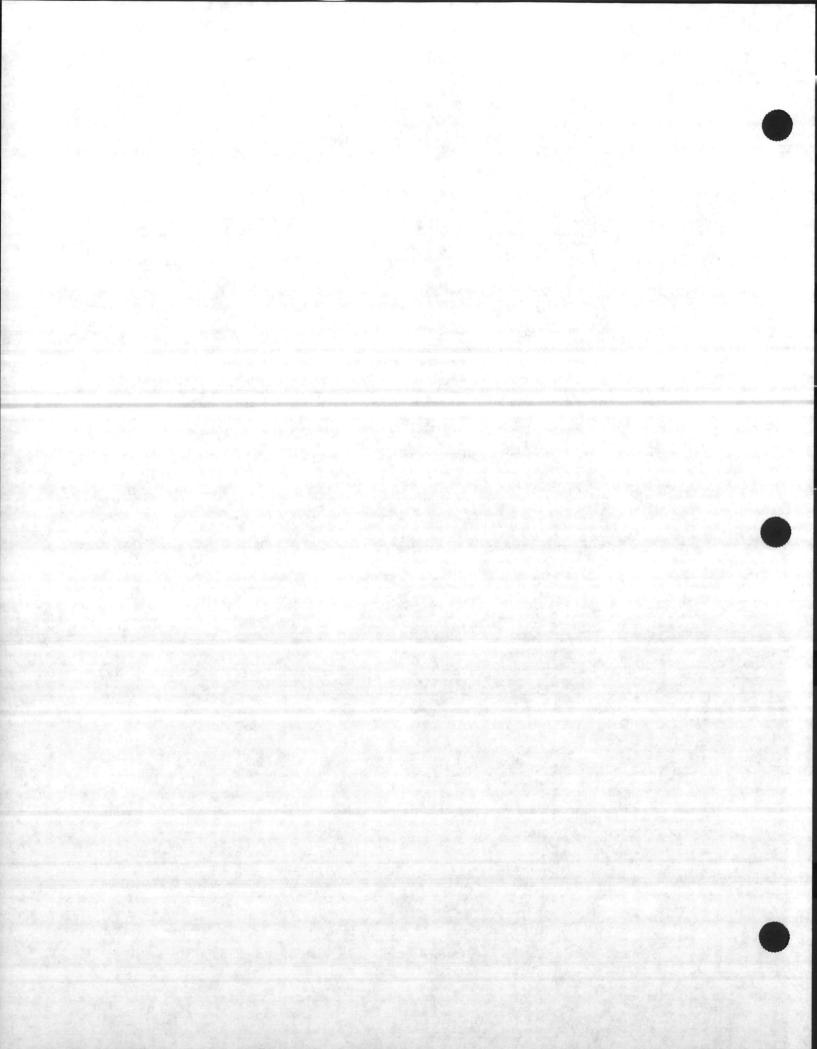




- (3) Measure 1 liter of groundwater using a 1 liter glass beaker and pour into the 9 gallon glass Pyrex vessel. Continue measuring and adding groundwater until approximately 10 liters is added to vessel. Record total volume of groundwater added.
- (4) Once groundwater has been completely added to vessel, start tracking time. Collect samples at the following time intervals: 15 minutes, 30 minutes, and 60 minutes. Record observations of settling or separation (i.e., visible layer(s) of oil and grease, sediment), as well as the general appearance of sample in vessel. The sampling procedure is discussed in more detail below.
  - (a) After each time interval is reached, turn on sampling pump and withdraw a 1 liter sample. The tubing with pipette end from pump suction should be inserted below the discernible oil layer to ensure that floating oil and grease is not collected in sample withdrawn from vessel.
  - (b) Place each 1 liter sample in a 1 liter amber glass jar for analysis of oil and grease. In addition to the three samples, collect an additional sample at 60 minutes for Quality Assurance/Quality Control.
  - (c) Record the following information on all samples to be submitted for analysis:
    - Project Name
    - Client
    - Sample No.
    - Date of Sample
    - Sampler(s) Initials
- (5) Fill out chain-of-custody form(s) for samples and submit for analysis.
- (6) Place residuals from treatability study in 5-gallon plastic buckets and firmly seal lid for subsequent disposal.

# 4.2.1.3 Gravity Settling

Gravity settling tests were conducted on groundwater samples collected from the HPIA Operable unit. The purpose of performing the tests was to determine if gravity settling will



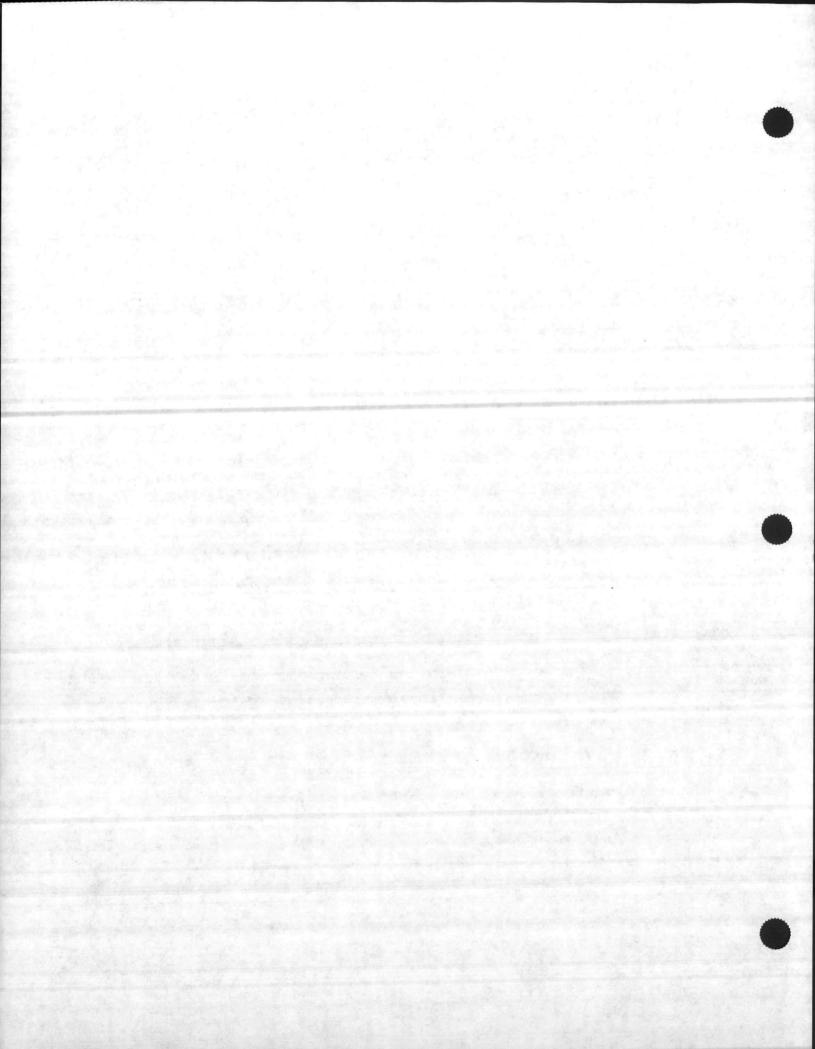
provide sufficient physical treatment to remove metals to levels that will meet anticipated discharge criteria. Based on the sample characterization results (presented in Section 5.0), it was determined that chemical treatment (metals precipitation jar tests) would not be necessary because the metals of concern were primarily associated with the suspended solids. However, because addition of appropriate polymers can enhance the coagulation and flocculation of solid particles, agglomeration of smaller particles and subsequent settling of solids, evaluation of cationic/anionic polymer addition was included in the treatability testing.

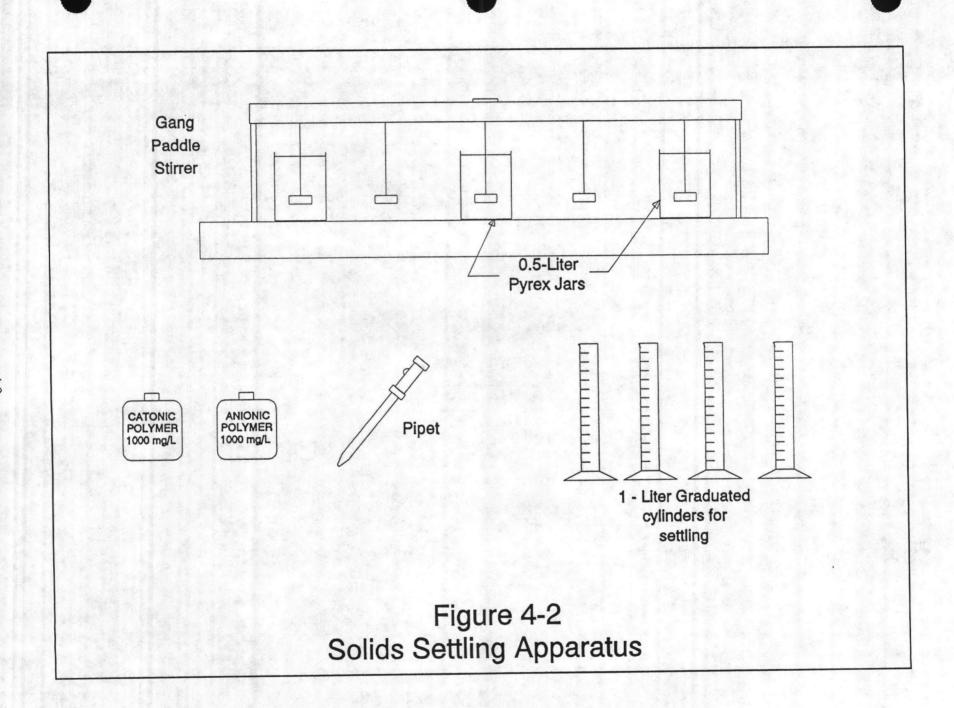
The treatability testing consisted of two test runs. The first run evaluated gravity settling of raw groundwater samples and the second run investigated the settling characteristics of raw groundwater when mixed with a predetermined optimal dosage of polymer. The optimal polymer type and dosage was determined by mixing aliquots of raw groundwater with three dosages each of cationic and anionic polymer and selecting the mixture that qualitatively appeared to yield the best settling.

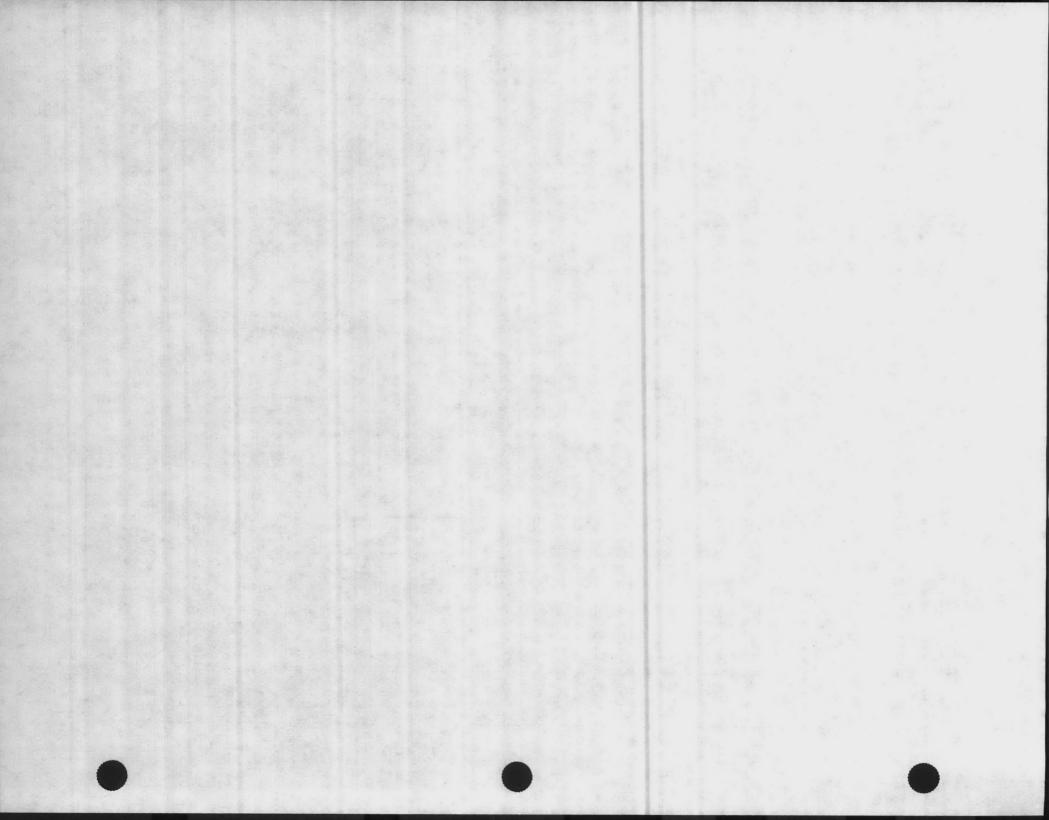
A description of the detailed test procedures implemented in the treatability testing are outlined below:

# TESTING PROCEDURES FOR GRAVITY SETTLING AND SELECTION OF OPTIMUM POLYMER DOSAGE

- (1) Set up bench-scale gravity settling apparatus and polymer testing equipment as shown in Figure 4-2.
- (2) Retrieve groundwater samples from cold storage (approximately 4 degrees C) and place in a warm water bath. Allow temperature of samples to reach approximate room temperature.
- (3) Pour raw groundwater sample into a beaker and mix with a glass stirring rod. Obtain and place two samples in plastic containers for initial analysis (before gravity settling) of total suspended solids (TSS) and metals (Al, As, Cr, Fe, Pb, and Mn).
- (4) Clean four 1000 ml graduated cylinders and identify as #1, #2, #3, and #4. Fill each cylinder with a well mixed sample of raw groundwater.







(5) Start clock after last cylinder is filled. Pump top 250 ml of supernatant out of cylinder #1 at 10 minutes, cylinder #2 at 20 minutes, cylinder #3 at 30 minutes, and cylinder #4 at 60 minutes. Each sample should be obtained by placing suction tubing of pump in top of cylinder and drawing sample off. Place samples in appropriate containers and designate for the following analysis:

Cylinder #1 10 min. TSS
Cylinder #2 20 min. TSS
Cylinder #3 30 min. TSS
Cylinder #4 60 min. TSS, Al, As, Cr, Fe, Pb, Mn

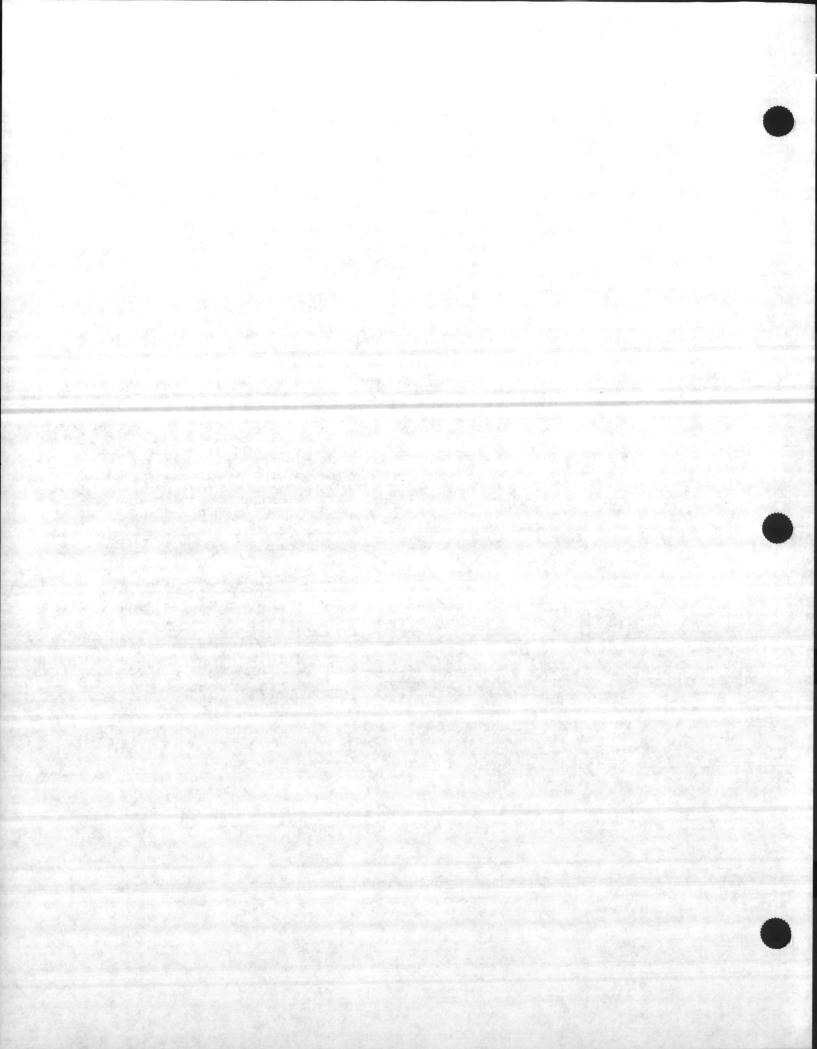
Observe and record settling characteristics of sample in each cylinder at each sampling interval.

(6) Evaluate mixtures of raw groundwater with several anionic and cationic polymer dosages to qualitatively determine an optimal polymer type and dosage. For this treatability study, the polymers evaluated were Armstrong APS (anionic) and Calgon Pol-E-Z 692 (cationic).

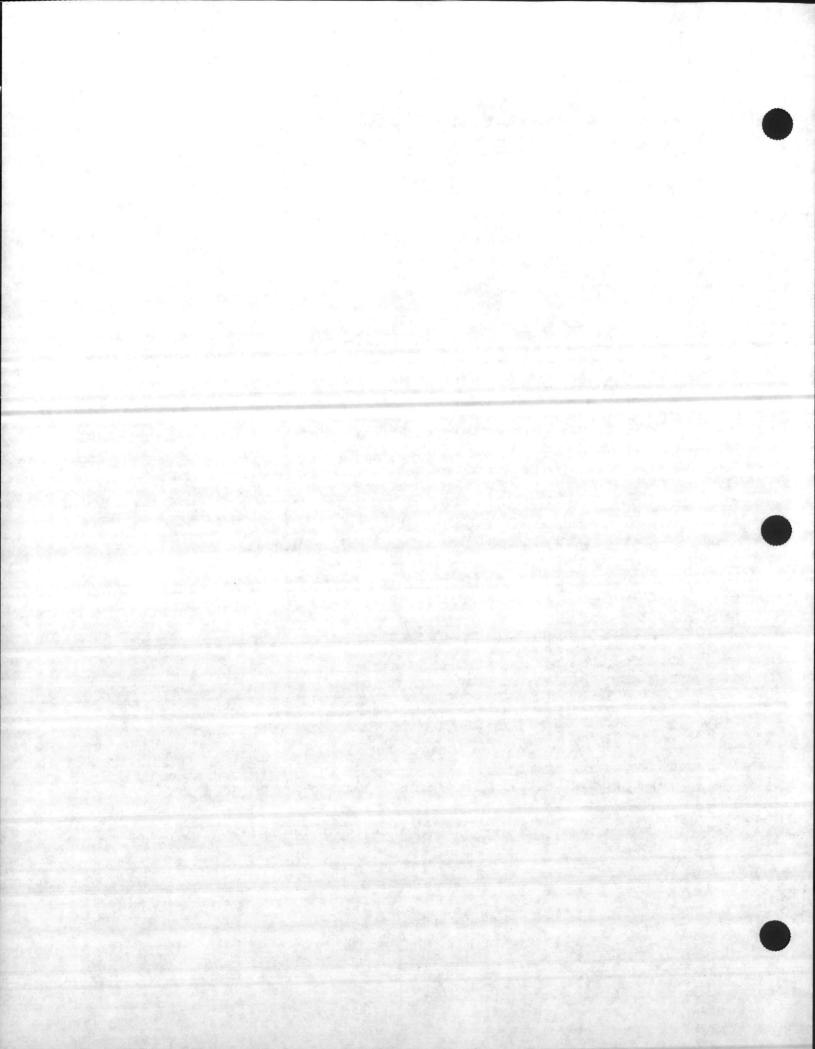
The evaluation was performed in the following manner:

Anionic/Cationic Polymer Evaluation

- (a) Mix in separate glass beakers an aliquot of raw groundwater with anionic polymer at dosages of 0.25, .5, 1, and 2 mg/L, respectively.
- (b) Place beakers under a paddle stirrer and agitate each mixture at a low speed for approximately 5 minutes.
- (c) Repeat Steps (a) and (b) above, except use cationic polymer.
- (d) Observe and record characteristics of mixtures (i.e. are there agglomerates of solids particles, settling of particles, and a well defined supernatant?)



- (e) Based on visual observations and best engineering judgment, identify the polymer and dosage which appears to yield the most favorable results with the minimum quantity of polymer used.
- (7) Obtain two additional raw groundwater samples and place in two separate containers for initial analysis (before gravity settling with chemical treatment) of TSS and metals (Al, As, Cr, Fe, Pb, and Mn). These will serve as QA/QC samples for the raw groundwater settling run.
- (8) Mix raw groundwater and polymer in a 2000 ml glass beaker. The type (anionic or cationic) and dosage should be that determined in step (6) outlined above. Fill each of four clean 1 liter graduated cylinders with a well mixed sample of raw groundwater and polymer and repeat Step (5) above, except collect samples at the following time intervals from each cylinder and designate for analysis as follows:
  - Cylinder #1 5 min. TSS
  - Cylinder #2 10 min. TSS
  - Cylinder #3 15 min. TSS
  - Cylinder #4 30 min. TSS; Al, As, Cr, Fe, Pb, Mn
- (9) Record the following information on all samples to be submitted for analysis:
  - Project Name
  - Client
  - Sample No.
  - Date of Sample
  - Sampler(s) Initials
- (10) Fill out chain-of-custody form(s) for samples and submit for analysis.
- (11) Place residuals from treatability study in 5-gallon plastic buckets and firmly seal lid for subsequent disposal.



## 4.2.2 Equipment and Materials

This subsection presents a description of the test equipment and materials used in the benchscale treatability testing of groundwater samples from the HPIA Operable unit.

## 4.2.2.1 Oil/Water Separation

The following equipment is required to set up the treatability apparatus and complete the oil/water separation bench-scale treatability testing:

## Equipment

- (1) 9-gallon glass Pyrex vessel
- (2) Ring stands with adjustable clamps
- (2) Masterflex peristaltic pumps, including drive, pump head (#7016), and tygon tubing (#7016)
- (2) Glass Pipettes (attach to pump suction tubing)
  Miscellaneous glass beakers
- (2) Rubber stoppers (use as weight on pipette suction tubing)
- (1) Thermometer (-20 to 110 deg. C)
- (1) Tape ruler
- (4) Amber glass jars, preserved with H<sub>2</sub>SO<sub>4</sub> to pH < 2
- (1) 5-gallon plastic bucket with lid (residual disposal)

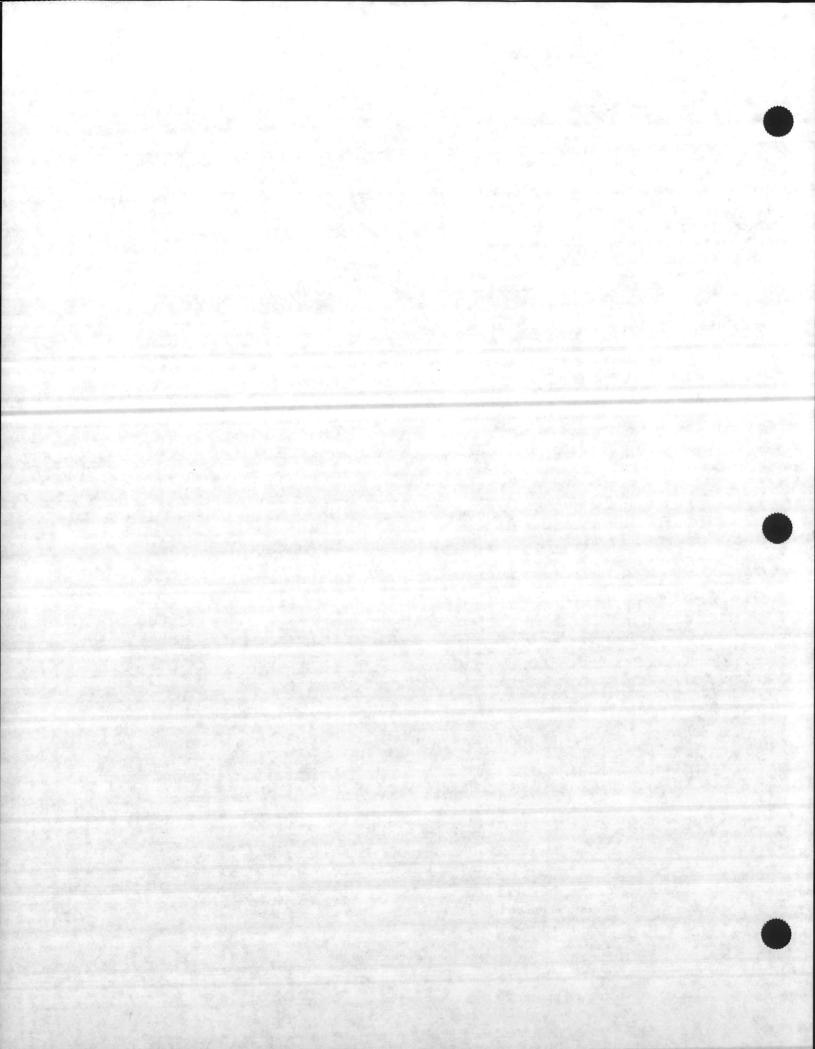
Set up the test apparatus, as depicted in Figure 4-1.

#### 4.2.2.2 Gravity Settling

The equipment and materials required to set up the treatability apparatus, determine the optimum polymer type and dosage, and perform gravity settling tests are summarized below:

## Equipment

- (4) 1-liter graduated cylinders
- (1) Gang Paddle Stirrer
- (1) Portable Mixer (to prepare stock polymer solutions)



Miscellaneous glass beakers

- (1) Ring stand w/clamp (for portable mixer)
  Clear plastic jars with teflon lined caps for sample collection
  Anionic Polyelectrolyte (APS Armstrong) 1000 mg/L solution
  Cationic Polymer (Calgon Pol-E-Z 692) 1000 mg/L solution
- (1) Pipette and Pipette Pump
- (1) 5-gallon plastic bucket with lid (residual disposal)

Set up the test apparatus, as depicted in Figure 4-2.

## 4.2.3 Sampling and Analysis

Analytical methods, bottle requirements, and preservation and storage details used in the bench-scale treatability study are presented on Table 4-2.

## 4.3 Pilot-Scale Testing

In order to determine the effectiveness and implementability of using an air stripper and liquid phase carbon adsorption unit to treat groundwater, pilot-scale testing of this equipment was performed. This task consisted of extracting the groundwater through a submersible pump and discharging it through an air stripper and a carbon adsorption unit.

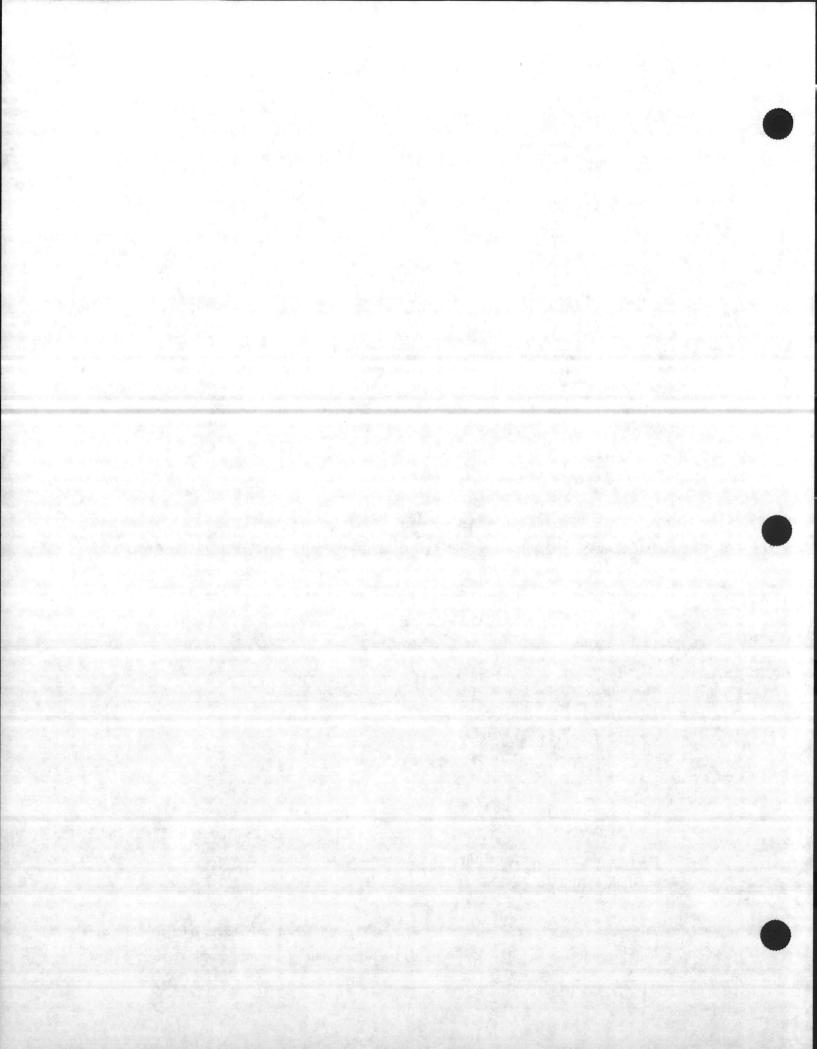
#### 4.3.1 Experiment Design and Procedures

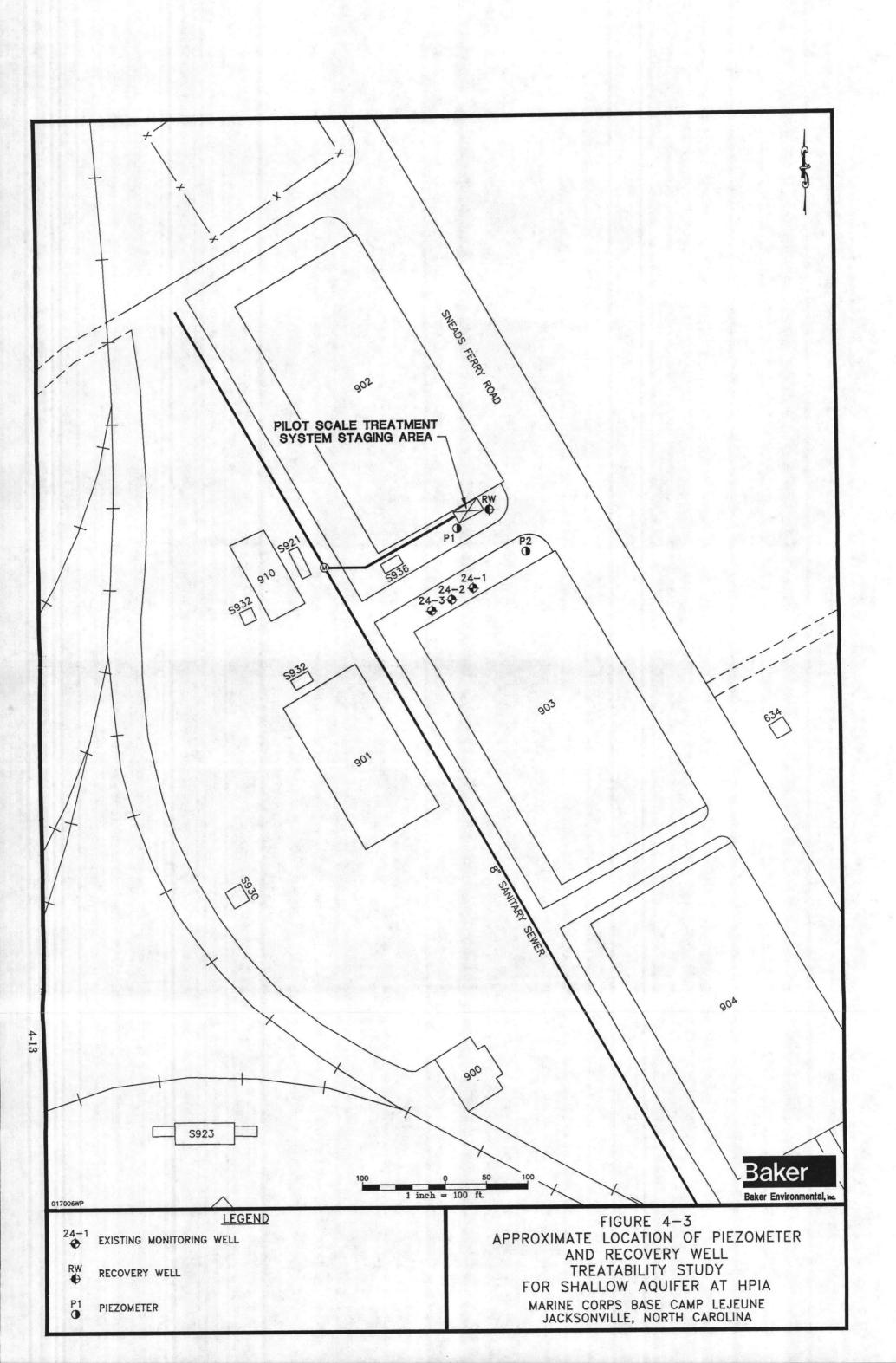
This subsection describes the design and procedures for conducting the pilot-scale test.

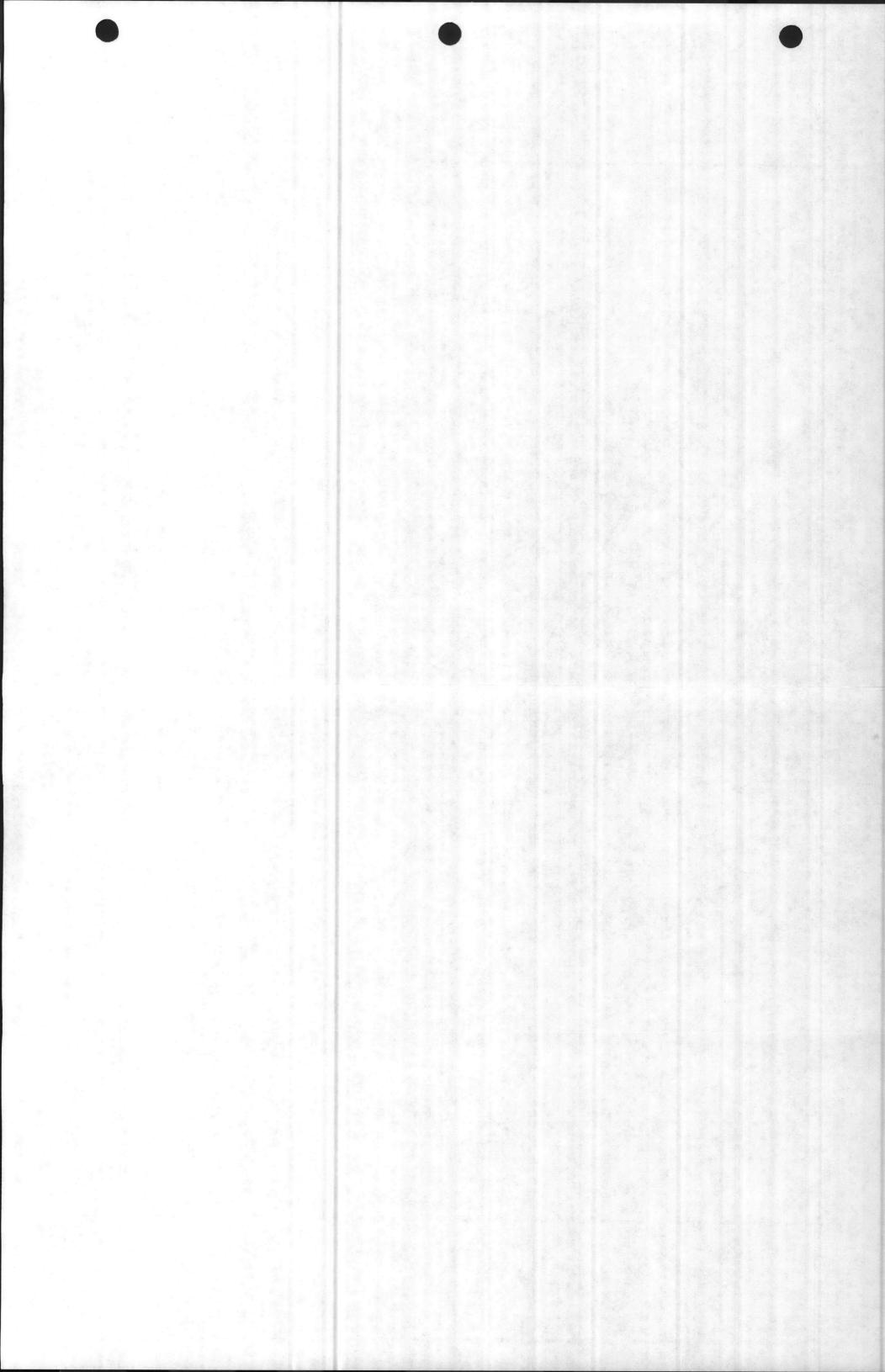
#### 4.3.1.1 Aquifer Pump Test

During the week of January 24, 1993 Baker personnel installed a recovery well, and two piezometers for aquifer test activities. The recovery well and monitoring system consisted of a single 6-inch recovery well, three monitoring wells (previously installed) and two, 2-inch piezometers. The location of the wells, piezometers and pilot-scale treatment equipment are shown in Figure 4-3.

The recovery system consisted of a pressure transducer and an electric submersible pump installed 6 inches from the bottom of the well. The pump and transducer were secured to an







adjacent concrete filled post with a nylon rope. A solid 1 inch PVC pipe was used as the discharge line and extended from the pump to the flow meter. To allow for clear downhole observation of the recovery well, the electric cable, discharge line, and the rope were taped together at periodic intervals.

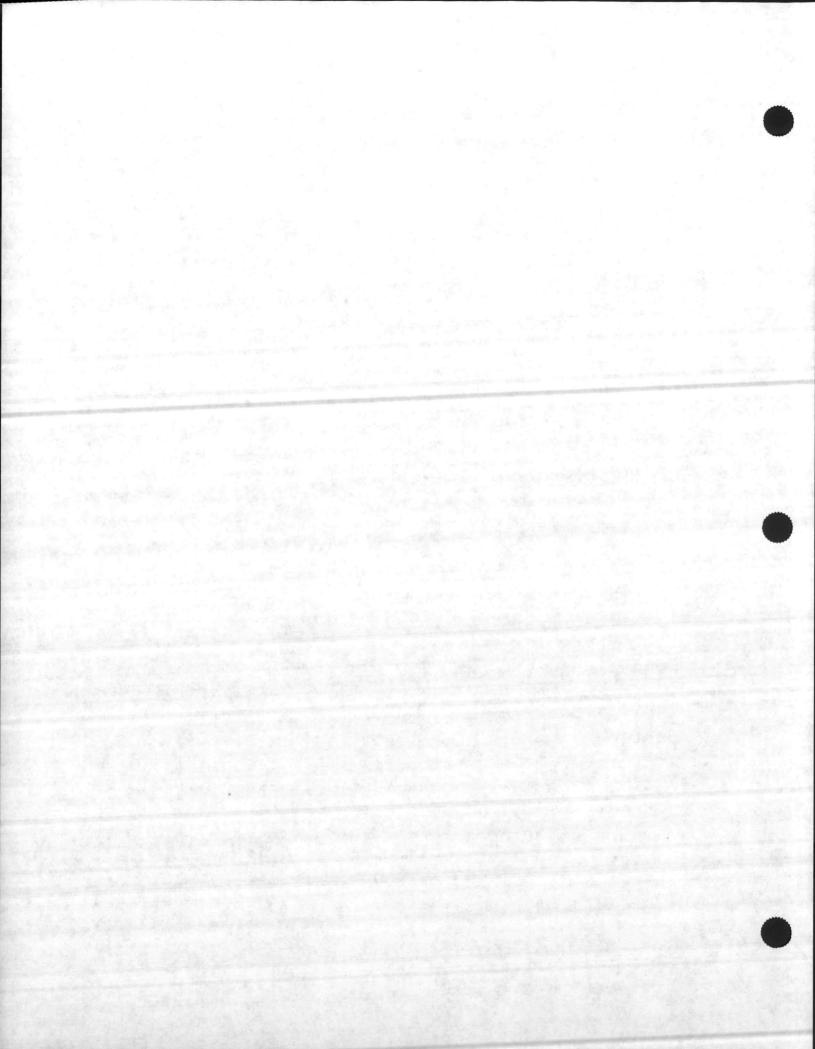
At the top of the well, the discharge line was connected to a totalizing flow meter with an accuracy of 0.1 gpm. To regulate discharge flow from the pump a 3/4" gate valve was installed downstream from the flow meter. Groundwater pumped from the recovery well was discharged to the pilot-scale treatment system (see Section 4.3.1.2).

# 4.3.1.1.1 Recovery Well and Piezometer Construction

The recovery well, RW-1, was constructed of 6-inch nominal diameter, flush-joint and threaded stainless steel casing, with a 10-foot long, 0.010-inch slotted, continuous wrap screen. A medium-grained sand pack extending above the top of the screen was placed in the annulus between the screen and the borehole wall. A bentonite pellet seal was placed above the sand pack and hydrated with potable water. The remaining annular space was backfilled with a cement/bentonite mixture to ground surface. A PVC locking cap was fitted at the top of the well. A diagram of the well is located in Appendix L.

Following well construction activities, the recovery well was developed to remove fine grain sediments from the well boring and to facilitate the hydraulic connection between the well and the water-bearing layer. The recovery well was developed using a submersible pump. The well was overpumped and then allowed to recover. This process was repeated until the water was visually sediment-free. Approximately 150 gallons of water (5-6 well volumes) were removed. The water recovered from each well was contained in 55-gallon steel drums and labeled.

Piezometers P-1 and P-2 were constructed of 2-inch nominal diameter Schedule 40, flush-joint and threaded PVC casing, with a 10-foot long, 0.010-inch slotted screen. A medium-grained sand pack extending to a depth of one foot below the surface was placed in the annulus between the screen and the borehole wall. A one-foot thick bentonite pellet seal was placed above the sand pack and hydrated with potable water. A PVC locking cap was fitted at the top of the well. The piezometers are temporary and will be removed at a later date.



Following installation, the piezometers and recovery well were surveyed by James E. Stewart and Associates, Inc., of Jacksonville, North Carolina (registered in the State of North Carolina) using standard procedures. The top of casing and ground surface elevations were measured for the piezometer locations to the nearest 0.01-foot. A temporary benchmark was established on site based on existing National Geodetic Vertical Datum (NGCD) elevations relative to Mean Sea Level (MSL).

## 4.3.1.1.2 Step-Drawdown Test

#### Test Set Up

The step-drawdown test was initiated on February 1, 1993. Prior to the start of this test, static water levels were measured at all the locations equipped with pressure transducers and in seven outlying monitoring wells. These measurements were taken with a water level meter. These fluid levels are shown in Table 4-3.

To monitor hydrogeologic activity induced from the step-drawdown test, transducers were placed in four wells and two piezometers between Buildings 902 and 903. Transducers in piezometer P-1 and recovery well RW-1, located adjacent to Building 902, were controlled by a two channel In-Situ SE-1000C data logger. Transducers in piezometer P-2, and monitoring wells HPGW24-3, HPGW24-2, and HPGW24-1, located adjacent to Building 903, were controlled by a four channel In-Situ SE-2000 data logger. Each pressure was referenced to the initial static water levels. To maintain a constant position relative to the test datum the cable of each pressure transducer was secured to the protective casing of the well.

Both the SE-1000C and the SE-2000 were set to obtain water level data on a logarithmic scale. Water levels were recorded by the hydrologic monitors from pressure transducers according to the following schedules:

#### SE-2000 (Well RW-1 and piezometer P-2)

Elapsed Time		Sampling Interval	
-	0-5 seconds	0.5 seconds	
	5-20 seconds	1.0 seconds	
•	20-120 seconds	5.0 seconds	
•	2-10 minutes	0.5 minutes	
	10-100 minutes	2.0 minutes	
	100 minutes-end	5.0 minutes	

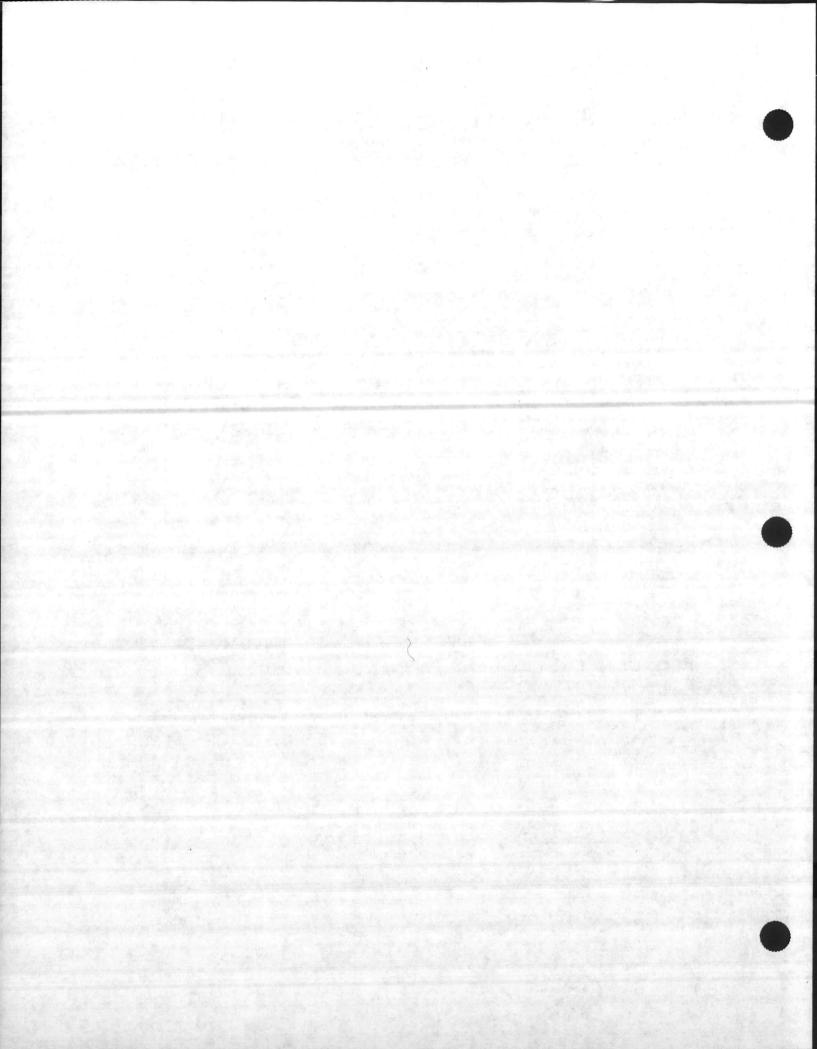


Table 4-3
Summary of Fluid Level Measurements Prior to Step-Drawdown Test
February 1,1993

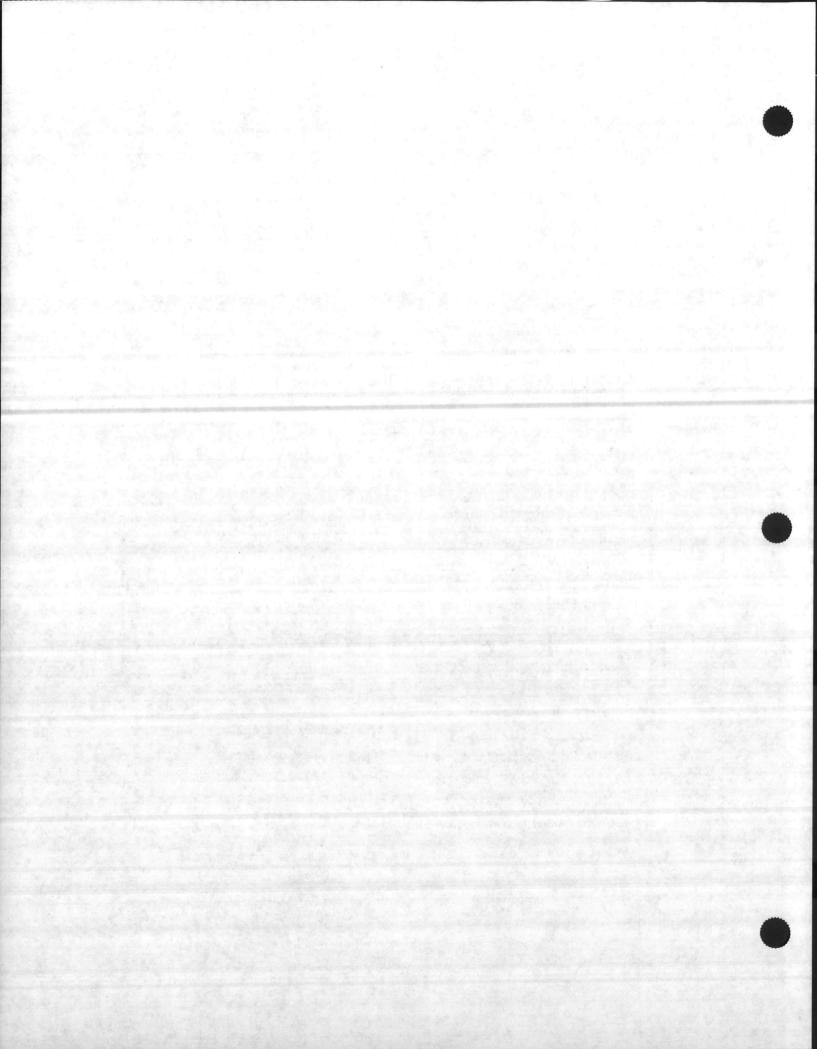
# Hadnot Point Industrial Area CTO-017

Date	Time	Well Number	Top of Casing Elevation (feet above MSL)	Depth to Groundwater (feet below top of casing)	Groundwater Elevation (feet above MSL)
2/01/93	13:12	RW-1	33.22	6.88	26.34
2/01/93	13:10	P-1	30.67	6.76	23.91
2/01/93	13:10	P-2	30.68	4.44	26.24
2/01/93	13:19	HPGW24-	32.82	6.68	26.14
2/01/93	13:23	HPGW24-	33.75	12.72	21.03
2/01/93	13:26	HPGW24-	32.34	11.61	20.73
2/01/93	11:08	HPGW21	33.59	10.57	23.02
2/01/93	11:15	GW22-1	31.52	9.14	22.38
2/01/93	11:20	GW22-2	28.84	8.13	20.71
2/01/93	09:01	HPGW22	32.35	6.72	25.63
2/01/93	08:57	HPGW23	32.09	9.27	22.82
2/01/93	09:07	HPGW25	32.58	6.75	25.83
2/01/93	10:41	HPGW30-	29.75	9.28	20.47
2/01/93	10:43	HPGW30-	29.72	9.25	20.47

Notes:

(MSL) - Mean Sea Level

Top of casing elevations for RW-1, P1, P2, HPIA 24-1, HPIA 24-2 and HPIA 24-3 were taken by James B.Stewart and Associates during February 1993. The remaining elevations were taken from the Remedial Action Report For Hadnot Point Industrial Area Operable Unit Shallow Soils and Castle Hayne Aquifer Study (E.S.E, Inc., April 1992).



• SE-1000C (Wells HPGW24-3, HPGW24-2, HPGW24-1 and piezometer P-2)

El	apsed Time	Sampling Interval
•	0-5 seconds	0.5 seconds
•	5-20 seconds	1.0 seconds
•	20-120 seconds	5.0 seconds
•	2-10 minutes	0.5 minutes
•	10-100 minutes	2.0 minutes
	100 minutes-end	2.0 minutes

The step-drawdown test was initiated on February 1, 1993 at 4:42 PM. Based upon previous investigations at the site, it was originally estimated that the maximum sustained discharge capacity of the recovery well would be 5 gpm. The proposed initial discharge rates for the step-drawdown test were 3 gpm (60 percent of maximum), 4 gpm (80 percent of maximum), 5 gpm (100 percent), and 6 gpm (120 percent).

All groundwater extracted during the step-drawdown tests was treated in accordance with the procedures outlined in Section 4.3.1.1.1.

#### Recovery Well RW-1

Based on flow rates observed during installation and mobilization of the pump, two discharge rates, 1.0 gpm (step one) and 2.0 gpm (step two), were selected for the step-drawdown test. After some slight initial adjustments of the flow meter, the discharge rate stabilized at 1.00 gpm. After 62 minutes at 1 gpm (step 1) step two was initiated. To initiate step 2, the flow was increased to 1.7 gpm. Gradually the discharge rate was increased to 2.2 gpm. At this discharge rate the well was pumped dry at 7:27 PM. At this time the flow was adjusted to 1.5 gpm and remained stable until the test was terminated. The step 2 pumping rate (1.5 gpm) was maintained for 124 minutes.

Based on the observed flow rates and drawdown observed in this well no additional steps above 2.0 gpm were performed and a rate of 1.5 gpm was selected for the constant rate test.

Average flow rates, duration of each step, and observed drawdowns are summarized in Table 4-4.

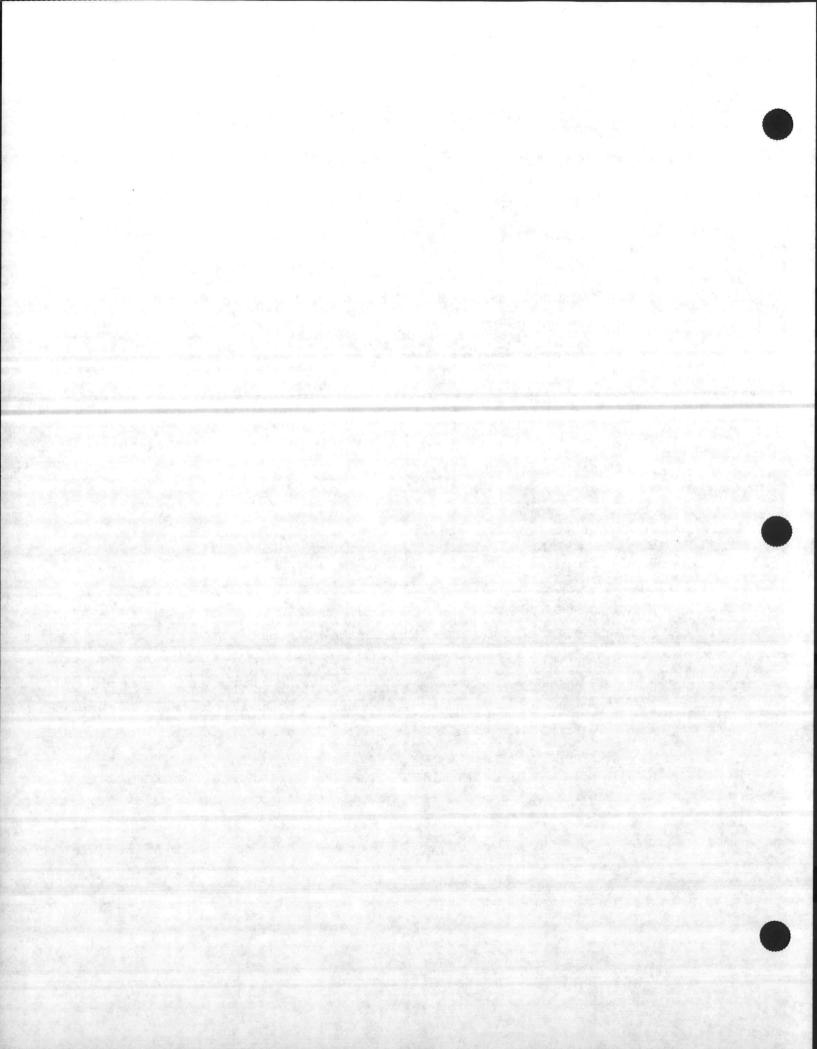
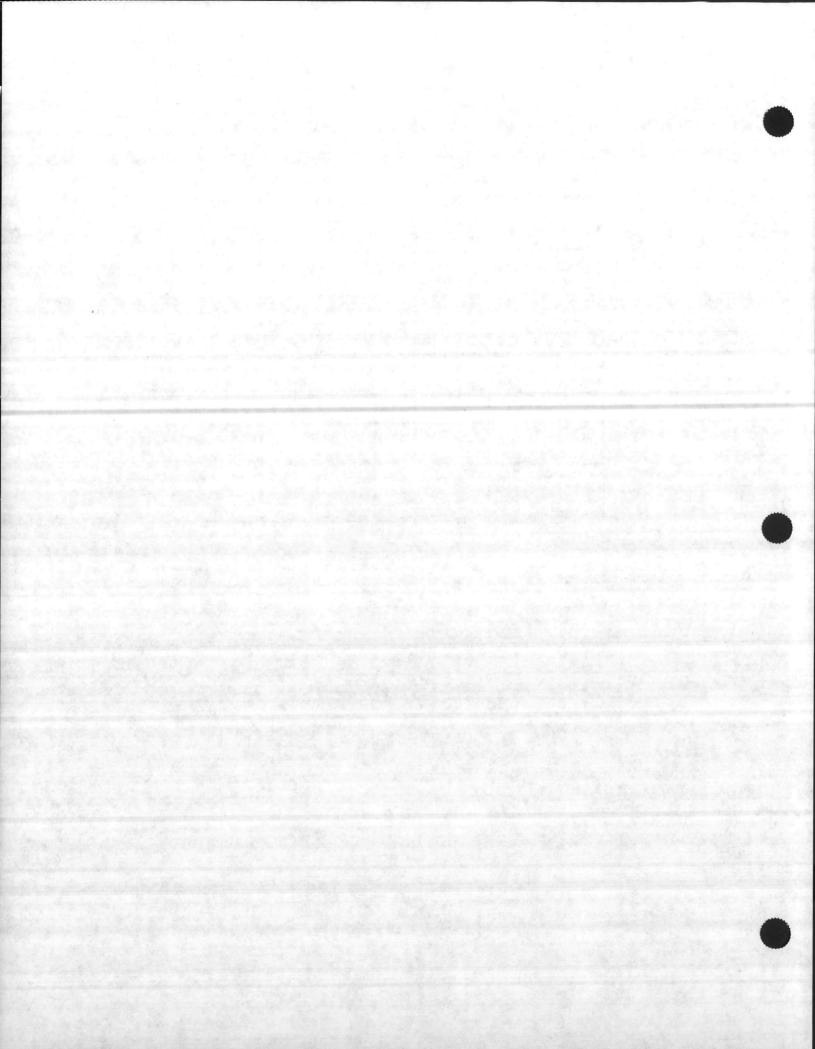


TABLE 4-4

## SUMMARY OF STEP-DRAWDOWN ACTIVITIES HADNOT POINT INDUSTRIAL AREA CTO-0017

Well Number	Flow Rate (gpm)	Duration (minutes)	Maximum Drawdown (feet)
RW-1	1.0	62	4.96
	1.5	124	9.55



## Monitoring Well and Piezometer Observations

The SE-2000 data logger recorded water levels in P-2, HPGW24-1, HPGW24-2, and HPGW24-3 and the SE-1000C data logger recorded levels in P-1 and RW-1. A drawdown of 1 foot was observed at P-2 which is 60 feet from the recovery well. At location P-1 (28 feet from the recovery well) 3 inches of drawdown was observed and at HPGW24-1 (75 feet from the recovery well) 4.5 inches of drawdown was observed. No drawdown was observed in HPGW24-2 (97 feet from the recovery well) and HPGW24-3 (119 feet from the recovery well). These values are summarized in Table 4-5. The data obtained by these data loggers is presented in Appendix A.

#### 4.3.1.1.3 Constant Rate Aquifer Test

#### Test Set Up

The purpose of the constant rate aquifer pump test was to evaluate aquifer characteristics (hydraulic conductivity, transmissivity, and storativity). The results of this test will be used in the design of a groundwater extraction remediation system for the shallow aquifer at HPIA.

Prior to the initiation of the 72-hour constant rate aquifer test, static water levels were manually measured in RW-1, P-1, P-2, HPGW24-1, HPGW24-2, HPGW24-3 and 8 other previously installed monitoring wells that were within approximately 1000 feet of the of the recovery well. These fluid level measurements are summarized on Table 4-6.

As in the step-drawdown test, the SE-2000 data logger recorded water levels in P-2, HPGW24-1, HPGW24-2, and HPGW24-3 and the SE1000C data logger recorded levels in P-1 and RW-1.

The SE-2000 (Well RW-1 and piezometer P-2) data logger was programed according to the following schedule:

E	apsed Time	Sampling Interval
	0-20 seconds	0.5 seconds
	20-60 seconds	1.0 seconds
	1-10 minutes	0.2 minutes
	10-100 minutes	2.0 minutes
	100 minutes-end	5.0 minutes

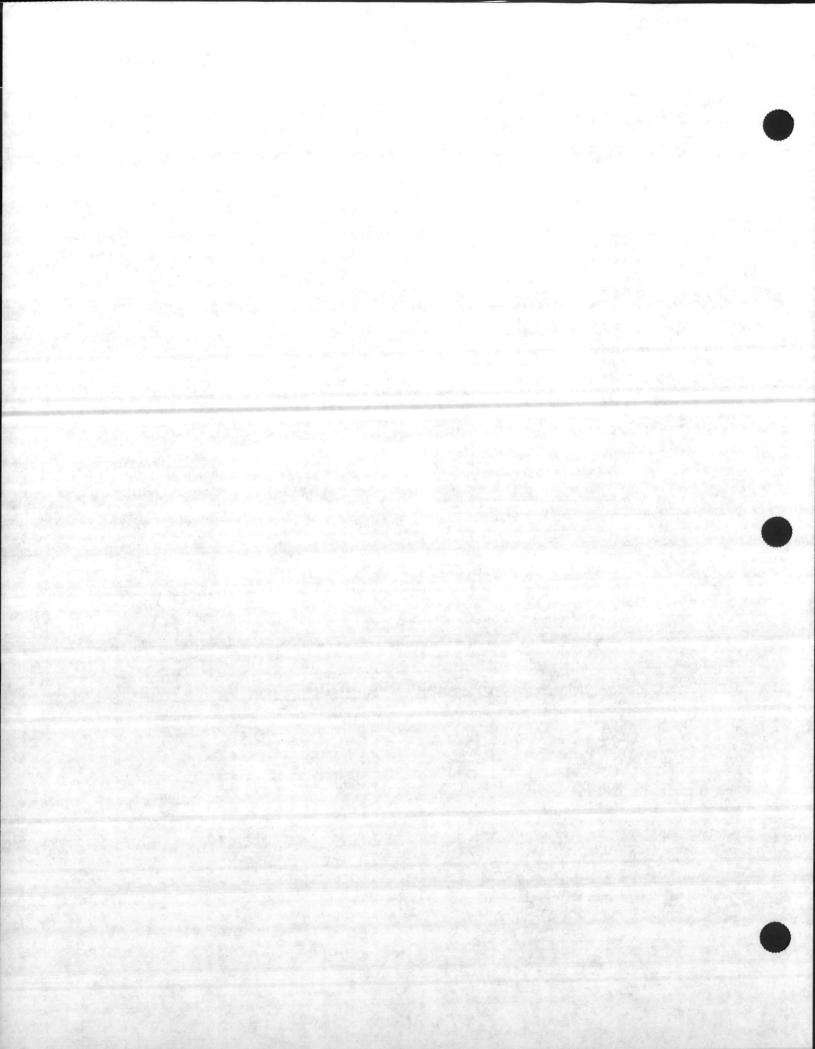


Table 4-5
Summary of Maximum Drawdowns During Step Test
CTO-017

Well Number	Datum(TOC) Elevation (feet, MSL)	Initial Depth to Groundwater (feet)	Final Depth to Groundwater (feet)	Drawdown (feet)	Initial Groundwater Elevation (feet, MSL)	Final Groundwater Elevation (feet, MSL)
RW-1	33.22	6.88	21.26	14.38	26.34	11.96
P-1	30.67	6.76	7.00	0.24	23.91	23.67
P-2	30.68	4.44	5.42	0.98	26.24	25.26
HPGW24-1	32.82	6.68	7.05	0.37	26.14	25.77
HPGW24-2	33.75	12.72	12.77	0.05	21.03	20.98
HPGW24-3	32.34	11.61	11.66	0.05	20.73	20.68

(MSL) - Mean Sea Level

(TOC) - Top of Casing

Top of casing elevations for RW-1, P1, P2, HPIA 24-1, HPIA 24-2 and HPIA 24-3 were taken by James B.Stewart and Associates during February 1993. The remaining elevations were taken from the Remedial Action Report For Hadnot Point Industrial Area Operable Unit Shallow Soils and Castle Hayne Aquifer Study (E.S.E, Inc., April 1992).

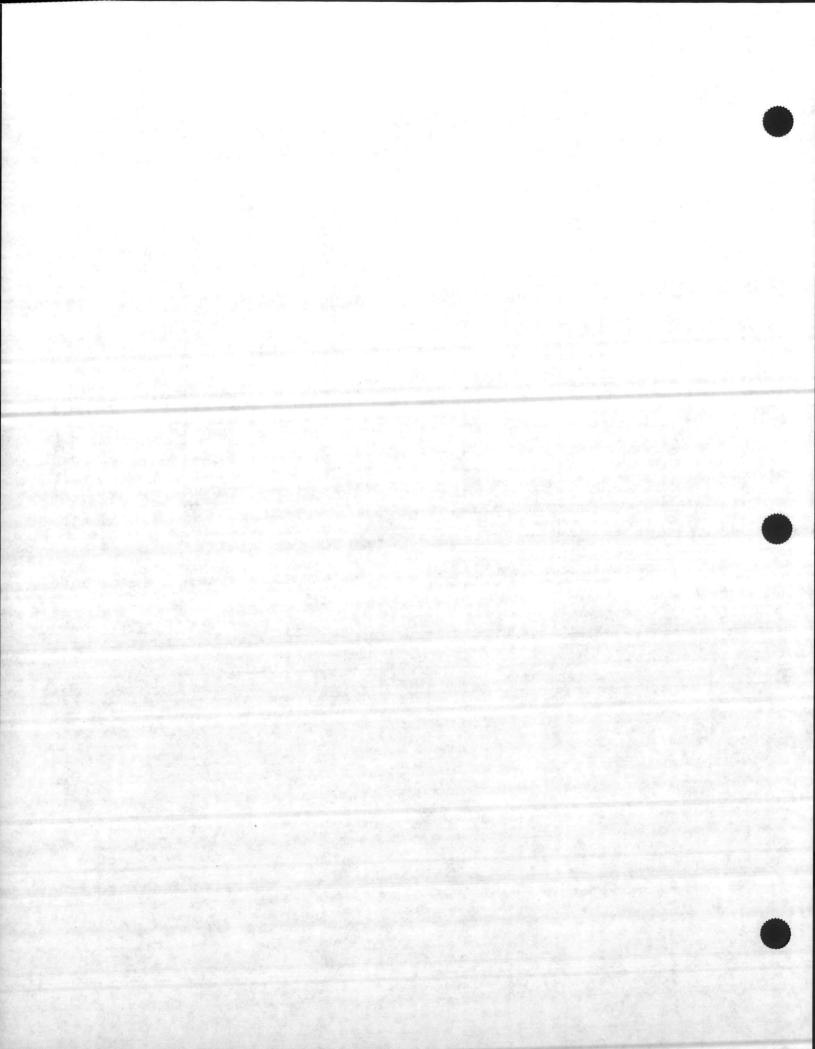


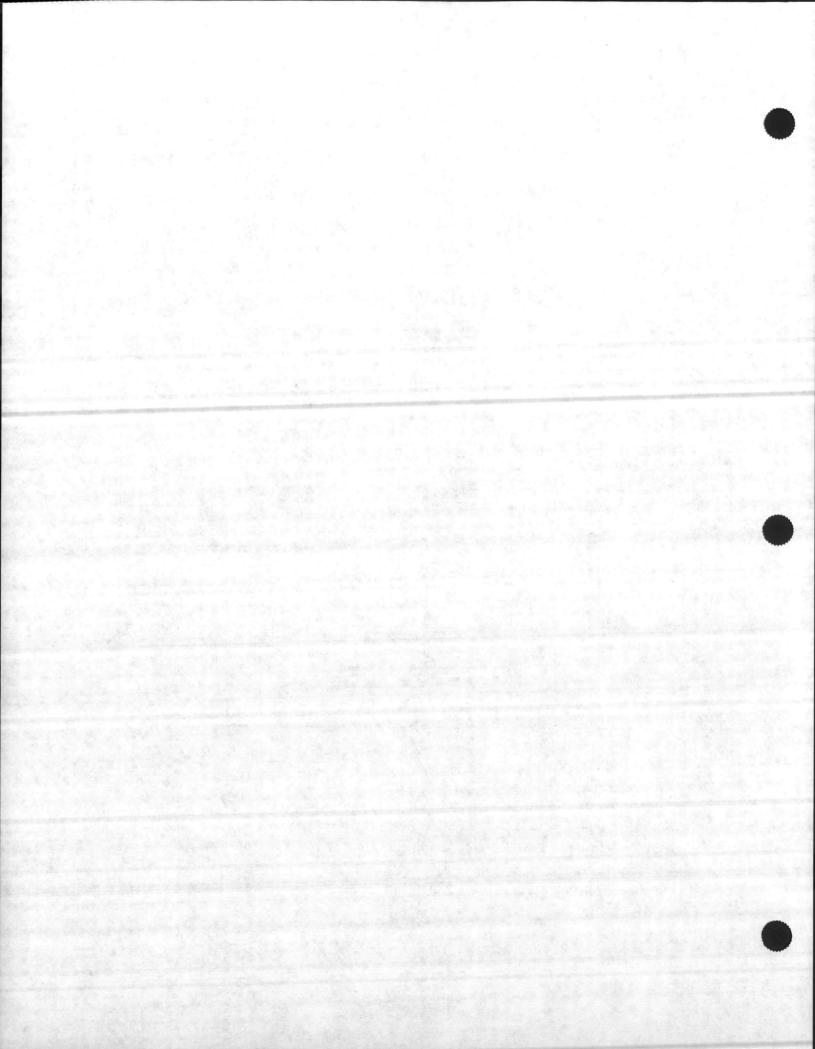
Table 4-6
Summary of Fluid Level Measurements
Prior to the Start of the Constant Rate Pump Test
February 6, 1993
Hadnot Point Industrial Area
CTO-017

Date	Time	Well Number	Top of Casing Elevation (feet above MSL)	Depth to Groundwater (feet below top of casing)	Groundwater Elevation (feet above MSL)
2/02/93	07:50	RW-1	33.22	7.45	25.77
2/02/93	07:55	P-1	30.67	7.30	23.37
2/02/93	07:51	P-2	32.34	5.10	27.24
2/02/93	07:59	HPGW24-1	32.31	7.30	25.01
2/02/93	08:07	HPGW24-2	33.73	12.75	20.98
2/02/93	08:12	HPGW24-3	32.80	13.00	19.8
2/02/93	09:20	HPGW21	33.59	10.70	22.89
2/02/93	09:31	HPGW22-1	31.52	9.59	21.93
2/02/93	09:40	HPGW22-2	28.84	8.47	20.37
2/02/93	09:07	HPGW22	32.35	7.00	25.35
2/02/93	08:55	HPGW23	32.09	9.75	22.34
*	*	HPGW25	32.58		
2/02/93	08:45	HPGW30-2	29.75	9.55	20.2
2/02/93	08:39	HPGW30-3	29.72	9.60	20.12

(MSL) - Mean Sea Level

\* - Not initially measured

Top of casing elevations for RW-1, P1, P2, HPIA 24-1, HPIA 24-2 and HPIA 24-3 were taken by James B.Stewart and Associates during February 1993. The remaining elevations were taken from the Remedial Action Report For Hadnot Point Industrial Area Operable Unit Shallow Soils and Castle Hayne Aquifer Study (E.S.E, Inc., April 1992). April 1992).



The SE-1000C (Wells HPGW24-3, HPGW24-2, HPGW24-1 and piezometer P-2) was programed according to the following schedule:

El	apsed Time	Sampling Interval
<b>&gt;</b>	0-2 seconds	0.2 seconds
	2-120 seconds	5.0 seconds
•	2-10 minutes	0.5 minutes
•	10-100 minutes	2.0 minutes
	100-end	10.0 minutes

#### **Test Operation**

The constant rate aquifer pump test began on February 2, 1993, at 10:05 AM. Over the length of the 72.5 hour drawdown phase of the aquifer test, a total of 5,312 gallons of groundwater were produced for an average flow rate of 1.22 gpm. Flow rate measurements recorded for the recovery well are provided in Appendix B.

Test flows were continually monitored during the drawdown phase. Difficulty was experienced achieving a constant flow rate of 1.2 gpm. Flow rates ranged from .6 gpm to 1.6 gpm. As flows began to deviate from 1.2 gpm by more than .25 gpm the 3/4 inch gate valve was appropriately adjusted.

The groundwater levels and the maximum drawdowns measured in the recovery well piezometers and monitoring wells, at an elapsed time of approximately 1,260 minutes are provided in Table 4-7. Drawdown data obtained by the data loggers is presented in Appendix C.

Upon termination of the drawdown phase of the test on February 5,1993 at 10:45 AM, both data loggers were set to monitor recovery data using the same scale that was used for the drawdown phase of the test. This data are provided in Appendix D and are summarized in Table 4-8.

All extracted groundwater was pumped through the pilot-scale treatment system before being released into the HPIA sanitary system. The capacity of the mobile pilot-scale treatment system was adequate to treat the groundwater as it was discharged and no additional liquid storage was needed.

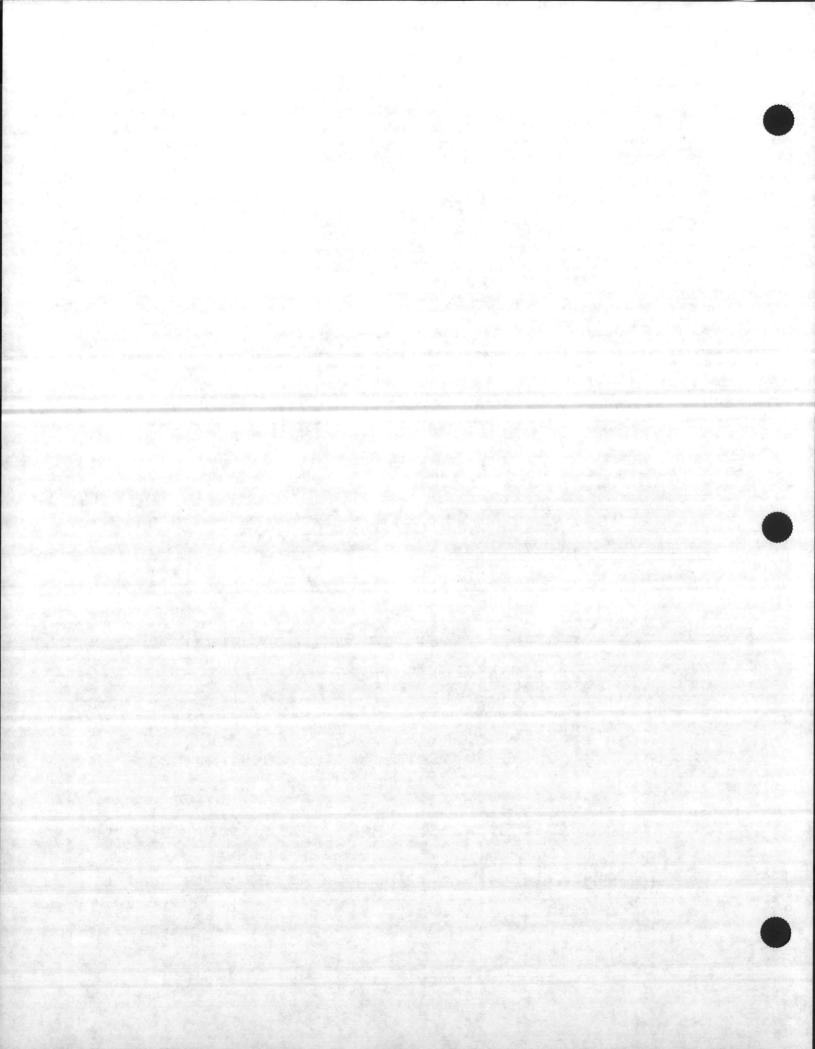


Table 4-7
Summary of Maximum Drawdowns During Constant Rate Aquifer Test
CTO-017

Well Number	Datum(TOC) Elevation (feet,MSL)	Initial Depth to Groundwater (feet)	Final Depth to Groundwater (feet)	Drawdown (feet)	Initial Groundwater Elevation (feet, MSL)	Final Groundwater Elevation (feet, MSL)
RW-1	33.22	7.45	20.87	13.42	25.77	12.35
P-1	30.67	7.30	7.92	0.62	23.37	22.75
P-2	32.34	5.10	6.96	1.86	27.24	25.38
HPGW24-1	32.31	7.30	8.17	0.87	25.01	24.14
HPGW24-2	33.73	12.75	12.89	0.14	20.98	20.84
HPGW24-3	32.80	13.00	13.16	0.16	19.80	19.64
HPGW21	33.59	10.70	10.70	0.00	22.89	22.89
GW22-1	31.52	9.59	9.56	0.00	21.93	21.96
GW22-2	28.84	8.47	8.56	0.09	20.37	20.28
HPGW22	32.35	7.00	7.30	0.30	25.35	25.05
HPGW23	32.09	9.75	9.86	0.11	22.34	22.23
HPGW25	32.58	7.08	7.34	0.26	25.50	25.24
HPGW30-2	29.75	9.55	9.68	0.13	20.20	20.07
HPGW30-3	29.72	9.60	9.44	0.00	20.12	20.28

(MSL) - Mean Sea Level

(TOC) - Top of Casing

Top of casing elevations for RW-1, P1, P2, HPIA 24-1, HPIA 24-2 and HPIA 24-3 were taken by James B.Stewart and Associates during February 1993. The remaining elevations were taken from the Remedial Action Report For Hadnot Point Industrial Area Operable Unit Shallow Soils and Castle Hayne Aquifer Study (E.S.E, Inc., April 1992).

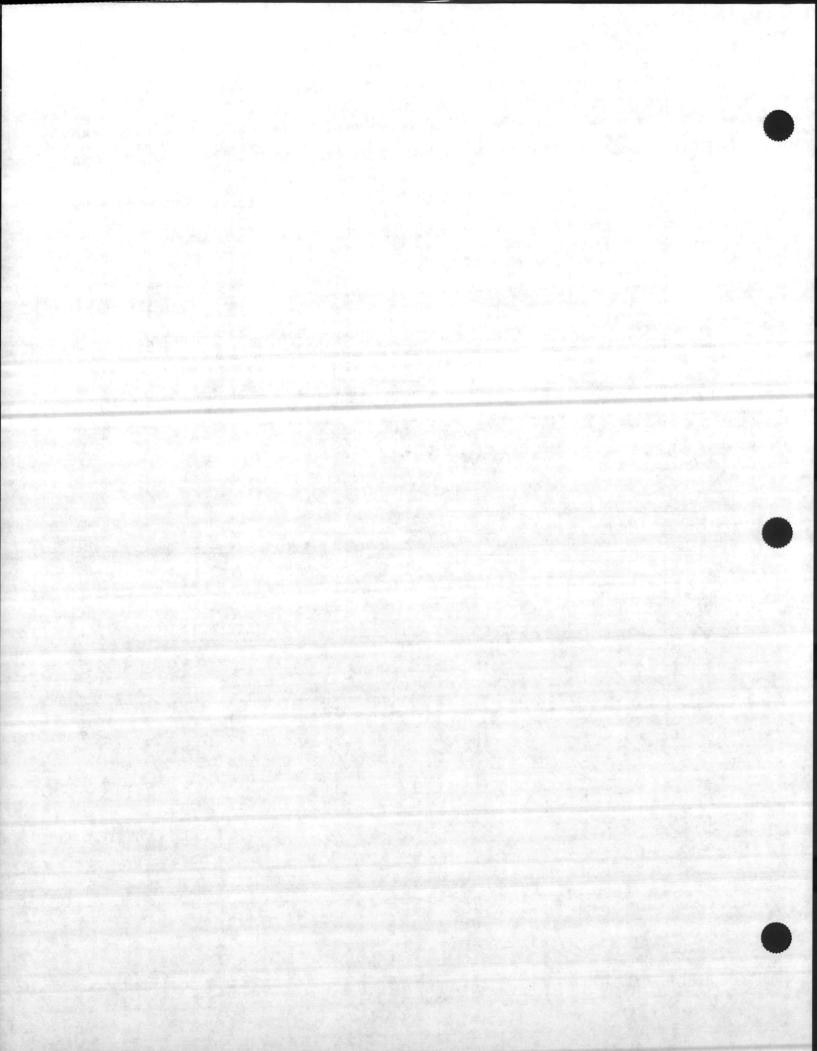
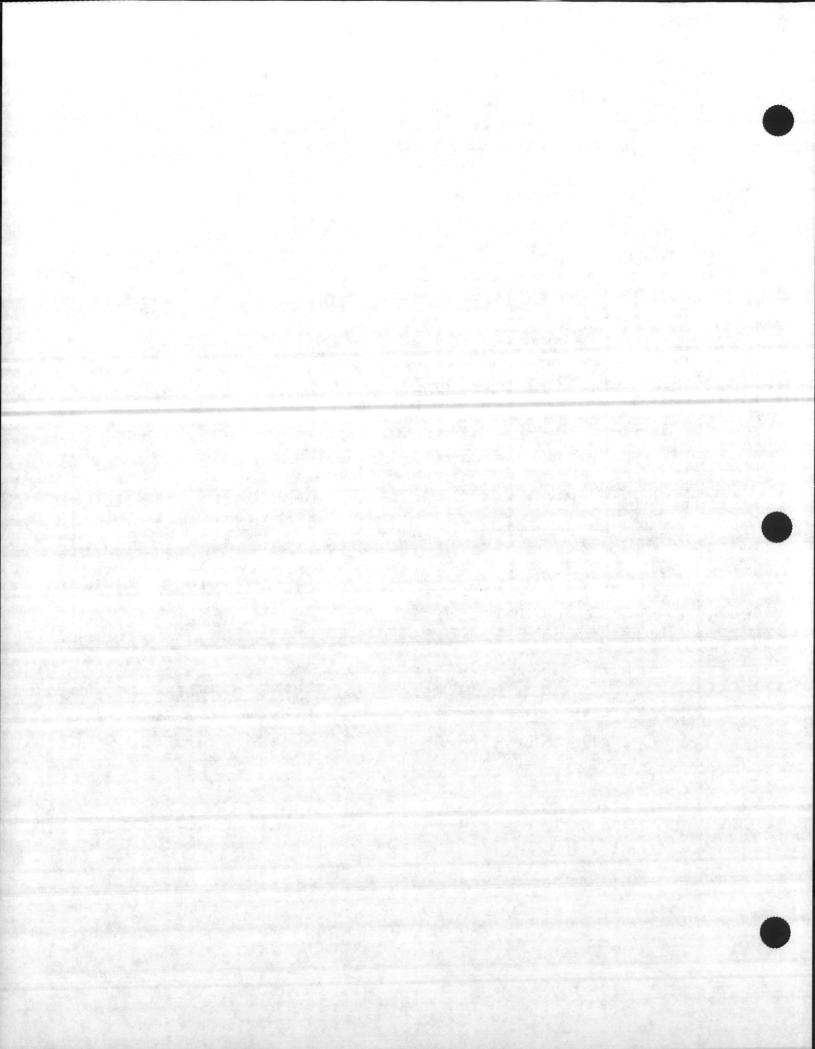


Table 4-8
Summary of Fluid Level Measurements After Recovery
February 6, 1993
Hadnot Point Industrial Area
CTO-017

Date	Time	Well Number	Top of Casing Elevation (feet above MSL)	Depth to Groundwater (feet below top of casing)	Groundwater Elevation (feet above MSL)
2/06/93	10:34	RW-1	33.22	7.78	25.44
2/06/93	10:44	P-1	30.67	7.48	23.192
2/06/93	10:34	P-2	30.68	5.45	25.226
2/06/93	10:44	HPGW24-1	32.82	7.53	25.287
2/06/93	10:44	HPGW24-2	33.75	12.77	20.985
2/06/93	10:44	HPGW24-3	32.34	13.05	19.294
2/06/93	10:01	HPGW21	33.59	10.66	22.93
2/06/93	10:08	GW22-1	31.52	9.42	22.1
2/06/93	10:12	GW22-2	28.84	8.46	20.38
2/06/93	09:46	HPGW22	32.35	7.46	24.89
2/06/93	09:38	HPGW23	32.09	9.72	22.37
2/06/93	09:08	HPGW25	32.58	9.60	22.98
2/06/93	9:30	HPGW30-2	29.75	9.60	20.15
2/06/93	09:30	HPGW30-3	29.72	9.64	20.08

(MSL) - Mean Sea Level

Top of casing elevations for RW-1, P1, P2, HPIA 24-1, HPIA 24-2 and HPIA 24-3 were taken by James B.Stewart and Associates during February 1993. The remaining elevations were taken from the Remedial Action Report for Hadnot Point Industrial Area Operable Unit Shallow Soils and Castle Hayne Aquifer Study (E.S.E., Inc., April 1992).



# 4.3.1.2 Pilot-Scale Treatability Testing

Groundwater pumped from recovery well RW-1 during the aquifer pump test was discharged to a pilot-scale treatment system. This treatment system was mobilized and set-up along side the recovery well and adjacent to Building 904, as shown on Figure 4-3. Effluent from the treatment system was discharged to the 8-inch sanitary sewer line at the south end of Building 902. Final discharge of the treated groundwater was through the HPIA Sewage Treatment Plant (STP).

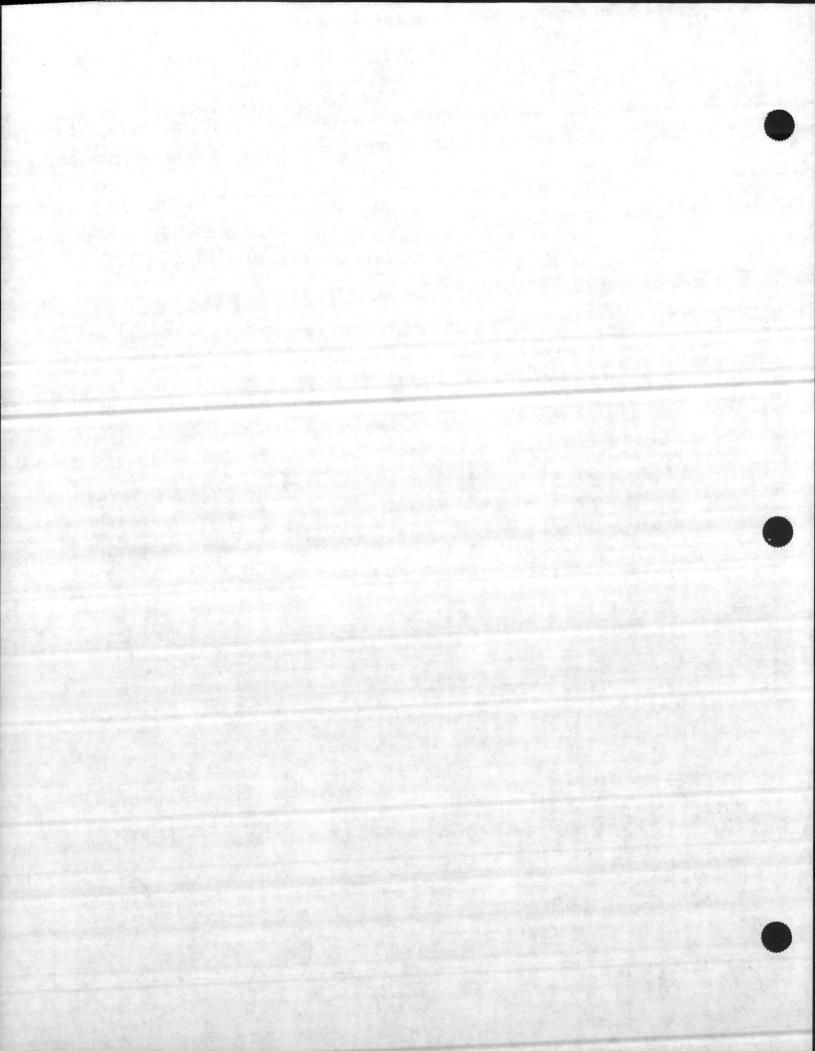
The pilot-scale treatment system consisted of an oil/water separator, an air stripper, and a carbon adsorption tank as shown schematically on Figure 4-4. The oil/water separator consisted of two, 350-gallon FRP tanks connected in series. A 300-gallon steel surge tank was placed downstream of the oil/water separator and equipped with an electric sump pump and float switch to discharge water to the air stripper. The air stripper was a shallow tray-style stripper consisting of two trays and equipped with a one horsepower, 625 cubic feet per minute (CFM) air blower. The holding capacity of the air stripper tank was 400 gallons. Hydrostatic pressure caused by influent from the oil/water separator surge tank forced effluent from the air stripper to the carbon adsorption tank. The carbon adsorption unit was a single tank with 800 pounds of activated carbon manufactured by Hadley Industries. Effluent from the carbon adsorption unit was discharged to the HPIA sanitary sewer system.

#### 4.3.2 Sampling and Analysis

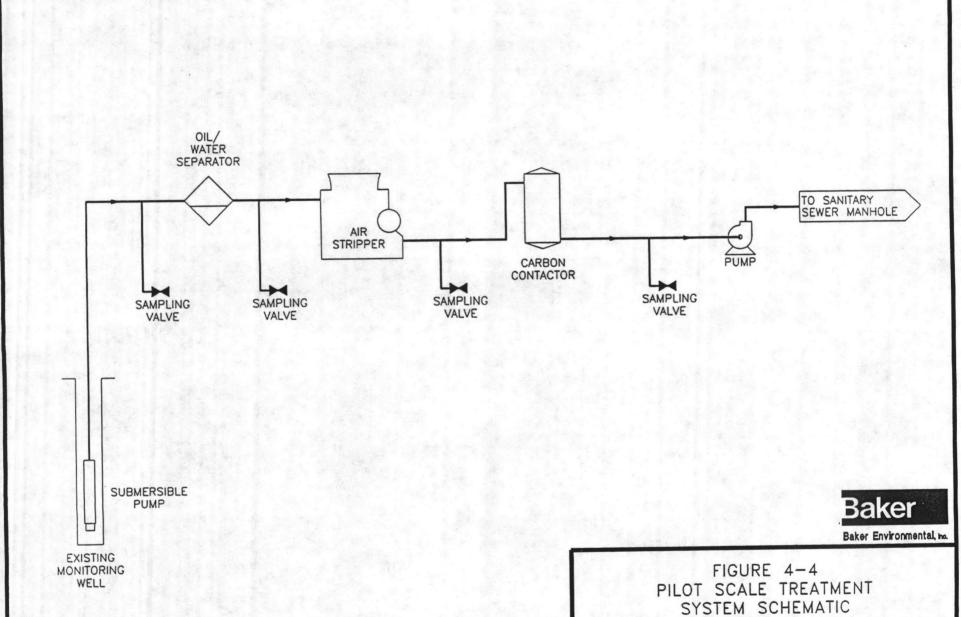
A sampling and analysis program was conducted during the duration of the aquifer pump test and pilot-scale treatability study in order to quantify the effectiveness of the various treatment components. This program included chemical analysis for volatile organics, metals, and engineering parameters, as well as multi-concentration acute toxicity testing. Table 4-9 summarizes the analytical requirements of the pilot-scale study.

Samples were collected at the start-up, at regular intervals (approximately 12 hours), and at completion of the aquifer pump test. These samples were collected from sampling ports at the following locations:

- Influent to the air stripper
- Effluent from the air stripper
- Effluent from the carbon adsorption



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TREATABILITY STUDY FOR SHALLOW AQUIFER AT HPIA

MARINE CORPS BASE CAMP LEJEUNE JACKSONVILLE, NORTH CAROLINA

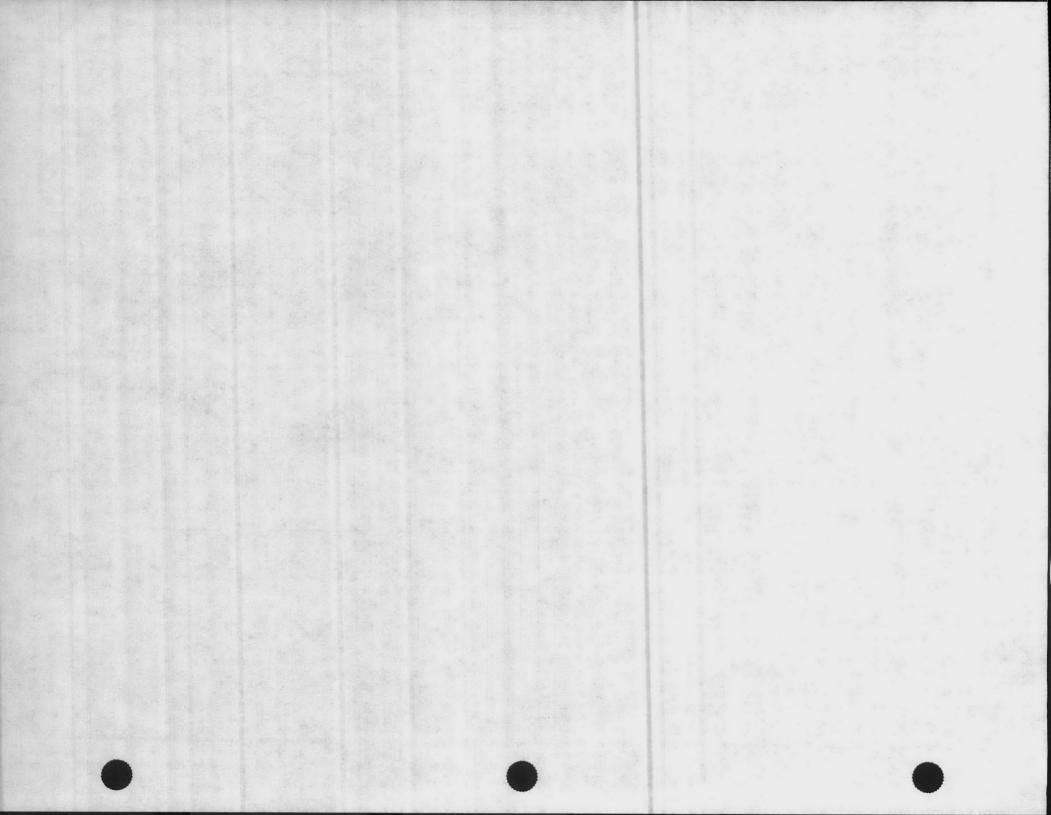


Table 4-9
Pilot-Scale Treatability Testing Analytical Requirements Summary Table

Parameter	Method	Practical Quantitation Limit (ug/l)	Sample Volume Requirement	Container Type	Sample Preservation	Holding Time
Purgeable Halocarbons						
Bromodichloromethane		2				
Bromoform		5			200 TO 100 TO 100	
Bromomethane		2	and the second			
Carbon Tetrachloride		2				
Chlorobenzene	100000000000000000000000000000000000000	2	the second second			
Chloroethane		2				230
2-Chloroethylvinyl ether		2				
Chloroform		2				
Chloromethane		2				
Dibromochloromethane		2				
1,2-Dichlorobenzene		5				
1,3-Dichlorobenzene		5				1.32
1,4-Dichlorobenzene		5				
Dichlorodifluoromethane		2		Glass;		145
1,1-Dichloroethane	EPA 601	2	3 x 40 ml	Teflon	Cool to 4 C	14 Days
1,2-Dichloroethane		2		Lined		
1,1-Dichloroethene		2		Septum		
trans-1,2-Dichloroethene		2				
1,2-Dichloropropane		2				
cis-1,3-Dichloropropene		2				1
trans-1,3-Dichloropropene		2				
Methylene chloride		5				
1,1,2,2-Tetrachloroethane		2				
Tetrachloroethene	1000	2				
1,1,1-Trichloroethane		2				
1,1,2-Trichloroethane	4	2				
Trichloroethene		2 2				
Trichlorofluoromethane		5				10
Vinyl chloride		3	40.1			
Purgeable Aromatics	The second	-1 5				
Benzene		2				
Chlorobenzene	. Egh	2		A		7 50
1,2-Dichlorobenzene	1 6 13	5	ACT TO THE STATE OF	Glass;		
1,3-Dichlorobenzene	EPA 602	5	3 x 40 ml	Teflon	Cool to 4 C	14 Days
1,4-Dichlorobenzene	The second	5		Lined	HCl to pH < 2	
Ethylbenzene	170 50	2		Septum		
Toluene		2				
Xylene		2				to be a

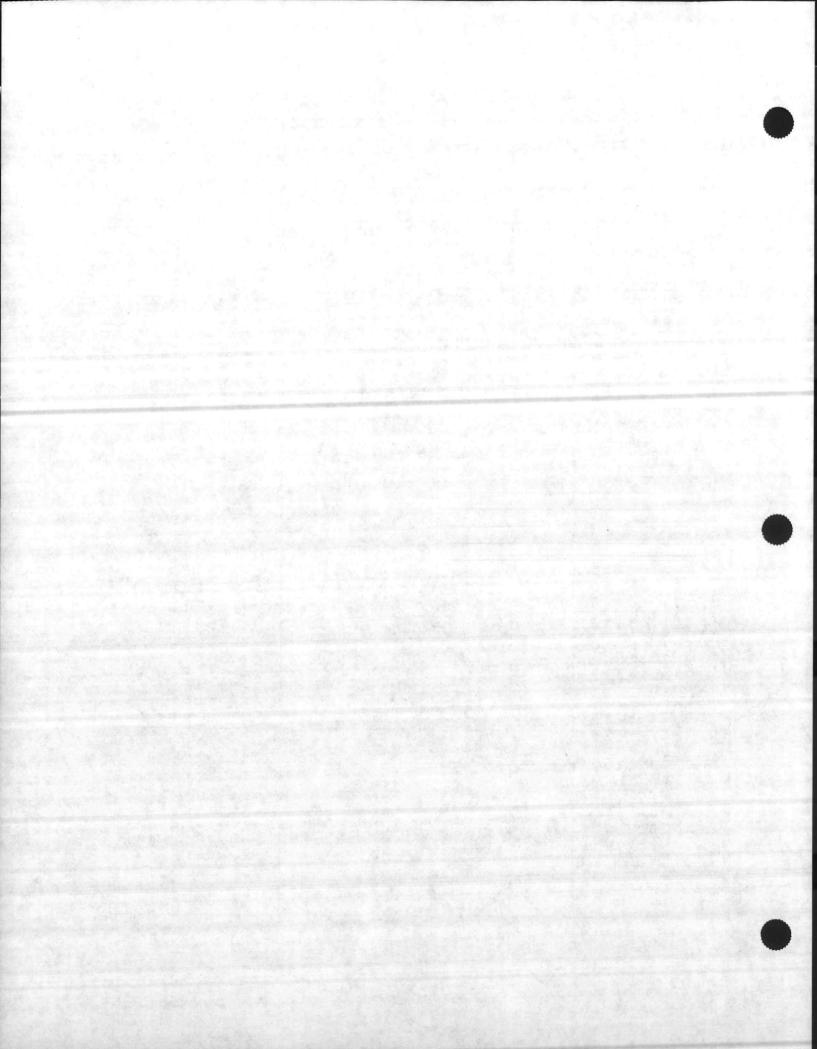
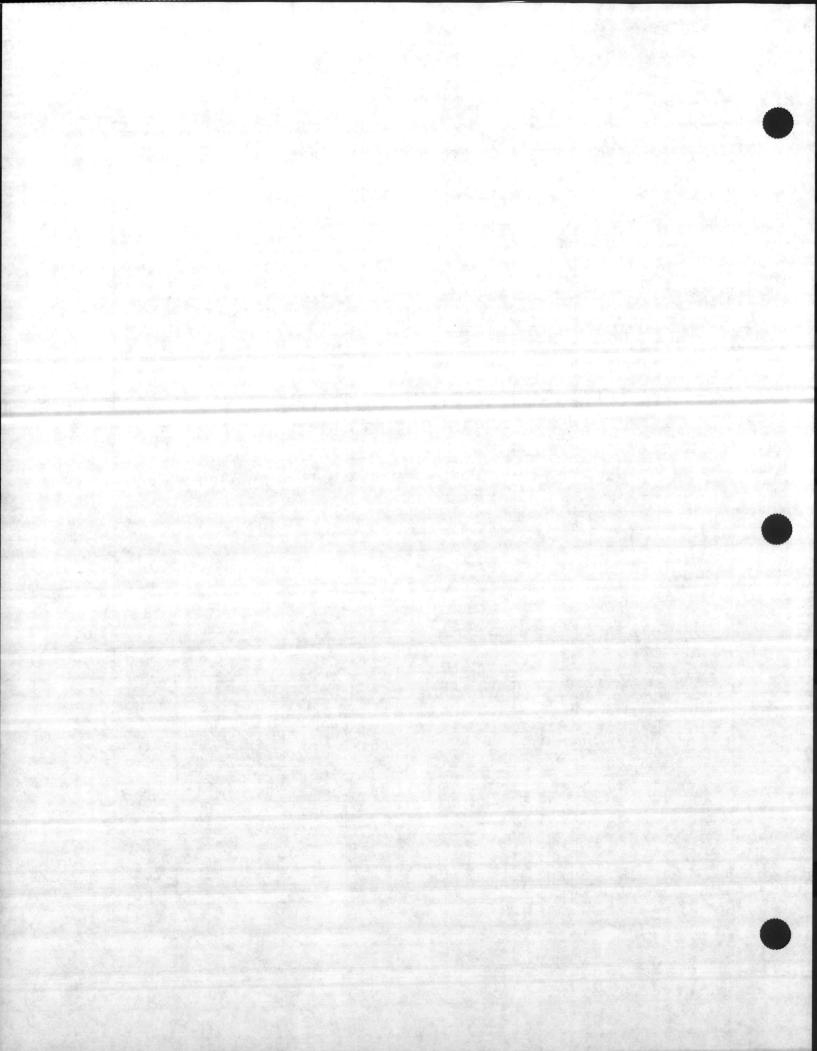


Table 4-9 (continued)
Pilot-Scale Treatability Testing Analytical Requirements Summary Table

Parameter	Method	Practical Quantitation Limit (ug/l)	Sample Volume Requirement	Container Type	Sample Preservation	Holding Time
Target Analyte List Metals				4.		
Aluminum	EPA 200.7	40				
Antimony	EPA 204.2	2			A TOWNS	S. Valence
Arsenic	EPA 206.2	5				
Barium	EPA 200.7	2				
Beryllium	EPA 200.7	2	Normal Agent and the Analysis			edys myren and Ago
Cadmium	EPA 213.2	1				
Calcium	EPA 200.7 EPA 215.1	5				
Chromium	EPA 218.2	5				
Cobalt	EPA 200.7	5	5 - Con-			
Copper	EPA 200.7	7				
Iron	EPA 200.7	6				
Lead	EPA 239.2	5				180 Days
Magnesium	EPA 200.7	100	500 ml	Plastic	Cool to 4 C	Except
Manganese	EPA 200.7	1			HNO3 to pH < 2	Mercury at
Mercury	EPA 245.1	0.2				28 Days
Nickel	EPA 200.7	20				at the
Potassium	EPA 200.7	200				
Selenium	EPA 270.2	2				
Silver	EPA 200.7	20		die e ed i		
Sodium	EPA 200.7	100	the of the second			
Thallium	EPA 279.2	5				
Vanadium	EPA 200.7	7				
Zinc	EPA 200.7	50				
Engineering Parameters						
Ammonia	EPA 350.2	100	500 ml	Plastic	Cool to 4 C H2SO4 to pH < 2	28 Days
Bicarbonate	SM 403/40	1000	500 ml	Plastic	None Required	14 Days
Carbonate	SM 403/40	1000	500 ml	Plastic	None Required	14 Days
Chloride	EPA 325.2	1000	250 ml	Plastic	None Required	28 Days
Hardness	EPA 130.2	1000	150 ml	Plastic	HNO3 to pH < 2	180 Days
Nitrate/Nitrite	EPA 353.2	10	250 ml	Plastic	Cool to 4 C H2SO4 to pH < 2	28 Days
Oil and Grease	EPA 413.1	2000	1000 ml	Glass	Cool 4 C H2SO4 to pH < 2	28 Days
Total Dissolved Solids	EPA 160.1	1000	250 ml	Plastic	Cool to 4 C	7 Days
Total Suspended Solids	EPA 160.2	1000	250 ml	Plastic	Cool to 4 C	7 Days
Aquatic Toxicity Bioassays				DI .:	0.11.10	2611
Multi-Concentration Acute Toxicity	EPA/600/ 4-90-027	NA	2000 ml	Plastic	Cool to 4 C	36 Hours



Samples from these three locations were analyzed for volatile organics (EPA Method 601/602) and inorganic using CLP protocol, Level III data quality.

Samples were also collected at start-up and completion of the aquifer pump test from the influent and effluent from the oil/water separator and analyzed for oil and grease. Additional samples were taken at this time from the influent to the air stripper and analyzed for engineering parameters, including ammonia, carbonate, bicarbonate, chlorides, total dissolved solids, total suspended solids, hardness, nitrate, nitrite, and pH.

One of the seven rounds of samples taken from the influent and effluent to the carbon adsorption unit also underwent a 48 hour test for multi-concentration acute toxicity using fathead minnows (*Pimephales promelas*) as the test organism.

#### 4.4 Data Management

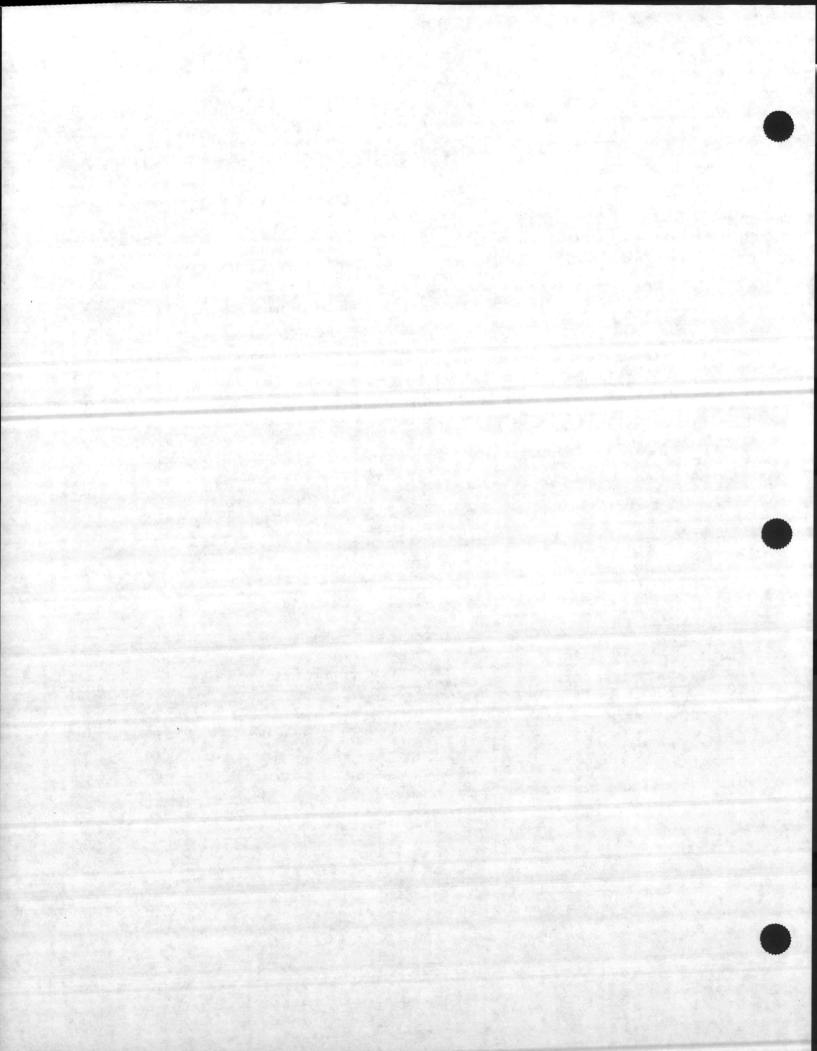
Due to the quantity of data to be collected during the treatability study, the way the data was documented was vital. The following guidelines were used in the documentation of samples and general observations.

Five types of documentation were used in tracking and shipping analytical samples:

- Field logbook;
- Sample labels;
- Chain-of-custody records;
- Custody seals; and
- Commercial carrier air bills.

The label for each sample bottle contained the following information:

- Site name;
- Sample number;
- Monitoring well I.D. number;
- Date and time of collection;
- Sample type (grab or composite);
- Preservatives;



- · Sample matrix; and,
- · Samplers initials.

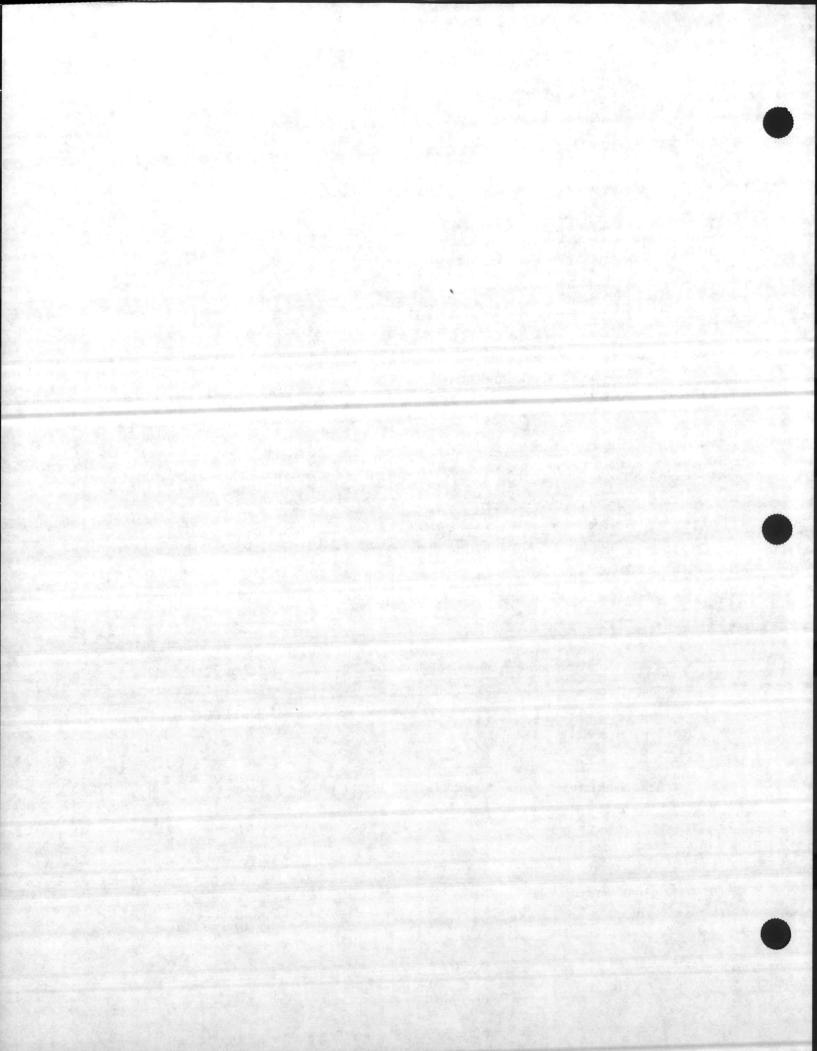
Additionally, the following items also were entered:

- · Date and time;
- Name of field personnel on site;
- Names of visitors on site;
- Field conditions;
- Description of activities;
- Sampling remarks and observations;
- QA/QC samples collected; and,
- Sketch of sample location and site conditions.

Custody of the samples were maintained by field personnel from the time of sampling until the time they were forwarded to the analytical laboratory, Halliburton NUS Environmental Corporation. The sample custody was documented using Chain-of-Custody (COC) records which were completed by field personnel. These were complete in waterproof ink and accompanied each cooler forwarded from the site to the laboratory. Any errors in the COC record were not erased. Instead, a line was drawn through the error and initialed by the person completing the form. The original COC was placed in a sealable plastic bag, placed in the appropriate cooler, and secured to the cooler's lid.

Two sample coolers were shipped by commercial air carrier and secured with custody seals so that the seals would be broken if the cooler was opened. The commercial air carrier did not sign the COC record because the custody seals remained intact and the COC record stayed in the cooler. Prior to shipping the completed air bill was secured to lid of the cooler.

The laboratory maintained internal logbooks and records that provide a custody record during sample preparation and analysis.



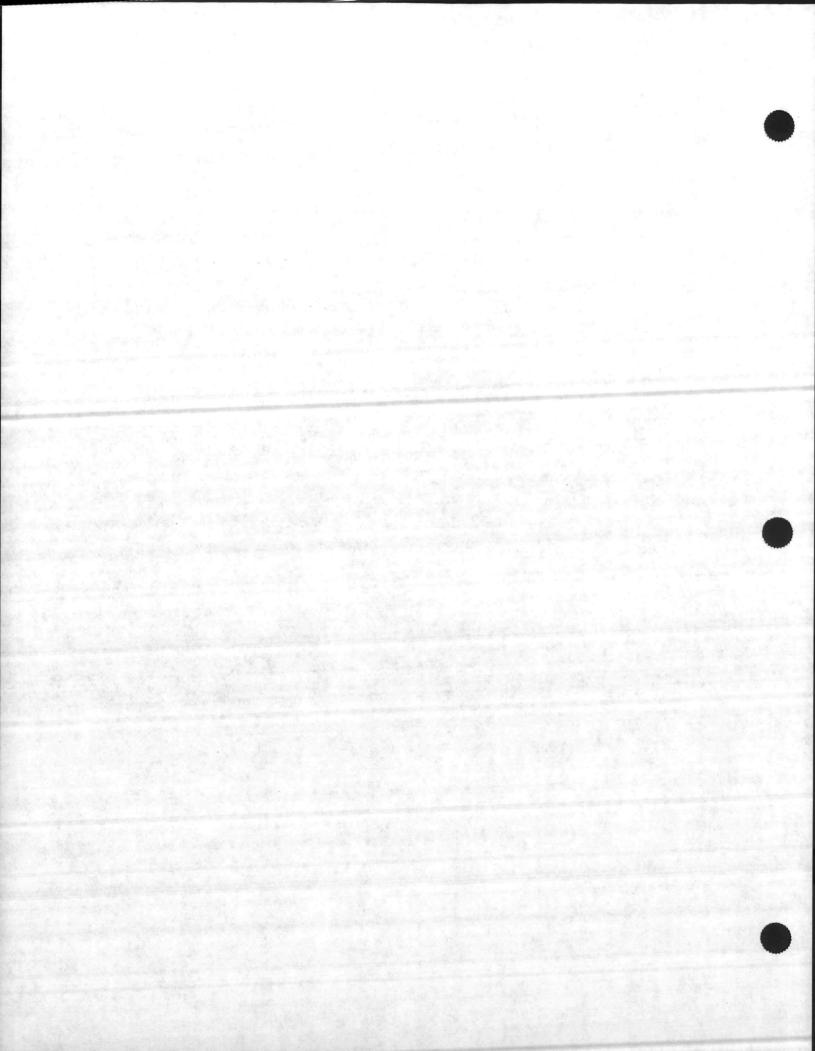
#### 4.5 Deviations from the Work Plan

## 4.5.1 Bench-Scale Study

Based on the sample characterization results (presented in Section 5.0), it was determined that chemical treatment (metals precipitation jar tests) would not be necessary as proposed in the Work Plan because the metals of concern were primarily associated with the suspended solids. However, because addition of appropriate polymers can enhance the coagulation and flocculation of solid particles, agglomeration of smaller particles and subsequent settling of solids, evaluation of cationic/anionic polymer addition was included in the treatability study.

#### 4.5.2 Pilot-Scale Study

Based on the results of the step-drawdown test (Section 4.3.1.1.2), a flow rate of 1.5 gpm was selected for the constant rate aquifer test, which was less than the anticipated production of 5 gpm projected in the Work Plan. The treatment equipment proposed in the Work Plan (Oil/Water Separator, Air Stripper, Carbon Adsorption Unit) were provided, and the Sampling and Analysis Plan was followed. Due to the low flow rate, retention time through the stripper was 333 percent greater than anticipated in the Work Plan.



#### 5.0 RESULTS AND DISCUSSION

## 5.1 Bench-Scale Studies

The results of the bench-scale studies performed to determine the pretreatment requirements (oil and grease, suspended solids, and metals removal) for the HPIA groundwater are presented and discussed in the sections below. Raw analytical data for all of the bench-scale tests is included in Appendices E, F, and G. Recommendations for pretreatment equipment of the HPIA groundwater prior to organics removal are also discussed.

#### 5.1.1 HPIA Groundwater Characteristics

The groundwater sample from the HPIA was analyzed for metals and other engineering parameters in order to define contamination levels and determine pretreatment requirements. Engineering parameter analyses including TSS, TDS, hardness, and alkalinity are presented on Table 5-1. Total and dissolved metals analyses for groundwater characterization are presented on Table 5-2. For comparison purposes, North Carolina criteria for groundwater and surface water as well as Federal Drinking Water Primary and Secondary Maximum Contaminant Levels (MCLs) also are presented on Table 5-2.

Of the engineering parameters, only TSS appears to be of potential concern. The groundwater characterization sample showed 910 mg/L TSS which would rapidly foul treatment system piping and equipment. Other subsequent treatability samples showed lower levels of TSS, however even at these 60 to 100 mg/L levels significant system fouling would result. Therefore, it is necessary to remove the suspended solids up-front via some form of physical treatment (e.g., flocculation, settling, filtration).

Analyses showed that a significant proportion of the metals concentrations are associated with the suspended solids. The following metals exceeded at least one of the discharge criteria listed on Table 5-2 on a total constituent basis: aluminum, chromium, iron, lead, manganese, and zinc. However, once the suspended material is removed, the resulting dissolved metals are likely to be acceptable for discharge. Although dissolved zinc levels slightly exceeded the NC surface water discharge criteria, it is believed that this criteria would not apply as long as the groundwater is discharged to the HPIA STP, as anticipated. Therefore, Baker believes that pretreatment to remove metal-laden particles and not dissolved metals would be required.

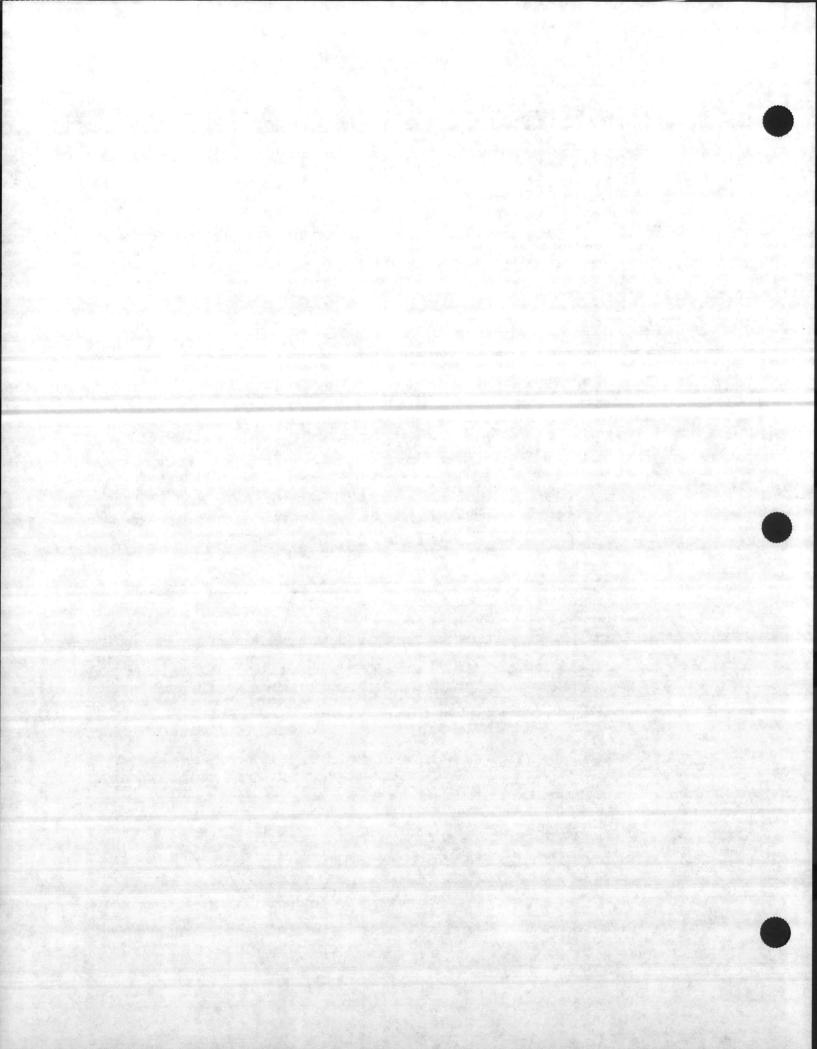
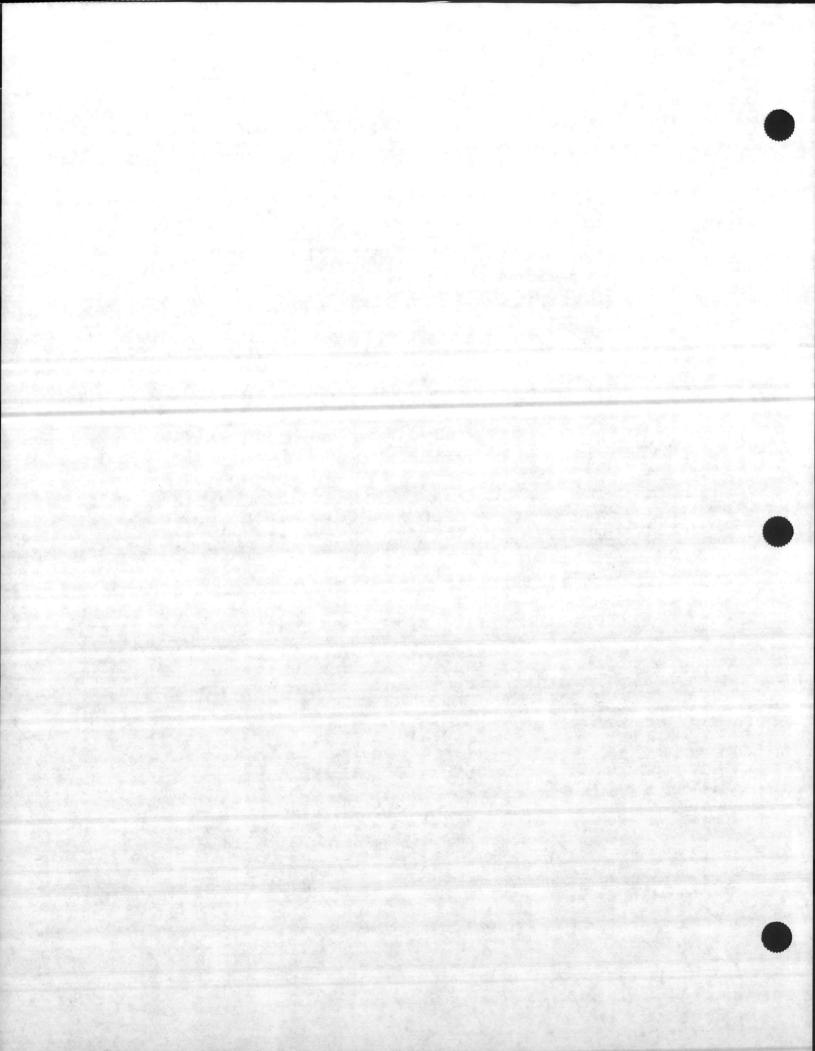


Table 5-1
HPIA Groundwater Sample Characterization Analyses:
Engineering Parameters

Parameter	Concentration (mg/l)
Ammonia (as N)	0.8
Alkalinity, Bicarbonate (as CaCO3)	35
Alkalinity, Carbonate (as CaCO3)	0
Alkalinity, Total (as CaCO3)	35
Chloride (as Cl)	22
Hardness, Total (as CaCO3)	65
Nitrate/Nitrite	<0.1
Nitrite (as N)	<0.02
Total Dissolved Solids	110
Total Suspended Solids	910
Oil and Grease	6



## Table 5-2 HPIA Groundwater Sample Characterization Analyses: **Total and Dissolved Metals**

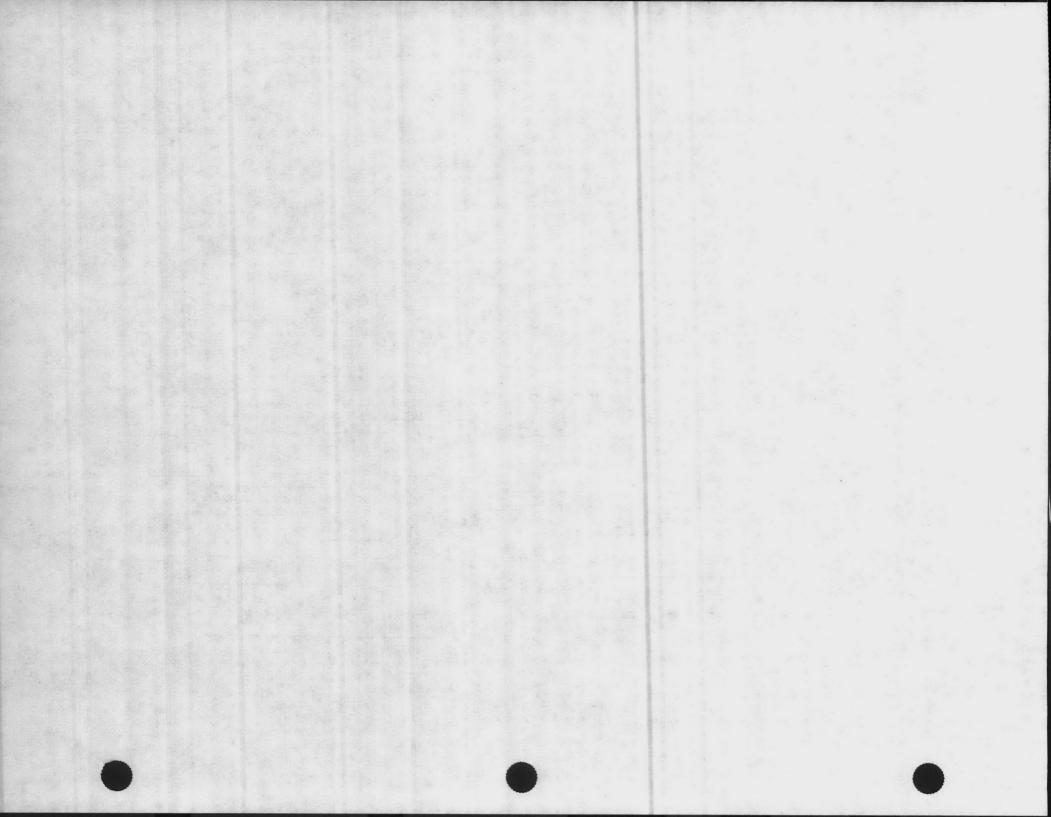
Metals (ug/L)		Dissolved Metals (ug/L)		Primary/Secondary Drinking Water MCLs (ug/L)	NC Ground- Water Criteria (ug/L)	NC Surface Water Criteria (3) (ug/L)
			3	50 to 200	<b>—</b> (2)	-
	U (1)	20.0 U	J	6	12	-
			_	50	50	50
			_	2000	1000	-
	_	1.0 U	J	4	<b>-</b>	65
			_	5	5	2
				-	-	-
			J	100	50	50
	11				-	
				1300	1000	7
	5			300	300	1000
				15 (4)	50	25
	D			_		
	B			50	50	-
	11		II		1.1	0.012
					150	88
					- 1	-
					10	5
					50	0.06
	U	the same of the sa				- No.
	11		11			-
	U			_		
			<u> </u>		5000	50
	9.7 78.0 1.0 5.0 18600 32.0 8.0 14.0 26400 22.4 3100 84.0 0.20 22.0 2330 1.5 3.0 8620	25900 20 U (1) 9.7 B (1) 78.0 B 1.0 B 5.0 U 18600 32.0 8.0 U 14.0 B 26400 22.4 3100 B 84.0 0.20 U 22.0 B 2330 B 1.5 B 3.0 U 8620 2.0 U 73.0	25900 35.0 E 20 U (1) 20.0 U 9.7 B (1) 2.0 U 78.0 B 146 E 1.0 B 1.0 U 5.0 U 5.0 U 18600 15000 32.0 10.0 U 8.0 U 8.0 U 14.0 B 2.0 U 26400 31.0 U 22.4 1.0 U 3100 B 1530 84.0 24.0 0.20 U 0.20 22.0 B 20.0 U 2330 B 830 1.5 B 1.0 3.0 U 3.0 8620 9910 2.0 U 2.0 73.0 4.0	25900 35.0 B 20 U (1) 20.0 U 9.7 B (1) 2.0 U 78.0 B 146 B 1.0 B 1.0 U 5.0 U 5.0 U 18600 15000 32.0 10.0 U 8.0 U 8.0 U 14.0 B 2.0 U 26400 31.0 B 22.4 1.0 U 3100 B 1530 B 84.0 24.0 0.20 U 0.20 U 22.0 B 20.0 U 2330 B 830 B 1.5 B 1.0 U 3.0 U 3.0 U 8620 9910 2.0 U 73.0 4.0 U	25900   35.0 B   50 to 200	25900

### NOTES:

## (1) CONCENTRATION QUALIFIERS:

B = entered if the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL) but greater than or equal to the Instrument Detection Limit (IDL). U = entered if the analyte was analyzed for but not detected, quantitation limit reported.

- (2) "---" = No standard established.
- (3) Protection of Aquatic Life.
- (4) MCL is action level for public water supply systems.



### 5.1.2 Oil/Water Separation Tests

Free phase oil was visible in the treatability study samples. Although the characterization analyses showed O&G to be only 6 mg/L (less than the 10 mg/L specified in the Work Plan), visible oil sheens are not typically acceptable for discharge and, consequently, an oil/water separation test was performed. Analytical results of test samples are presented in Table 5-3.

The oil/water separation test indicated that at 28°C (82°F) most of the oil in the groundwater was free phase and not emulsified. Removal of this oil to below detection limits within a reasonable time frame (less than sixty minutes) appears to be possible in a conventional oil/water separator. In addition, an oil water separator could be used to remove some of the suspended material from the groundwater.

The data in Table 5-3 is not extensive or diverse enough to be able to determine an actual rate of oil removal. However, enough information has been generated to be able to conceptually design an oil/water separator.

### 5.1.3 Solids Settling

Generally sand and multi-media filters are designed for the anticipated hydraulic capacity and a suspended solids concentration of 30 to 50 mg/L in the influent. The levels of suspended solids in the HPIA groundwater samples taken to date appear to be excessive for cost-effective direct filtration of the groundwater.

Settling of some of the suspended material may serve to reduce much of the load to a filter, possibly even eliminating the need for the filter itself. Therefore, bench-scale settling tests discussed in Section 4.2 were performed to investigate the extent of physical treatment required. Qualitative tests to determine an adequate polymer and optimum polymer dosage rate were performed. Subsequently, settling tests using both raw groundwater and groundwater flocculated with polymers were performed.

Qualitative polymer addition tests using both a cationic and an anionic polymer showed good results in each case. However, the anionic polymer (Armstrong APS) appeared to perform slightly better than the cationic polymer (Calgon Pol-E-Z 692). For the settling tests, the anionic polymer at an optimum dosage level of 2 mg/L was selected.

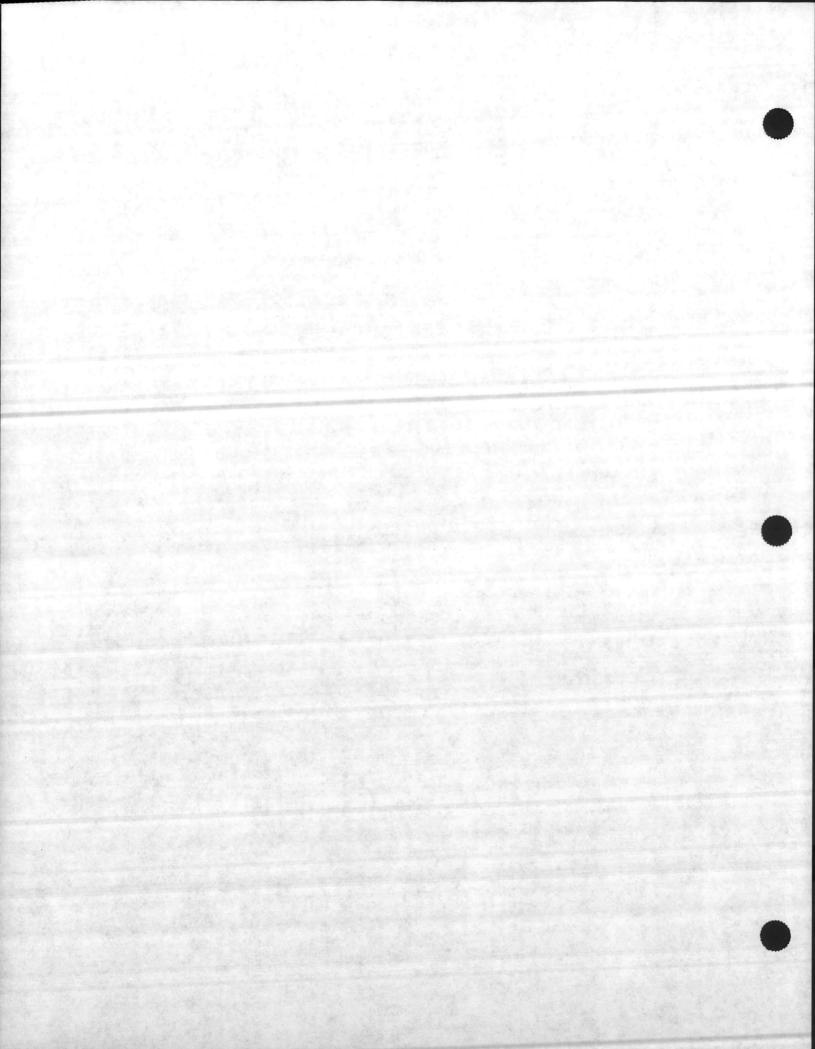
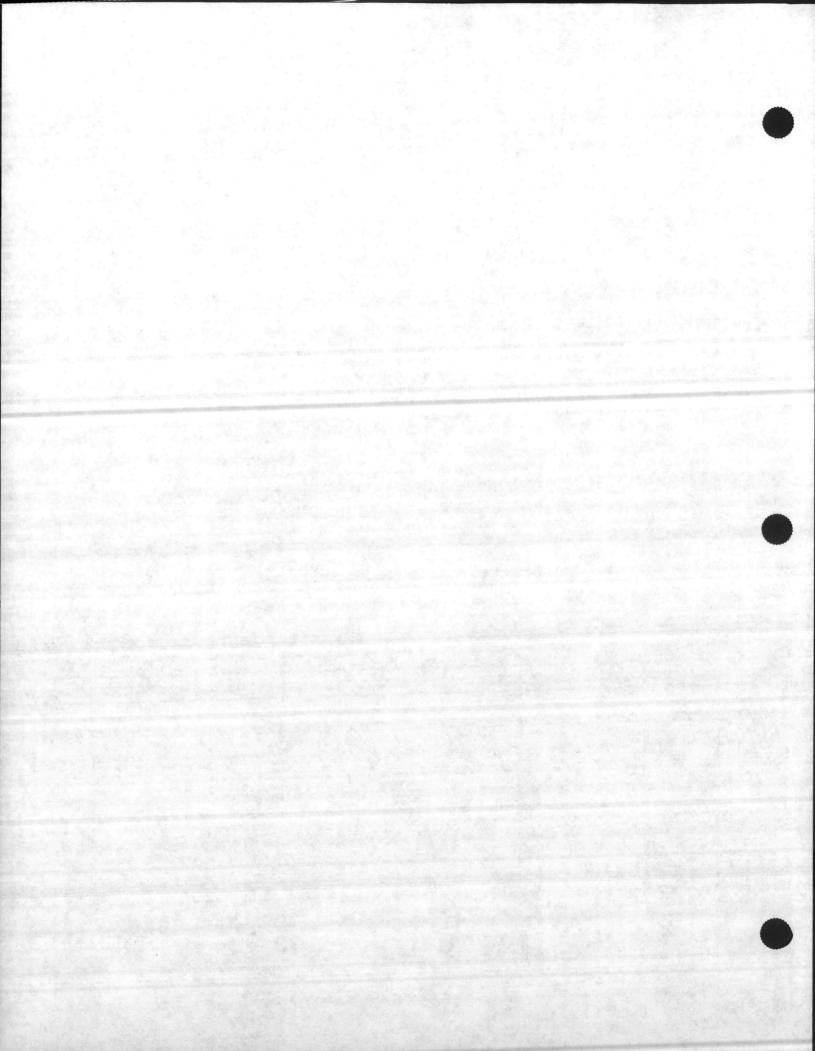


TABLE 5-3
OIL/WATER SEPARATION BENCH-SCALE TEST
ANALYTICAL RESULTS

Time (minutes)	Oil and Grease (mg/L)	Sample Temp. (°C)
0	6	NA
15	<3	28
30	4	28
60	<3	28



The TSS results associated with the settling tests for the raw and polymer enhanced groundwater are presented on Table 5-4. Clearly, polymer addition had a significant impact on the settling rate of the suspended particles. The residual suspended solids concentration of the raw sample following 60 minutes of quiescent settling was roughly equivalent to the residual suspended solids concentration of the polymer enhanced sample after only 5 to 10 minutes (about 25 mg/L), even with a 50 percent higher initial TSS reading in the initial polymer aliquot. After 30 minutes of settling, the polymer enhanced sample TSS concentration fell below 20 mg/L.

Samples of water were extracted for metals analyses (aluminum, arsenic, chromium, iron and lead) after 60 minutes of settling for the raw sample and 30 minutes for the polymer enhanced sample. These analyses are presented on Table 5-5. Comparing these values to water quality criteria presented previously (Table 5-2) one can see that aluminum and iron levels were not reduced. However, these levels probably reflect naturally-occurring levels for the site. In this case, settling alone does not appear to be adequate, and a combination of flocculation, settling and filtration will be required.

Once the on site treatment plant is in place and the groundwater extraction wells are developed (i.e., operating), much of the suspended material that was present in the treatability study samples may not be present in treatment plant influent. In fact, this phenomenon was apparent in the pilot-scale testing, when TSS levels were measured to be less than 10 ppm.

### 5.1.4 QA/QC

Quality Assurance/Quality Control samples were taken during the bench-scale treatability testing to ensure that analytical results are reliable for design purposes. Duplicate raw and filtered groundwater samples for the characterization study were taken. Also, a duplicate oil/water separation study sample was collected at the 60 minute mark in the test and a duplicate initial sample for the settling tests was analyzed for TSS, aluminum, arsenic, chromium, iron, and lead. In addition, two trip blanks prepared by the laboratory were analyzed. No unusual variances were observed in any of the QA/QC samples. The QA/QC results are included in Appendix H.

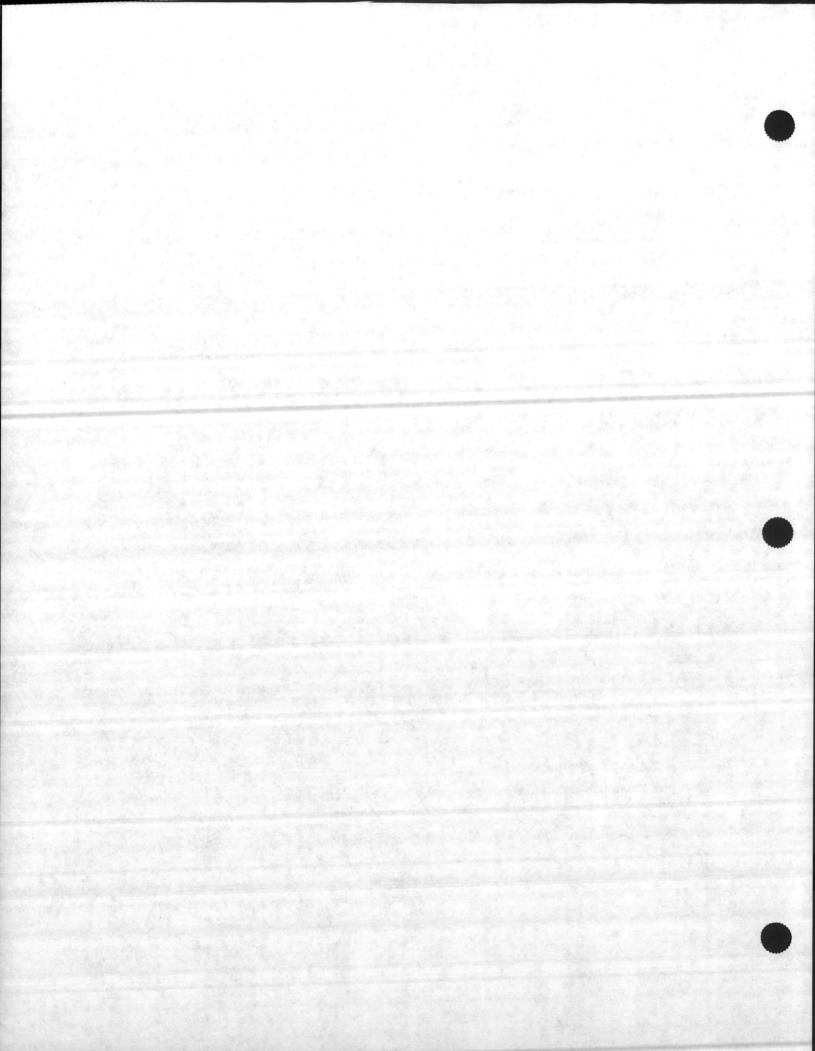


TABLE 5-4
SOLIDS SETTLING TESTS: SUSPENDED SOLIDS
CONCENTRATION AS A FUNCTION OF TIME

	Total Suspended Solids (mg/L)						
Settling Time (minutes)	Raw Sample	Sample with Polymer at 2 mg/L					
0	62	62					
5	-	28					
10	48	27					
15		20					
20	35	-					
30	32	16					
60	25	-					

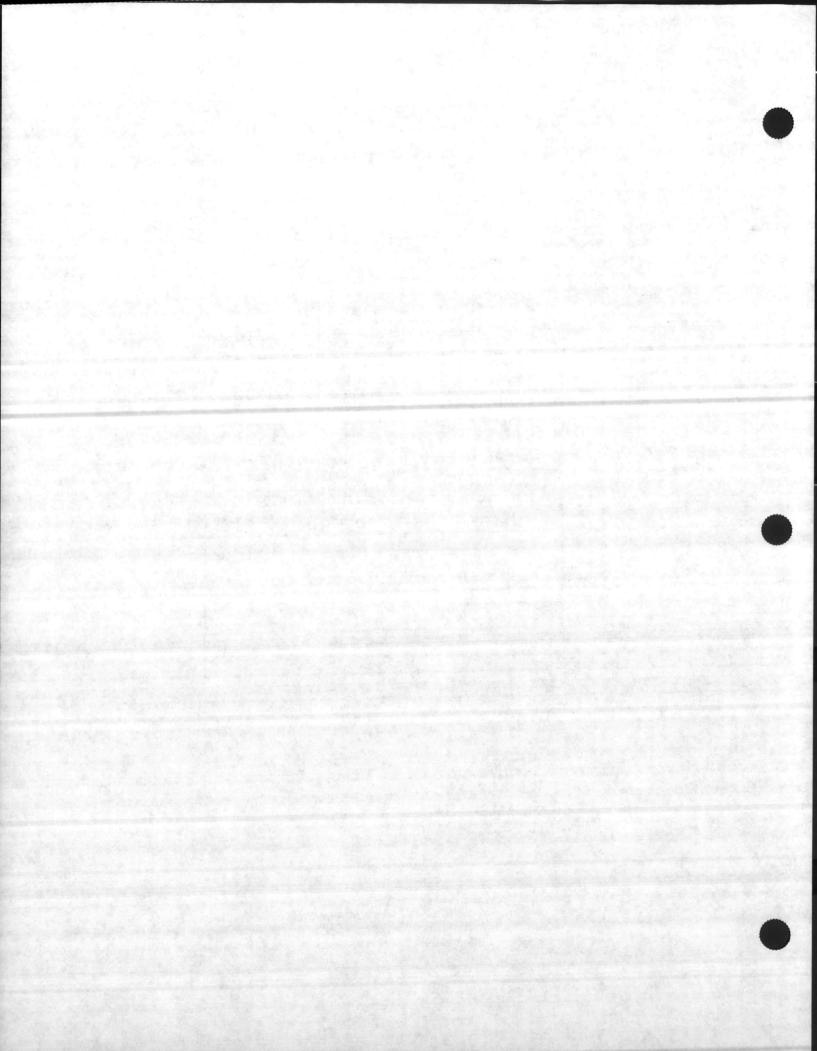
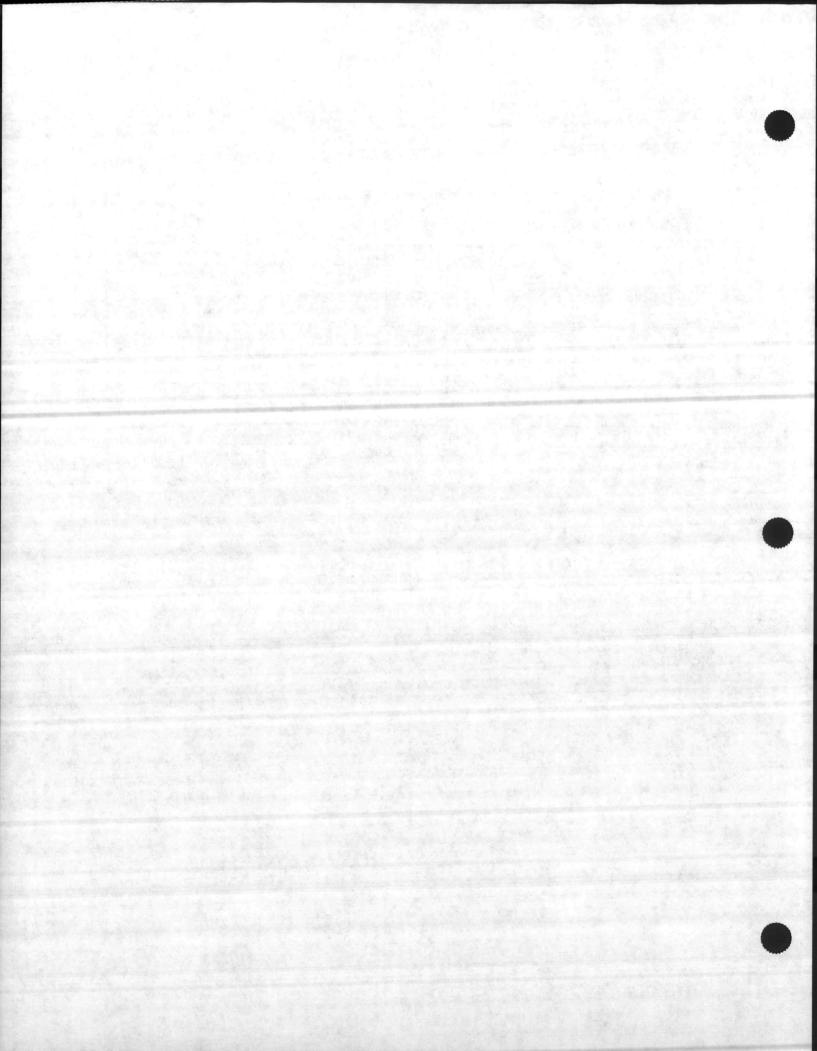


Table 5-5
Solids Settling Tests: Total Metals and TSS Concentrations

			Concentration	
Parameter	Units	Raw Initial Sample	Raw Sample After 60 Min. Settling	Sample with Polymer at 2 mg/l After 30 Min. Settling
Aluminum	ug/l	2780	2290	282
Arsenic	ug/l	< 4.0	< 4.0	< 4.0
Chromium	ug/l	20	14	< 10.0
Iron	ug/l	8930	6400	2310
Lead	ug/l	4.4	3.2	11
TSS	mg/l	62	25	16



## 5.2 Pilot-Scale Study

### 5.2.1 Data Analysis and Interpretation

### 5.2.1.1 Analysis of Waste Stream Characteristics

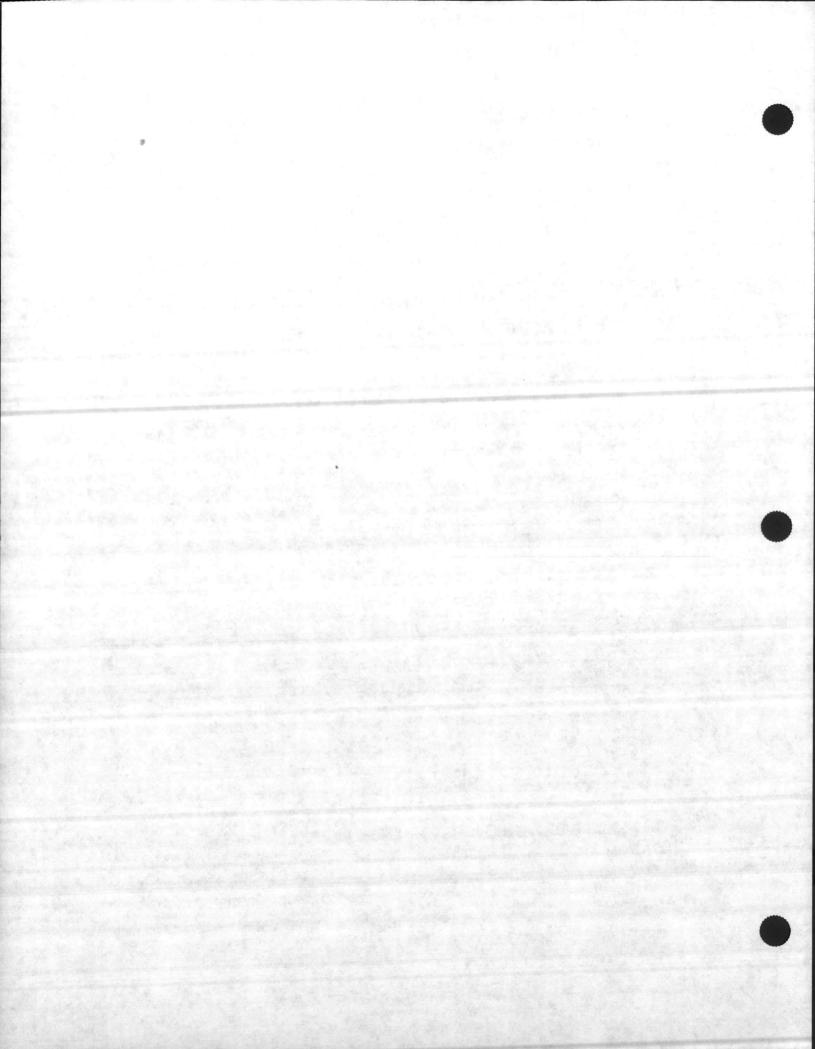
Previous studies indicate that the shallow groundwater is contaminated primarily with fuel-related compounds, benzene, 1,2-dichloroethene (1,2-DCE), trichloroethene (TCE), solvents and metals, such as antimony, arsenic, beryllium, chromium, iron, lead, manganese, mercury, and nickel. Prior to this study, the most recent shallow groundwater data was collected in January 1991 by ESE. This data is similar to the results of earlier studies with the exception that the compound concentrations from the January data were generally lower than the concentrations identified in the earlier studies. Table 5-6 presents the summary of the 1991 shallow aquifer groundwater data with respect to the contaminants of concern.

Groundwater samples taken for the bench-scale study were analyzed for metals and other engineering parameters. The results of these analyses are discussed in Section 5.1.1 of this report. Based on the sample characterization results, it was determined that the metals of concern were primarily associated with the suspended solids.

Groundwater samples were taken for the pilot-scale treatability study from the influent to the air stripper. Based on the analytical results (presented in Section 5.2.1.2), the characteristics of the waste stream flowing into the pilot-scale treatment system were similar to the results of earlier studies, with the exception of the presence of vinyl chloride in the groundwater. The presence of vinyl chloride, which had not been detected in previous investigations, was unexpected and may possibly be the result of the microbial decomposition of the chlorinated compounds of concern.

### 5.2.1.2 Analysis of Treatability Study Data

This section of the report presents the results of the chemical analysis and toxicity testing from the pilot-scale treatability study. A discussion of the results in relation to the test objectives is also provided. Laboratory data from the pilot-scale study is attached to this report in Appendix I. The results are presented by parameter in Tables 5-7 through 5-21, organized to show the change in contaminant level across the air stripper and carbon adsorption unit.



# SUMMARY OF CONTAMINANTS OF CONCERN DETECTED IN THE SHALLOW GROUNDWATER AQUIFER, JANUARY 1991

Potential Contaminants of Concern	HPGW1	HPGW2	HPGW3	HPGW4-1	HPGW5	HPGW6	HPGW7	HPGW8	HPGW9-1	HPGW10	HPGW11	HPGW12	HPGW13	HPGW14	HPGW15
VOC (µg/L)	The Bulletin Bulletin		7-1-1-12-15												
Benzene	5 <	5 <	5 <	5 <	5 <	5 <	5 <	5 <	5 <						
1,2-Dichloroethene	73	10 <	10 <	5 <	5 <	5 <	-	-		5 <	5 <	5 <	5 <	5 <	5 <
Trichloroethene	91	5 <	5 <	0.9 J			5 <	5 <	1200	5 <	5 <	5 <	5 <	5 <	7
Inorganics (µg/L)		0 1	0 \	0.9 0	5 <	5 <	5 <	2 J	14000	5 <	5 <	5 <	5 <	5 <	4 J
Chromium	87	64.3	16.7	187	3.6 B	1590	313	91.8	66.4	310	140	25.5	48.9	127	01.4
Iron	64100	34800	10400	100000	3100	265000	65700	40900	19800	119000					21.4
Lead	16.6	29.4	11.4	66.6	13.6	60.7	12				31800	5600	33500	87200	4800
Manganese	168	77	53.9				112	54.1	128	186	45.2	15.7	9	66.5	16.6
Antimony				425	162	487	136	46.5	45	255	103	18.3	30.3	80	18.3
	13.3 <	15.6 B	46.5 B	21.9 B	13.3 <	13.3 <	22 <	22	17.6 B	22 <	22 <	22 <	13.3 <	13.3 <	22 <
Arsenic	8 B	24.1	15.6	15.5	1.5 <	31.5	18.3	28.4	3 B	39.9	9.1 B	1.8 <	47	45.6	1.8 <
Beryllium	6	1.7 BG	1.2 B	6.7	0.86 B	20	4.8 B	2.1	0.79 B	5.6	2.1 <	2.1 <	0.59 B	2.7 B	2.1 <
Mercury	0.1 <	0.1 <	0.1 <	0.1 <	0.1 <	1.4	0.25	0.13	0.1 <	0.82	0.1 B	0.1 <	0.35 B		
Nickel	31.3 B	16.9 B	12.1 B	57	5.2 <	161	50.7	25.2	15.1 B	92.2	23.6 B	11 <	21.2 B	0.26 41.6	0.1 <

Potential Contaminants of Concern	HPGW16	HPGW17-1	HPGW18	HPGW19	HPGW20	HPGW21	HPGW22	HPGW23	HPGW24-1	HPGW25	HPGW26	HPGW29	22GW1	22GW2
VOC (µg/L)		200	5 1 3 50											
Benzene	5 <	5 <	N/A	5 <	5 <	5 <	5 <	24	3 J	5 <	5 <	5 <	7900	5 <
1,2-Dichloroethene	5 <	5 <	N/A	0.8 J	5 <	5 <	5 <	8900		5 <	5 <	5 <		5 <
Trichloroethene	5 <	5 <	N/A	2 J	5 <	3 J	5 <	3700		5 <	5 <	5 <		5 <
Inorganics (µg/L)								0100	100	0 (	0 \	3 \	2 1	3 <
Chromium	209	37	N/A	13.8	424	45	79.8	76.3	26.3	205	13	179	457	26.3
Iron	47200	10500	N/A	36200	2E+05	56600	24400	23300		46600	19000		1E+05	16200
Lead	100	23.7	N/A	31.7	20	49.4	39.4	45		71.6	9	29.1	307	16.2
Manganese	98.3	31.3	N/A	79	217	136	94.1	68.8		118	10.6 B	236	284	763
Antimony	22 <	22 <	N/A	13.3	21.9B	13.3 <	24.6 B	24.6 <	22 <	13.3 <	13.3 <	13.3 <	20.9 B	13.3
Arsenic	17.3	1.8 <	N/A	5 B	49.4	12.1	7.2 B	6.6 B	4.2 B	13.2	1.5 <	25.6		11
Beryllium	5.3	2.1 <	N/A	2.3 B	9.5	3.7 B	0.6 B	1 B		2.8 B	0.5 <	8.7	5.8	0.5
Mercury	0.13 B	0.1 <	N/A	N/A	0.5	0.1 <	0.1 <	0.1 <		0.1 <	0.1 <	0.1 <	0.35	0.1
Nickel	41	11.9 B	N/A	7.3 B	168	30.8 B	23.2 B	33.2 B		39.2 B	5.2 <	93.5	186	17

Notes: < = Compound was analyzed, but not detected at the listed detection limit

J = Value is estimated

B = Reported value is < contract required detection limit (CRDL), but > instrument detection limit (IDL)
D = Compound identified in an analysis at a secondary dilution factor

N/A = Not Analyzed

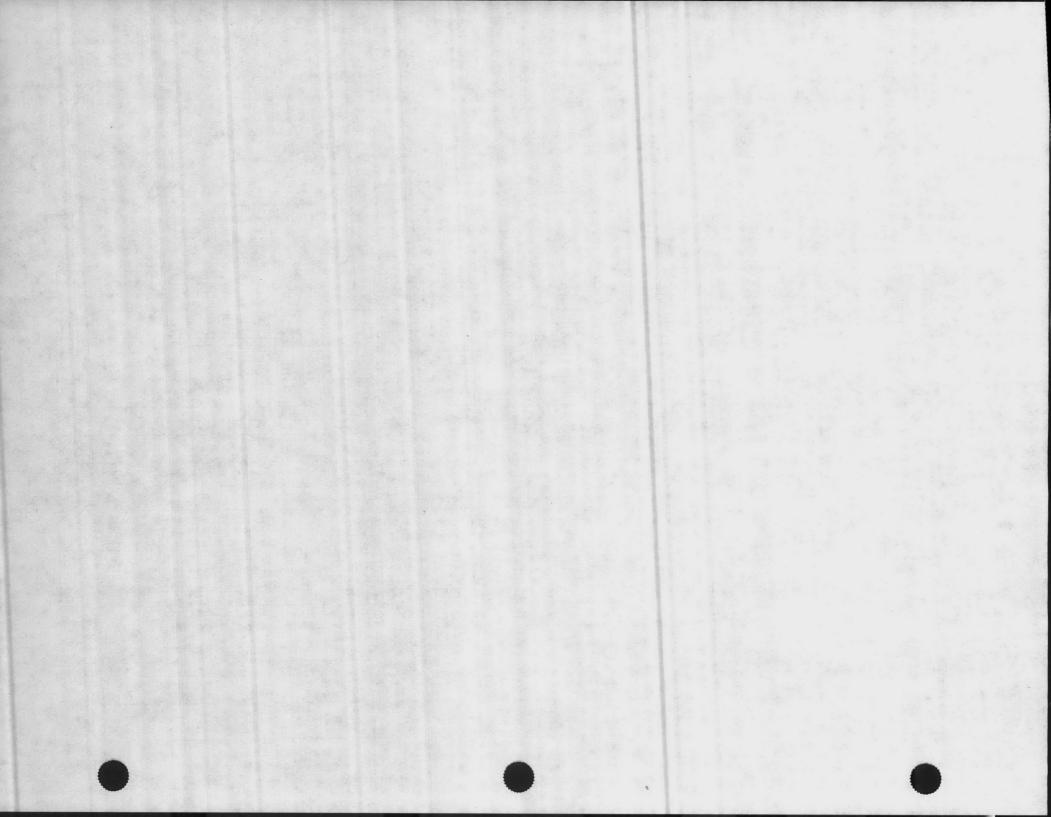


Table 5-7
Summary of Analytical Results
Benzene
CTO-017

	en de la companya del companya de la companya del companya de la c	Location/Sample Name	
Sampling Interval	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L
1	4	5	<2
2	3	3	<2
3	3	3	<2
4	3	<2	<2
5	3	<2	<2
6	3	<2	<2
7	3	<2	<2
Duplicate	3	2	<2

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.

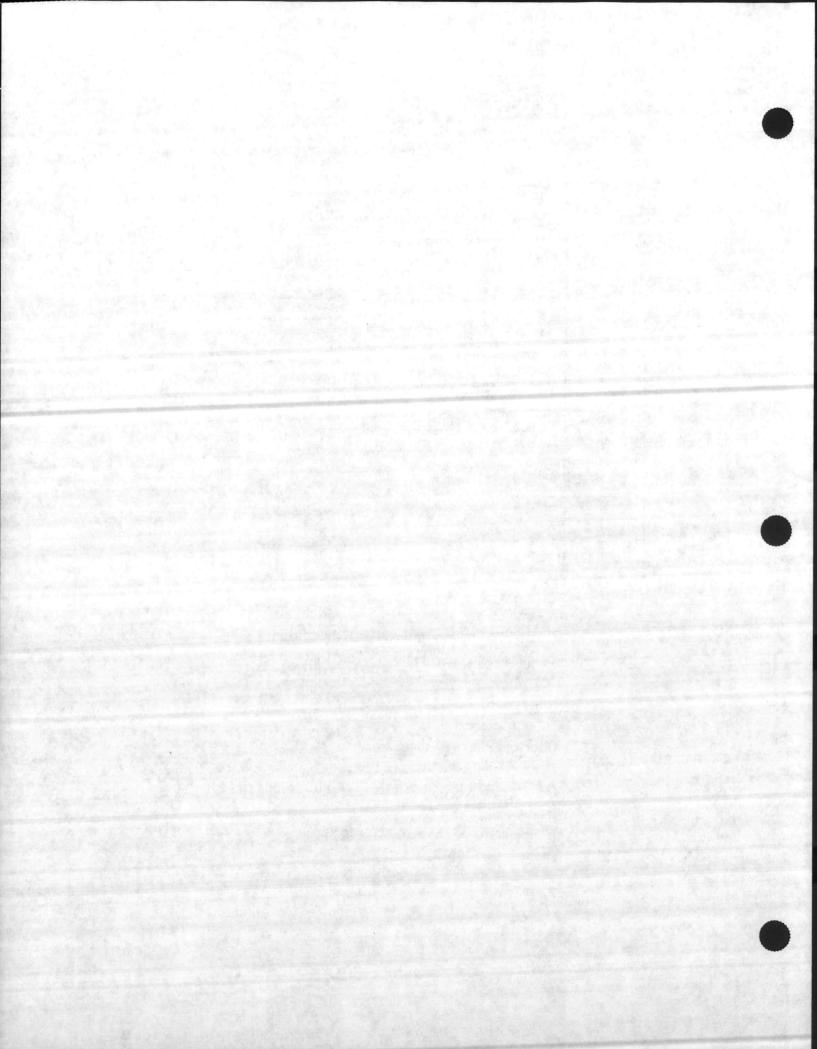


Table 5-8
Summary of Analytical Results
Trans-1-2,Dichloroethene (DCE)
CTO-017

	Location/Sample Name							
Sampling Interval	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L					
1	<40 D	6	<2					
2	40	<2	<2					
3	<40 D	<2	<2					
4	<40 D	<2	<2					
5	<40 D	<2	<2					
6	<40 D	<2	<2					
7	<40 D	<2	<2					
Duplicate	<40 D	<2	<2					

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.

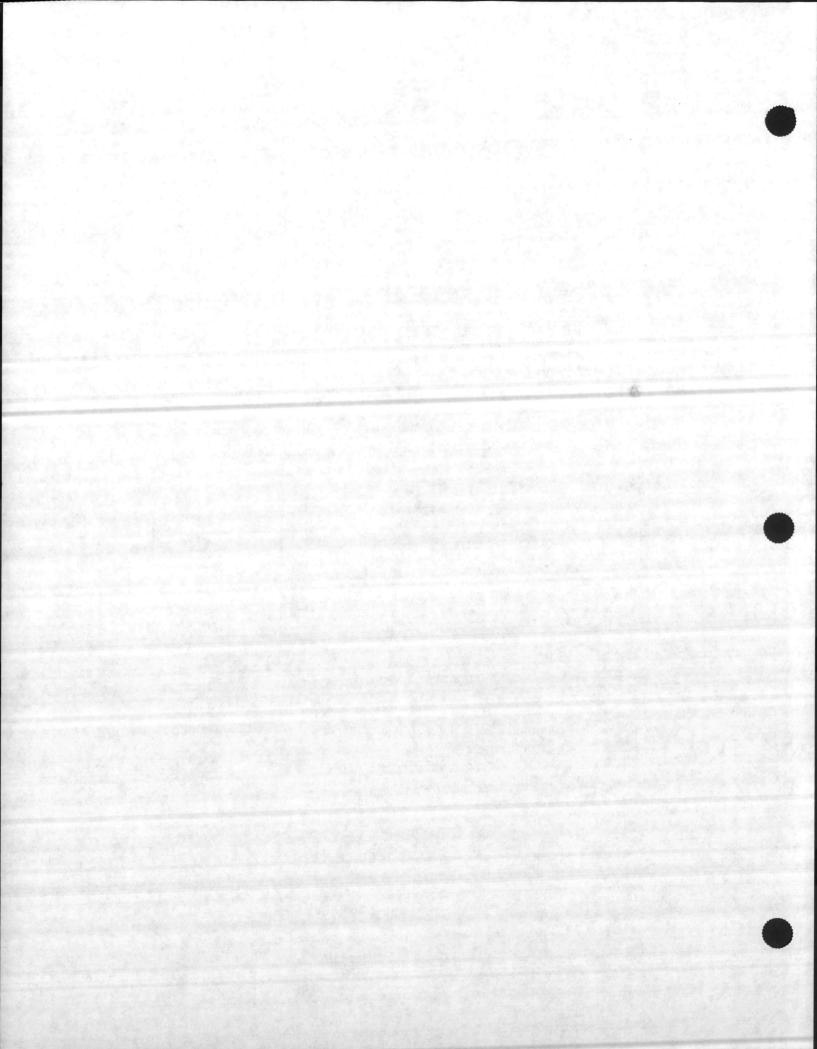


Table 5-9
Summary of Analytical Results
Ethylbenzene
CTO-017

	the way of the control of the Marketine	Location/Sample Name	3
Sampling Interval	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L
1	4	17	<2
2	<2	14	3
3	2	14	<2
4	<2	<2	<2
5	<2	<2	<2
6	<2	<2	<2
7	<2	<2	<2
Duplicate	<2	13	3

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.

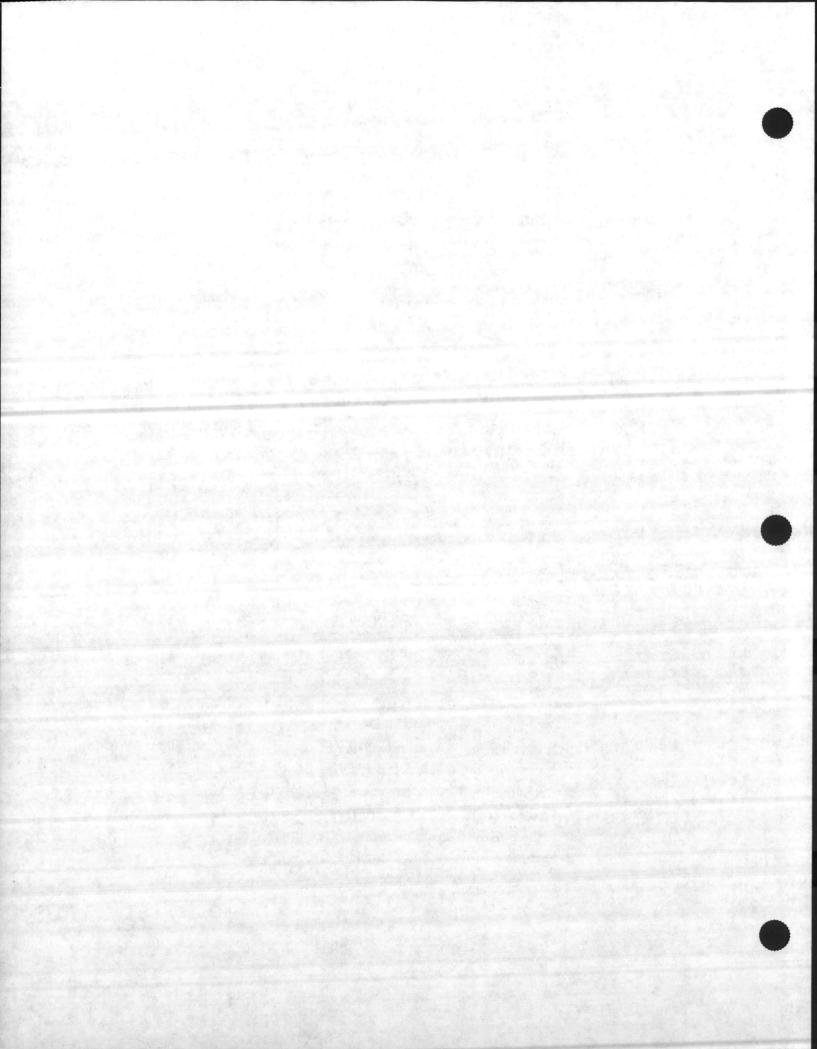


Table 5-10
Summary of Analytical Results
Trichloroethene (TCE)
CTO-017

	Location/Sample Name							
Sampling Interval	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L					
1	<2	<2	<2					
2	160 D	<2	<2					
3	180 D	<2	<2					
4	190 D	<2	<2					
5	180 D	<2	<2					
6	180 D	<2	<2					
7	120 D	<2	<2					
8	180 D	<2	<2					

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.

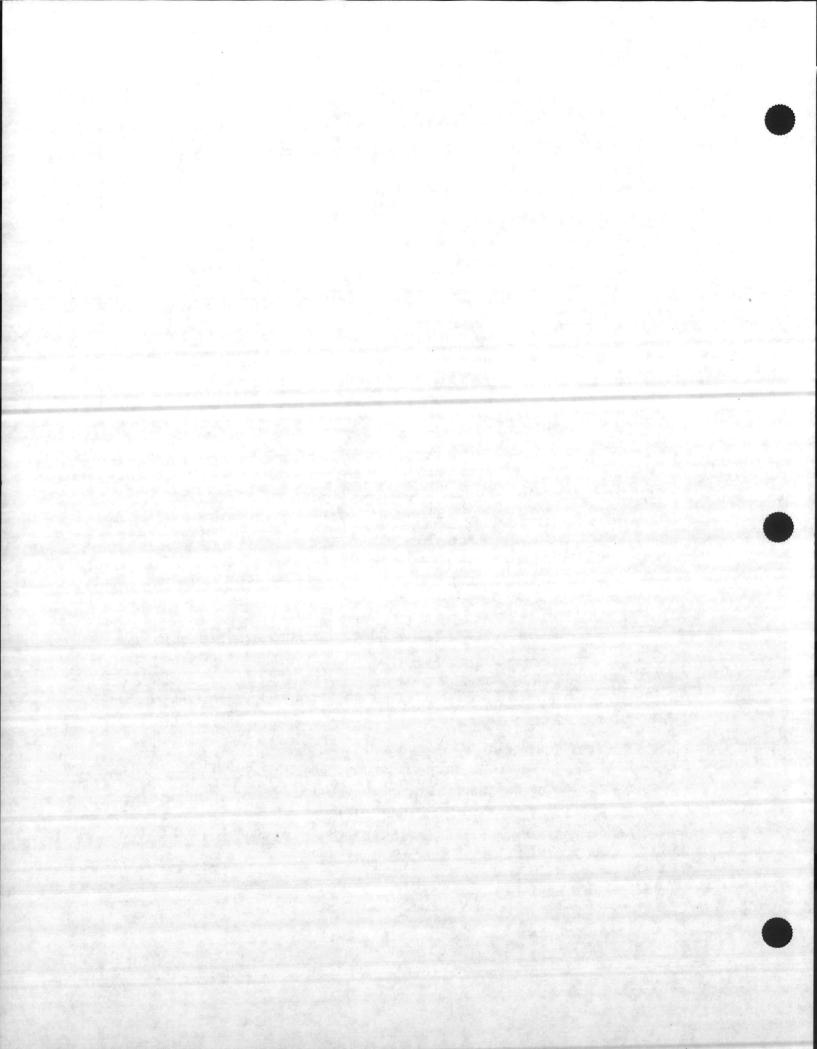


Table 5-11
Summary of Analytical Results
Tolulene
CTO-017

	THE PROPERTY OF THE PARTY OF	Location/Sample Name	
Sampling Interval	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L
1	5	25	<2
2	5	10	2
3	5	9	<2
4	5	8	<2
5	6	10	3
6	10	10	4
7	12	11	10
8	9	13	4

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.

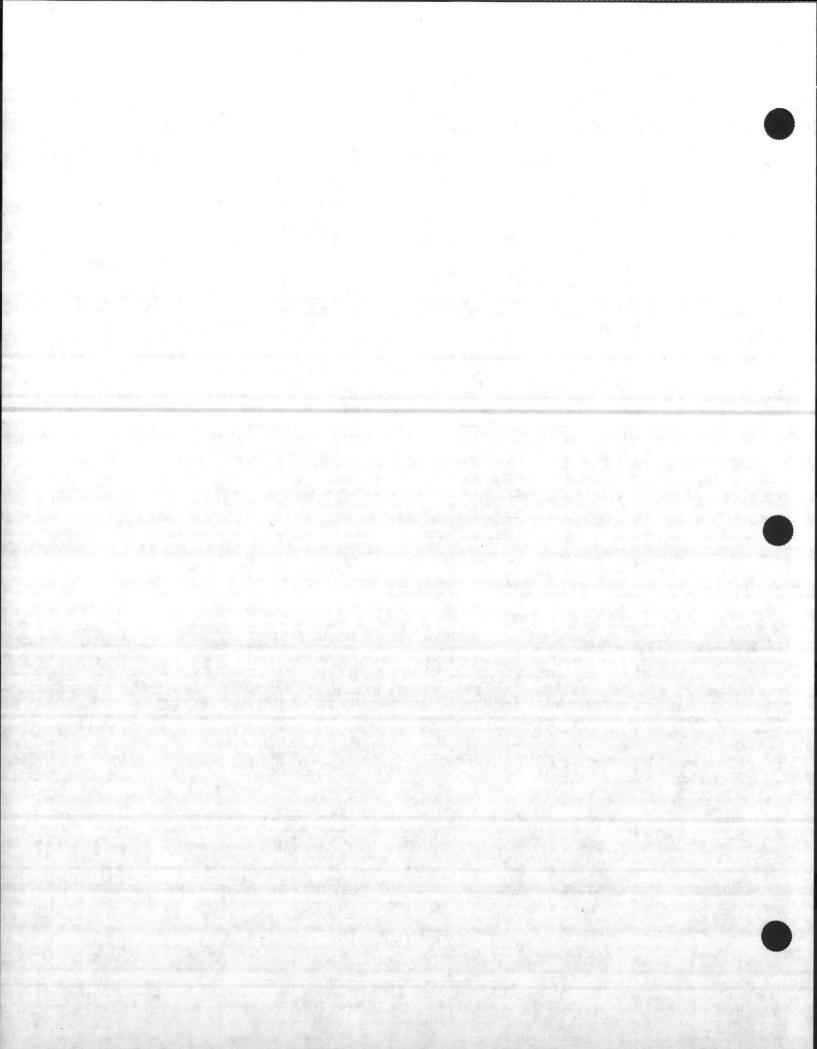


Table 5-12
Summary of Analytical Results
Vinyl Chloride
CTO-017

47.44	Location/Sample Name							
Sampling Interval	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L					
1	270 D	<5	<5					
2	290 D	<5	<5					
3	320 D	<5	<5					
4	330 D	<5	<5					
5	350 D	<5	<5					
6	360 D	<5	<5					
7	336 D	<5	<5					
8	340 D	<5	<5					

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.

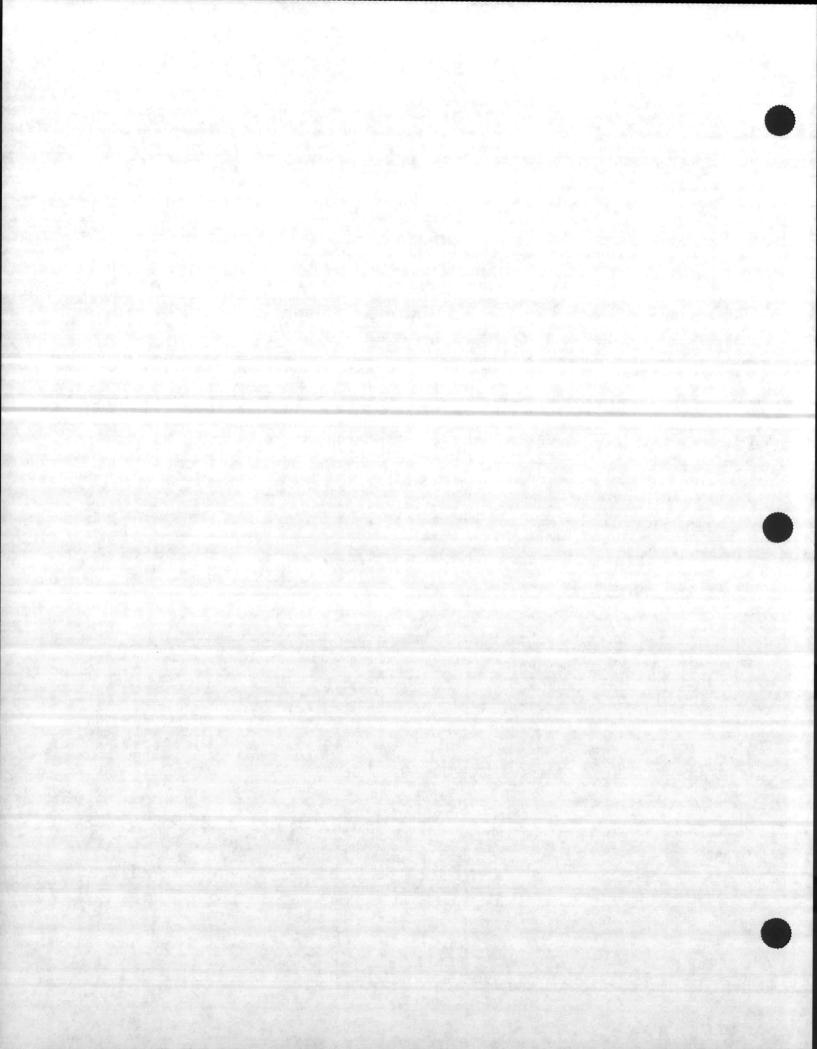


Table 5-13
Summary of Analytical Results
Antimony
CTO-017

Sampling Interval	Location/Sample Name			
	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L	
1	10 U	10 U	26.5 B	
2	10 U	10 U	10 U	
3	10 U	10 U	10 U	
4	10 U	10 U	10 U	
5	10 U	10 U	10 U	
6	10 U	10 U	10 U	
7	10 U	10 U	10 U	
Duplicate	10 U	10 U	10 U	

g

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.

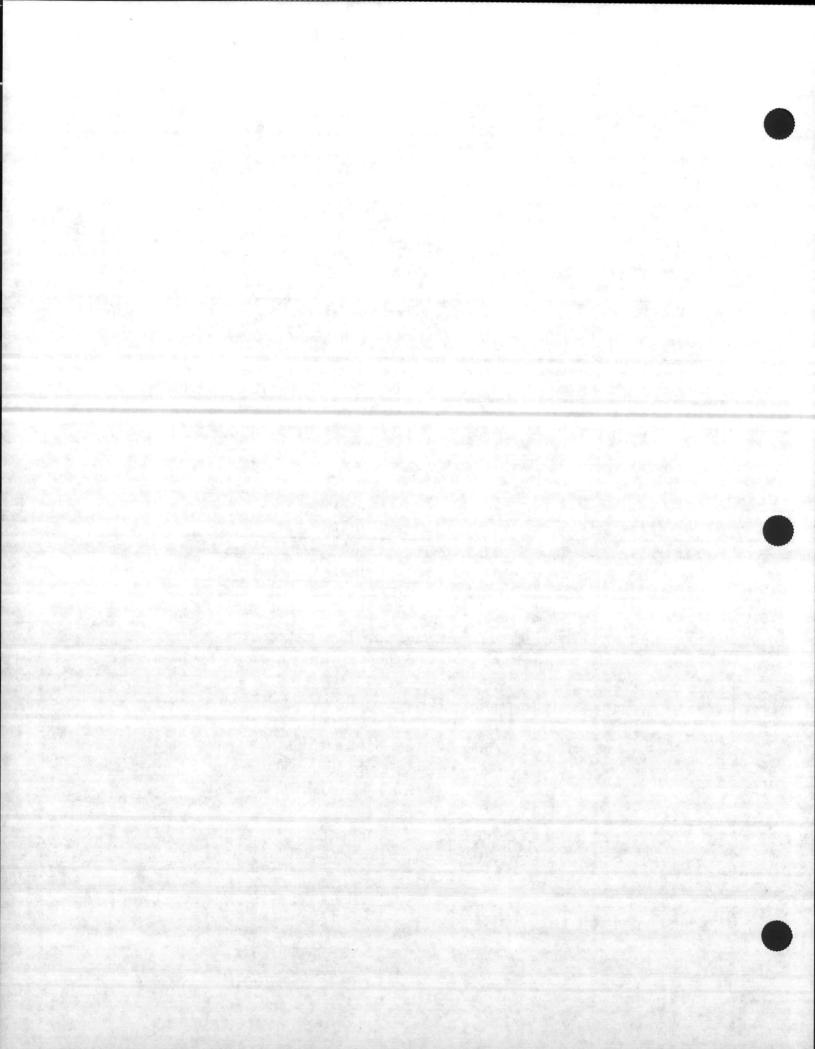


Table 5-14
Summary of Analytical Results
Arsenic
CTO-017

Sampling Interval	Location/Sample Name		
	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L
1	2 U	15.4	137
2	2 U	2 U	11.1
3	2 U	2 U	9.1 B
4	2 U	2 U	7.9 B
5	2 U	2 U	2
6	2 U	2 U	5.9 B
7	2 U	2 U	2 B
8	2 U	2 U	7 B

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.

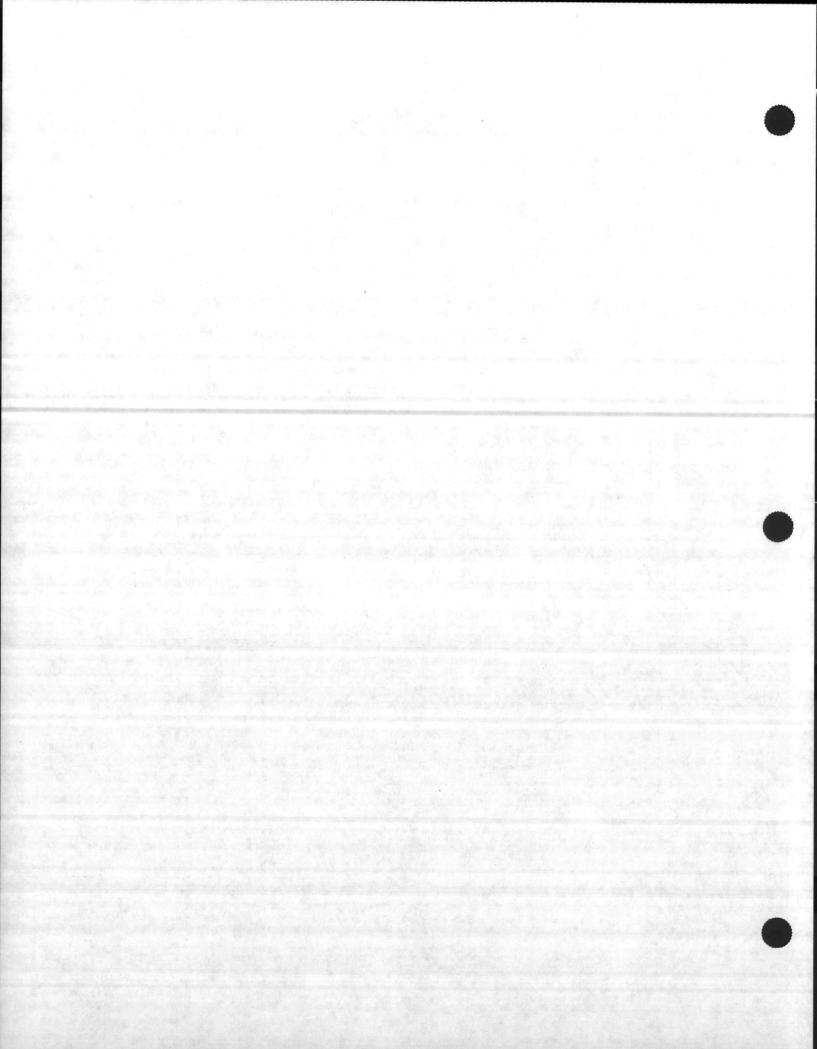


Table 5-15
Summary of Analytical Results
Beryllium
CTO-017

Sampling Interval	Location/Sample Name		
	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L
1	1 B	1 U	1 B
2	1	1 B	1 U
3	1 U	1 U	1 B
4	1 U	1 U	1 B
5	1 U	1 U	1 U
6	1 U	1 U	1 U
7	1 U	1 U	1 U
Duplicate	1 U	1 U	1 U

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.

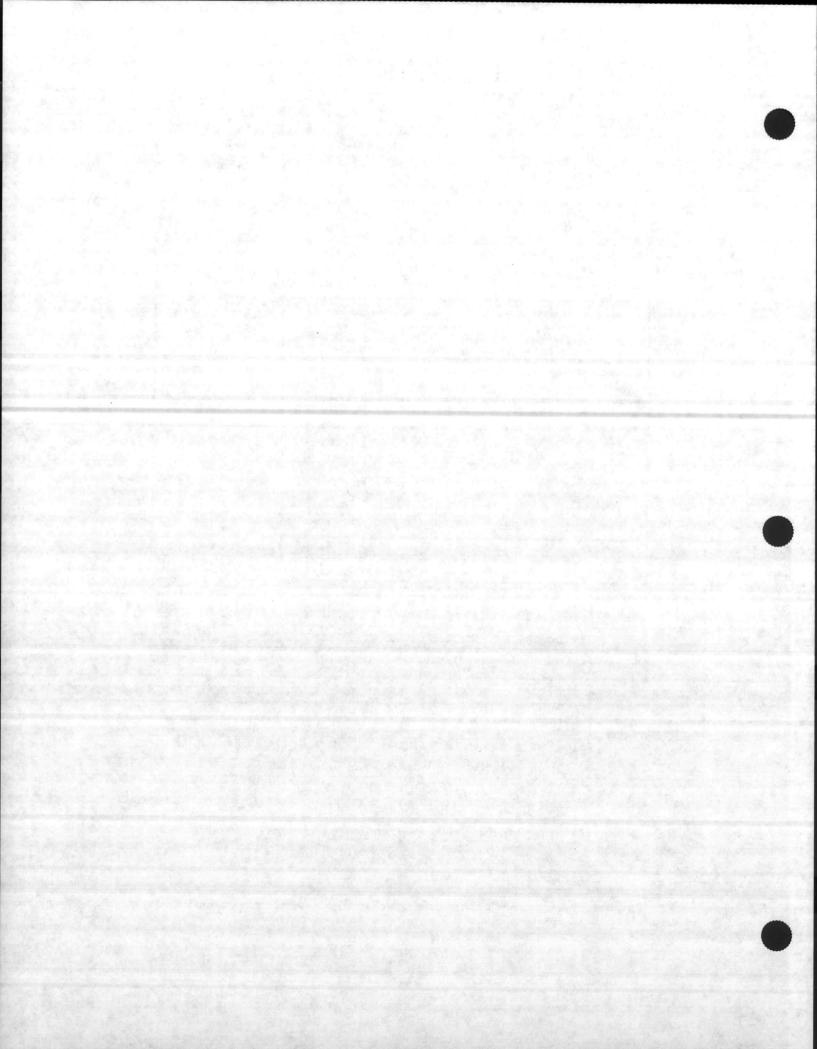


Table 5-16
Summary of Analytical Results
Chromium
CTO-017

Sampling Interval	Location/Sample Name		
	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L
1	10 U	10 U	19
2	10	10 U	18
3	10 U	10 U	23
4	10 U	10 U	10 U
5	10 U	10 U	10 U
6	10 U	10 U	10 U
7	10 U	10 U	10 U
8	10 U	10 U	10 U

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.

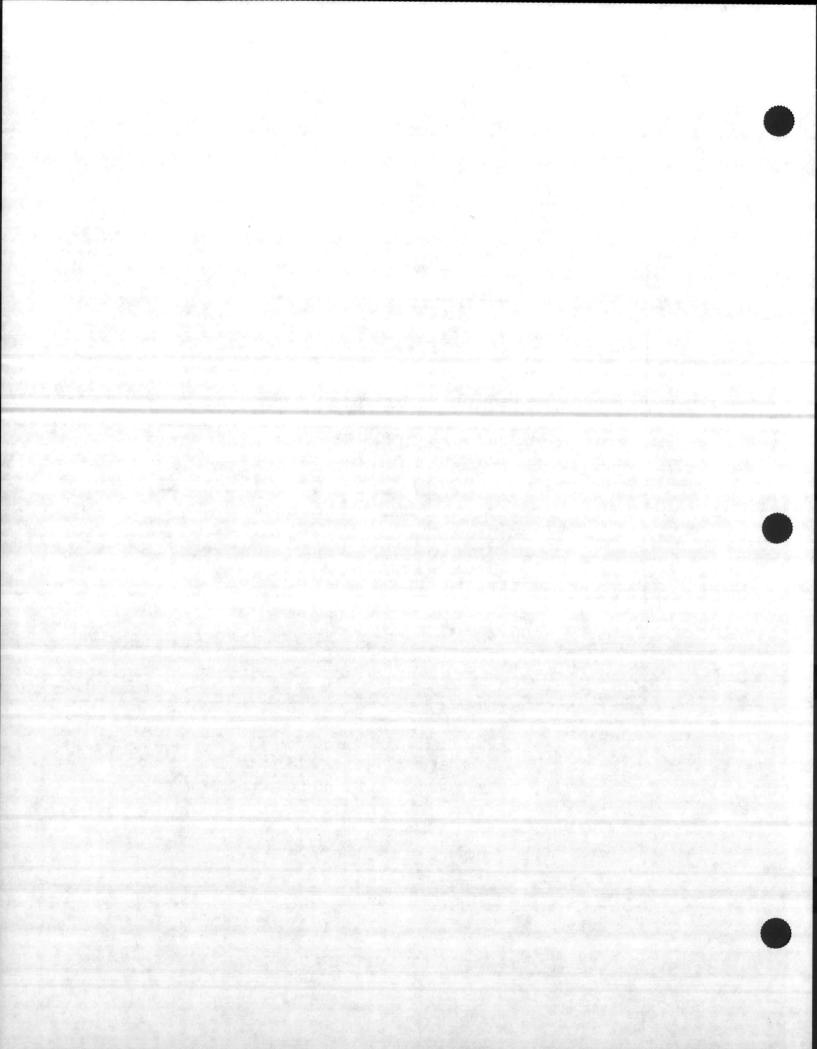


Table 5-17
Summary of Analytical Results
Iron
CTO-017

		Location/Sample Name	
Sampling Interval	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L
1	8,618	39,000	17,200
2	7,740	8,340	13,200
3	7,270	6,910	19,200
4	7,390	6,590	2,730
5	7,700	7,150	1,140
6	7,570	6,790	4,760
7	7,580	6,870	1,580
Duplicate	7,540	6,690	3,140

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.

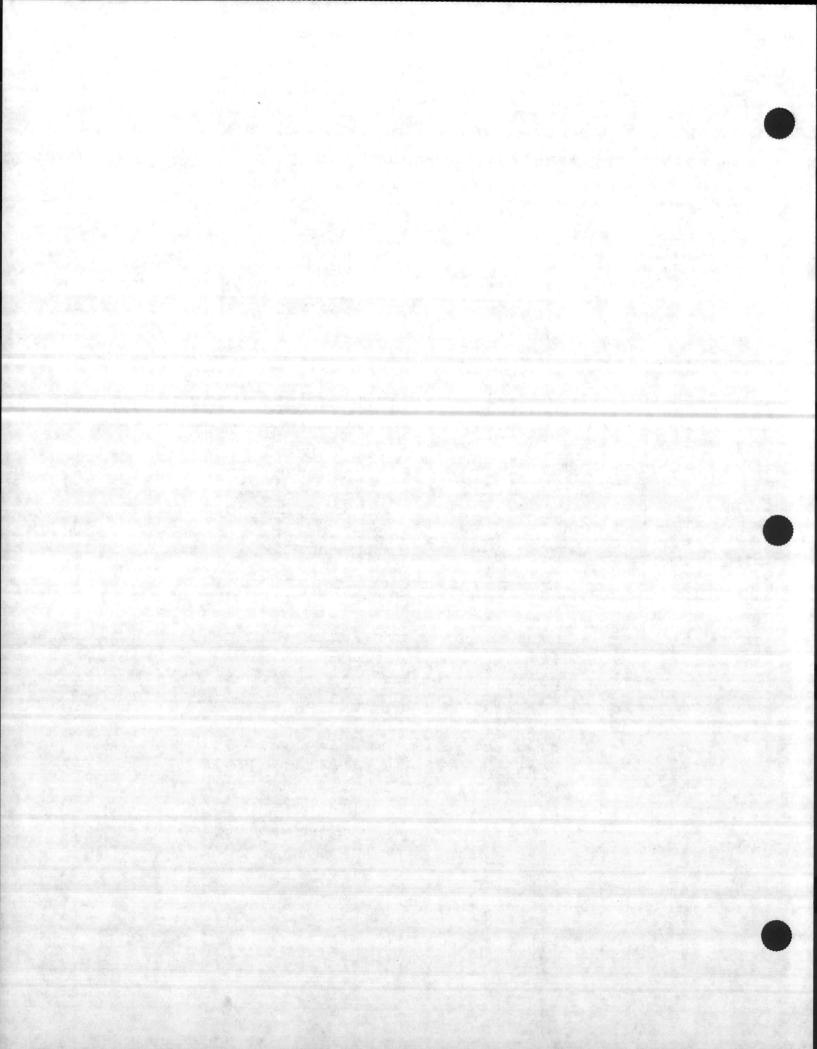


Table 5-18
Summary of Analytical Results
Lead
CTO-017

	Location/Sample Name			
Sampling Interval	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L	
1	52.0	80.0	13.4	
2	34.6	89.5	14.1	
3	25.2	45.0	23.6	
4	13.2	27.2	10.3	
5	17.6	11.6	3.7	
6	12.7	10.8	9.7	
7	9.4	18.2	5.0	
Duplicate	13.0	20.8	5.3	

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.

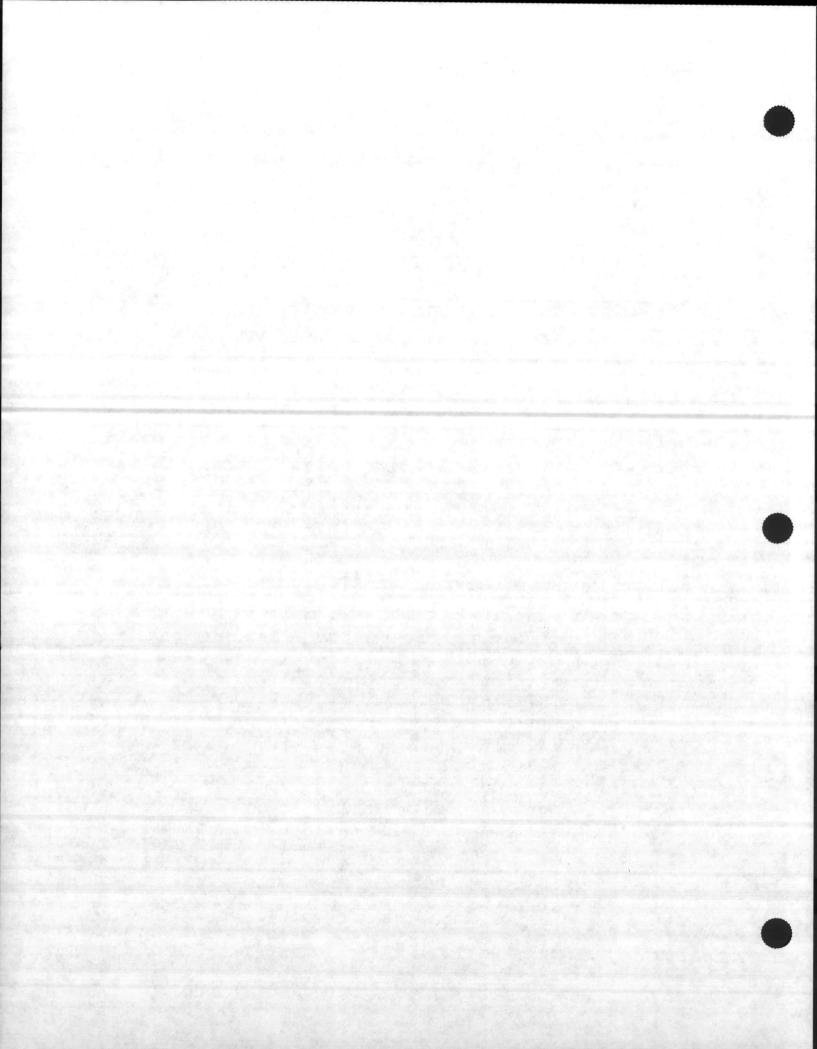


Table 5-19
Summary of Analytical Results
Manganese
CTO-017

	Location/Sample Name			
Sampling Interval	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L	
1	56	199	191	
2	51	65	149	
3	46	57	193	
4	45	51	19	
5	46	51	83	
6	48	54	28	
7	46	51	7 B ·	
Duplicate	46	51	23	

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.

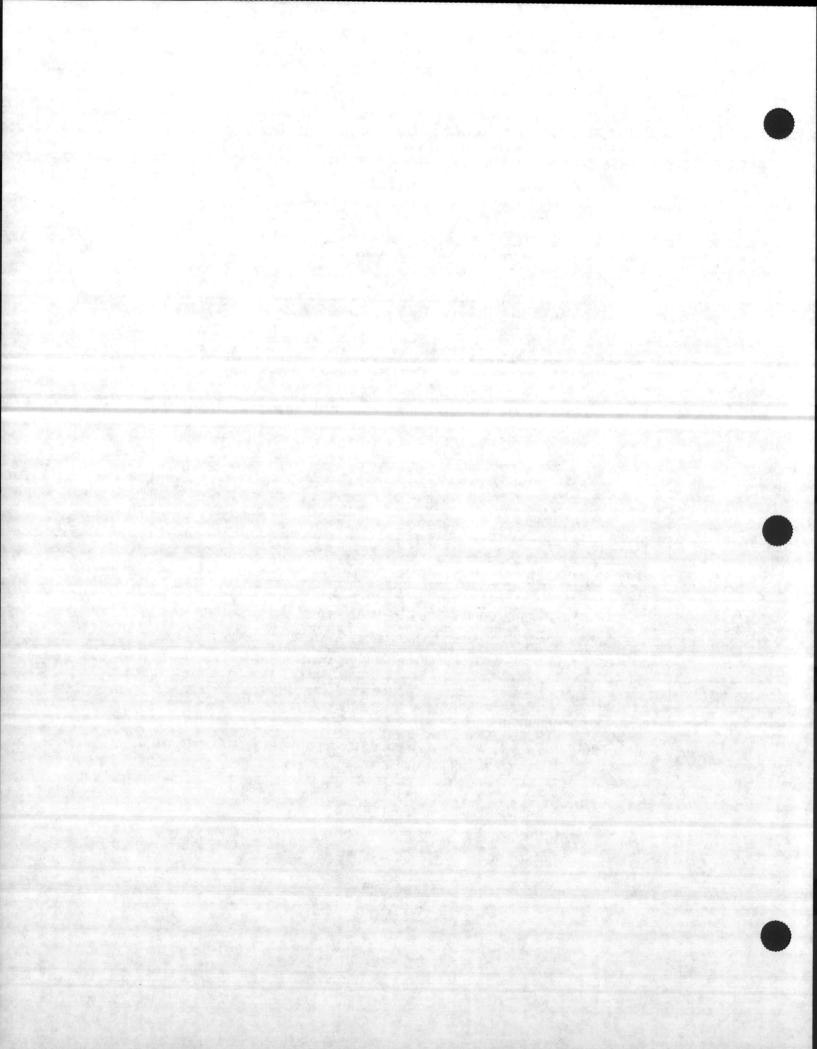


Table 5-20
Summary of Analytical Results
Mercury
CTO-017

	Location/Sample Name			
Sampling Interval	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L	
1	.2 U	.2 U	.2 U	
2	.2 U	.2 U	.2 U	
3	.2 U	.2 U	.2 U	
4	.2 U	.2 U	.2 U	
5	.2 U	.2 U	.2 U	
6	.2 U	.2 U	.2 U	
7	.2 U	.2 U	.2 U	
Duplicate	.2 U	.2 U	.2 U	

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.

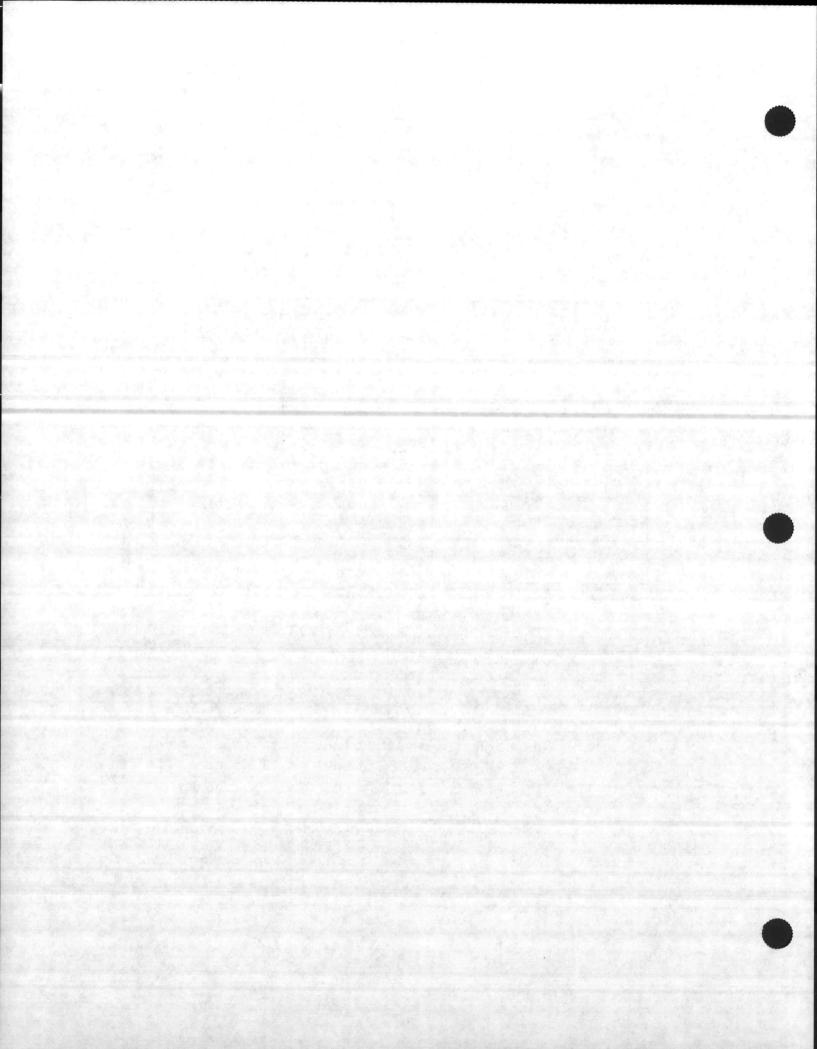
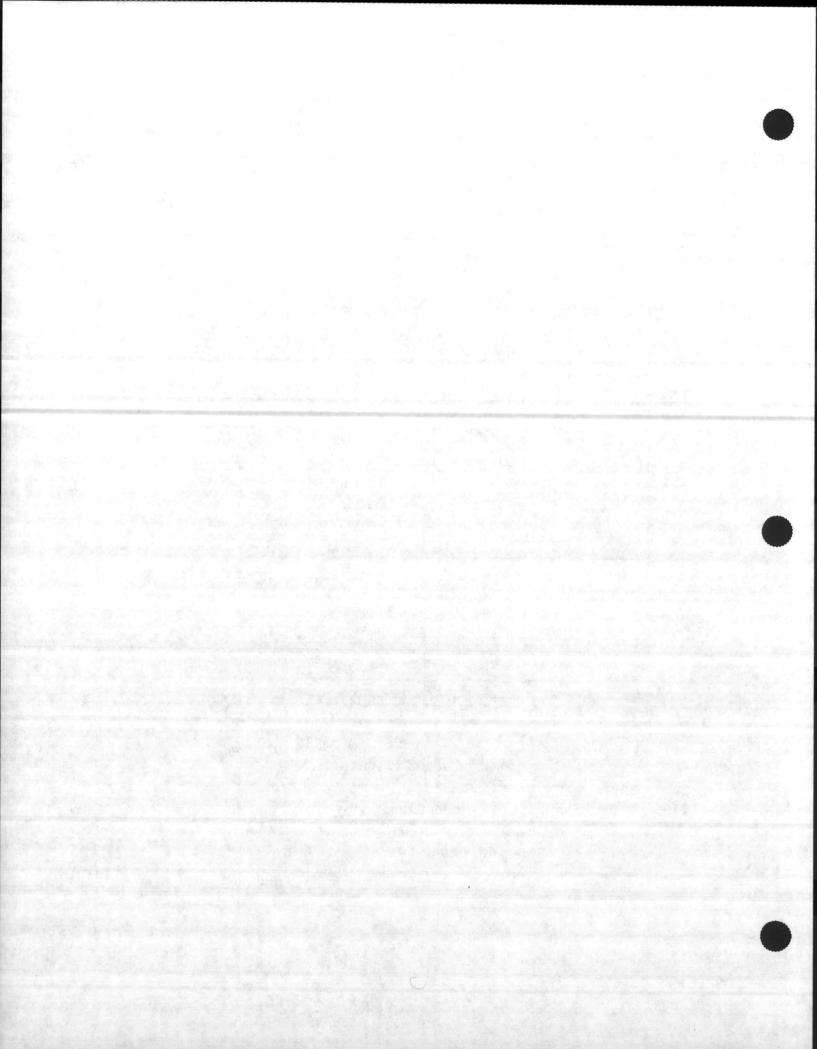


Table 5-21
Summary of Analytical Results
Nickel
CTO-017

	Location/Sample Name			
Sampling Interval	After Oil/Water Separator Sample OW ug/L	After Air Stripper Sample AS ug/L	After Carbon Filter Sample CF ug/L	
1	20 U	23	28	
2	20 U	20 U	186	
3	20 U	20 U	33	
4	20 U	20 U	20 U	
5	20 U	20 U	20 U	
6	20 U	20 U	20 U	
7	20 U	20 U	20 U	
Duplicate	20 U	20 U	20 U	

- (1) A sample interval was a 12 hour period. This test consisted of seven consecutive 12 hour sampling intervals.
- (2) Samples were collected during the first 4 hours of a sampling interval.
- (3) If the qualifier "U" is present, the analyte was analyzed for but not detected.
- (4) If the qualifier "B" is present, the reported value was obtained from a reading that was less than the Contract Required Detection Limit (CRDL), but, greater than or equal to the Instrument Detection Limit (IDL).
- (5) If the qualifier "D" is present, the result was obtained from an analysis performed at a secondary dilution.



The results of the chemical analysis indicate that trans-1,2-dichloroethene (DCE), trichloroethene (TCE), and vinyl chloride were consistently removed from the waste stream to non-detectable levels by the air stripper. Benzene, and to a lesser extent, toluene and ethylbenzene, remained in the waste stream after the air stripper at levels roughly equivalent to the influent levels to the air stripper until the fourth sampling interval, when the levels consistently dropped to non-detectable levels. The initial levels may be attributable to equipment start-up inefficiencies.

A review of the results of the inorganic analyses reveal that the air stripper and carbon adsorption unit did not have a substantial effect on the removal of the metal contaminants. The first three sampling intervals revealed inconsistencies in the analytical results, including apparent increases in chromium, iron, lead, nickel, and manganese levels across the treatment units. These apparent increases can be accounted for by noting that samples were taken from the influent to the treatment equipment at the same time as samples were collected from the effluent, and noting varying flow-through times in the equipment. For example, with a 400-gallon capacity air stripper and a flow rate of 1.5 gpm, there was a 4.44 hour time difference between influent and effluent to the air stripper. Therefore, increases across equipment may not be caused by equipment but rather are most likely due to fluctuations in influent concentrations. Subsequent sampling intervals revealed these metals to be at non-detectable levels before and after both major treatment units (air stripper and carbon adsorption). Iron, lead, and manganese showed little decline across the air stripper; however, there was a notable decline in the levels of these metals with time, possibly due to the decreased turbidity of the waste stream as the pump test progressed and the recovery well and aquifer become better developed. After the second sampling interval, lead levels after the air stripper were consistently below the NCWQCG levels of 50 µg/L.

The results of the analyses for engineering parameters are presented in Table 5-22. A review of the results indicate that the concentrations of oil and grease and total suspended solids were significantly lower than the groundwater characterization samples taken for the bench-scale study. The low levels, even at start-up of the study, may possibly be due to the extended pumping during the step-drawdown test causing a similar drop in the levels of oil and grease and total suspended solids as was detected in the reduced levels of organics and metals with time.

Samples from the fourth sampling interval, approximately midway through the 72-hour study, underwent multi-concentration acute toxicity testing. These samples were drawn from

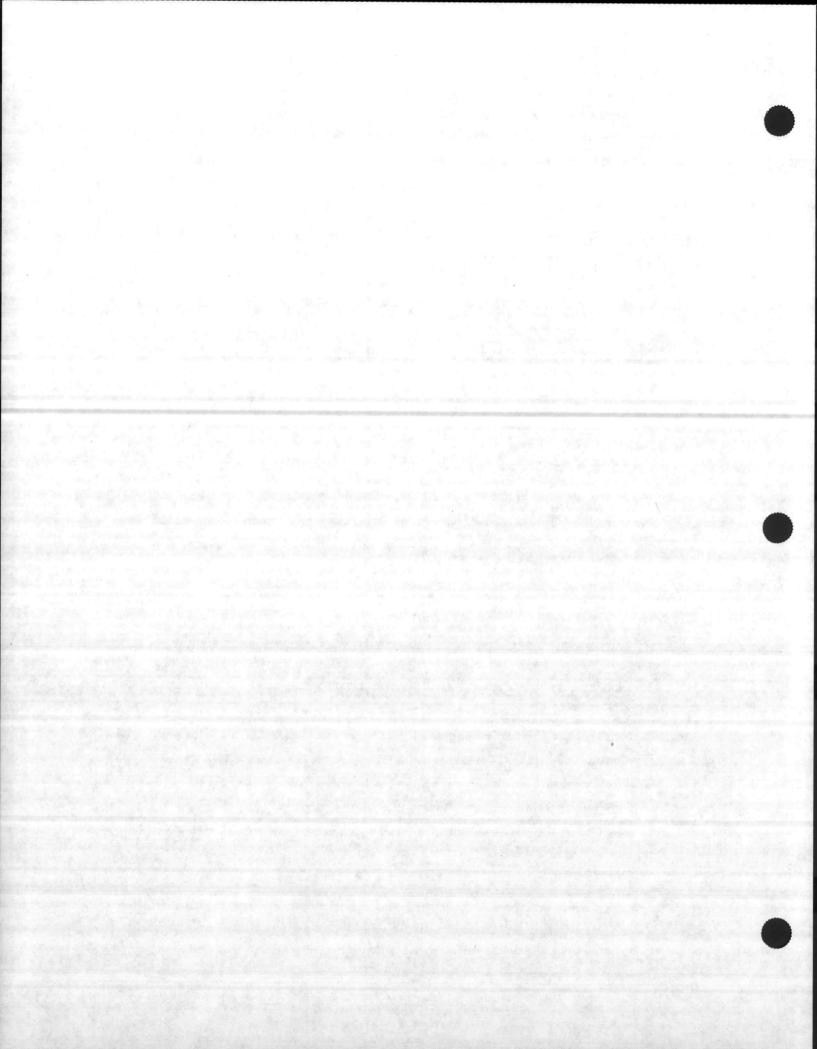
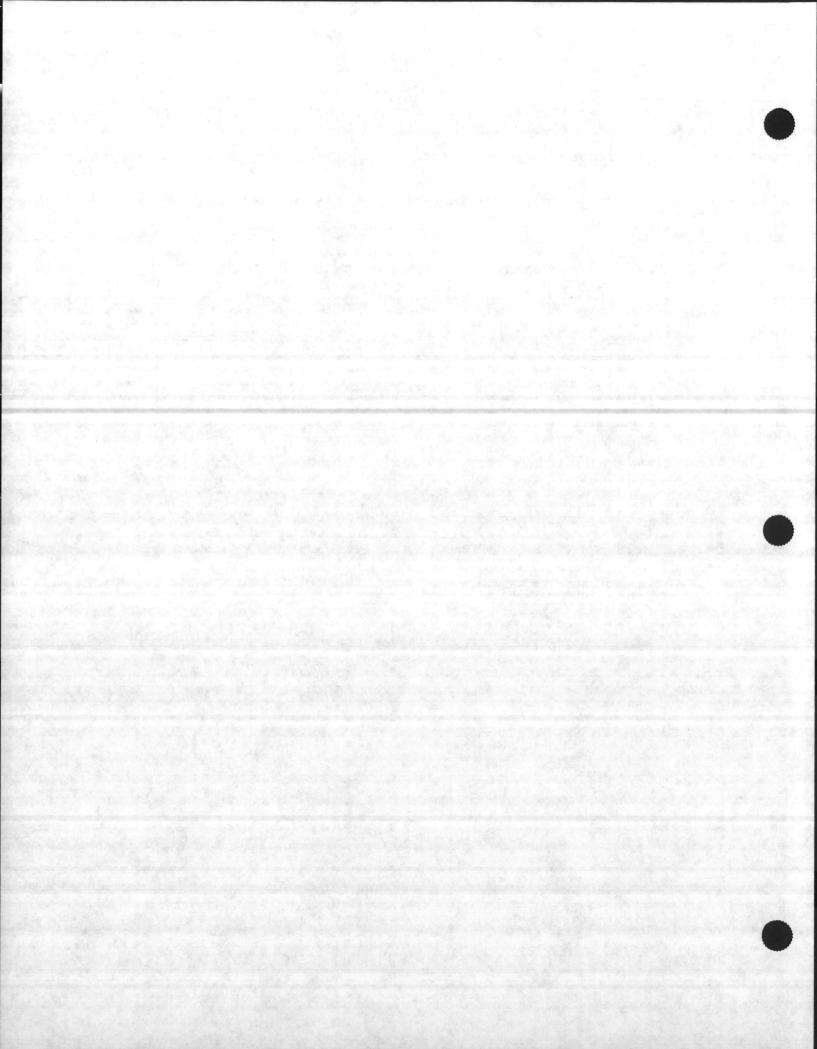


Table 5-22
HPIA Pilot Scale Treatability Study
Engineering Parameters

Parameter	Concentration  @ Start Up  (mg/l)	Concentration @ 72 hours (mg/l)
Oil and Grease, Gravimetric	<3	<3
Nitrate/Nitrite	< 0.1	< 0.1
Hardness, Total (as CaCO3)	46	44
Ammonia (N), Direct		
Ammonia (as N), Direct	0.4	0.5
Alkalinity, Pht (as CaCO3)	0	0
Alkalinity, Total (as CaCO3)	30	26
Alkalinity, Bicarbonate (as CaCO3)	30	26
Alkalinity, Carbonate (as CaCO3)	0	0
Chloride (as Cl)	23	24
Nitrite (as N)	< 0.02	< 0.02
Solids, Dissolved at 180C	110	87
Solids, Suspended at 103C	< 10	<10



the air stripper effluent as well as the carbon adsorption unit effluent. The raw data from this test is included in Appendix I, Pilot-Scale Treatability Study Analytical Results. A review of the results indicates that neither the unfinished effluent from the air stripper nor the carbon-polished effluent resulted in a LC50, or lethal concentration to 50 percent of the test organisms (fathead minnow) at any dilution volume from 0 to 100 percent. The fact that the air stripper effluent passed the toxicity test, combined with chemical analytical results showing removal of organic contaminants by air stripping alone to non-detectable levels, will be used in the design of the full-scale treatment system.

## 5.2.1.3 Analysis of Constant Rate Aquifer Test

The aquifer characteristics derived from an analysis of aquifer test data are transmissivity, storativity or specific yield, and hydraulic conductivity. These characteristics can be subsequently used to derive an estimate of the representative shallow groundwater flow rate.

Transmissivity (T) is defined as the rate of flow under a unit hydraulic gradient through a cross-section unit width over the whole thickness of the aquifer (Kruseman and deRidder, 1989). This parameter is designated as T and has the dimensions of length<sup>2</sup>/time.

Storativity or specific yield (S) is defined as the volume of water released per unit surface area of the aquifer per unit decline in the component of head normal to that surface (Kruseman and deRidder, 1976). This aquifer characteristic is dimensionless. In unconfined or semi-confined aquifers, the effects of the elasticity and compressibility of the aquifer material and the fluid are generally negligible. Storativity generally refers to confined aquifers, while specific yield refers to unconfined.

Hydraulic conductivity (K) is defined as the capacity of a porous medium to transmit water (Driscoll, 1986). This aquifer characteristic has the dimensions of length/time.

T, K, and S values were calculated using a computer software program designed by Groundwater Graphics of Oceanside, California. This program is called the "Graphical Well Analysis Package" (GWAP). The Neuman Method for unconfined aquifers with an elastic response was selected for use in this program based on the site conditions. The program generated log-log graphs for each monitoring well to calculate these values. Only data that indicated adequate drawdown curves were used for evaluation of aquifer characteristics. A printout of all graphs and data generated using GWAP is provided in Appendix J.

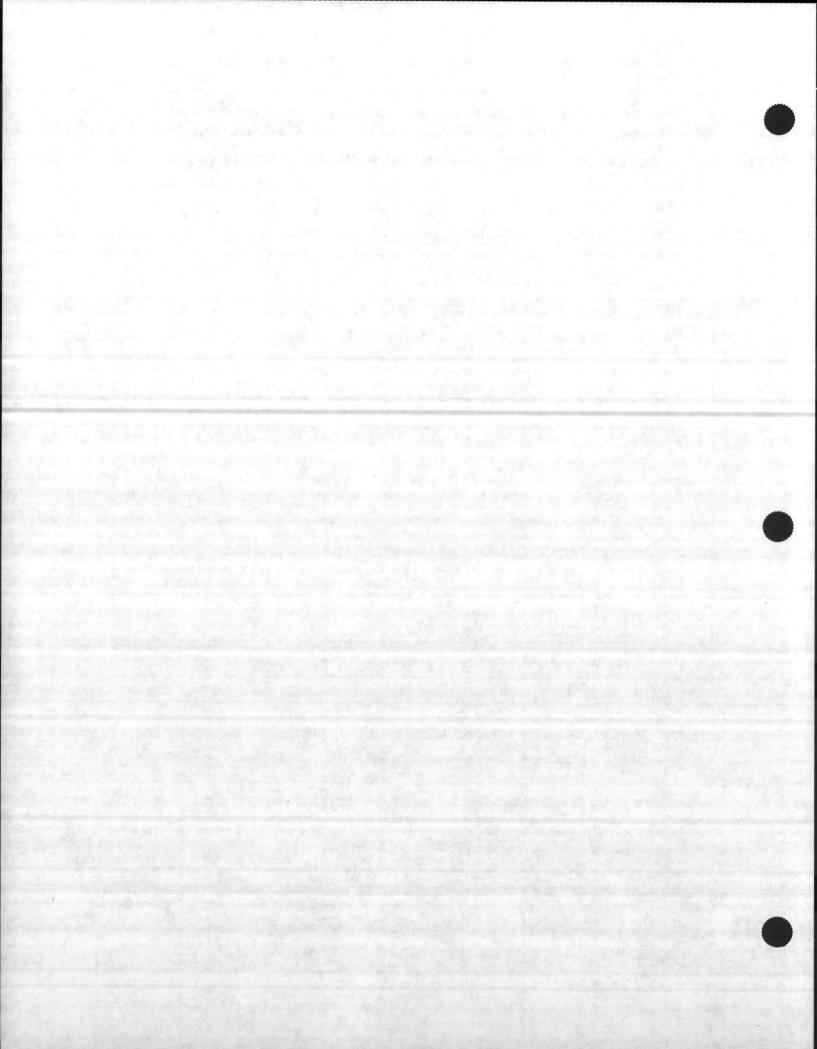


Table 5-23 summarizes of all the aquifer characteristics. The estimated, average T and S values are 5.61 x 10-2 gal/day/ft and 1.55 x 10-2, respectively. Aside from the values obtained from piezometer P-2, these values are representative of the materials underlying the site (Kruseman and deRidder, 1989). Values obtained from the pumping wells was not used to calculate the average values since they may not be representative of the aquifer. In addition, estimates of K were calculated using the following formula:

K = T/b

Where: K = hydraulic conductivity

T = transmissivity

b = estimated aquifer thickness

An approximate aquifer thickness of 25 feet was used, based on the total depth of the recovery wells. The estimated, average K value for the site is 22.45 gal/day/sq. ft. These values are representative of a fine-grained or silty sand (Fetter, 1988). This material is consistent with those present underlying the site. The values calculated are also consistent with values obtained during previous reports.

# 5.2.2 QA/QC

Quality assurance/quality control samples were taken during the pilot-scale treatability testing to ensure that analytical results are reliable for remedial technology selection and design purposes. Field duplicates were collected for the VOC and metals analyses, as well as for oil and grease. In addition, trip blanks were analyzed for VOCs for each cooler, and matrix spike/matrix spike duplicates were run by the laboratory. No unusual variances were observed in any of the QA/QC samples. The QA/QC results are included in Appendix K.

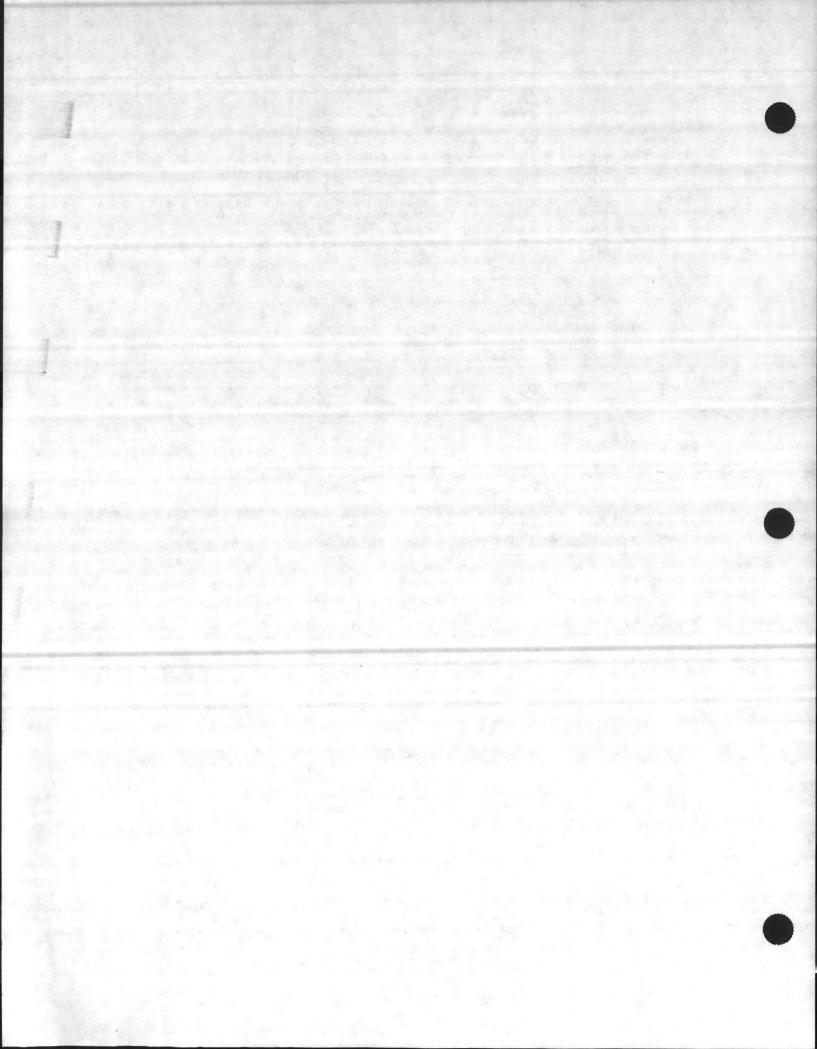
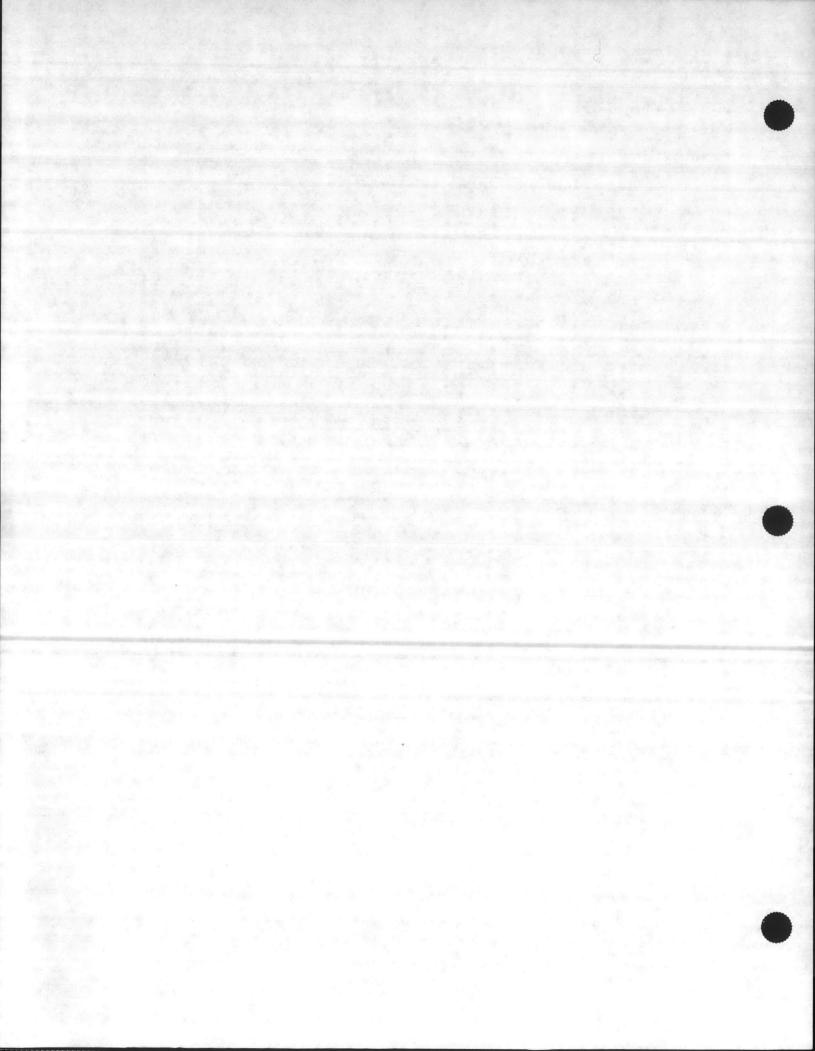


TABLE 5-23

AQUIFER CHARACTERISTICS FOR THE SHALLOW AQUIFER
AT THE HPIA

Well Number	Transmissivity (gal/day/ft)	Hydraulic Conductivity (gal/day/sq. ft.)	Storativity
RW-1	$1.30 \times 10^{2}$	5.215	6.87 x 10-2
P-1	$8.04 \times 10^{2}$	32.15	4.06 x 10-2
P-2	$3.85 \times 10^{2}$	15.39	8.67 x 10-4
24-1	4.96 x 10 <sup>2</sup>	19.83	4.89 x 10-3

<sup>(1)</sup> Values from RW-1 may not be representative of aquifer conditions And were not included in average.



#### 6.0 CONCLUSIONS AND RECOMMENDATIONS

This Treatability Study Report presented the results of the bench-scale and pilot-scale treatability study and aquifer pump test for the shallow aquifer at the HPIA Operable Unit. The objectives of this study were to provide remedy selection testing to evaluate the performance of metals removal, oil separation, air stripping and carbon adsorption in meeting the site-specific clean-up goals for the HPIA Operable Unit. The purpose of the aquifer pump test was to provide aquifer characteristics necessary for the design of the groundwater extraction system.

#### 6.1 Conclusions

### 6.1.1 Bench-Scale Testing

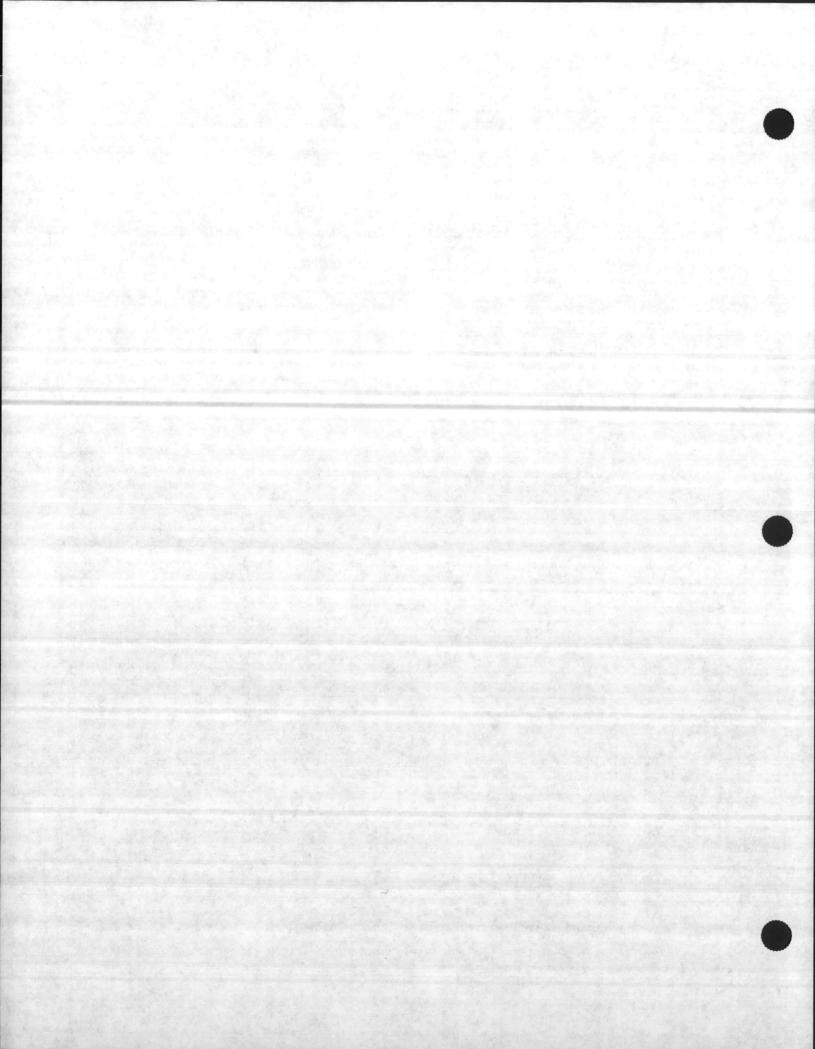
Groundwater characterization and bench-scale studies for oil and grease removal and suspended solids removal were conducted to determine the pretreatment requirements for the HPIA shallow groundwater. Based on the sample characterization results, it was determined that the metals of concern were primarily associated with the suspended solids. Based on the settling rates witnessed during the bench-scale testing, it is recommended that polymer addition with adequate settling time via a settling tank be incorporated into the full-scale treatment system.

The oil/water separation test indicated that most of the oil in the groundwater was free phase and not emulsified. Removal of this oil appears to be possible using a conventional oil/water separator. Suspended solids removal tests showed that physical treatment with an anionic polymer at an optimum dosage of 2 mg/L accelerated the settling rate of the suspended particles. The raw groundwater used in the bench-scale study had a much higher suspended solids content than was present after prolonged groundwater pumping during the pilot-scale study.

#### 6.1.2 Pilot-Scale Study

## 6.1.2.1 Aquifer Pump Test

A 6-inch diameter recovery well and two 2-inch diameter piezometers were installed at the location of the contaminated groundwater plume at the HPIA in the vicinity of the 900 series



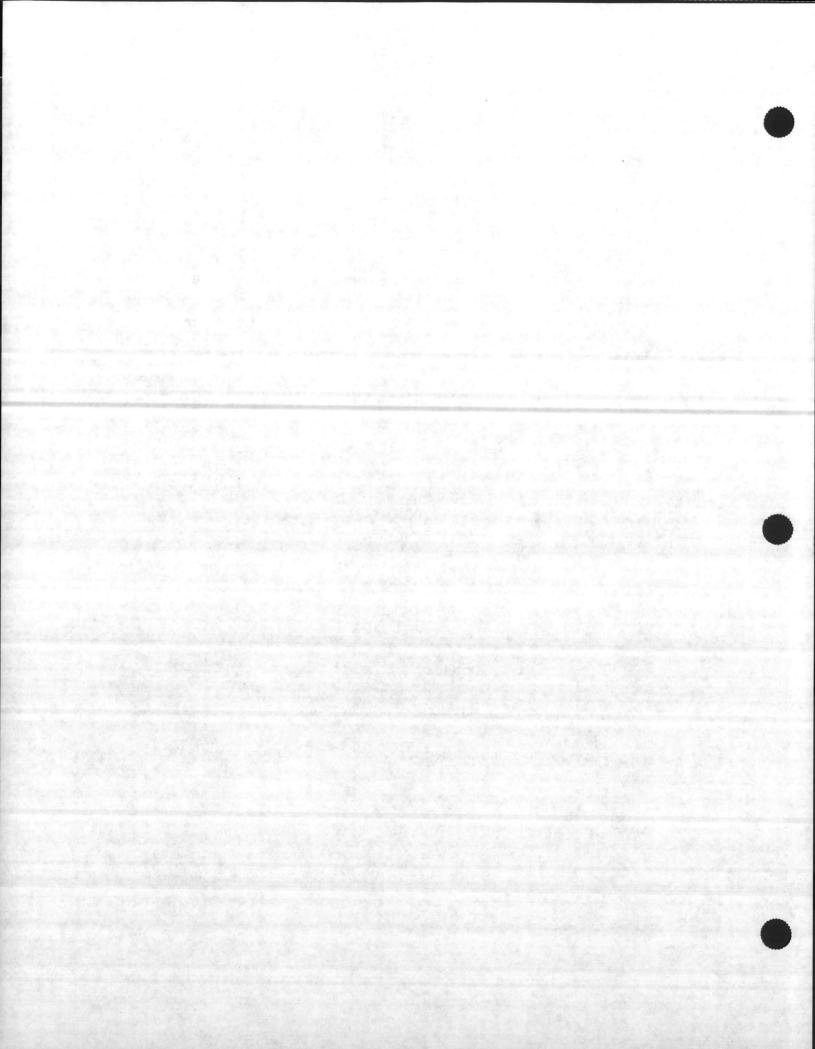
buildings for the purpose of conducting a 72-hour constant rate aquifer pump test. Based on the results of a step-drawdown test, a flow rate of 1.5 gpm was chosen for the constant rate aquifer test, which varied from the anticipated flow rate of 5 gpm proposed in the Work Plan, but is not unusual for the shallow aquifer at the Hadnot Point Industrial Area judging from previous studies (Appendix O). Existing monitoring wells and the new piezometers were continuously monitored for water level throughout the duration of the 72-hour test. A maximum drawdown of one foot was observed in piezometer P-2 located 60 feet from the recovery well. Drawdown in the other monitoring wells varied with distance from the recovery well.

The aquifer characteristics derived from the analysis of test data are transmissivity, storativity, and hydraulic conductivity. These values were calculated using a computer software package based on the Newman Method for unconfined aquifers with an elastic response based on site conditions. The estimated average transmissivity and storativity values are  $5.61 \times 10^2$  gal/day/ft and  $1.55 \times 10^{-2}$ , respectively, which are representative of the materials underlying the site. Using a estimated aquifer thickness of 25 feet, the estimated, average hydraulic conductivity for the site is 22.45 gal/day/sq. ft. These values are consistent with values obtained from previous reports. These results will be utilized in the Remedial Design of the Interim Remedial Action to determine zones of influence needed for the design of the groundwater extraction system.

Based on EPA and State concerns over the low flow rate obtained during the aquifer test and the applicability of the results for use in the design of the extraction system, Baker recommends that the design specifications require an aquifer test be conducted as part of the recovery well installation and that an option to install a limited quantity of additional recovery wells based on the results of the aquifer test be provided.

#### 6.1.2.2 Pilot-Scale Treatability Study

The Pilot-Scale Treatability Study evaluated the performance of oil/water separation, air stripping, and carbon adsorption in meeting the site-specific clean-up goals for the HPIA Operable Unit. Raw groundwater pumped during the 72-hour aquifer pump test was treated by the pilot-scale system and discharged to the HPIA sanitary sewer system. Samples of the groundwater were collected before and after the air stripper and carbon adsorption unit and analyzed for the contaminants of concern.



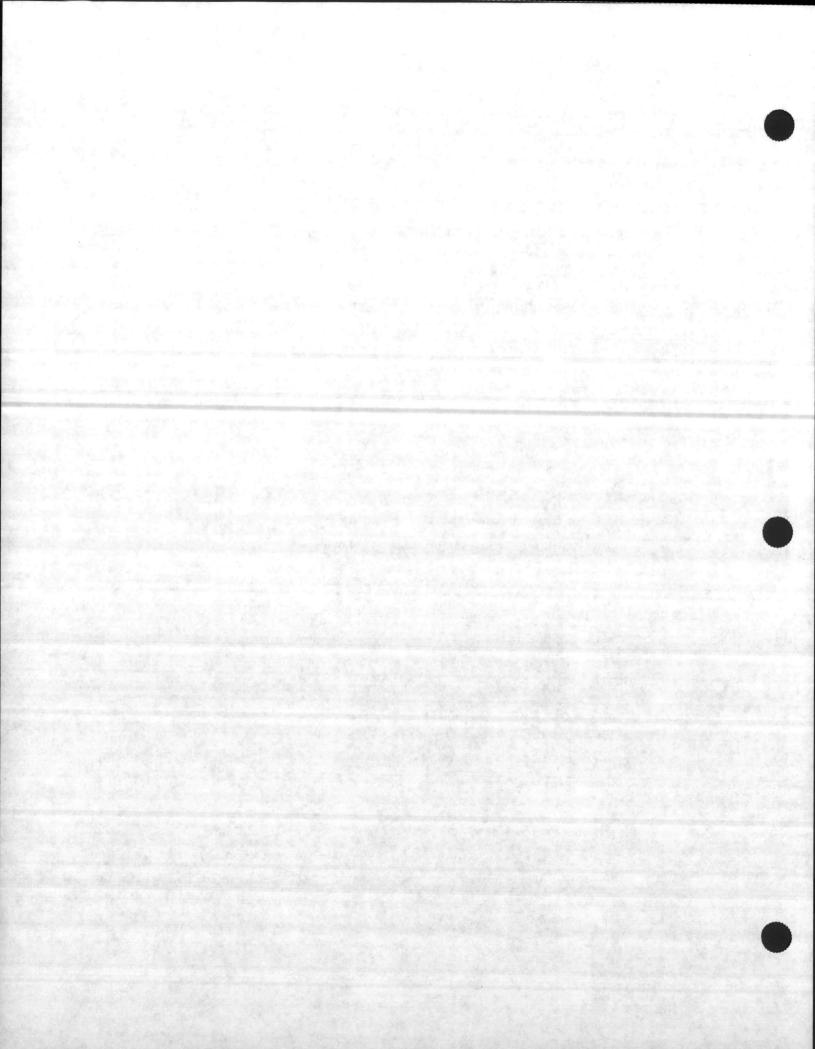
The waste characteristics of the pumped groundwater were similar to the results of earlier studies, with the exception of the presence of vinyl chloride. The results of the chemical analysis indicate that the DCE, TCE, and vinyl chloride were consistently removed from the waste stream to non-detectable levels by the air stripper. After initially low efficiencies at start-up, the air stripper was effective in reducing benzene, toluene, and ethylbenzene to non-detectable levels. Effluent from both the air stripper and carbon adsorption unit passed the multi-concentration acute toxicity test.

The results of the inorganic analyses showed a decline in the levels of metal in the influent to the air stripper with time. The air stripper and carbon adsorption unit were ineffective in reducing the levels of metals. Total suspended solids were much lower during the pump test and pilot-scale study than were evident during the bench-scale study, possible because the recovery well and aquifer became better developed as the pump test progressed.

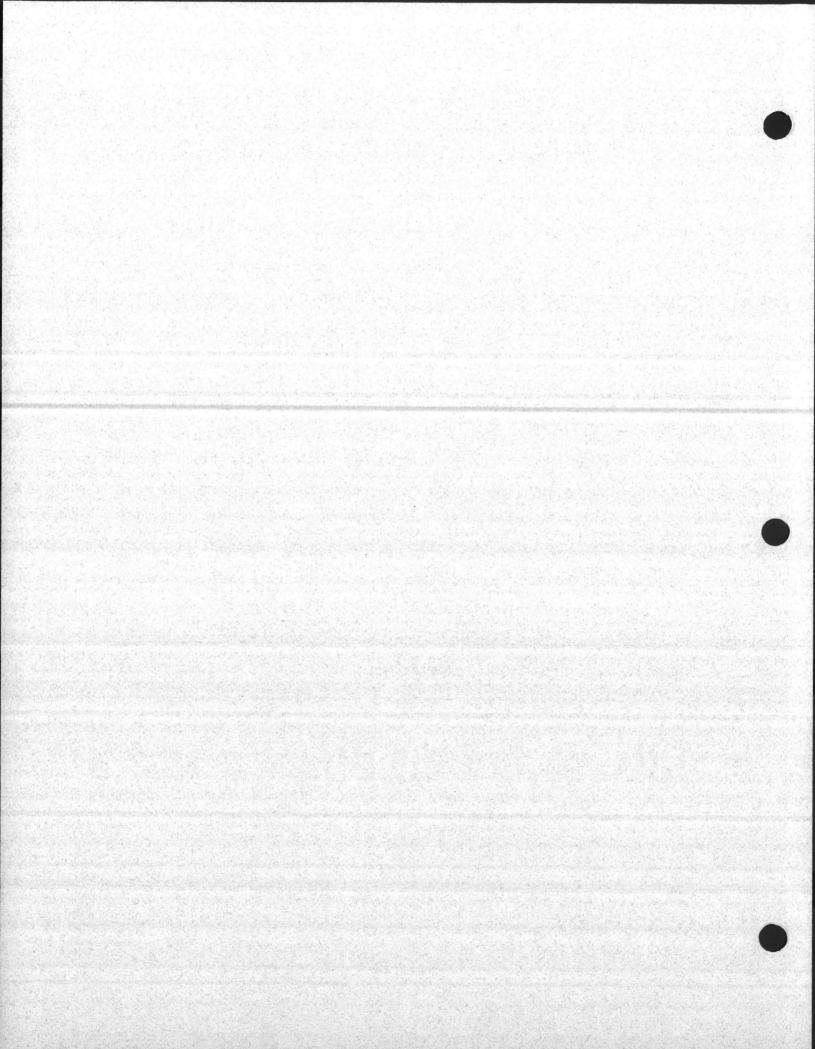
### 6.2 Recommendations

The results of this Treatability Study provide information to be used in the design of the full-scale treatment system for the Interim Remedial Action for the HPIA Operable Unit. Based on these results, the following recommendations are made:

- Air stripping as the primary treatment technology is effective in meeting the sitespecific clean-up goals for the HPIA Operable Unit. Because the contaminant levels witnessed during the treatability study were lower than previous monitoring results, carbon adsorption as a finishing process is recommended at start-up until monitoring results show that air stripping is effective in removing the organics.
- Pretreatment prior to air stripping should include a conventional oil/water separator
  to remove the low levels of oil and grease and a metals removal system including
  flocculation by polymer addition, settling, and filtration.
- During installation of the recovery wells, aquifer tests should be conducted to determine well yield. A limited quantity of additional wells should be installed should results similar to the treatability study's aquifer test be encountered.

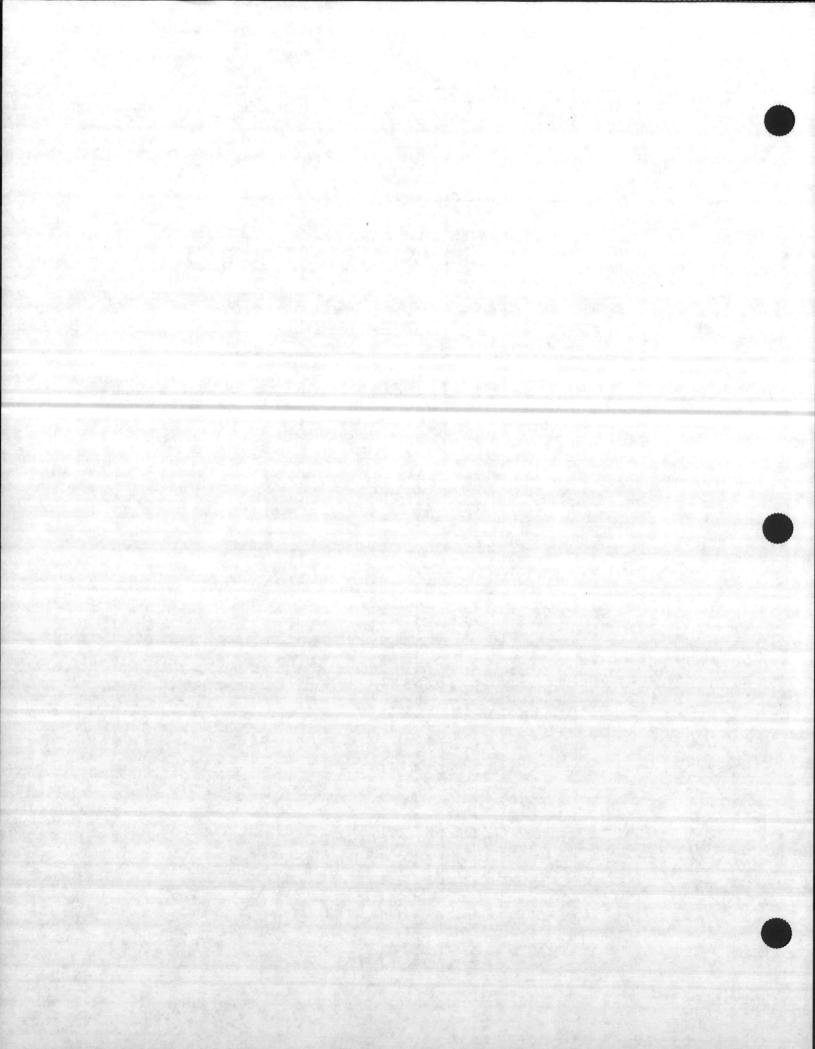


APPENDIX A STEP-DRAWDOWN TEST DATA



CONTRACT TASK ORDER: 0017 SITE I.D.: CAMP LEJEUNE, HPIA TEST: STEP 1

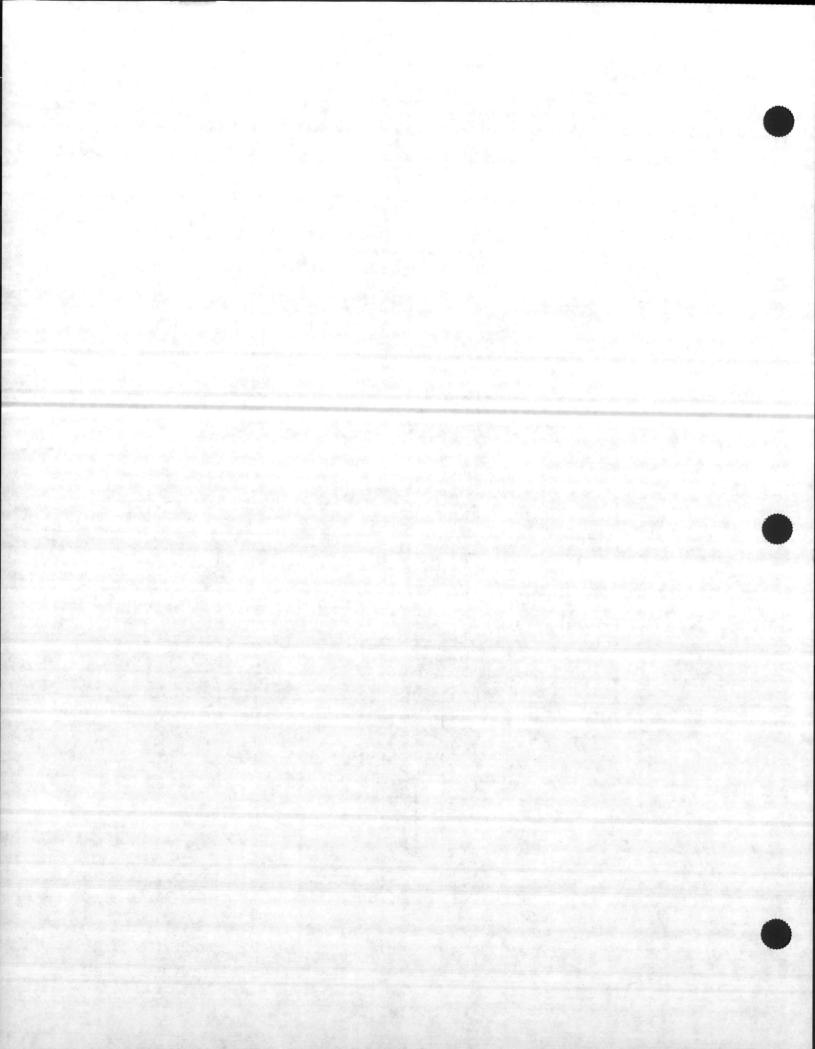
	WELL NUMBER		
TIME	RW-1	P-2	
(MIN)	SWL (FEET)	SWL (FEET)	
0.0000	7.247	4.509	
0.0033	7.177	4.509	
0.0066	6.924	4.509	
0.0100	7.108	4.516	
0.0133	7.184	4.509	
0.0166	7.000	4.509	
0.0200	7.070	4.509	
0.0233	7.387	4.516	
0.0266	7.380	4.509	
0.0300	6.956	4.516	
0.0333	7.070	4.516	
0.0500	7.507	4.509	
0.0666	7.234	4.516	
0.0833	7.215	4.516	
0.1000	7.291	4.516	
0.1166	7.285	4.516	
0.1333	7.285	4.516	
0.1500	7.285	4.516	
0.1666	7.298	4.522	
0.1833	7.304	4.516	
0.2000	7.304	4.516	
0.2166	7.317	4.516	
0.2333	7.323	4.516	
0.2500	7.330	4.516	
0.2666	7.330	4.516	
0.2833	7.342	4.516	
0.3000	7.349	4.516	
0.3166	7.361	4.516	
0.3333	7.380	4.509	
0.4166	7.399	4.516	
0.5000	7.431	4.509	
0.5833	7.475	4.509	
0.6666	7.501	4.509	
0.7500	7.539	4.522	
0.8333	7.564	4.516	
0.9166	7.596	4.516	
1.0000	7.627	4.516	
1.0833	7.665	4.516	
1.1666	7.684	4.516	
1.2500	7.710	4.516	
1.3333	7.741	4.516	



CONTRACT TASK ORDER: 0017 SITE I.D.: CAMP LEJEUNE, HPIA

TEST: STEP 1

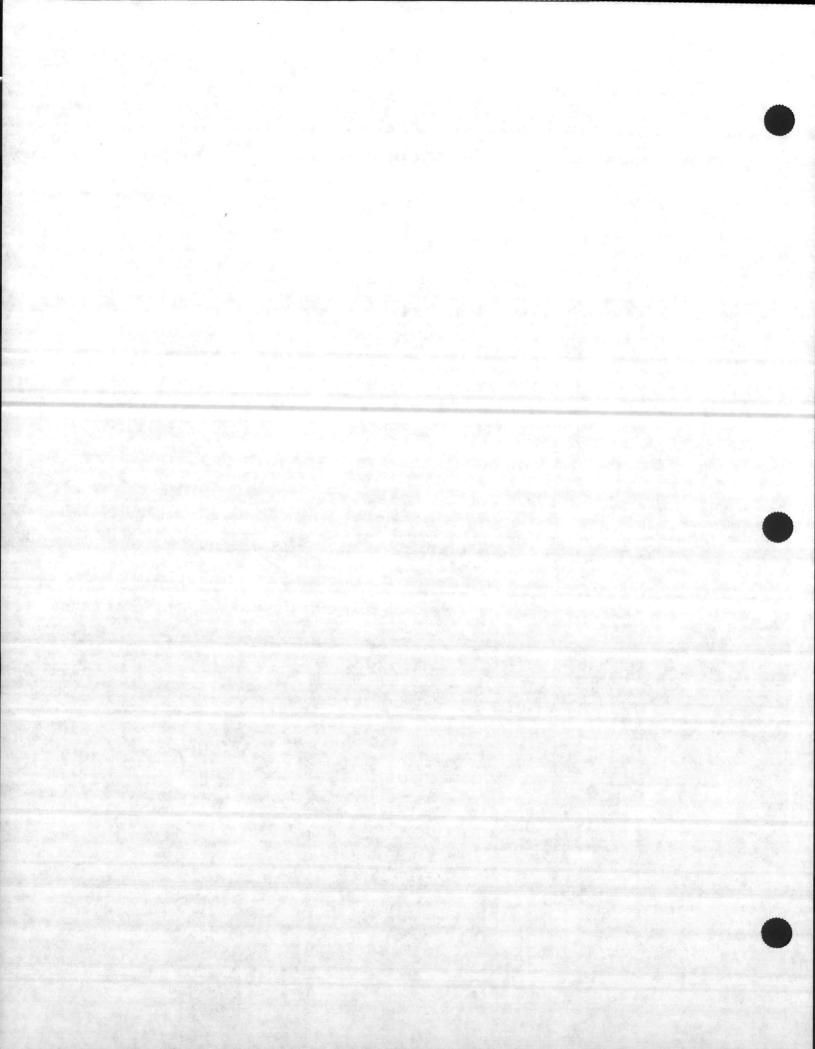
ELAPSED	WELL N	JMBER
TIME	RW-1	P-2
	SWL	SWL
(MIN)	(FEET)	(FEET)
1.4166	7.760	4.516
1.5000	7.792	4.516
1.5833	7.811	4.522
1.6666	7.830	4.522
1.7500	7.843	4.516
1.8333	7.868	4.516
1.9166	7.893	4.516
2.0000	7.912	4.516
2.5000	8.160	4.516
3.0000	8.388	4.516
3.5000	8.597	4.516
4.0000	8.793	4.522
4.5000	8.971	4.522
5.0000	9.142	4.516
5.5000	9.300	4.528
6.0000	9.439	4.522
6.5000	9.572	4.528
7.0000	9.705	4.535
7.5000	9.807	4.528
8.0000	9.914	4.535
8.5000	10.016	4.535
9.0000	10.010	4.535
9.5000	10.111	4.533
10.0000	10.193	4.535
12.0000	10.203	4.547
14.0000	10.333	4.554
16.0000	10.723	4.560
18.0000	10.870	4.566
20.0000	11.079	4.573
	11.079	4.585
22.0000	11.133	4.598
24.0000		4.598
26.0000	11.276	
28.0000	11.326	4.611
30.0000	11.358	4.617
32.0000	11.409	4.636
34.0000	11.440	4.642
36.0000	11.466	4.649
38.0000	11.510	4.668
40.0000	11.554	4.674
42.0000	11.586	4.680
44.0000	11.624	4.687



CONTRACT TASK ORDER: 0017 SITE I.D.: CAMP LEJEUNE, HPIA

TEST: STEP 1

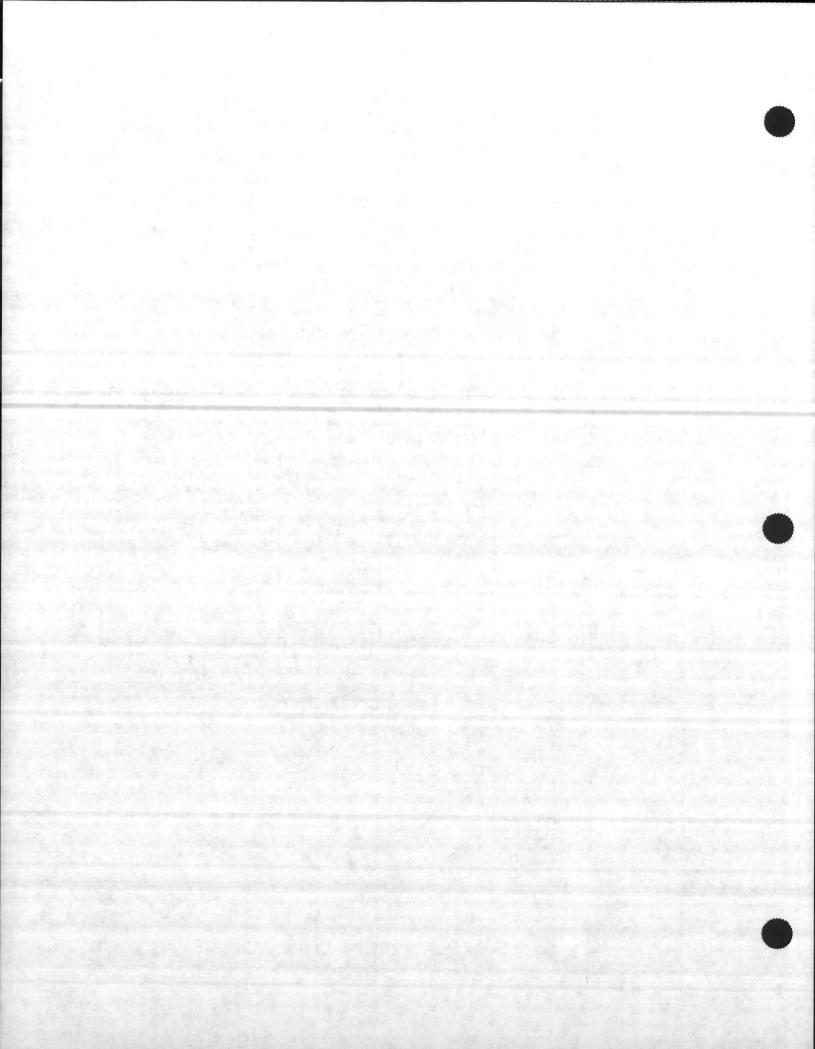
ELAPSED	WELL NUMBER		
TIME	RW-1	P-2	
(MIN)	SWL (FEET)	SWL (FEET)	
46.0000	11.643	4.693	
48.0000	11.681	4.712	
50.0000	11.706	4.718	
52.0000	11.725	4.725	
54.0000	11.738	4.731	
56.0000	11.750	4.744	
58.0000	11.725	4.750	
60.0000	11.706	4.763	
62.0000	11.719	4.782	



CONTRACT TASK ORDER: 0017 SITE I.D.: CAMP LEJEUNE, HPIA

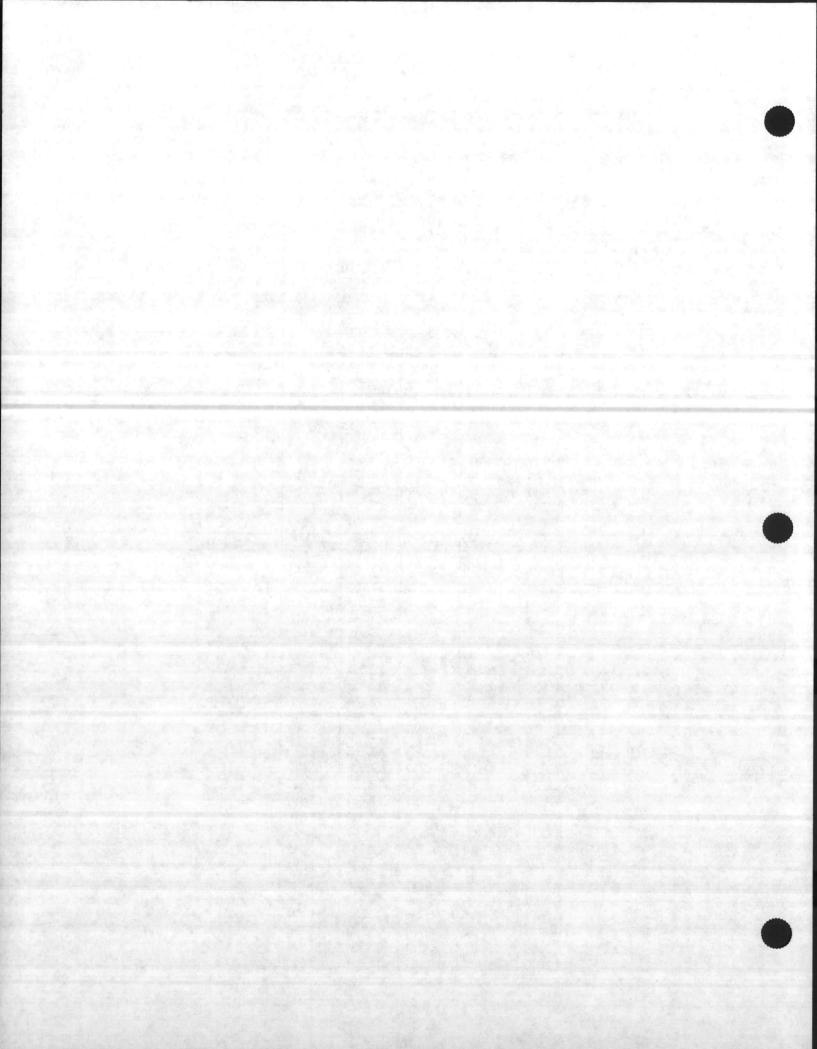
TEST: STEP 1

ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
	SWL	SWL	SWL	SWL
(MIN)	(FEET)	(FEET)	(FEET)	(FEET)
0.0000	6.804	6.780	12.704	11.610
0.0083	6.804	6.780	12.704	11.610
0.0065	6.798	6.780	12.704	11.610
0.0250	6.798	6.774	12.704	11.610
0.0333	6.798	6.774	12.704	11.610
0.0333	6.804	6.780	12.704	11.610
0.0500	6.798	6.780	12.704	11.594
0.0583	6.804	6.780	12.704	11.610
0.0666	6.804	6.780	12.704	11.610
0.0750	6.804	6.780	12.720	11.610
0.0833	6.804	6.780	12.720	11.610
0.0916	6.804	6.780	12.704	11.610
0.1000	6.804	6.780	12.704	11.610
0.1083	6.804	6.780	12.704	11.594
0.1166	6.804	6.774	12.704	11.610
0.1250	6.804	6.774	12.720	11.610
0.1333	6.804	6.780	12.704	11.610
0.1416	6.804	6.780	12.704	11.594
0.1500	6.804	6.780	12.704	11.594
0.1583	6.804	6.780	12.704	11.610
0.1666	6.804	6.780	12.704	11.610
0.1750	6.804	6.780	12.704	11.610
0.1833	6.804	6.780	12.704	11.610
0.1916	6.804	6.780	12.704	11.610
0.2000	6.804	6.780	12.720	11.594
0.2083	6.804	6.780	12.704	11.610
0.2166	6.804	6.780	12.704	11.610
0.2250	6.804	6.780	12.720	11.610
0.2333	6.811	6.774	12.704	11.610
0.2416	6.804	6.780	12.704	11.610
0.2500	6.804	6.780	12.704	11.610
0.2583	6.804	6.780	12.704	11.610
0.2666	6.804	6.780	12.704	11.610
0.2750	6.811	6.780	12.720	11.610
0.2833	6.804	6.780	12.704	11.610
0.2916	6.811	6.780	12.704	11.610
0.3000	6.804	6.780	12.704	11.610
0.3083	6.811	6.780	12.704	11.594
0.3166	6.804	6.780	12.720	11.594
0.3250	6.804	6.774	12.704	11.610
0.3233	6.804	6.780	12.704	11.610



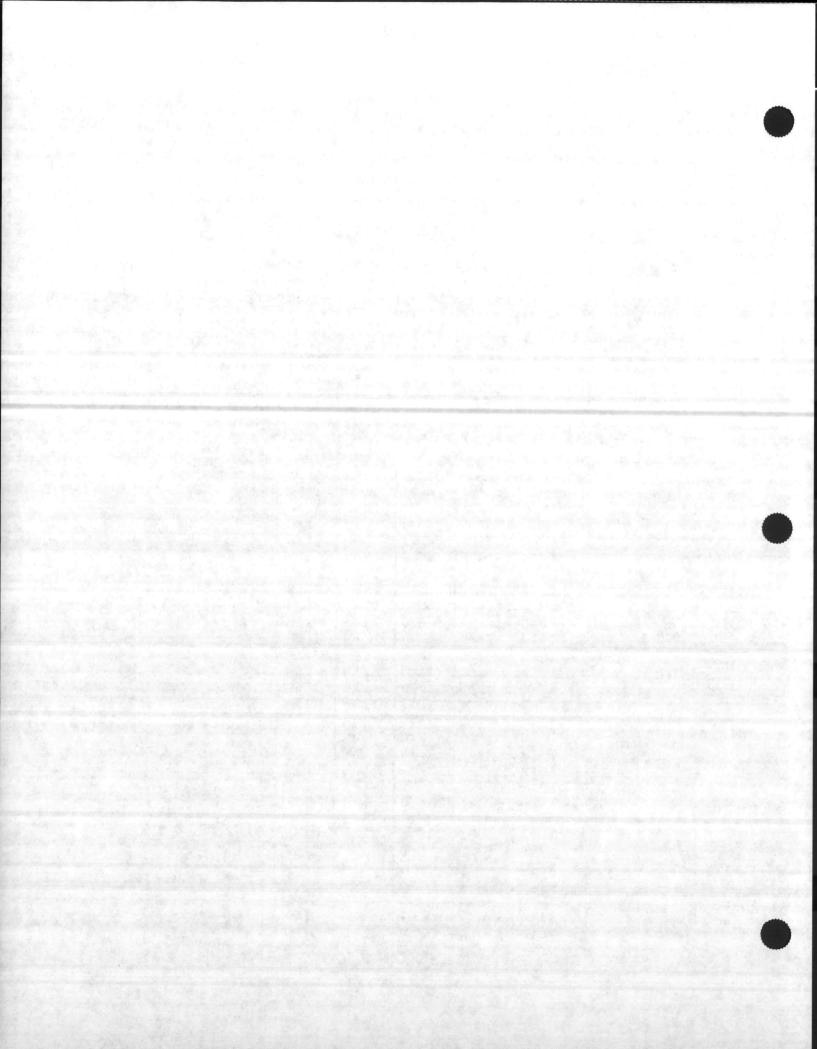
TEST: STEP 1

ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
(MIIIA)	(FEET)	(ILLI)	(ILLI)	(I LLI)
0.3500	6.804	6.780	12.704	11.610
0.3666	6.804	6.774	12.704	11.610
0.3833	6.804	6.774	12.704	11.610
0.4000	6.804	6.774	12.704	11.610
0.4166	6.804	6.774	12.704	11.610
0.4333	6.804	6.774	12.704	11.610
0.4500	6.804	6.774	12.704	11.610
0.4666	6.804	6.774	12.704	11.610
0.4833	6.798	6.774	12.704	11.610
0.5000	6.798	6.774	12.704	11.610
0.5166	6.798	6.774	12.704	11.610
0.5333	6.798	6.774	12.704	11.610
0.5500	6.804	6.774	12.704	11.610
0.5666	6.798	6.774	12.704	11.610
0.5833	6.804	6.780	12.704	11.594
0.6000	6.804	6.774	12.704	11.610
0.6166	6.804	6.780	12.704	11.610
0.6333	6.798	6.774	12.704	11.594
0.6500	6.798	6.774	12.704	11.594
0.6666	6.798	6,774	12.704	11.610
0.6833	6.804	6,774	12.704	11.594
0.7000	6.798	6.774	12.704	11.594
0.7166	6.798	6.774	12.704	11.594
0.7333	6.804	6.780	12.704	11.610
0.7500	6.804	6.774	12.704	11.610
0.7666	6.804	6.780	12.704	11.610
0.7833	6.804	6.780	12.720	11.610
0.8000	6.811	6.780	12.720	11.610
0.8166	6.811	6,780	12.720	11.610
0.8333	6.811	6.780	12.720	11.610
0.8500	6.811	6.780	12.720	11.610
0.8666	6.811	6.780	12.704	11.610
0.8833	6.811	6.780	12.704	11.610
0.9000	6.804	6.780	12.704	11.610
0.9166	6.804	6.774	12.704	11.594
0.9333	6.804	6.774	12.704	11.594
0.9500	6.804	6.780	12.704	11.594
0.9666	6.804	6.780	12.688	11.594
0.9833	6.804	6.780	12.704	11.594
1.0000	6.804	6.774	12.704	11.594
1.2000	6.804	6.774	12.704	11.610



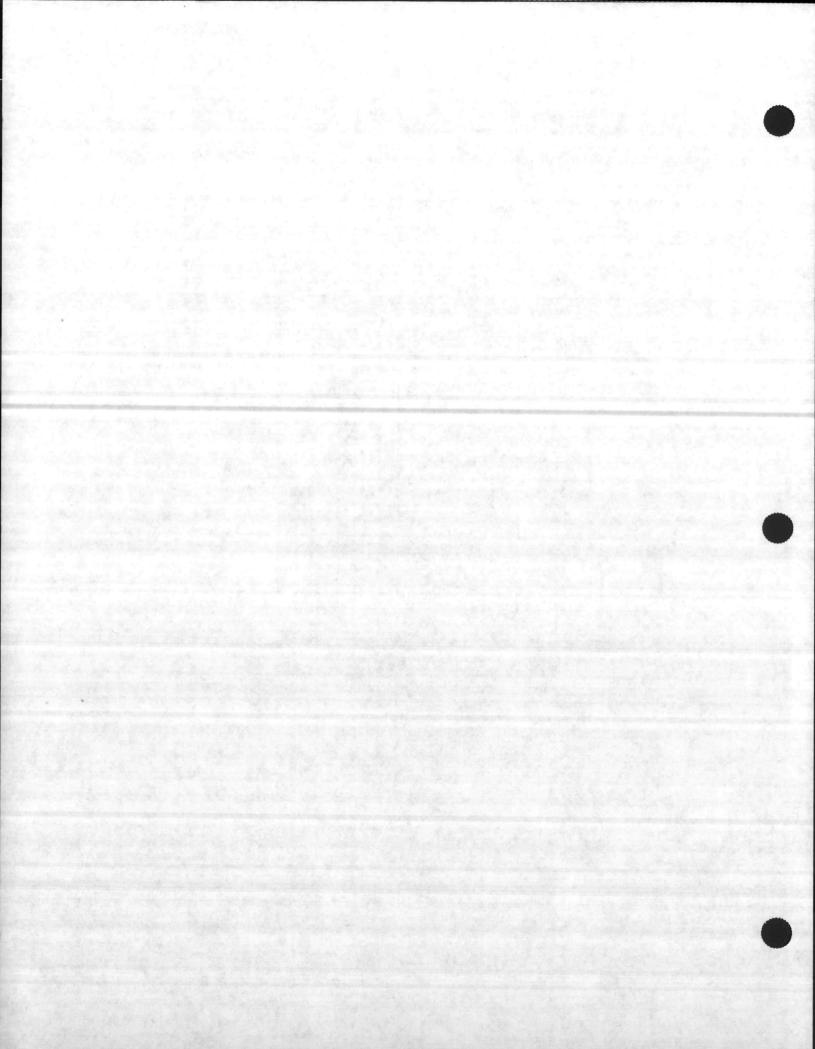
TEST: STEP 1 FLOW RATE: 1 GPM

ELAPSED	133	WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
	SWL	SWL	SWL	SWL
(MIN)	(FEET)	(FEET)	(FEET)	(FEET)
1.4000	6.804	6.774	12.704	11.594
1.6000	6.811	6.780	12.720	11.610
1.8000	6.798	6.774	12,704	11.594
2.0000	6.804	6.774	12.704	11.594
2.2000	6.817	6.768	12.704	11.594
2.4000	6.804	6.787	12.704	11.594
2.6000	6.804	6.774	12.688	11.610
2.8000	6.804	6.780	12.704	11.594
3.0000	6.804	6.774	12.704	11.610
3.2000	6.804	6.774	12.704	11.594
3.4000	6.804	6.780	12.704	11.594
3.6000	6.804	6.774	12.704	11.594
3.8000	6.798	6.774	12.704	11.594
4.0000	6.804	6.780	12.704	11.610
4.2000	6.804	6.774	12.688	11.610
4.4000	6.804	6.780	12.704	11.610
4.6000	6.811	6.780	12.704	11.610
4.8000	6.811	6.780	12.704	11.610
5.0000	6.811	6.780	12.704	11.594
	6.804	6.780	12.704	11.610
5.2000	6.804	6.780	12.704	11.610
5.4000	The second secon	The state of the s	12.704	11.594
5.6000	6.804	6.780	12.704	11.610
5.8000	6.804	6.780	12.704	11.610
6.0000	6.811	6.780		11.594
6.2000	6.804	6.780	12.688	11.594
6.4000	6.811	6.780	12.704	11.594
6.6000	6.804	6.780	12.704	
6.8000	6.811	6.780	12.704	11.594
7.0000	6.811	6.787	12.704	11.610
7.2000	6.804	6.780	12.704	11.59
7.4000	6.811	6.780	12.704	11.59
7.6000	6.804	6.787	12.704	11.59
7.8000	6.811	6.787	12.704	11.610
8.0000	6.811	6.780	12.704	11.610
8.2000	6.811	6.780	12.704	11.61
8.4000	6.804	6.780	12.704	11.61
8.6000	6.804	6.780	12.704	11.59
8.8000	6.804	6.774	12.704	11.59
9.0000	6.804	6.780	12.704	11.61
9.2000	6.804	6.780	12.704	11.59
9.4000	6.804	6.780	12.704	11.610

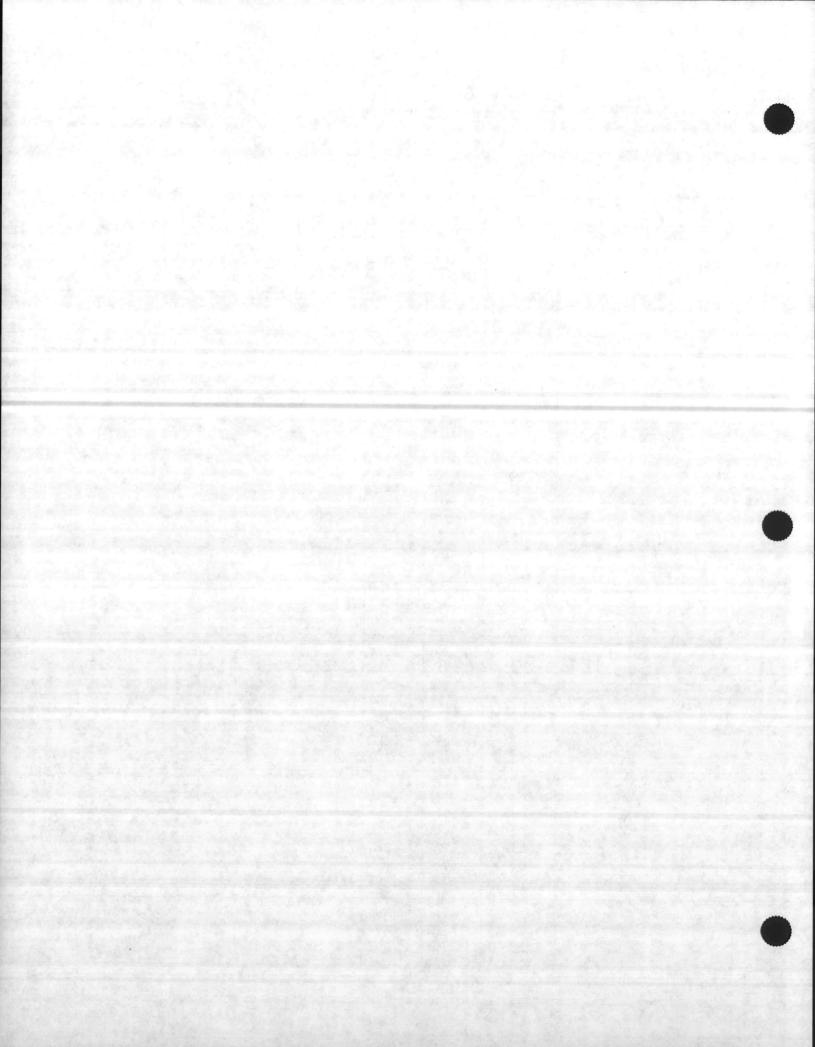


CONTRACT TASK ORDER: 0017 SITE I.D.: CAMP LEJEUNE, HPIA TEST: STEP 1 FLOW RATE: 1 GPM

ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
9,6000	6.811	6.787	12.704	11.594
9.8000	6.811	6.787	12.704	11.594
10.0000	6.811	6.787	12.704	11.610
12.0000	6.811	6.787	12.720	11.625
14.0000	6.811	6.793	12.720	11.610
16.0000	6.817	6.793	12.720	11.625
18.0000	6.817	6.793	12.720	11.625
20.0000	6.817	6.793	12.720	11.610
22.0000	6.817	6.799	12.720	11.625
24.0000	6.817	6.793	12.720	11.610
26.0000	6.817	6.793	12.720	11.610
28.0000	6.817	6.793	12.720	11.610
30,0000	6.824	6.806	12.720	11.625
32.0000	6.824	6.806	12.720	11.625
34.0000	6.824	6.806	12.735	11.610
36.0000	6.824	6.812	12.720	11.610
38.0000	6.830	6.812	12.720	11.610
40,0000	6.830	6.812	12.751	11.625
42.0000	6.830	6.825	12.720	11.625
44.0000	6.836	6.818	12.720	11.625
46.0000	6.830	6.825	12.735	11.625
48.0000	6.836	6.825	12.735	11.625
50.0000	6.836	6.825	12.720	11.610
52.0000	6.836	6.825	12.720	11.625
54.0000	6.843	6.831	12.720	11.625
56.0000	6.843	6.831	12.735	11.625
58.0000	6.843	6.837	12.720	11.625
60.0000	6.849	6.837	12.720	11.625
62.0000	6.849	6.837	12.735	11.625

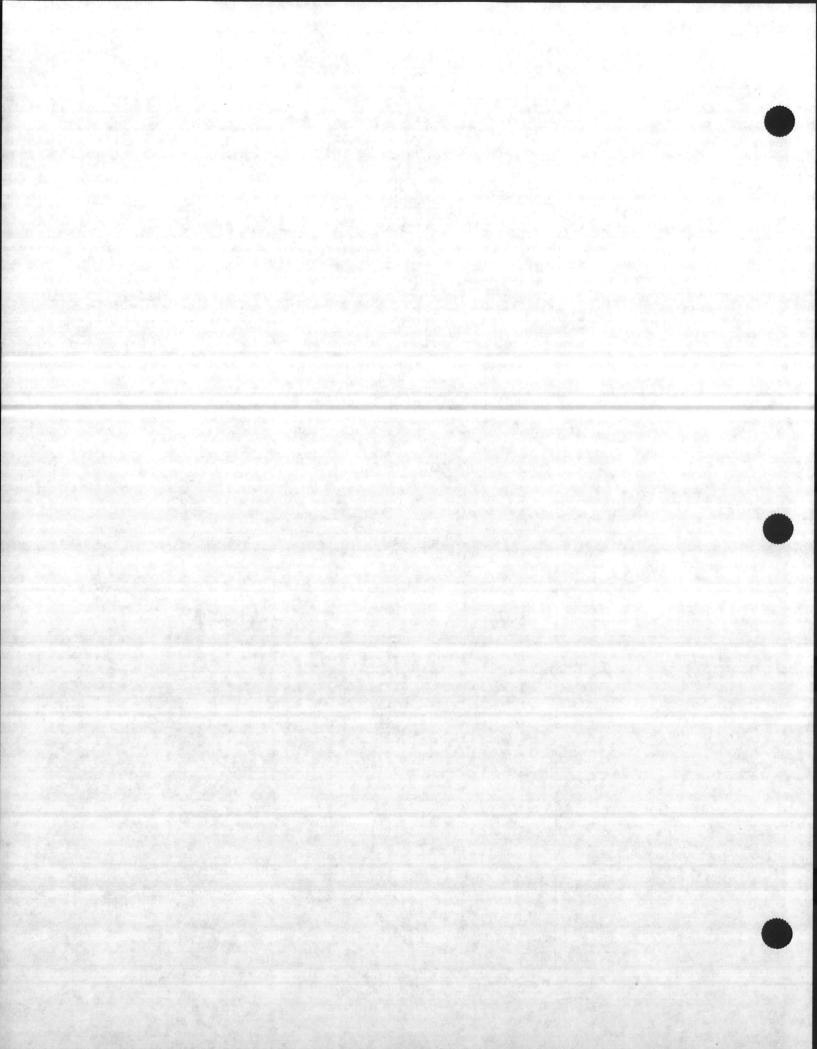


	WELL NU	JMBER
TIME	RW-1	P-2
	SWL	SWL
(MIN)	(FEET)	(FEET)
0.0000	11.706	4.782
0.0033	11.706	4.782
0.0066	11.712	4.782
0.0100	11.719	4.782
0.0133	11.712	4.788
0.0166	11.706	4.788
0.0200	11.706	4.782
0.0233	11.719	4.788
0.0266	11.712	4.788
0.0300	11.712	4.788
0.0333	11.706	4.788
0.0500	11.712	4.782
0.0666	11.712	4.788
0.0833	11.719	4.788
0.1000	11.712	4.788
0.1166	11.712	4.788
0.1333	11.706	4.788
0.1500	11.712	4.788
0.1666	11.719	4.788
0.1833	11.706	4.788
0.2000	11.719	4.788
0.2166	11.706	4.788
0.2333	11.719	4.788
0.2500	11.712	4.788
0.2666	11.712	4.788
0.2833	11.712	4.795
0.3000	11.719	4.795
0.3166	11.712	4.788
0.3333	11.712	4.795
0.4166	11.712	4.788
0.5000	11.719	4.795
0.5833	11.719	4.795
0.6666	11.719	4.795
0.7500	11.706	4.788
0.8333	11.719	4.788
0.9166	11.719	4.795
1.0000	11.719	4.795
1.0833		4.795
1.1666	11.712	4.795
1.2500	The second second second second	4.795
1.3333	11.719	4.795

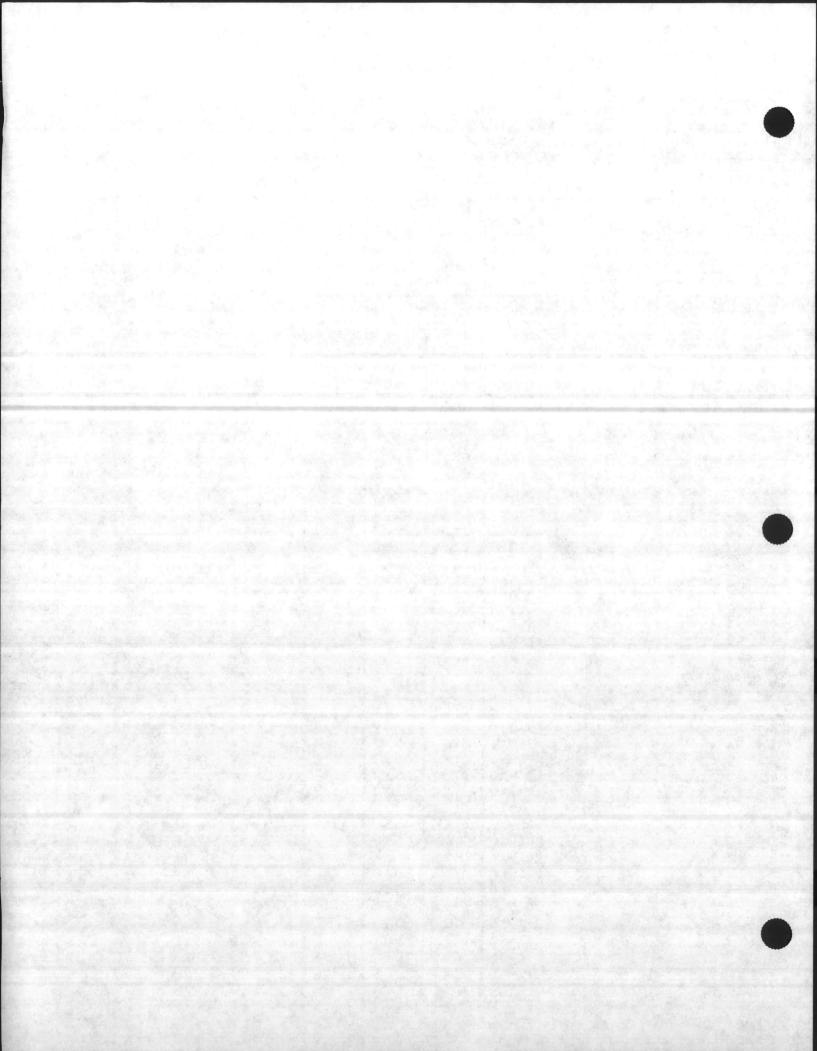


TEST: STEP 2 FLOW RATE: 1.5 GPM

1.4166 11.719 4.795 1.5000 11.706 4.795 1.5833 11.719 4.795 1.6666 11.719 4.795 1.7500 11.725 4.795 1.8333 11.706 4.795 1.9166 11.712 4.801 2.0000 11.725 4.788 2.5000 11.719 4.795 3.0000 11.725 4.801 3.5000 11.725 4.801 3.5000 11.725 4.801 4.5000 11.731 4.795 4.5000 11.744 4.801 5.0000 11.833 4.807 5.5000 11.896 4.807 6.5000 12.048 4.814 7.5000 12.181 4.814 7.5000 12.295 4.814 8.5000 12.618 4.820 9.0000 13.061 4.826 9.0000 13.061 4.826 9.0000 13.333 4.835 14.0000 13.250 4.826 10.0000 13.250 4.826 10.0000 13.333 4.835 14.0000 13.554 4.826 16.0000 14.218 4.858 18.0000 14.554 4.871 22.0000 15.047 4.896 24.0000 15.047 4.896 24.0000 15.433 4.921 28.0000 15.604 4.934 30.0000 15.762 4.946 32.0000 15.914 4.953 38.0000 16.046 4.977 38.0000 16.046 4.977 38.0000 16.046 4.977 38.0000 16.046 4.977 38.0000 16.046 4.977 38.0000 16.046 4.977 38.0000 16.046 4.977 38.0000 16.046 4.977 38.0000 16.046 4.977 38.0000 16.046 4.977 38.0000 16.046 4.977 38.0000 16.046 4.977 38.0000 16.046 4.997	ELAPSED	WELL N	JMBER
(MIN)         (FEET)         (FEET)           1.4166         11.719         4.795           1.5000         11.706         4.795           1.5833         11.719         4.795           1.6666         11.719         4.795           1.7500         11.725         4.795           1.8333         11.706         4.795           1.9166         11.712         4.801           2.5000         11.719         4.795           3.0000         11.725         4.788           2.5000         11.719         4.795           3.5000         11.725         4.801           3.5000         11.725         4.795           4.0000         11.731         4.795           4.5000         11.744         4.801           5.0000         11.833         4.807           6.5000         11.896         4.807           6.5000         12.048         4.814           7.5000         12.295         4.814           7.5000         12.295         4.814           7.5000         12.966         4.820           9.5000         13.130         4.826           9.5000         13.130	TIME	RW-1	P-2
1.5000       11.706       4.795         1.5833       11.719       4.795         1.6666       11.719       4.795         1.7500       11.725       4.795         1.8333       11.706       4.795         1.9166       11.712       4.801         2.0000       11.725       4.788         2.5000       11.719       4.795         3.0000       11.725       4.801         3.5000       11.725       4.795         4.0000       11.731       4.795         4.5000       11.744       4.807         5.0000       11.833       4.807         5.5000       11.896       4.807         6.5000       12.048       4.814         7.5000       12.295       4.814         7.5000       12.295       4.814         7.5000       12.295       4.826         9.0000       13.061       4.826         9.0000       13.061       4.826         9.5000       13.130       4.826         12.0000       13.333       4.836         14.0000       13.820       4.852         16.0000       14.218       4.858	(MIN)		SWL (FEET)
1.5000       11.706       4.795         1.5833       11.719       4.795         1.6666       11.719       4.795         1.7500       11.725       4.795         1.8333       11.706       4.795         1.9166       11.712       4.801         2.0000       11.725       4.788         2.5000       11.719       4.795         3.0000       11.725       4.801         3.5000       11.725       4.795         4.0000       11.731       4.795         4.5000       11.744       4.807         5.0000       11.833       4.807         5.5000       11.896       4.807         6.5000       12.048       4.814         7.5000       12.295       4.814         7.5000       12.295       4.814         7.5000       12.295       4.826         9.0000       13.061       4.826         9.0000       13.061       4.826         9.5000       13.130       4.826         12.0000       13.333       4.836         14.0000       13.820       4.852         16.0000       14.218       4.858			XX EXP
1.5833         11.719         4.795           1.6666         11.719         4.795           1.7500         11.725         4.795           1.8333         11.706         4.795           1.9166         11.712         4.801           2.5000         11.719         4.795           3.0000         11.725         4.801           3.5000         11.725         4.795           4.0000         11.731         4.795           4.5000         11.744         4.801           5.0000         11.833         4.807           5.5000         11.896         4.807           6.5000         12.048         4.814           7.5000         12.181         4.814           7.5000         12.295         4.814           7.5000         12.295         4.814           7.5000         12.618         4.820           8.5000         12.966         4.820           9.5000         13.130         4.826           9.5000         13.130         4.826           12.0000         13.333         4.836           16.0000         14.218         4.858           18.0000         14.554			AN ARTHUR STATE OF THE PARTY OF
1.6666       11.719       4.795         1.7500       11.725       4.795         1.8333       11.706       4.795         1.9166       11.712       4.801         2.0000       11.725       4.788         2.5000       11.719       4.795         3.0000       11.725       4.801         3.5000       11.725       4.795         4.0000       11.731       4.795         4.5000       11.744       4.801         5.0000       11.833       4.807         6.0000       11.959       4.814         7.0000       12.048       4.814         7.5000       12.048       4.814         7.5000       12.295       4.814         8.5000       12.618       4.820         9.5000       13.061       4.826         9.5000       13.130       4.826         9.5000       13.130       4.826         12.0000       13.333       4.836         14.0000       13.820       4.852         16.0000       14.218       4.853         18.0000       14.554       4.870         24.0000       15.047       4.896		CARLO DE MERCO ANTONIO	
1.7500       11.725       4.795         1.8333       11.706       4.795         1.9166       11.712       4.801         2.0000       11.725       4.788         2.5000       11.719       4.795         3.0000       11.725       4.801         3.5000       11.725       4.795         4.0000       11.731       4.795         4.5000       11.744       4.801         5.0000       11.896       4.807         6.5000       12.048       4.814         7.0000       12.181       4.814         7.5000       12.295       4.814         7.5000       12.295       4.814         8.5000       12.966       4.820         9.5000       13.130       4.826         9.5000       13.130       4.826         9.5000       13.333       4.836         16.0000       14.218       4.853         18.0000       14.554       4.871         20.0000       15.047       4.896         24.0000       15.433       4.921         26.0000       15.433       4.921         32.0000       15.914       4.952		provide the same of the state of the	The second second second second second
1.8333       11.706       4.795         1.9166       11.712       4.801         2.0000       11.725       4.788         2.5000       11.719       4.795         3.0000       11.725       4.801         3.5000       11.725       4.795         4.0000       11.731       4.795         4.5000       11.744       4.801         5.0000       11.833       4.807         6.0000       11.959       4.814         7.0000       12.048       4.814         7.5000       12.295       4.814         7.5000       12.295       4.814         7.5000       12.966       4.820         9.0000       13.061       4.826         9.0000       13.130       4.826         9.5000       13.130       4.826         12.0000       13.250       4.826         12.0000       13.333       4.836         18.0000       14.218       4.858         18.0000       14.554       4.871         22.0000       15.047       4.896         24.0000       15.262       4.905         26.0000       15.433       4.921			
1.9166       11.712       4.801         2.0000       11.725       4.788         2.5000       11.719       4.795         3.0000       11.725       4.801         3.5000       11.725       4.795         4.0000       11.731       4.795         4.5000       11.744       4.807         5.0000       11.833       4.807         5.5000       11.896       4.807         6.5000       12.048       4.814         7.5000       12.295       4.814         8.0000       12.618       4.820         8.5000       12.966       4.820         9.0000       13.061       4.826         9.5000       13.130       4.826         12.0000       13.250       4.826         12.0000       13.333       4.836         16.0000       14.218       4.858         18.0000       14.554       4.871         20.0000       15.047       4.896         24.0000       15.262       4.905         26.0000       15.433       4.921         26.0000       15.762       4.940         32.0000       15.914       4.953			
2.0000         11.725         4.788           2.5000         11.719         4.795           3.0000         11.725         4.801           3.5000         11.725         4.795           4.0000         11.731         4.795           4.5000         11.744         4.807           5.0000         11.833         4.807           5.5000         11.896         4.807           6.5000         12.048         4.814           7.0000         12.181         4.814           7.5000         12.295         4.814           7.5000         12.295         4.814           7.5000         12.295         4.814           7.5000         12.618         4.820           8.5000         12.966         4.820           9.5000         13.130         4.826           9.5000         13.130         4.826           12.0000         13.333         4.836           14.0000         13.820         4.852           16.0000         14.218         4.858           18.0000         14.554         4.871           20.0000         15.047         4.896           24.0000         15.433			
2.5000 11.719 4.795 3.0000 11.725 4.801 3.5000 11.725 4.795 4.0000 11.731 4.795 4.5000 11.744 4.801 5.0000 11.833 4.807 5.5000 11.896 4.807 6.0000 11.959 4.814 7.0000 12.048 4.814 7.5000 12.048 4.814 7.5000 12.295 4.814 8.0000 12.618 4.820 8.5000 12.966 4.820 9.0000 13.061 4.826 9.0000 13.061 4.826 9.5000 13.130 4.826 12.0000 13.333 4.835 14.0000 13.820 4.852 16.0000 14.218 4.858 18.0000 14.554 4.871 22.0000 15.047 4.896 24.0000 15.262 4.905 24.0000 15.433 4.922 24.0000 15.762 4.940 32.0000 15.762 4.940 32.0000 15.914 4.953 34.0000 16.046 4.977 38.0000 16.179 4.983 38.0000 16.306 4.997		Programme and the second secon	
3.0000 11.725 4.801 3.5000 11.725 4.795 4.0000 11.731 4.795 4.5000 11.744 4.801 5.0000 11.833 4.807 5.5000 11.896 4.807 6.0000 11.959 4.814 7.0000 12.048 4.814 7.5000 12.048 4.814 7.5000 12.048 4.814 7.5000 12.618 4.820 8.5000 12.618 4.820 9.0000 13.061 4.826 9.0000 13.061 4.826 9.5000 13.130 4.826 12.0000 13.333 4.839 14.0000 13.820 4.852 12.0000 14.218 4.858 18.0000 14.554 4.871 22.0000 15.047 4.896 24.0000 15.433 4.922 24.0000 15.604 4.934 30.0000 15.762 4.940 32.0000 15.914 4.953 38.0000 16.046 4.977 38.0000 16.046 4.977 38.0000 16.179 4.983			
3.5000 11.725 4.795 4.0000 11.731 4.795 4.5000 11.744 4.801 5.0000 11.833 4.807 5.5000 11.896 4.807 6.0000 11.959 4.814 7.0000 12.048 4.814 7.5000 12.048 4.814 7.5000 12.295 4.814 8.5000 12.618 4.820 8.5000 12.966 4.820 9.0000 13.061 4.826 9.0000 13.130 4.826 10.0000 13.250 4.826 12.0000 13.333 4.839 14.0000 13.820 4.852 16.0000 14.218 4.858 18.0000 14.554 4.871 22.0000 15.047 4.896 24.0000 15.433 4.925 26.0000 15.762 4.906 32.0000 15.762 4.940 32.0000 15.914 4.955 34.0000 16.046 4.977 38.0000 16.046 4.977 38.0000 16.179 4.985			
4.0000       11.731       4.795         4.5000       11.744       4.807         5.0000       11.833       4.807         5.5000       11.896       4.807         6.0000       11.959       4.814         6.5000       12.048       4.814         7.5000       12.295       4.814         7.5000       12.295       4.814         8.0000       12.618       4.820         9.0000       13.061       4.820         9.5000       13.130       4.826         9.5000       13.130       4.826         12.0000       13.333       4.832         16.0000       14.218       4.852         18.0000       14.554       4.871         22.0000       15.047       4.896         24.0000       15.262       4.905         26.0000       15.433       4.921         28.0000       15.604       4.934         30.0000       15.914       4.953         34.0000       16.046       4.977         38.0000       16.306       4.997			
4.5000       11.744       4.801         5.0000       11.833       4.807         5.5000       11.896       4.807         6.0000       11.959       4.814         6.5000       12.048       4.814         7.0000       12.181       4.814         7.5000       12.295       4.814         8.0000       12.618       4.820         8.5000       12.966       4.820         9.0000       13.061       4.826         9.5000       13.130       4.826         12.0000       13.333       4.839         14.0000       13.820       4.852         16.0000       14.218       4.858         18.0000       14.554       4.871         22.0000       15.047       4.896         24.0000       15.262       4.905         26.0000       15.433       4.921         28.0000       15.604       4.934         30.0000       15.914       4.953         34.0000       16.046       4.977         38.0000       16.306       4.997		CONTROL DESIGNATION OF THE	
5.0000         11.833         4.807           5.5000         11.896         4.807           6.0000         11.959         4.814           6.5000         12.048         4.814           7.0000         12.181         4.814           7.5000         12.295         4.814           8.0000         12.618         4.820           8.5000         12.966         4.820           9.0000         13.061         4.826           9.5000         13.130         4.826           10.0000         13.250         4.826           12.0000         13.333         4.839           14.0000         13.820         4.852           16.0000         14.218         4.858           18.0000         14.554         4.871           20.0000         15.047         4.896           24.0000         15.262         4.905           26.0000         15.433         4.921           28.0000         15.604         4.934           30.0000         15.914         4.953           34.0000         16.046         4.976           38.0000         16.306         4.996			
5.5000         11.896         4.807           6.0000         11.959         4.814           6.5000         12.048         4.814           7.0000         12.181         4.814           7.5000         12.295         4.814           8.0000         12.618         4.820           8.5000         12.966         4.820           9.0000         13.061         4.826           9.5000         13.130         4.826           12.0000         13.250         4.826           12.0000         13.333         4.832           14.0000         13.820         4.852           16.0000         14.218         4.853           18.0000         14.554         4.871           22.0000         15.047         4.896           24.0000         15.262         4.905           26.0000         15.433         4.922           26.0000         15.762         4.940           32.0000         15.914         4.952           34.0000         16.046         4.976           38.0000         16.306         4.997			
6.0000 11.959 4.814 7.0000 12.048 4.814 7.5000 12.181 4.814 7.5000 12.295 4.814 8.0000 12.618 4.820 8.5000 12.966 4.820 9.0000 13.061 4.826 9.5000 13.130 4.826 10.0000 13.250 4.826 12.0000 13.333 4.839 14.0000 13.820 4.852 16.0000 14.218 4.858 18.0000 14.554 4.879 22.0000 15.047 4.896 24.0000 15.262 4.909 24.0000 15.433 4.922 26.0000 15.604 4.934 30.0000 15.762 4.940 32.0000 15.914 4.953 34.0000 16.046 4.977 38.0000 16.306 4.999			Section will be the second
6.5000 12.048 4.814 7.0000 12.181 4.814 7.5000 12.295 4.814 8.0000 12.618 4.820 8.5000 12.966 4.820 9.0000 13.061 4.826 9.5000 13.130 4.826 10.0000 13.250 4.826 12.0000 13.333 4.833 14.0000 13.820 4.852 16.0000 14.218 4.858 18.0000 14.554 4.873 22.0000 15.047 4.896 24.0000 15.262 4.909 24.0000 15.433 4.923 28.0000 15.604 4.934 30.0000 15.762 4.940 32.0000 15.914 4.953 34.0000 16.046 4.973 38.0000 16.306 4.993			
7.0000 12.181 4.814 7.5000 12.295 4.814 8.0000 12.618 4.820 8.5000 12.966 4.820 9.0000 13.061 4.826 9.5000 13.130 4.826 10.0000 13.250 4.826 12.0000 13.333 4.833 14.0000 13.820 4.852 16.0000 14.218 4.858 18.0000 14.554 4.871 20.0000 15.047 4.896 22.0000 15.047 4.896 24.0000 15.262 4.905 26.0000 15.433 4.921 28.0000 15.604 4.934 30.0000 15.762 4.940 32.0000 15.914 4.953 34.0000 16.046 4.977 38.0000 16.179 4.983 38.0000 16.306 4.997			
7.5000 12.295 4.814 8.0000 12.618 4.820 8.5000 12.966 4.820 9.0000 13.061 4.826 9.5000 13.130 4.826 10.0000 13.250 4.826 12.0000 13.333 4.839 14.0000 13.820 4.852 16.0000 14.218 4.858 18.0000 14.554 4.871 22.0000 15.047 4.896 24.0000 15.262 4.909 24.0000 15.433 4.922 26.0000 15.433 4.922 26.0000 15.762 4.940 32.0000 15.914 4.953 34.0000 16.046 4.977 38.0000 16.306 4.999			
8.0000		A CONTRACTOR OF THE PROPERTY O	1 1 2 2 2 3 3 3
8.5000 12.966 4.826 9.0000 13.061 4.826 9.5000 13.130 4.826 10.0000 13.250 4.826 12.0000 13.333 4.839 14.0000 13.820 4.852 16.0000 14.218 4.858 18.0000 14.554 4.879 22.0000 15.047 4.896 24.0000 15.262 4.909 24.0000 15.433 4.929 26.0000 15.762 4.946 32.0000 15.914 4.953 34.0000 16.046 4.976 36.0000 16.179 4.983 38.0000 16.306 4.999		The Carlotte State of	
9.0000 13.061 4.826 9.5000 13.130 4.826 10.0000 13.250 4.826 12.0000 13.333 4.833 14.0000 13.820 4.852 16.0000 14.218 4.858 18.0000 14.554 4.877 22.0000 15.047 4.896 24.0000 15.262 4.909 26.0000 15.433 4.923 28.0000 15.604 4.934 30.0000 15.762 4.946 32.0000 15.914 4.953 34.0000 16.046 4.977 38.0000 16.306 4.997		The second second second second second	
9.5000 13.130 4.826 10.0000 13.250 4.826 12.0000 13.333 4.833 14.0000 13.820 4.852 16.0000 14.218 4.858 18.0000 14.554 4.877 20.0000 14.807 4.876 22.0000 15.047 4.896 24.0000 15.262 4.905 26.0000 15.433 4.923 28.0000 15.604 4.934 30.0000 15.762 4.946 32.0000 15.914 4.953 34.0000 16.046 4.977 38.0000 16.179 4.983 38.0000 16.306 4.997		Control of the Contro	
10.0000     13.250     4.826       12.0000     13.333     4.839       14.0000     13.820     4.852       16.0000     14.218     4.858       18.0000     14.554     4.871       20.0000     14.807     4.876       22.0000     15.047     4.896       24.0000     15.262     4.909       26.0000     15.433     4.921       28.0000     15.604     4.934       30.0000     15.762     4.940       32.0000     15.914     4.952       34.0000     16.046     4.977       38.0000     16.306     4.997			
12.0000 13.333 4.833 14.0000 13.820 4.852 16.0000 14.218 4.858 18.0000 14.554 4.871 20.0000 14.807 4.877 22.0000 15.047 4.896 24.0000 15.262 4.905 26.0000 15.433 4.922 26.0000 15.604 4.934 30.0000 15.762 4.940 32.0000 15.914 4.952 34.0000 16.046 4.977 38.0000 16.306 4.997			
14,0000     13,820     4,852       16,0000     14,218     4,858       18,0000     14,554     4,871       20,0000     14,807     4,877       22,0000     15,047     4,896       24,0000     15,262     4,905       26,0000     15,433     4,927       30,0000     15,762     4,940       32,0000     15,914     4,957       34,0000     16,046     4,977       36,0000     16,179     4,985       38,0000     16,306     4,997			
16.0000 14.218 4.858 18.0000 14.554 4.871 20.0000 14.807 4.877 22.0000 15.047 4.896 24.0000 15.262 4.909 26.0000 15.433 4.921 28.0000 15.604 4.934 30.0000 15.762 4.940 32.0000 15.914 4.952 34.0000 16.046 4.977 36.0000 16.179 4.983 38.0000 16.306 4.997			
18.0000 14.554 4.877 20.0000 14.807 4.877 22.0000 15.047 4.896 24.0000 15.262 4.909 26.0000 15.433 4.923 28.0000 15.604 4.934 30.0000 15.762 4.946 32.0000 15.914 4.953 34.0000 16.046 4.977 36.0000 16.179 4.983 38.0000 16.306 4.997			
20.0000 14.807 4.877 22.0000 15.047 4.896 24.0000 15.262 4.909 26.0000 15.433 4.921 28.0000 15.604 4.934 30.0000 15.762 4.946 32.0000 15.914 4.952 34.0000 16.046 4.977 36.0000 16.179 4.985 38.0000 16.306 4.997			
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24.0000 15.262 4.909 26.0000 15.433 4.923 28.0000 15.604 4.934 30.0000 15.762 4.940 32.0000 15.914 4.953 34.0000 16.046 4.977 36.0000 16.179 4.983 38.0000 16.306 4.997			
26.0000 15.433 4.923 28.0000 15.604 4.934 30.0000 15.762 4.940 32.0000 15.914 4.953 34.0000 16.046 4.973 36.0000 16.179 4.983 38.0000 16.306 4.993			
28.0000 15.604 4.934 30.0000 15.762 4.944 32.0000 15.914 4.953 34.0000 16.046 4.973 36.0000 16.179 4.983 38.0000 16.306 4.993			
30.0000 15.762 4.940 32.0000 15.914 4.953 34.0000 16.046 4.977 36.0000 16.179 4.983 38.0000 16.306 4.997			
32.0000 15.914 4.952 34.0000 16.046 4.972 36.0000 16.179 4.983 38.0000 16.306 4.992			
34.0000 16.046 4.97% 36.0000 16.179 4.98% 38.0000 16.306 4.99%	Control of the Contro		The second secon
36.0000 16.179 4.985 38.0000 16.306 4.997			Company of the Compan
38.0000 16.306 4.99			
10,0000 1 16,412 1 500	40.0000	16.413	5.004
			5.023
			5.035

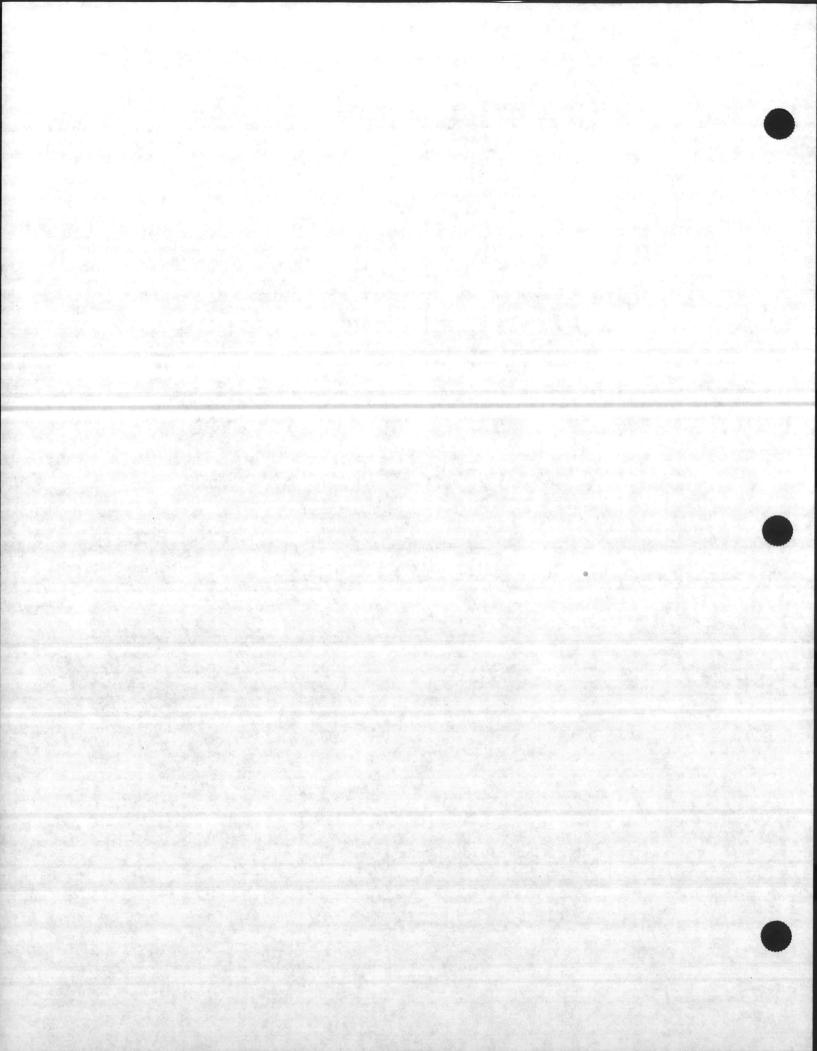


ELAPSED	WELL N	JMBER
TIME	RW-1	P-2
(MIN)	SWL (FEET)	SWL (FEET)
(2.22.)		
46.0000	17.058	5.042
48.0000	17.368	5.054
50.0000	17.703	5.067
52.0000	18.031	5.080
54.0000	18.341	5.093
56.0000	18.644	5.105
58.0000	18.979	5.124
60.0000	19.301	5.124
62.0000	19.668	5.131
64.0000	19.996	5.150
66.0000	20.249	5.162
68.0000	20.211	5.169
70.0000	20.205	5.181
72.0000	20.179	5.194
74.0000	20.293	5.200
76.0000	20.811	5.213
78.0000	21.253	5.226
80.0000	21.234	5.238
82.0000	21.234	5.245
84.0000	21.253	5.257
86.0000	21.234	5.264
88.0000	21.234	5.270
90.0000	21.228	5.283
92.0000	21.253	5.289
94.0000	21.259	5.302
95.0000	21.234	5.308
96.0000	21.234	5.308
97.0000	21.234	5.321
98.0000	21.240	5.321
99.0000	21.234	5.321
100.0000	21.234	5.327
101.0000	21.234	5.333
102.0000	21.234	5.333
103.0000	21.234	5.346
104.0000	21.240	5.346
106.0000	21.253	5.352
108.0000	21.234	5.365
110.0000	21.259	5.371
112.0000	21.234	5.378
114.0000	21.259	5.384
116.0000	21.259	5.390



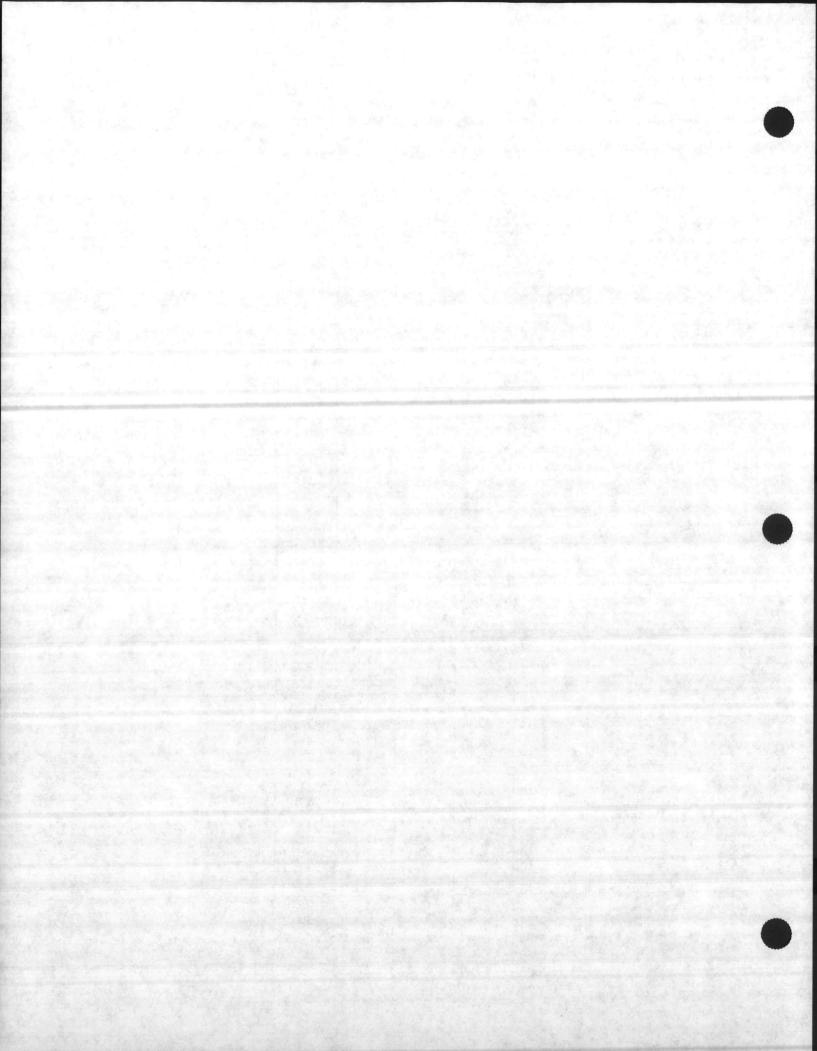
TEST: STEP 2

ELAPSED	WELL NUMBER		
TIME	RW-1	P-2	
(MIN)	SWL (FEET)	SWL (FEET)	
118.0000	21.234	5.403	
120.0000	21.253	5.409	
122.0000	21.234	5.416	
124.0000	21.259	5.422	



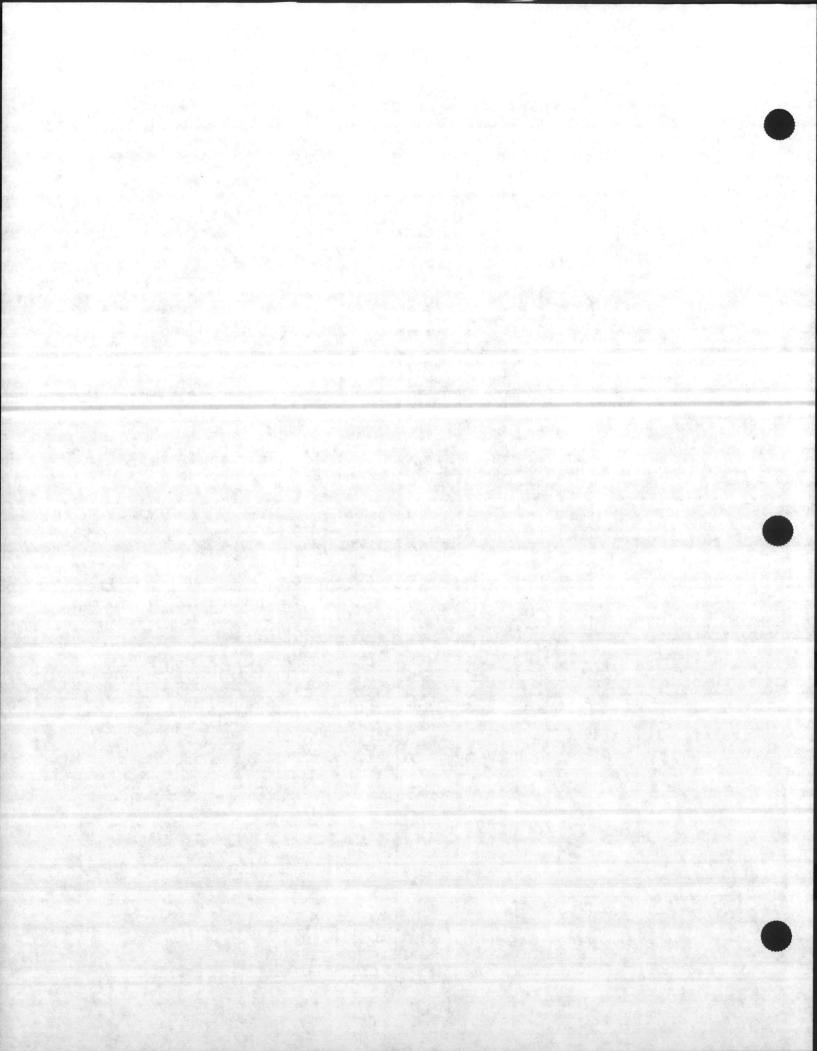
TEST: STEP 2

ELAPSED		WELL N	JMBER	2 4 2 2 3
TIME	P-1	24-1	24-2	24-3
	SWL	SWL	SWL	SWL
(MIN)	(FEET)	(FEET)	(FEET)	(FEET)
0.0000	6.843	6.837	12.720	11.61
0.0083	6.843	6.837	12.720	11.61
0.0166	6.849	6.837	12.720	11.61
0.0250	6.849	6.837	12.720	11.61
0.0333	6.843	6.837	12.720	11.61
0.0416	6.849	6.837	12.720	11.61
0.0500	6.843	6.837	12.720	11.61
0.0583	6.843	6.837	12.720	11.61
0.0666	6.849	6.837	12.720	11.61
0.0750	6.843	6.837	12.720	11.61
0.0833	6.843	6.837	12.720	11.61
0.0916	6.843	6.837	12.720	11.61
0.1000	6.849	6.837	12.720	11.61
0.1083	6.849	6.837	12.720	11.61
0.1166	6.849	6.837	12.720	11.61
0.1250	6.849	6.837	12.720	11.61
0.1333	6.843	6.837	12.720	11.61
0.1416	6.849	6.837	12.720	11.61
0.1500	6.849	6.844	12.720	11.61
0.1583	6.849	6.837	12.720	11.61
0.1666	6.849	6.837	12.720	11.61
0.1750	6.849	6.837	12.720	11.61
0.1833	6.849	6.837	12.720	11.61
0.1916	6.849	6.837	12.720	11.61
0.2000	6.849	6.837	12.720	11.61
0.2083	6.849	6.837	12.720	11.61
0.2166	6.849	6.837	12.720	11.61
0.2250	6.849	6.837	12.720	11.61
0.2333	6.849	6.837	12.720	11.61
0.2416	6.849	6.837	12.720	11.61
0.2500	6.849	6.837	12.720	11.61
0.2583	6.849	6.837	12.720	11.61
0.2666	6.849	6.837	12.720	11.61
0.2750	6.849	6.837	12.720	11.61
0.2833	6.849	6.837	12.720	11.61
0.2916	6.849	6.837	12.720	11.61
0.3000	6.849	6.837	12.720	11.61
0.3083	6.849	6.837	12.720	11.61
0.3166	6.849	6.844	12.720	11.6
0.3250	6.849	6.837	12.720	11.6
0.3333	6.849	6.837	12.720	11.61



TEST: STEP 2

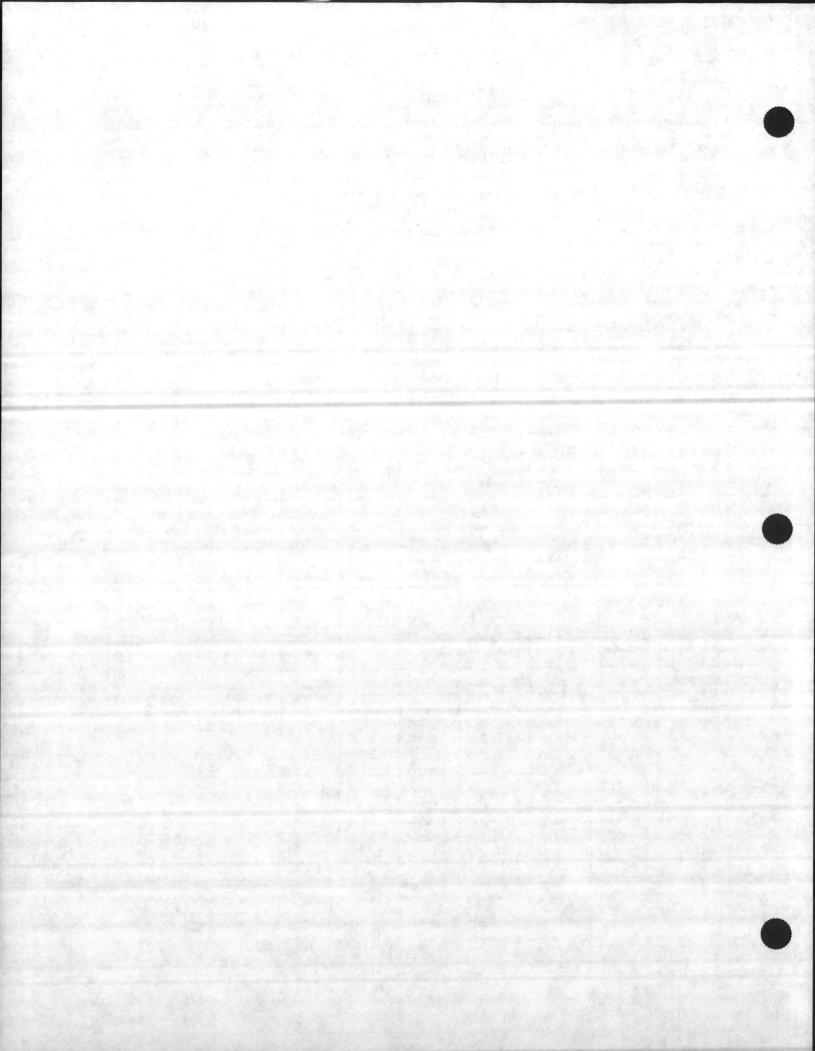
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
0.2500	6040	6044	12.720	11.61
0.3500	6.849	6.844	12.720	11.61
0.3666 0.3833	6.849 6.849	6.837	12.720	11.61
0.4000	6.849	6.837	12.720	11.61
0.4000	6.849	6.837	12.720	11.61
0.4333	6.849	6.844	12.720	11.61
0.4500	6.849	6.837	12.720	11.61
0.4666	6.849	6.837	12.720	11.61
0.4833	6.849	6.837	12.720	11.61
0.5000	6.849	6.837	12.720	11.61
0.5166	6.849	6.837	12.720	11.625
0.5333	6.849	6.837	12.720	11.61
0.5500	6.849	6.837	12.720	11.61
0.5666	6.849	6.837	12.720	11.61
0.5833	6.849	6.837	12.720	11.61
0.6000	6.849	6.837	12.720	11.61
0.6166	6.849	6.837	12.720	11.61
0.6333	6.843	6.837	12.720	11.61
0.6500	6.843	6.837	12.720	11.61
0.6666	6.849	6.837	12.720	11.6
0.6833	6.849	6.837	12.720	11.61
0.7000	6.843	6.837	12.720	11.61
0.7166	6.843	6.837	12.720	11.6
0.7333	6.843	6.844	12.720	11.6
0.7500	6.843	6.837	12.720	11.6
0.7666	6.843	6.844	12.720	11.625
0.7833	6.843	6.837	12.720	11.6
0.8000	6.843	6.837	12.720	11.625
0.8166	6.849	6.837	12.720	11.6
0.8333	6.843	6.837	12.720	11.6
0.8500	6.849	6.837	12.720	11.6
0.8666	6.849	6.837	12.720	11.6
0.8833	6.843	6.844	12.720	11.6
0.9000	6.843	6.837	12.720	11.6
0.9166	6.849	6.837	12.720	11.6
0.9333	6.849	6.837	12.720	11.62
0.9500	6.849	6.837	12.720	11.6
0.9666	6.849	6.844	12.720	11.62
0.9833	6.849	6.837	12.720	11.6
1.0000	6.849	6.844	12.720	11.6
1.2000	6.849	6.837	12.720	11.6



CONTRACT TASK ORDER: 0017 SITE I.D.: CAMP LEJEUNE, HPIA

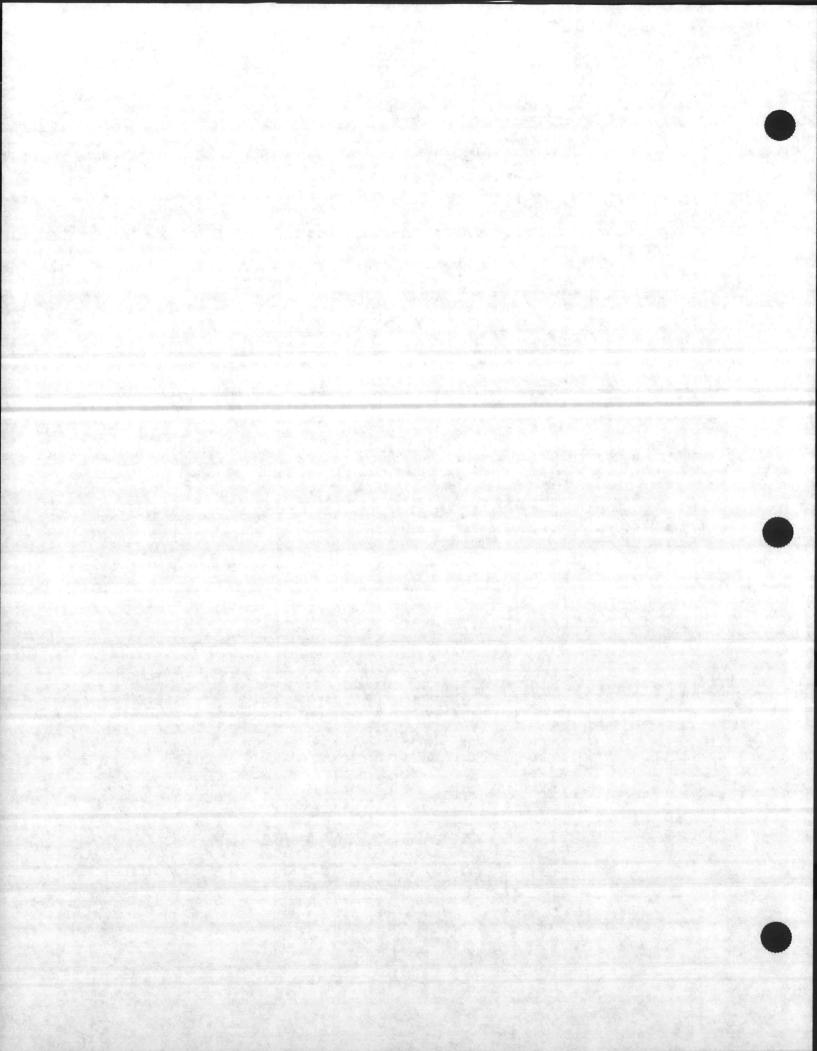
TEST: STEP 2

ELAPSED	17.0	WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
gen een	e e la lagra	te - Laur - S	10.500	44.64
1.4000	6.849	6.837	12.720	11.61
1.6000	6.849	6.837	12.720	11.61
1.8000	6.849	6.837	12.720	11.61
2.0000	6.849	6.837	12.720	11.61
2.2000	6.849	6.837	12.720	11.61
2.4000	6.849	6.837	12.720	11.61
2.6000	6.849	6.837	12.720	11.61
2.8000	6.849	6.844	12.720	11.61
3.0000	6.849	6.844	12.720	11.61
3.2000	6.849	6.837	12.720	11.61
3.4000	6.849	6.844	12.720	11.61
3.6000	6.849	6.837	12.720	11.61
3.8000	6.849	6.837	12.704	11.61
4.0000	6.849	6.844	12.720	11.61
4.2000	6.849	6.837	12.720	11.61
4.4000	6.849	6.844	12.704	11.61
4.6000	6.849	6.844	12.704	11.61
4.8000	6.849	6.837	12.720	11.61
5.0000	6.849	6.844	12.720	11.61
5.2000	6.849	6.844	12.720	11.61
5.4000	6.849	6.837	12.720	11.61
5.6000	6.849	6.844	12.720	11.61
5.8000	6.856	6.844	12.704	11.61
6.0000	6.856	6.844	12.720	11.61
6.2000	6.849	6.844	12.720	11.61
6.4000	6.849	6.844	12.720	11.61
6.6000	6.856	6.844	12.720	11.61
6.8000	6.856	6.844	12.704	11.61
7.0000	6.849	6.844	12.720	11.61
7.2000	6.849	6.844	12.704	11.61
7.4000	6.856	6.844	12.704	11.61
7.6000	6.849	6.844	12.720	11.61
7.8000	6.856	6.844	12.720	11.61
8.0000	6.856	6.844	12.704	11.61
8.2000	6.856	6.844	12.720	11.61
8.4000	6.856	6.850	12.720	11.61
8.6000	6.856	6.844	12.720	11.61
8.8000	6.856	6.850	12.720	11.61
9.0000	6.856	6.844	12.720	11.61
9.2000	6.849	6.844	12.720	11.61
9.4000	6.856	6.850	12.720	11.61



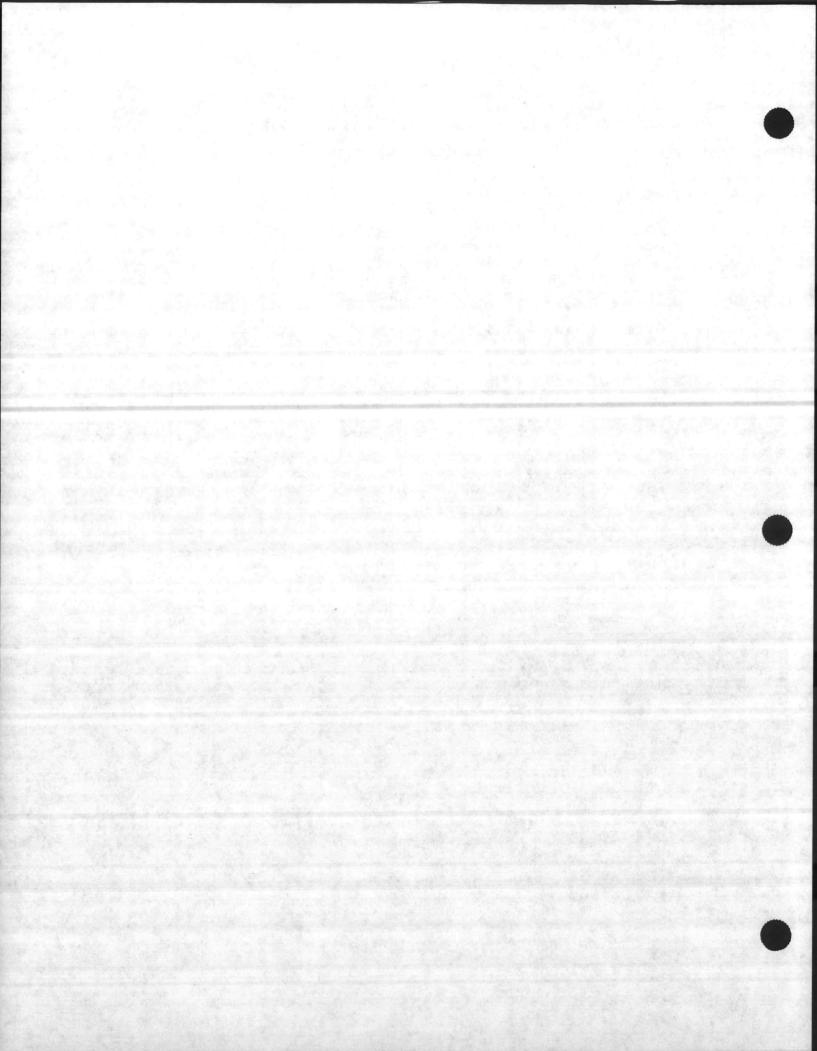
TEST: STEP 2

ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
9.6000	6.856	6.850	12.720	11.61
9.8000	6.856	6.850	12.704	11.61
10.0000	6.856	6.850	12.720	11.625
12.0000	6.856	6.856	12.735	11.625
14.0000	6.862	6.862	12.735	11.625
16.0000	6.862	6.869	12.735	11.625
18.0000	6.868	6.869	12.720	11.625
20.0000	6.868	6.875	12.735	11.625
22.0000	6.875	6.875	12.735	11.625
24.0000	6.875	6.881	12.735	11.625
26.0000	6.875	6.881	12.735	11.625
28.0000	6.875	6.881	12.735	11.625
30.0000	6.875	6.888	12.735	11.625
32.0000	6.881	6.894	12.735	11.625
34.0000	6.881	6.894	12.735	11.625
36.0000	6.888	6,900	12.751	11.64
38.0000	6.888	6.900	12.735	11.641
40.0000	6.894	6.907	12.735	11.64
42.0000	6.894	6.913	12.735	11.625
44.0000	6.900	6.913	12.751	11.64
46.0000	6.900	6.913	12.735	11.64
48.0000	6.907	6.919	12.751	11.625
50.0000	6.907	6.926	12.751	11.64
52.0000	6.907	6.932	12.735	11.64
54.0000	6.907	6.926	12.751	11.64
56.0000	6.907	6.932	12.735	11.62
58.0000	6.920	6.944	12.751	11.64
60.0000	6.920	6.944	12.735	11.64
62.0000	6.920	6.944	12.735	11.64
64.0000	6.920	6.951	12.751	11.64
66.0000	6.920	6.951	12.751	11.64
68.0000	6.926	6.957	12.735	11.64
70.0000	6.926	6.957	12.751	11.64
72.0000	6.932	6.963	12.735	11.64
74.0000	6.932	6.970	12.751	11.64
76.0000	6.939	6.970	12.751	11.64
78.0000	6.939	6.976	12.735	11.64
80.0000	6.945	6.976	12.751	11.64
82.0000	6.945	6.982	12.751	11.64
84.0000	6.952	6.989	12.751	11.65
86.0000	6.945	6.989	12.751	11.64

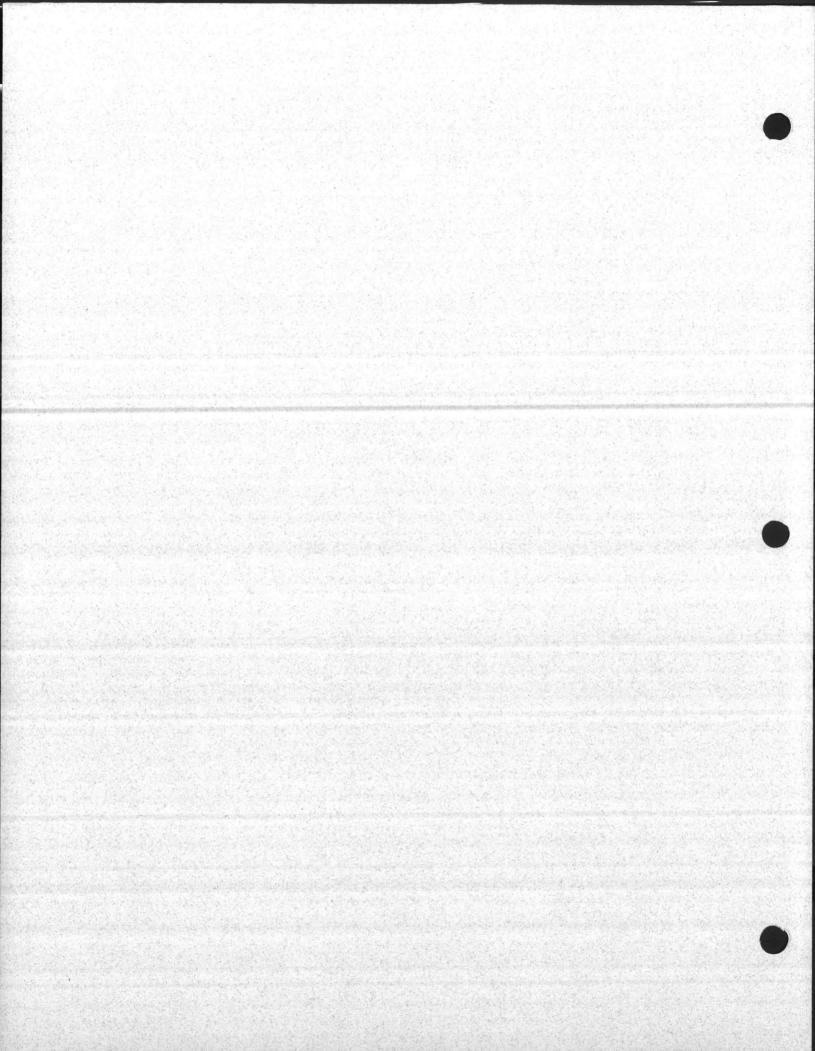


TEST: STEP 2

ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
88.0000	6.952	6.989	12.751	11.656
90.0000	6.952	6.995	12.751	11.641
92.0000	6.958	6.995	12.751	11.641
94.0000	6.958	7.008	12.751	11.641
96.0000	6.958	7.001	12.751	11.656
98.0000	6.964	7.008	12.751	11.641
100.0000	6.964	7.008	12.751	11.641
105.0000	6.971	7.020	12.751	11.656
110.0000	6.977	7.026	12.751	11.656
115.0000	6.984	7.033	12.751	11.656
120.0000	6.990	7.039	12.751	11.656
125.0000	6.996	7.052	12.766	11.656



APPENDIX B FLOW RATE MEASUREMENTS

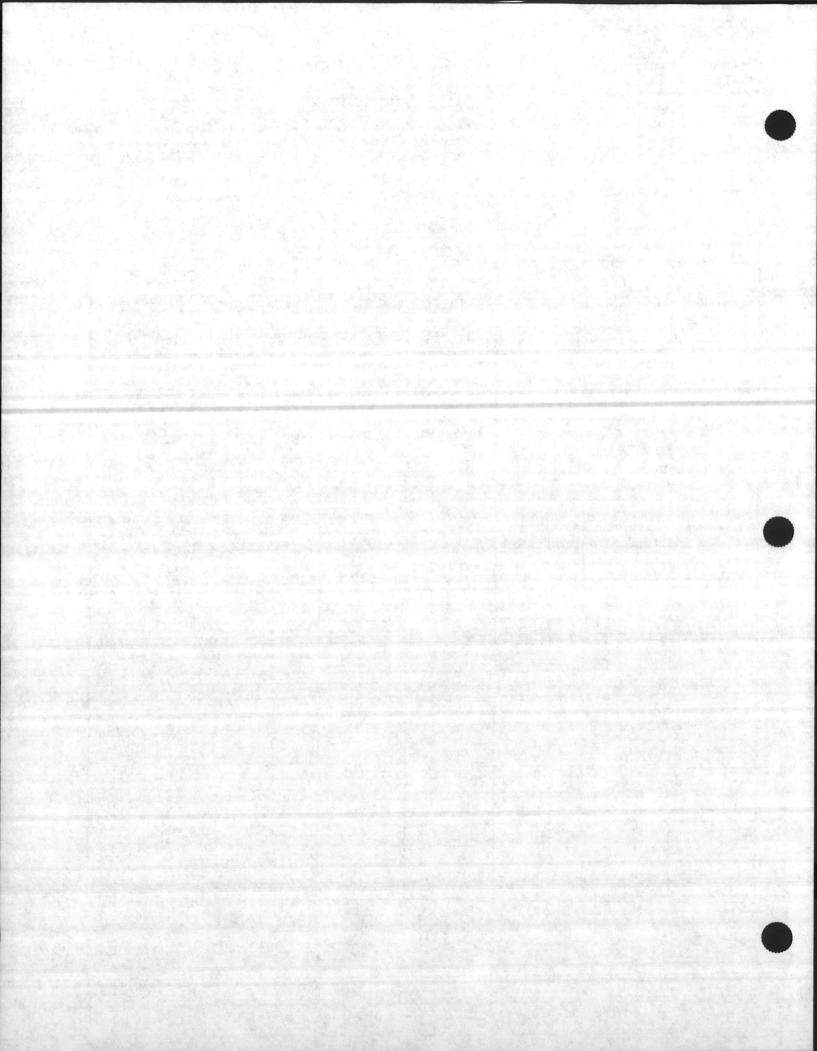




## FLOW LEVEL MEASUREMENTS

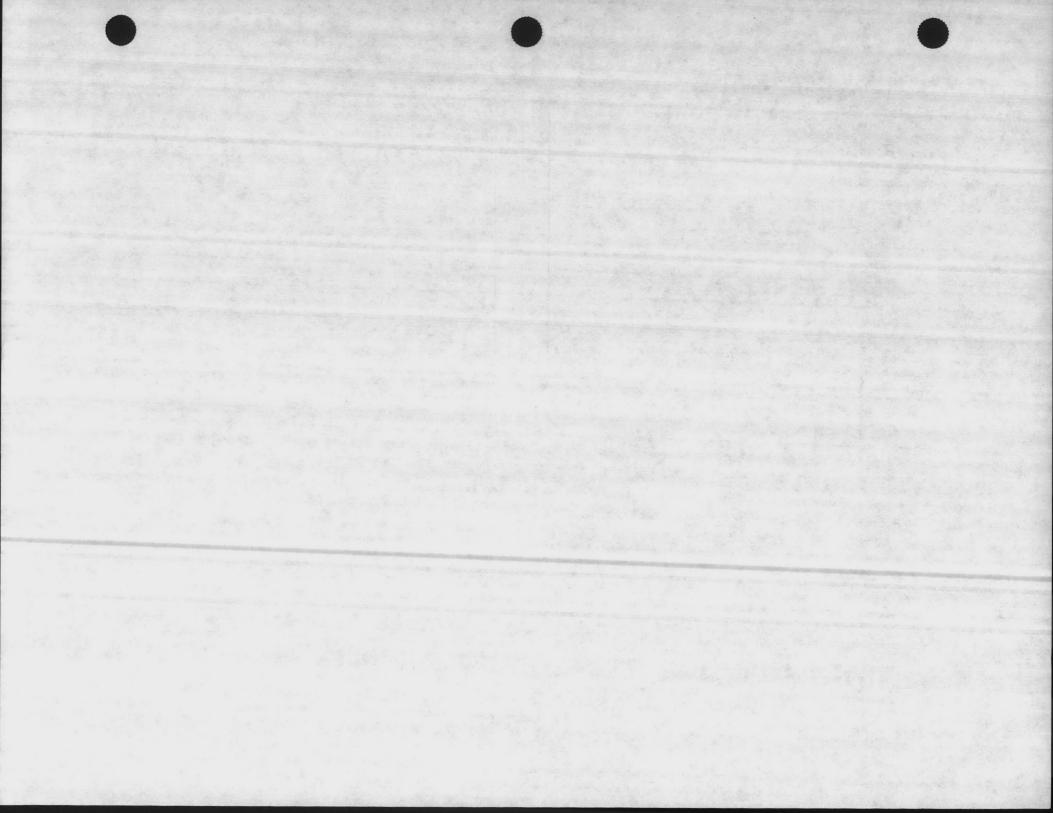
	그렇는 이렇게 지어가셨다면 하는 이 없는 어린 그는 것이 되는 어떻게 되어 있다면 그 모든데 그리지 않다면 됐다.	진 맛있다. 그 말으라면 세계성적하고 맛으셨다. 바셨다가 살았다.		
Project	HPIA	CTO Number	0011	
I lojou		[12][12] - 12] [14] [15] - 15] [16] [16] [16] [16] [16] [16] [16] [16		

Date	Time	Elapsed Time (min.)	Meter Reading (Gal.)	Average GPM	Comments
a/a/43	Instin		326.2		Pump ON At 10:05
ala193	10:09	4.0	333.6	1.85	Flow Adjusted until
1	10:12	3.0	338.1	1.5	10:09 Flowing Fast
1	10:16	4.0	343.8	1.4	
	10:26	10.0	358.3	1.45	
	10:38	12	375:1	1.4	
	10:45	7	384.8	1.39	
	11:00	15	405.6	1.39	
	11:17	17	429.1	1.38	
		13	447.1	1.38	
	11:30 11:41 H:40	11	462.3	1.38	Adjusted neter At 11:0
	12:08	27	499-7	1.38	
	13:09	61	584.7	1.39	Adoubted nater
	13:15	6	594.1	1.57	
	13:49	34	442.0	1.41	
	14:98	39	695.4	1.37	
2/2/93					14:44 - 16:06 IN DJM LOS
	16:46	•	888.2		
	161.50	4	892.0	.95	
	16:58	8	903.9	1.48	
	1617:17	19	931.1	1.43	incremental up adjustment
	17:301		948.1	1.54	
	17:52	21	974.1	1.23	Incremental up -
	18.18	34	1007.0	,97	



Flow meter master meter # 1430645 The AIR Stupper is the same a Tray system that was used at OCERUA NAS AQUIAN Test. Flow meter set UP. meter The pump test was mitualed At x 10:05 Am on 2/2/93 The flowerate ofter one in of general seems to be decreasing. it may be Necessary to adjust the flow mate

10:30	DABAL	And Bidn PASS.	17 20	
		unat be		The state of the s
meter TIME				
	TIME	Flow numb	00	Aug Q
14:44		719.8		-
nd sus bed	Flow	At 14:31	8.	
14:54	10	734.2	14.4	14.4
15:09	. 15	754.6	20.4	1.36
15.11 A	PAIN Ad:	subled Flo	u nate	
13:14	5	763.2	8.6	1.72
13:17	3	768.3	B1	
15:22	5	276.1	7.8	1.56
5133	u	>93.a	17.1	1.55
15:47	GOINS &	tost the	rottled A	ack
15:51	18	8/9.2		1.44
16:00	9	831.2	10	2.33
16:06	6	840.1	8.7	1.48
	l. i 1 i	1 - 1 - 1 - 1		LILLI

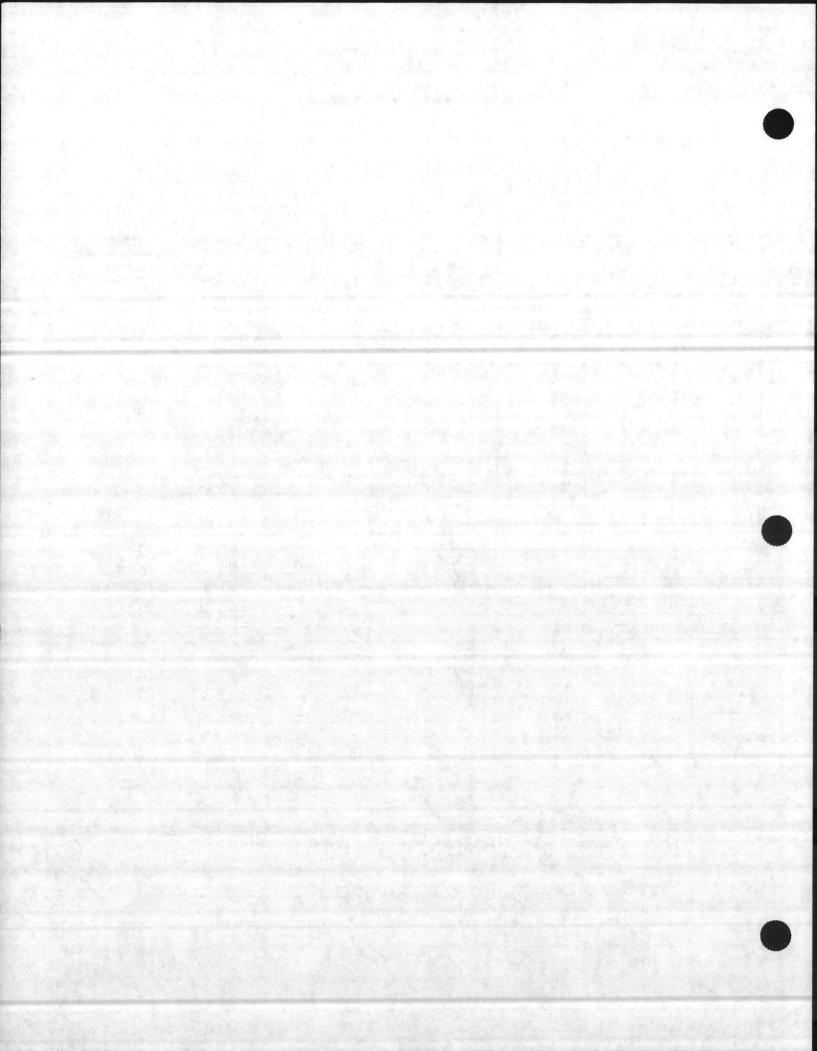




## FLOW LEVEL MEASUREMENTS

Project Hadnot Print industrial Area CTO Number 0017

Date	Time	Elapsed Time (min.)	Meter Reading (Gal.)	Average GPM	Comments
2-2-93	18:24	-	1023,3	-	Adousted Flow Rote
- 100 m	18:30	6	1031,7	1.4	
	18:36	6	1040.1	1.4	
	18:45	9	1051.8	1.3	
	18:49	4	10585		Advested
	19:04	1.5	710793	1.38	
• 1	19:17	13	1094.7	1,18	adjusted
	19:22	5	1102.2	15	
	19:36	14	1122.0	1.43	
	19:47	11	1136.5	1.3	
	19:53	6	11445	1.33	
	19:56	3	1149.1	1.53	Advasted
	20:24	39	134:0	1.57	
	20:53	29	1236,0	0.84	ADJUSTED
	20:56	3	1238.5	1.16	Adjusted
	21:04	8	1249.0	1.31	
( C. C. C. S. A.)	21:14	10	1262.5	1.35	Landon Agradus Casas
	21:24	,0	1274.0	1.15	Alusted
	21:30	Catholical Catholical	1281.0	1.17	
	21:34	6	1287.5	1,62	Adjust
	21:43	9	1300.0	1.38	
	12:00	17		123	A9100T
	2204	57	1321.0	1.08	
	22:12	5	1337.5	150	

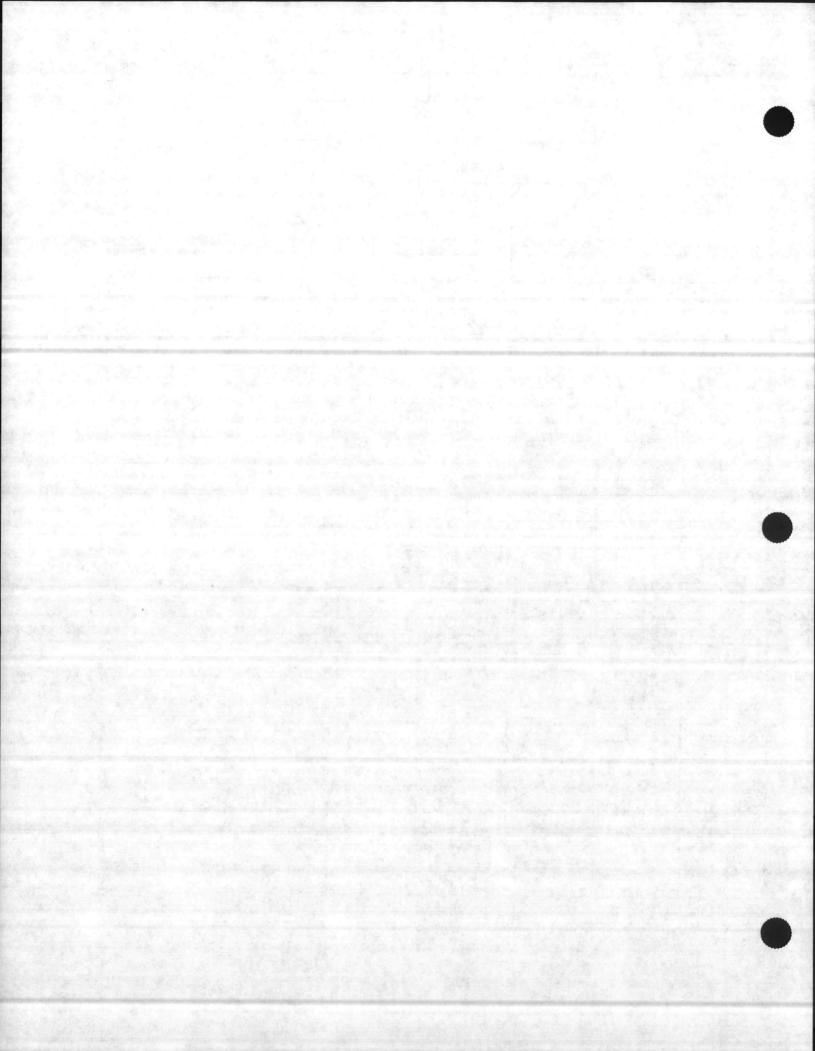




## FLOW LEVEL MEASUREMENTS

Project HADNOT POWT INDUSTRIAL SITE CTO Number 0017

Date	Time	Elapsed Time (min.)	Meter Reading (Gal.)	Average GPM	Comments
2-2-93	22:20	8	1348.0	1.31	
	22:39	19	1371.5	1.23	Advust
	22:43	4	1377.3	1.45	
	23:00	17	1485.0	1.33	
	23:09	9	1420.0	22	Afort
	23:37	20	1447.5	1.0	Afost
	23:48	И	1461.0	1.23	Alist
	23155	7	1470.0	1.28	1
2/3/93	0:05	10	1484.0	1.40	
	0.25	20	1510.0	1.3	
	0:45	20	1534.5	1.23	Adjust
	0:55	10	1547.0	1.25	Adjost
1,	1:07	12	1563.5	1.38	
V	1:42	35	1610.0	1.32	
	2:04	22	1637.0	1.22	
	2:22	18	1659.3	1-24	Adjust
	7:29	7	167.5	1.2	
	7:34	5	1674.0	1.3	
	3:00	76	17060	1.23	Adjust
	3:07	7	1711.8	0.82	Adjust
	3:15	9	1722.5	1.2	
	3:20	5	1731,5	1.0	
7 17 190	3:45	23	1731.5	1./3	Adjust
	3:46	3	1760.0	0.83	



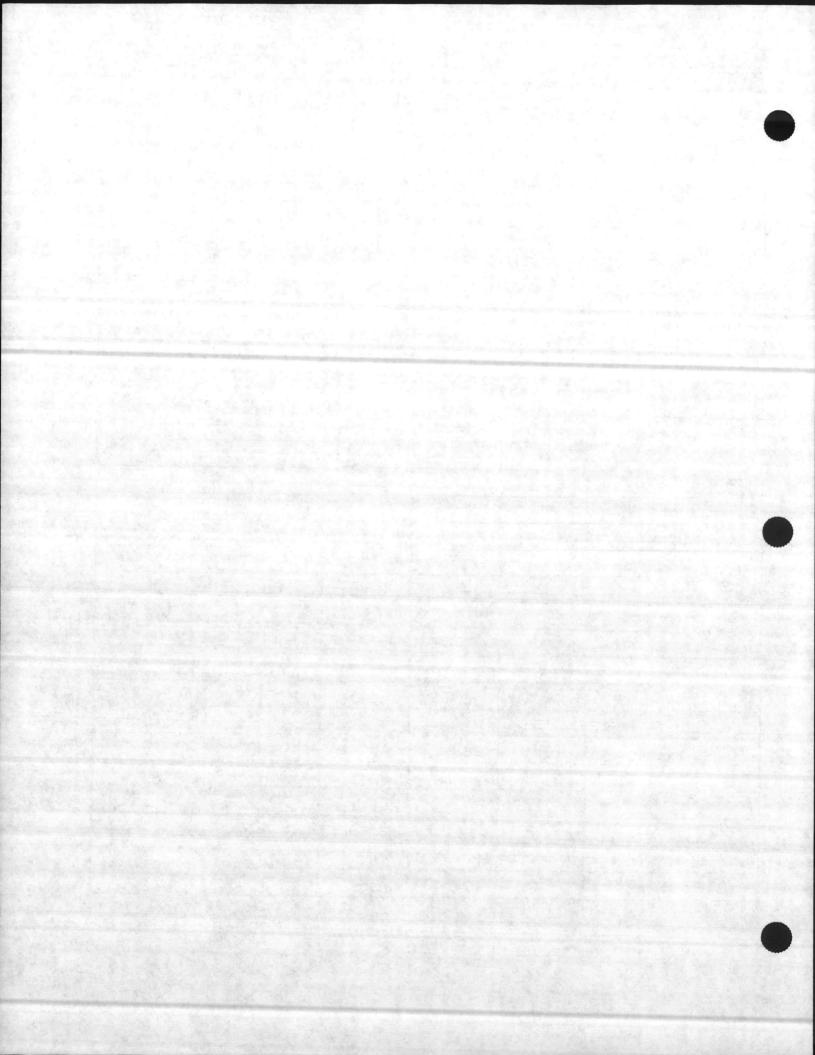


					. ~	
Project	FONDAH	POINT	I. A	CTO Number	001/	
riojeci _	THE INC.	1011	-			TANK IN I

Date	Time	Elapsed Time (min.)	Meter Reading (Gal.)	Average GPM	Comments
2-3-93	3:50	4	17650	1.25	
2-3-95	0400	10	1781.	460	at just ment top of pump
	0410	10	1794	1,30	7
2-3-93		11	1811	2.215	adjust promp
	0422				Flourstops
2-3-13	6429				Flow resumes
2-3-93	0\$34	13.	1821	1.3.7	
2-3-93	0440	6	1830	1,5	
2-3-93		15	1851	1,4	
1-3-93	640510	15	1877	4.7	(pamp) pumps howing
23-43	0536	26	1001	1.0	
2-3-93	P5 56	20	1926	1.25	pump showing
2.3-93	0615	19	1950	1.8	The state of the s
2-3-93		25	1981	1.24	pampshoring
1	0648	2	1791.5	1.31	
	0713	25	2023.0	1.26	ARIUST to summer pump
	0718	5	20290	1.20	
A STATE OF	0743	25	20600	1.24	
V	08:00	17	2078.5	0,91	
	8:15	15	2096.7	1.41	
	8:30				Flow Reduced - Redoud
	8:43		2128.7		the same of the sa
	0:46	3	2132.2	1.17	7.00
	6:53	7	2140.5	1.18	will try to increase
	8459	6	2148.8	1,38	Flow to 1.4 - 125 20M
	9:06	7	2158.8	1.42	
	4:12	6	2167.3	1.43	Pump visible manin in

2114.3 1.38 9:34 22

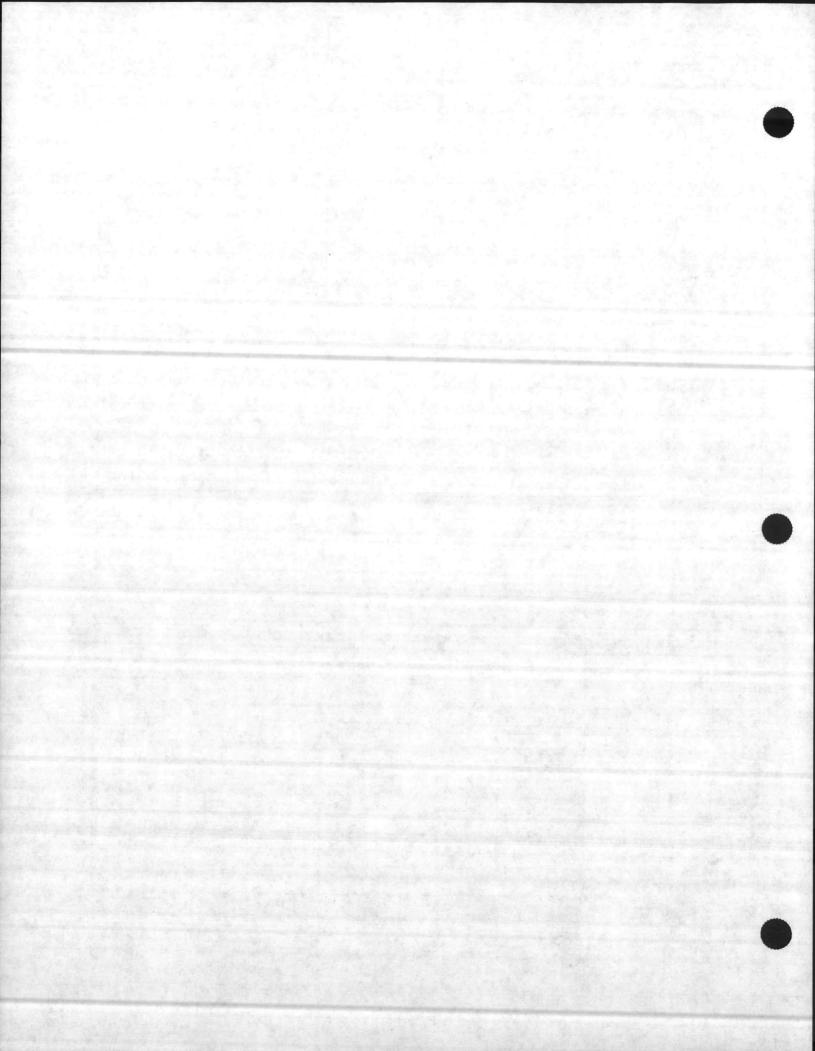
pump visible again after pumping at 1.4 gpm will try to operate at 1.2 gpm





Project HADNOT POINT IND. Area CTO Number 0017

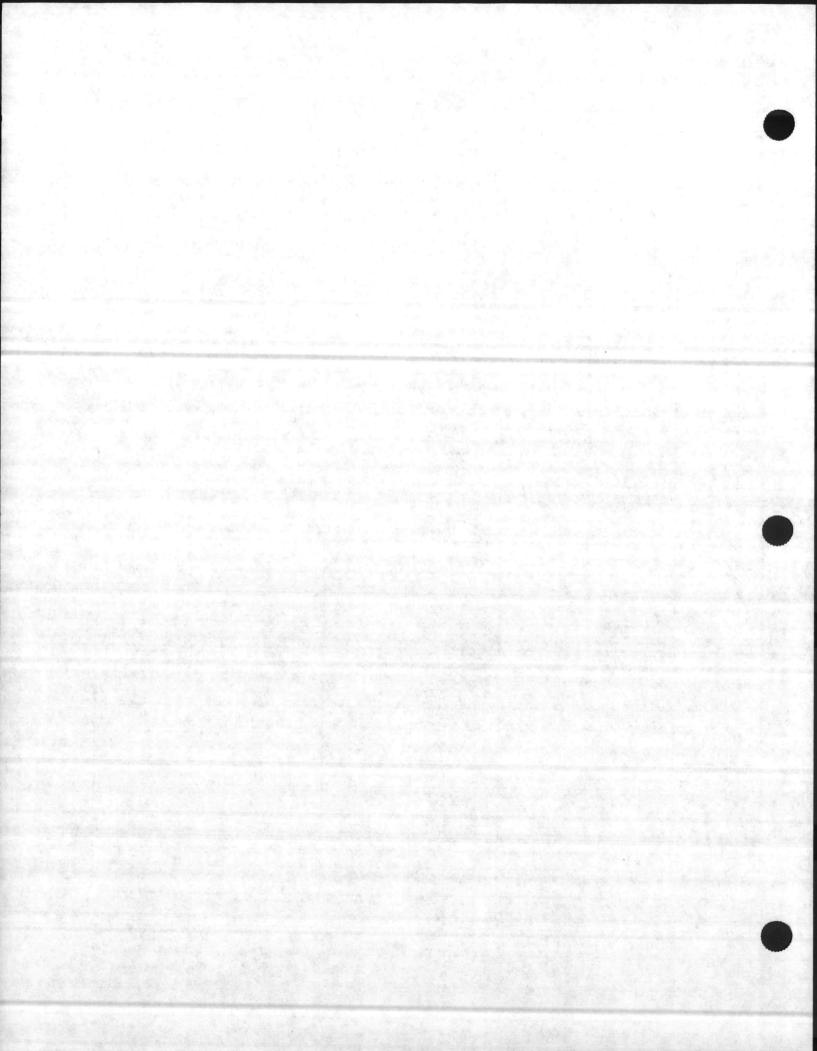
Date	Time	Elapsed Time (min.)	Meter Reading (Gal.)	Average GPM	Comments
2-3-93	9:34		2196.3		Rendsusted Pumpe 9:30
	9:40	6	2202.7	1.07	
	9,53	13	2216.7	1.08	
	10.04	11	2230.0	1.21	
	10:27	23	2256.5	1.15	
18-7	10:50	23	2290,7	1.46	
	11:08	13	2318.2	2.15	operator present
a de	11:12	INI+	2320	- 1	
A P	11:22	10	2330.7	1.07	
	11:43	aı	2351.0	0.97	
1	11:55	12	2363.9	1.08	
19 6	12:10	IS	2381.0	1.14	
	12:27	17	2400.0	1.12	
	12:37				
	17:43	le	24184	1.3	
	13:04	2	2446.4	1.08	
	13:12	8	2450.0	1.2	
W 100 min	13,57	45	2543.7	1.19	
	14:07	10	2516.2	1.25	
	14:18	11	2536.0	1.25	
	14:35	17	2551.0	1.24	
	14:47	12	2545.8	1.23	
	15:09	22	2572.8	1.23	
1	15: 28	19	3616.1	1.23	





Project Had not Point Ind. Area CTO Number 0017

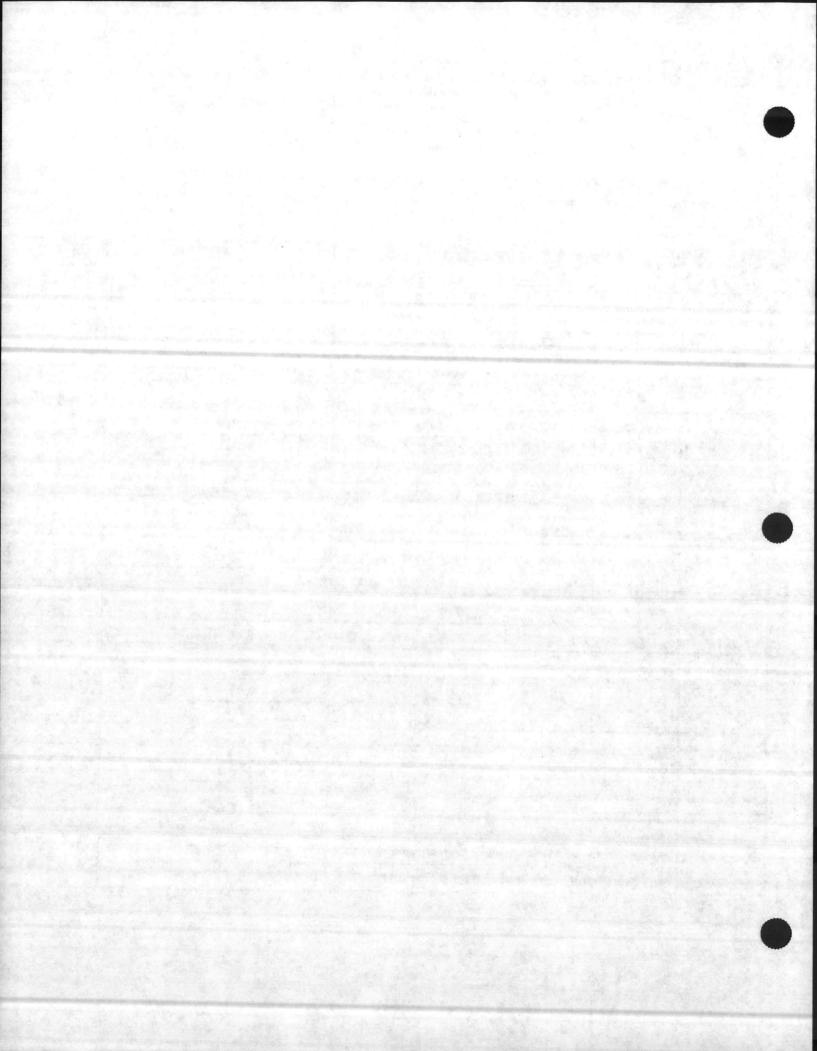
Date	Time	Elapsed Time (min.)	Meter Reading (Gal.)	Average GPM	Comments
2-3-93	15:48	10	2640.5	1.22	
0.1	16:19	31	2678.3	1.22	
	16:58	39	2726.4	1.23	
	17:25	27	2759.1	1.21	
	17:57	32	2797.1	1.18	1924 DT AVA Q= 1.292
V	18:09	12	2711.1	1.17	TOTAL Q 2484.9
	18:23	14	28275	1.17	14.17 - SWL IN RW-1
	18:34	u	2840.2	1.15	
-1 - 4 2-3	10:42	8	2851,2	1.39	
	1852	10	2864.3	1.31	
	1934	42	2917.5	1.26	
	010	36	29615	1.22	
	2043	33	3000.0	1-16	
	2111	28	3036.0	1.20	
	2137	26	30675	1.21	
	2159	22	30945	1.22	a start of the second
	2239	40	3144.0	1.23	
	2306	25	31770	1-26	
a Company (Company)	2332	26	3209.0	1.23	
	-357	-26			
2493		45	3264	1-22	
0	0042	25	32945	1.22	
	0103	21	3320	1.26	
V	0130	27	3554	1.25	



Page Zof\_

Project TADNOT POINT IND. HARA CTO Number 6017

Date	Time	Elapsed Time (min.)	Meter Reading (Gal.)	Average GPM	Comments	
2-4-93	020ව	30	3390	1-20	and the second s	11:5
	0218	18	3413	1.27		21
	0305	47	3465	1. 11		
	0413	68	3534	1.01		
	0532	79	36 0 5	1.00	3614	
	0556	24	3640	1-1		
	0631	35	3664	0.7	Adjust	
	0707	38	3899	0.9		
- X	0734	27	3726	1.0		
	0821	47	3772.1	.98	adjust to 1.2	
. ya. isa isa saka kana isa s	0910	51	3828.4	1.10		
-	0919	9	3839.1	1.18		
	0990	21	3863.9	1.18		
	10 15	35	3905.7	1.19		
	1433	258	4215.6	1.2	the large tim that elopsed was due to the official time tecting watch was momentarate	lost
	1457	24	4244.5	1.2		
	1558	6	4314.5	1.14	adjust to 1.2	
	1866	В	4323.7	1.15		
_	1626	28	4346.5	1	misread something	
Maria Maria	1628	-2	43\$8.7	1.1		
	Racio de la composición dela composición de la composición de la composición de la composición de la composición dela composición de la composición de la composición dela composición dela composición de la composición dela composición de la composición dela composición dela composi		4356.8		V	-
	1639	33	43.61.3	1.13		
	1646	7.	4369.3	1.14		
	1658	12	4386.9	1.47		

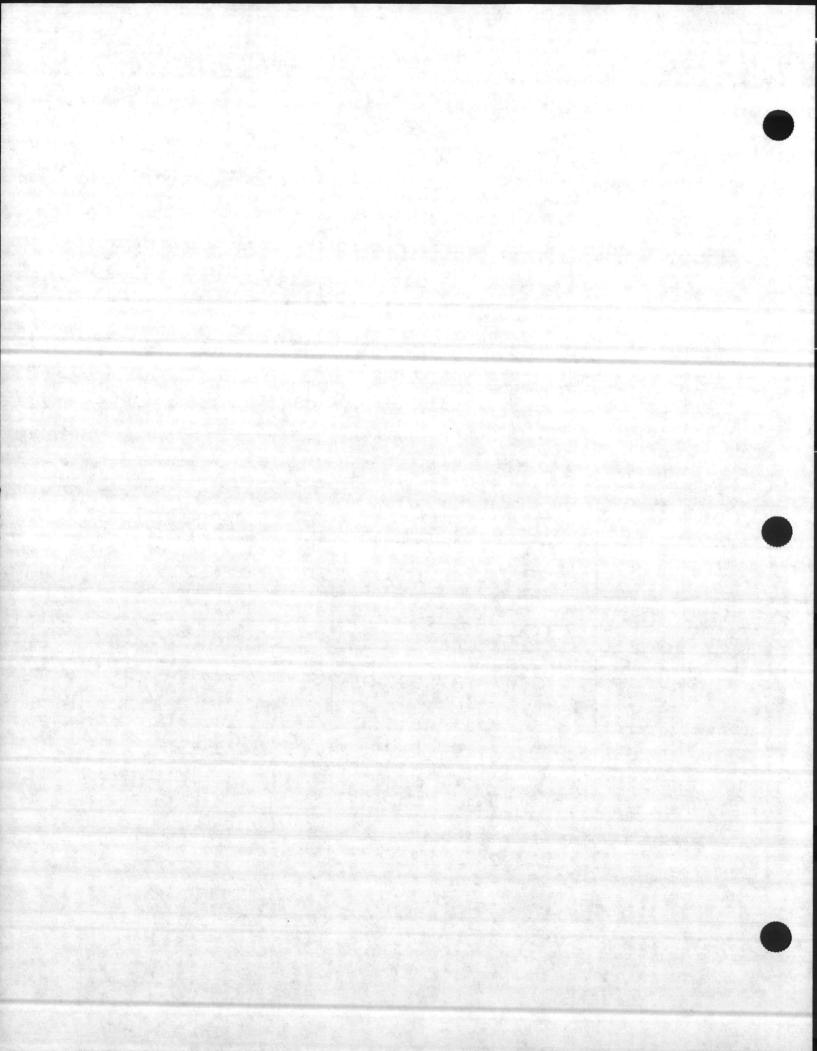




	Hadnat	2.+	Industrial	Aces
roject	Manie	Loin .	THUNDSTAGE	ATTUR

CTO Number 0017

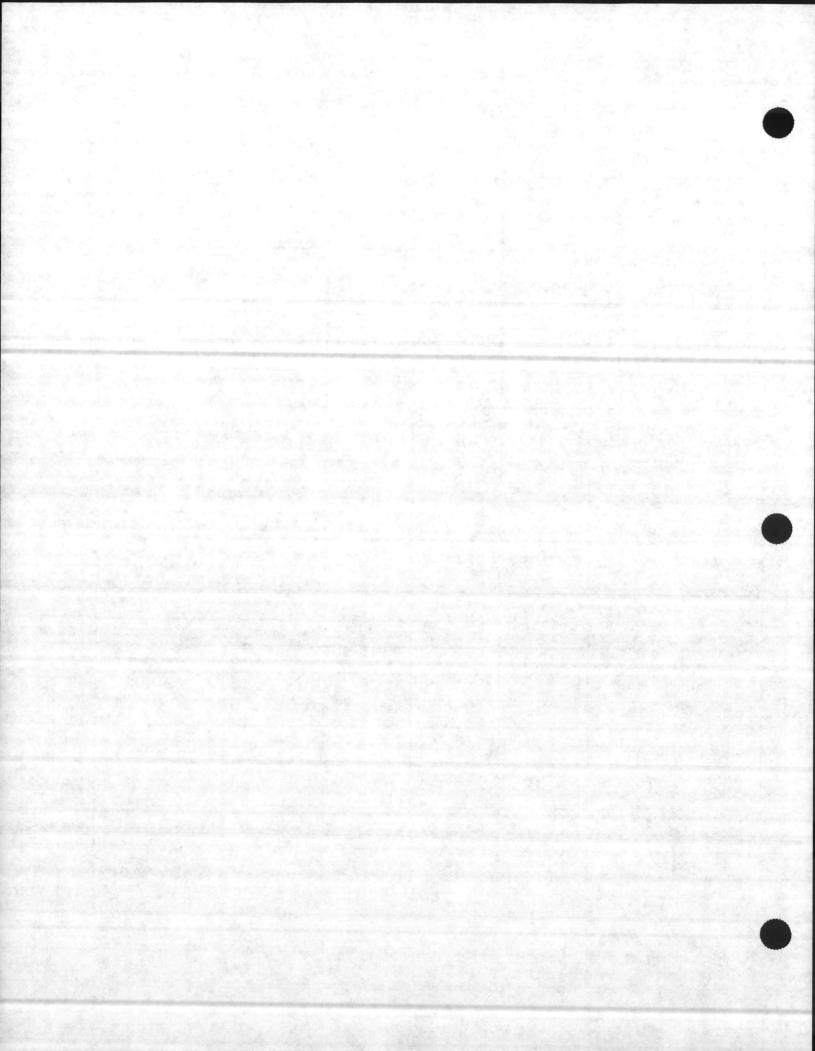
Date	Time	Elapsed Time (min.)	Meter Reading (Gal.)	Average GPM	Comments
2-4-93	1701	3	4390.1	1.07	
	1703	2	4398.0	.95	Tried adjusting flows turned value but note not responding after playing with value for 30 min
	1741	38	4437.6	1.18	able to get a proper rate - flow up to 1.25 with out adjust
	1803	22	4464.5	1.25	- flow up to 1.28 with out adjust
	1817	14	4481.9	1.24	
	1833	16	45013	1,21	X-
/	1849	16	4521.6	1.24	
	19.16	27	4554.4	1.21	
)	19.47	31	4592.9	1,24	going to try to cut rate back
/ .	20.31	44	4641.3	1.1	tried adjusting SWL rises
	20.38	8	447.9	0.825	tack to 15.8% attempt to readjust close to 1.2
1	20.50	11	A660.2	1.12	
	2122	32	4700	1.24	
5	2153	31	47365	1.20	
1	2230	37	4780	1.17	
V	2318	48	4835	1.14	
	2350	32	4870	1.1	
2-5-93	0027	37	4910	1.08	
-	0053	26	4940	1.15	
	0141	48	4999	1.22	adjustment
	0211	30	3031	1.06	Marine Committee of the
>	0242	31	5064	1.06	
5.	0333	51	3117	1.04	
4	0433	60	5200	1,38	Adjustment
71 10	0449	16	5228.5	1-78	Adjustment Adjustment
	0603	74	5310	1.1	
	635	32	5330	06	



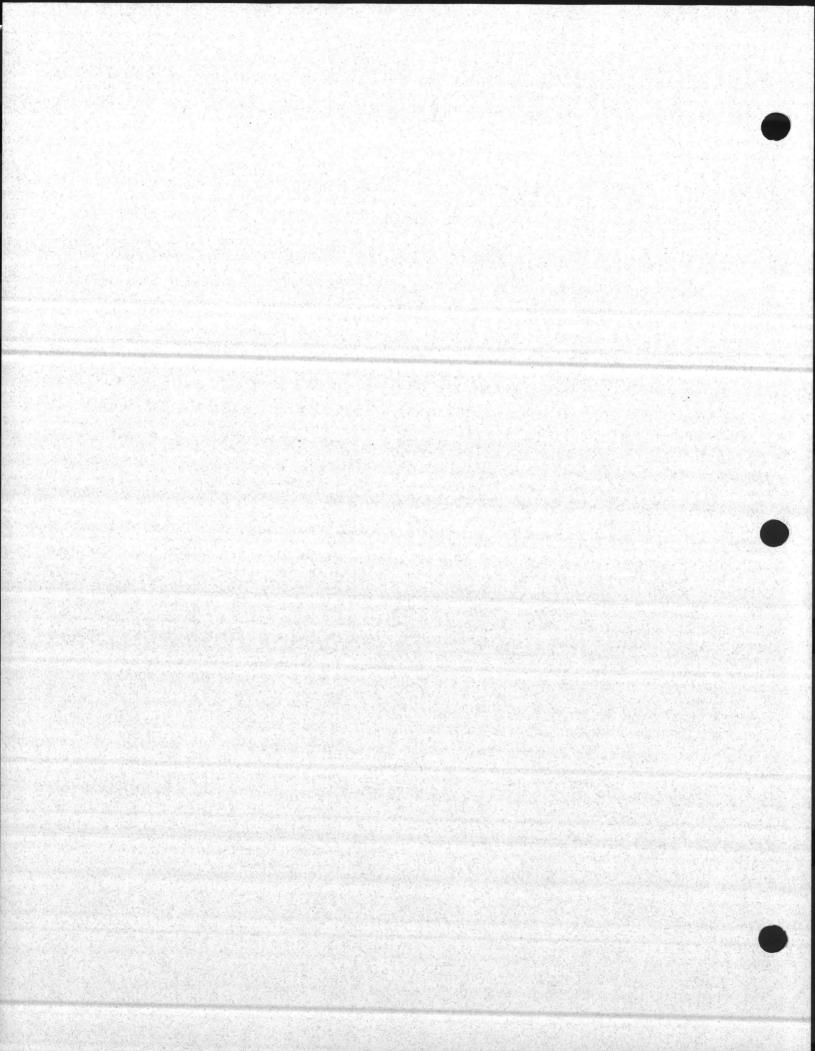


the state of the	11 4 6	1	1	A
Project	Hadast	Point	Industrual A	trea
Liojoon	1944	TOTTO	THATPELLE	

Date	Time	Elapsed Time (min.)	Meter Reading (Gal.)	Average GPM	Comments
2-5-93	0713	02+338	5382.4	1.37	adjust to21.2
100	1080	48	5444.1	1,28	4100 cl = 4770 m
	0827	24	5474.7	1.18	SWL rising 21.38 - 20.05
	0907	40	5521.2	1.16	
	926	19	5543.9	1.19	4260 min 20.15 abjustment 4280 min 20.10
	1004	38	5590.4	1.22	4310 2040
	1044	46	5638.0	1.19	Stepped to Recovery
		of second	15 July 1	4.5	
	Augusta Production	100000000000000000000000000000000000000			
				Electric services	
				7 10	
				al ere or the	
			ga - 49 - 74 - 1		
		The second secon			
-47					Action Committee Com

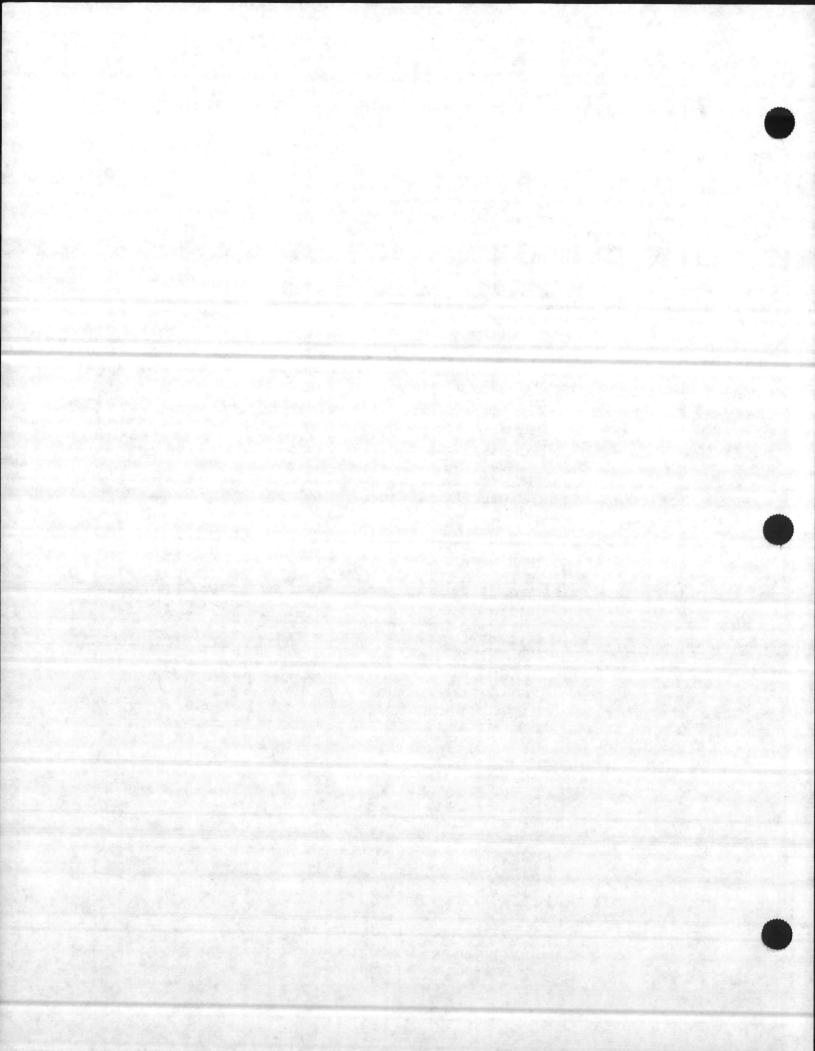


APPENDIX C AQUIFER TEST DATA - DRAWDOWN PHASE

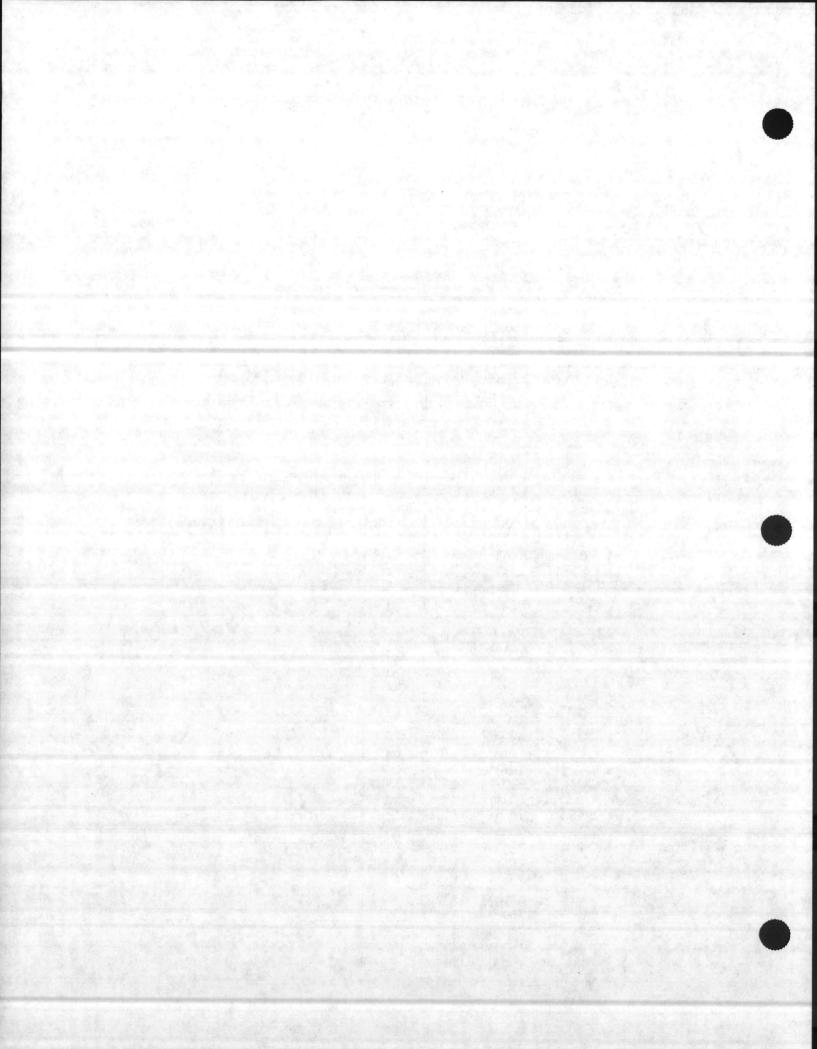


TEST: CONSTANT RATE DRAWDOWN

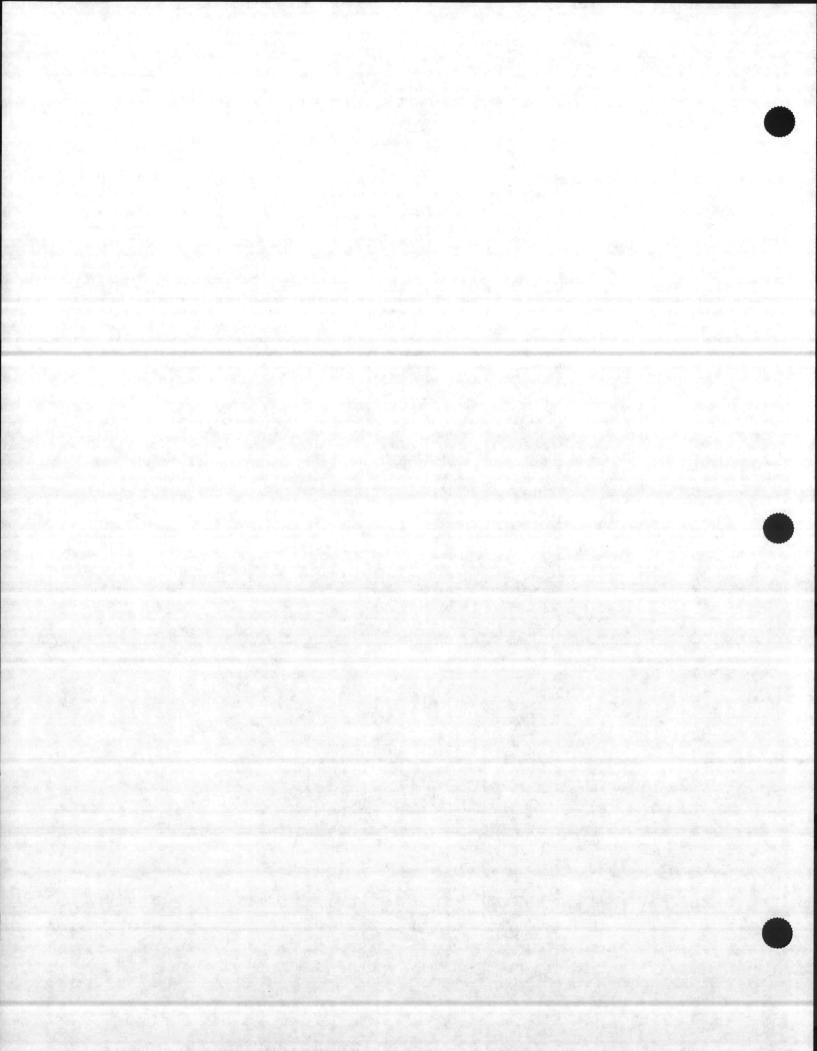
ELAPSED WELL NUMBER				
TIME	RW-1	P-2		
	SWL	SWL		
(MIN)	(FEET)	(FEET)		
0.0000	7.450	5.093		
0.0033	7.443	5.100		
0.0066	7.462	5.106		
0.0100	7.989	5.106		
0.0133	7.735	5.106		
0.0166	7.132	5.100		
0.0200	7.494	5.106		
0.0233	7.881	5.112		
0.0266	7.456	5.112		
0.0300	7.475	5.112		
0.0333	7.799	5.112		
0.0500	7.786	5.100		
0.0666	7.881	5.106		
0.0833	7.995	5.106		
0.1000	8.109	5.112		
0.1166	8.224	5.106		
0.1333	8.306	5.106		
0.1500	8.458	5.119		
0.1666	8.528	5.106		
0.1833	8.477	5.112		
0.2000	8.535	5.106		
0.2166	8.535	5.112		
0.2333	8.573	5.100		
0.2500	8.573	5.106		
0.2666	8.592	5.112		
0.2833	8.611	5.112		
0.3000	8.617	5.106		
0.3166	8.649	5.112		
0.3333	8.693	5.100		
0.4166	8.807	5.100		
0.5000	8.941	5.093		
0.5833	9.048	5.100		
0.6666	9.163	5.100		
0.7500	9.302	5.106		
0.8333	9.410	5.100		
0.9166	9.505	5.093		
1.0000	9.664	5.106		
1.0833	10.00	5.100		
1.1666	The second secon	5.100		
1.2500	10.038	5.100		
1.3333	10.127	5.100		



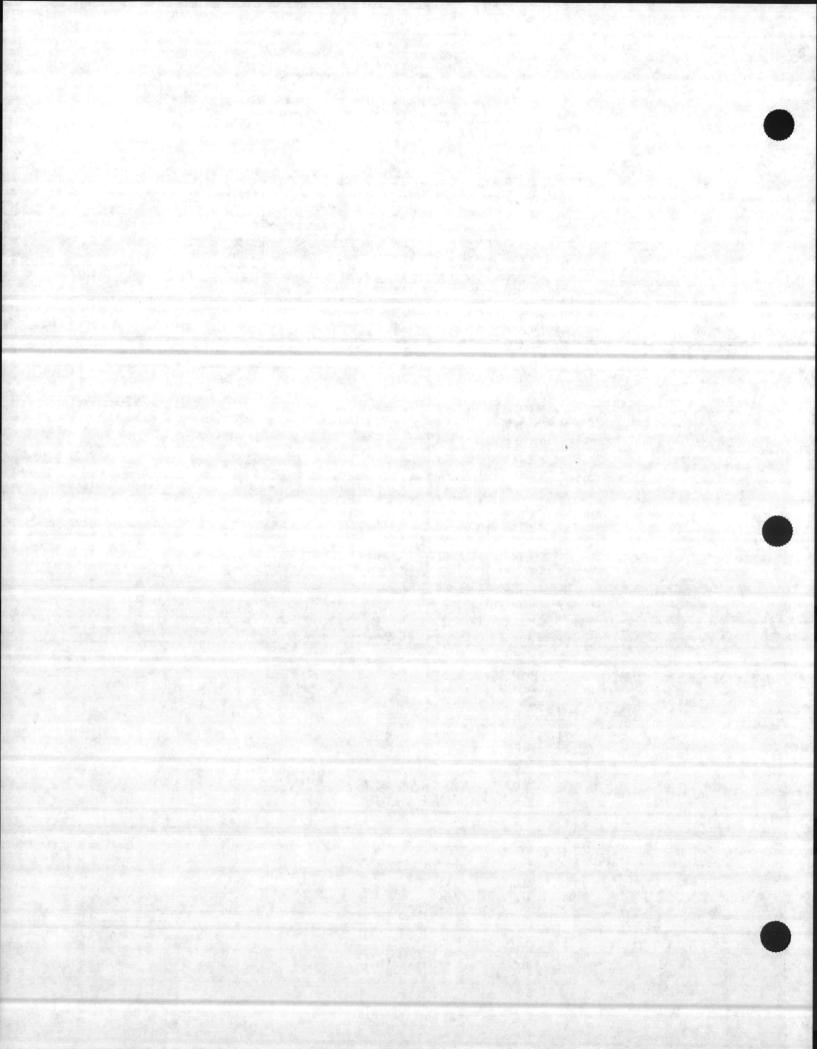
ELAPSED	WELL N	JMBER
TIME	RW-1	P-2
(MIN)	SWL (FEET)	SWL (FEET)
1.4166	10.215	5.106
1.5000	10.213	5.100
1.5833	10.200	5.100
1.6666	10.355	5.106
1.7500	10.374	5.106
1.8333	10.450	5.112
1.9166	10.495	5.112
2.0000	10.526	5.112
2.5000	10.697	5.100
3.0000	10.862	5.112
3.5000	11.033	5.100
4.0000	11.160	5.112
4.5000	11.293	5.112
5.0000	11.439	5.112
5.5000	11.541	5.112
6.0000	11.661	5.119
6.5000	11.750	5.119
7.0000	11.864	5.119
7.5000	11.959	5.131
8.0000	12.048	5.125
8.5000	12.117	5.131
9.0000	12.206	5.125
9.5000	12.257	5.125
10.0000	12.333	5.119
12.0000	12.612	5.150
14.0000	12.770	5.144
16.0000	12.764	5.163
18.0000	12.764	5.169
20.0000	12.777	5.182
22.0000	12.948	5.182
24.0000	13.144	5.207
26.0000	13.303	5.207
28.0000	13.455	5.214
30.0000	13.594	5.226
32.0000	13.676	5.245
34.0000	13.772	5.252
36.0000	13.867	5.271
38.0000	13.968	5.277
40.0000	14.019	5.283
42.0000	14.101	5.296
44.0000	14.190	5.309



	WELL NUMBER				
TIME	RW-1	P-2			
(MIN)	SWL (FEET)	SWL (FEET)			
46.0000	14.247	5.321			
48.0000	14.348	5.334			
50.0000	14.373	5.334			
52.0000	14.443	5.353			
54.0000	14.494	5.359			
56.0000	14.544	5.378			
58.0000	14.595	5.391			
60.0000	14.633	5.391			
62.0000	14.684	5.391			
64.0000	14.715	5.404			
66.0000	14.760	5.423			
68.0000	14.798	5.435			
70.0000	14.829	5.442			
72.0000	14.874	5.454			
74.0000	14.912	5.461			
76.0000	14.956	5.473			
78.0000	14.962	5.480			
80.0000	15.026	5.486			
82.0000	15.057	5.493			
84.0000	15.057	5.486			
86.0000	15.083	5.499			
88.0000	15.114	5.512			
90.0000	15.159	5.531			
92.0000	15.165	5.537			
94.0000	15.209	5.537			
96.0000	15.228	5.543			
98.0000	15.285	5.556			
100.0000	15.342	5.556			
110.0000	15.406	5.600			
120.0000	15.494	5.632			
130.0000	15.653	5.657			
140.0000	15.615	5.683			
150.0000	15.710	5.708			
160.0000	15.957	5.740			
170.0000	16.096	5.765			
180.0000	16.102	5.784			
190.0000	16.622	5.816			
200.0000	16.596	5.835			
210.0000	16.514	5.860			
220.0000	16.501	5.873			
230.0000	16.520	5.904			

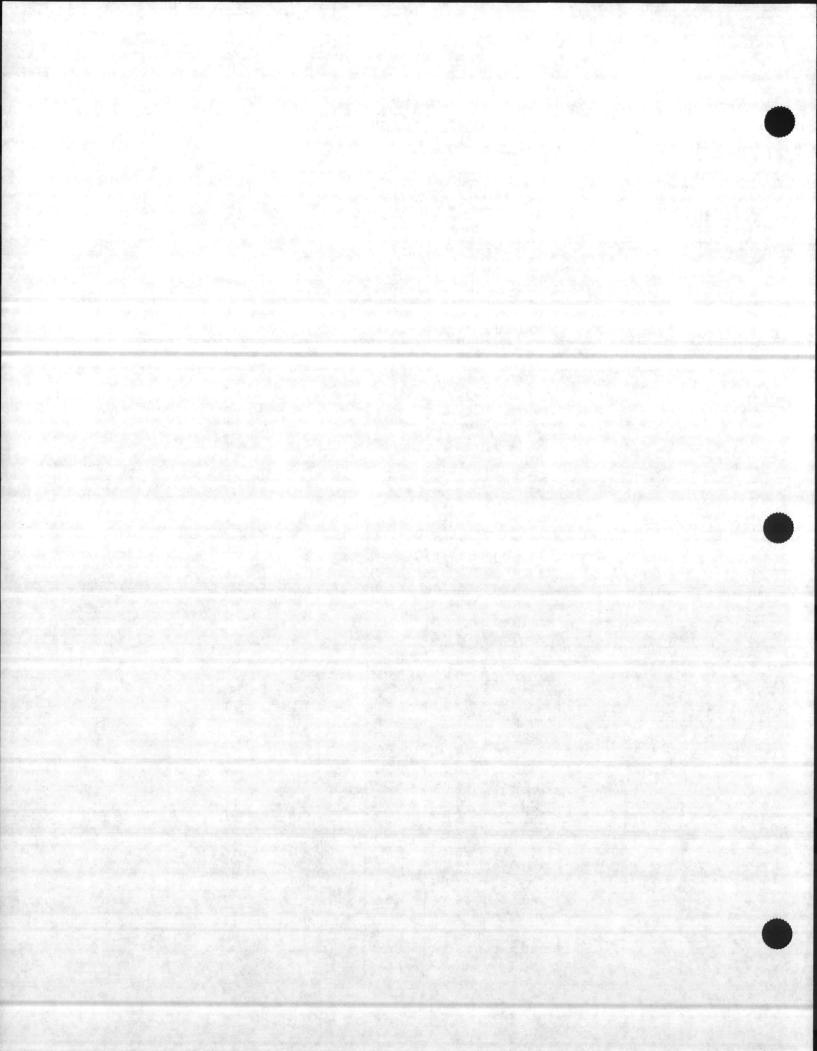


ELAPSED	WELL N	JMBER
TIME	RW-1	P-2
a mn	SWL	SWL
(MIN)	(FEET)	(FEET)
240.0000	16.419	5.917
250,0000	16.349	5.936
260.0000	16.324	5.955
270.0000	16.527	5.968
280.0000	17.704	5.987
290.0000	17.748	6.012
300.0000	17.489	6.031
310.0000	18.653	6.057
320.0000	19.723	6.069
330.0000	20.627	6.088
340.0000	21.266	6.101
350.0000	20.893	6.107
360.0000	20.981	6.126
370.0000	21.456	6.152
380.0000	21.196	6.158
390.0000	21.348	6.177
400.0000	20.621	6.190
410.0000	21.506	6.202
420.0000	21.961	6.221
430.0000	21.829	6.234
440.0000	21.032	6.253
450.0000	20.305	6.266
460.0000	19.526	6.278
470.0000	18.248	6.297
480.0000	18.071	6.310
490.0000	17.660	6.310
500.0000	18.995	6.329
510.0000	19.349	6.335
520.0000	19.286	6.348
530.0000	20.608	6.361
540.0000	20.475	6.373
550.0000	19.761	6.386
560.0000	20.463	6.386
570.0000	20.981	6.399
580.0000	20.975	6.405
590.0000	21.323	6.418
600.0000	21.835	6.430
610.0000	22.669	6.430
620.0000	23.997	6.437
630.0000	24.881	6.449
640.0000	25.747	6.456

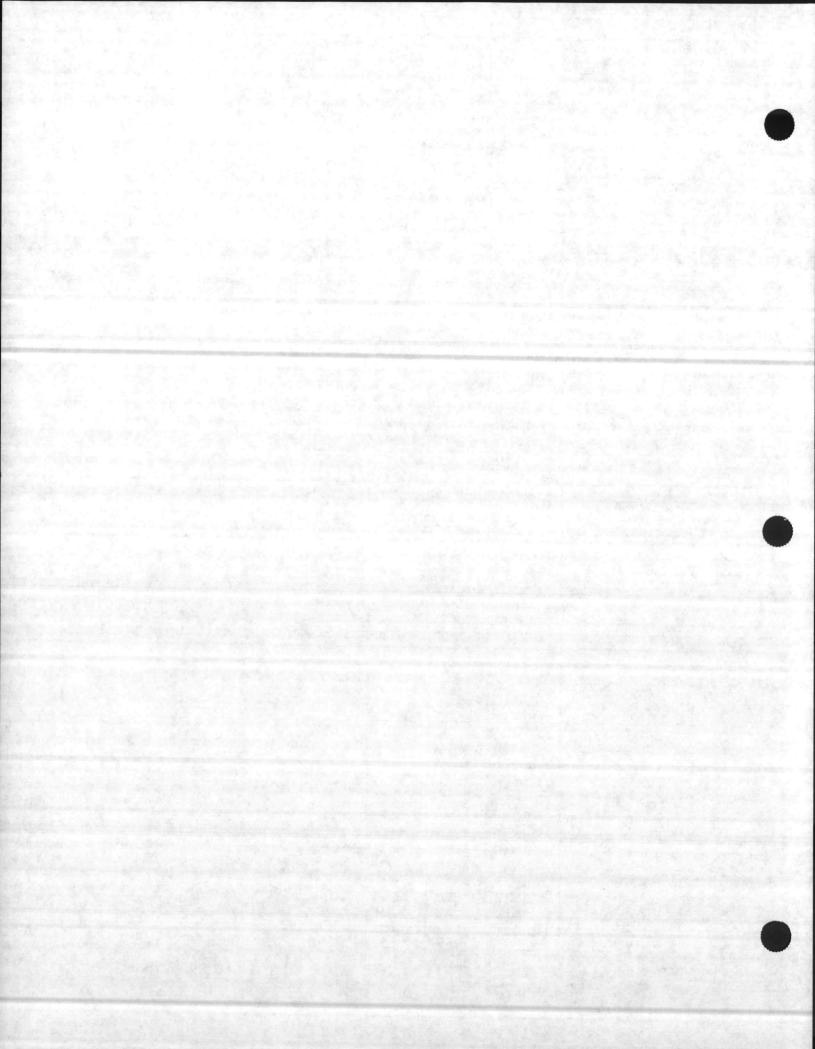


TEST: CONSTANT RATE DRAWDOWN

	WELL NUMBER				
TIME	RW-1	P-2			
	SWL	SWL			
(MIN)	(FEET)	(FEET)			
650.0000	26.176	6.462			
660.0000	26.126	6.475			
670.0000	26.151	6.487			
680.0000	26.157	6.494			
690.0000	26.157	6.494			
700.0000	26.170	6.500			
710.0000	26.163	6.506			
720.0000	26.170	6.506			
730.0000	26.163	6.513			
740.0000	26.145	6.525			
750.0000	26.157	6.525			
760.0000	26.138	6.532			
770.0000	26.170	6.544			
780.0000	26.170	6.544			
790.0000	26.170	6.551			
800.0000	26.151	6.551			
810.0000	26.157	6.557			
820.0000	26.138	6.557			
830.0000	26.145	6.563			
840.0000	26.163	6.563			
850.0000	26.157	6.563			
860.0000	26.157	6.570			
870.0000	26.157	6.576			
880.0000	26.151	6.576			
890.0000	26.157	6.576			
900.0000	26.163	6.576			
910.0000	26.151	6.582			
920.0000	26.145	6.589			
930.0000	26.163	6.589			
940.0000	26.176	6.595			
950.0000	26.157	6.601			
960.0000	26.157	6.601			
970.0000	26.151	6.601			
980.0000	26.050	6.614			
990.0000	25.601	6.620			
1000.0000	25.987	6.614			
1010.0000	26.044	6.620			
1020.0000	24.458	6.627			
1030.0000	24.521	6.633			
1040.0000	25.538	6.633			
1050.0000	24.483	6.633			

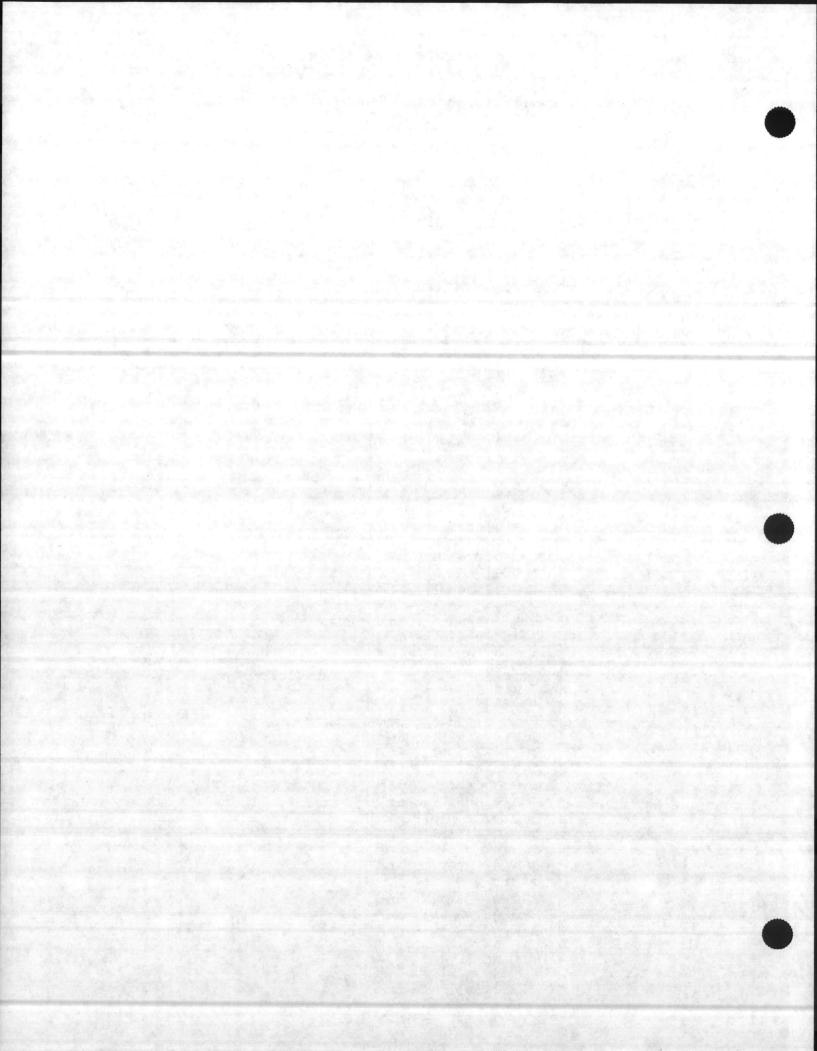


The state of the state of the state of	WELL NUMBER	
TIME	RW-1	P-2
(MIN)	SWL (FEET)	SWL (FEET)
1060.0000	24.218	6.633
1070.0000	24.199	6.633
1080.0000	25.980	6.639
1090.0000	26.081	6.639
1100.0000	25.772	6.633
1110.0000	24.098	6.646
1120.0000	25.974	6.646
1130.0000	26.170	6.646
1140.0000	25.450	6.652
1150.0000	25.159	6.652
1160.0000	25.646	6.652
1170.0000	25.684	6.658
1180.0000	24.793	6.658
1190.0000	25.431	6.658
1200.0000	24.925	6.671
1210.0000	25.753	6.671
1220.0000	26.176	6.677
1230.0000	25.892	6.677
1240.0000	25.867	6.684
1250.0000	26.050	6.690
1260.0000	25.627	6.690
1270.0000	25.791	6.696
1280.0000	25.867	6.696
1290.0000	25.816	6.703
1300.0000	25.494	6.709
1310.0000	23.169	6.709
1320.0000	23.984	6.715
1330.0000	24.780	6.715
1340.0000	25.425	6.722
1350.0000	24.407	6.728
1360.0000	23.339	6.722
1370.0000	22.992	6.722
1380.0000	24.054	6.728
1390.0000	24.818	6.734
1400.0000	25.671	6.734
1410.0000	25.235	6.741
1420.0000	24.414	6.734
1430.0000	23.655	6.741
1440.0000	23.535	6.747
1450.0000	23.213	6.753
1460.0000	22.682	6.747



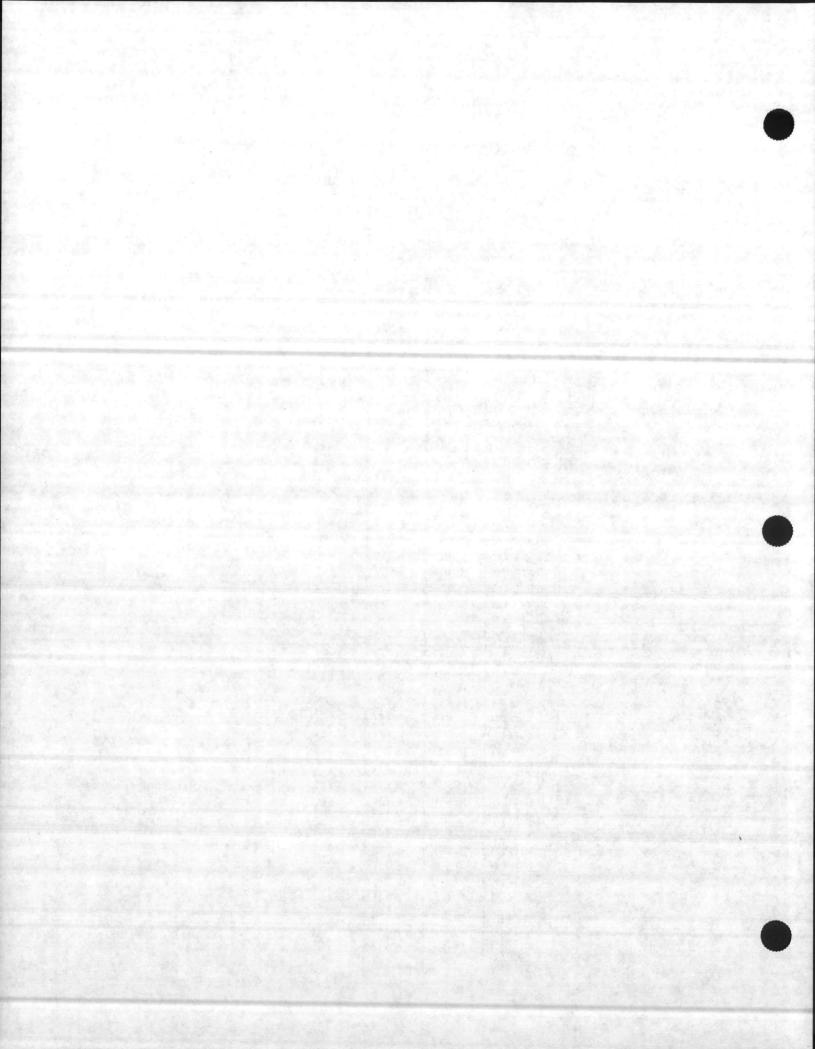
SITE I.D.: CAMP LEJEUNE, HPIA TEST: CONSTANT RATE DRAWDOWN

	WELL NUMBER	
TIME	RW-1	P-2
(MIN)	SWL (FEET)	SWL (FEET)
4.450.0000	22 200	(750
1470.0000	23.200 24.439	6.753 6.753
1480.0000	25.519	6.747
1490.0000 1500.0000	26.037	6.747
1510.0000	26.182	6.747
1520.0000	24.856	6.741
1530.0000	23.478	6.741
1540.0000	22.075	6.747
1550.0000	21.266	6.747
1560.0000	20.703	6.734
1570.0000	20.001	6.728
1580.0000	19.381	6.715
1590.0000	18.736	6.722
1600.0000	18.096	6.709
1610.0000	17.375	6.722
1620.0000	16.501	6.715
1630.0000	16.362	6.696
1640.0000	16.590	6.696
1650.0000	16.470	6.696
1660.0000	16.368	6.696
1670.0000	16.286	6.684
1680.0000	16.444	6.684
1690.0000	16.653	6.677
1700.0000	16.748	6.684
1710.0000	16.729	6.677
1720.0000	16.717	6.671
1730.0000	16.710	6.665
1740.0000	16.710	6.658
1750.0000	16.691	6.665
1760.0000	16.641	6.671
1770.0000	16.628	6,665
1780.0000	16.641	6.665
1790.0000	16.628	6.665
1800.0000	16.552	6.665
1810.0000	16.590	6.665
1820.0000	16.653	6.671
1830.0000	16.672	6.665
1840.0000	16.704	6.671
1850.0000	16.723	6.671
1860.0000	16.736	6.671
1870.0000	16.736	6.677

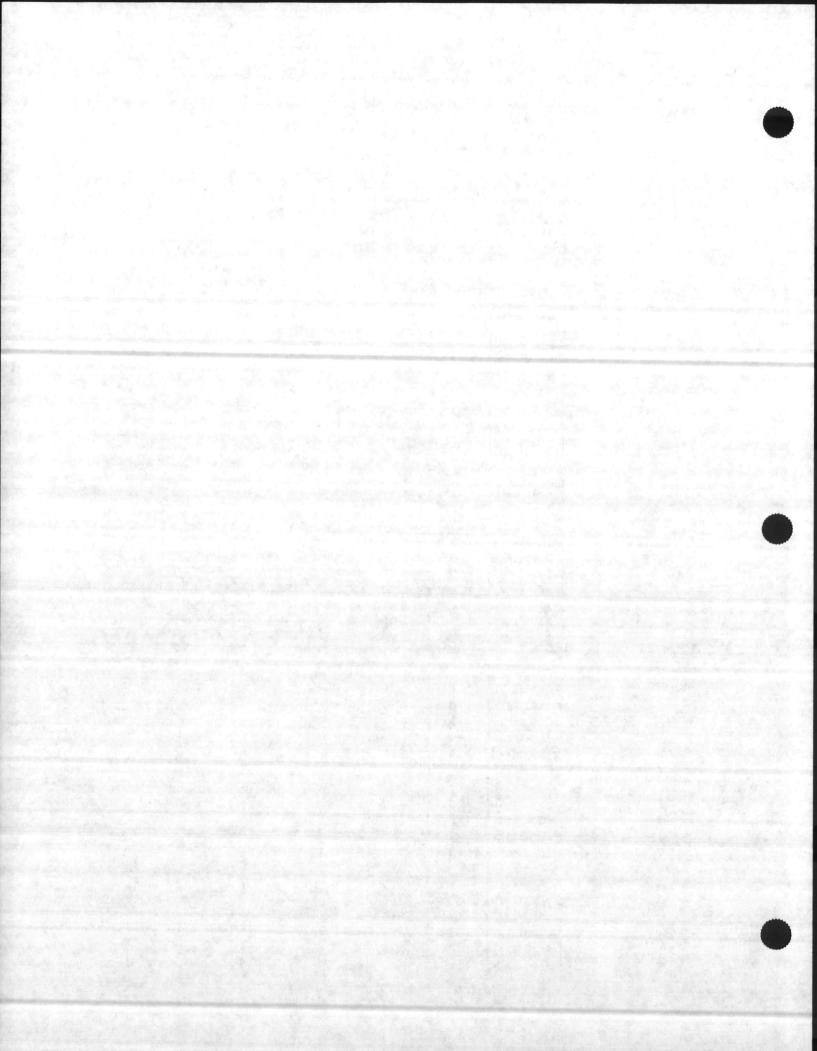


TEST: CONSTANT RATE DRAWDOWN

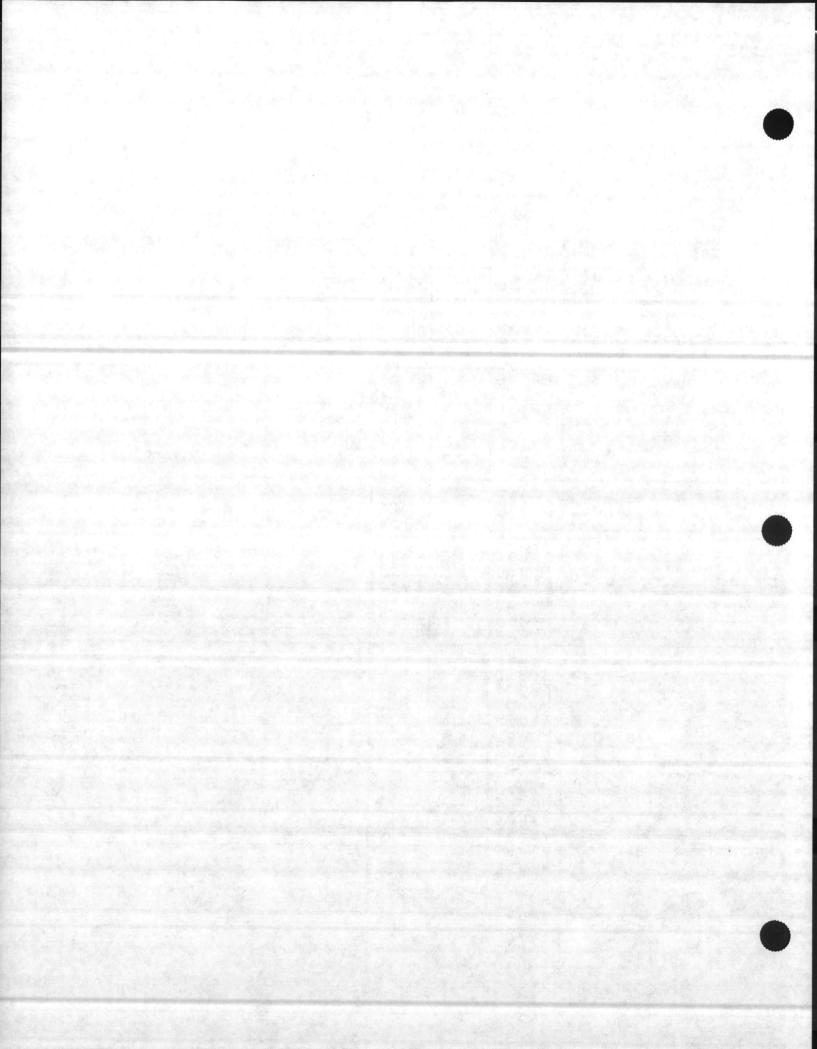
Section 1985 to the section of the section of the	APSED WELL NUMBER	
TIME	RW-1	P-2
ams	SWL	SWL
(MIN)	(FEET)	(FEET)
1880.0000	16.565	6.677
1890.0000	16.495	6.677
1900.0000	16.432	6.677
1910.0000	16.337	6.684
1920.0000	16.254	6.684
1930.0000	16.210	6.690
1940.0000	16.178	6.690
1950.0000	16.223	6.690
1960.0000	17.027	6.696
1970.0000	17.293	6.703
1980.0000	17.445	6.703
1990.0000	17.603	6.709
2000.0000	17.653	6.709
2010.0000	17.077	6.715
2020.0000	17.109	6.715
2030.0000	17.191	6.715
2040.0000	17.166	6.722
2050.0000	17.153	6.722
2060.0000	17.160	6.728
2070.0000	17.071	6.728
2080.0000	17.001	6.728
2090.0000	16.957	6.734
2100.0000	16.951	6.734
2110.0000	16.944	6.728
2120.0000	16.913	6.734
2130.0000	16.913	6.734
2140.0000	16.938	6.734
2150.0000	16.925	6.722
2160.0000	16.913	6.734
2170.0000	16.938	6.734
2180.0000	16.970	6.734
2190.0000	17.014	6.734
2200.0000	17.014	6.741
2210.0000	17.058	6.728
2220.0000	17.090	6.747
2230.0000	17.027	6.741
2240.0000	16.995	6.734
2250.0000	16.951	6.734
2260.0000	17.052	6.728
2270.0000	17.096	6.734
2280.0000	17.027	6.734



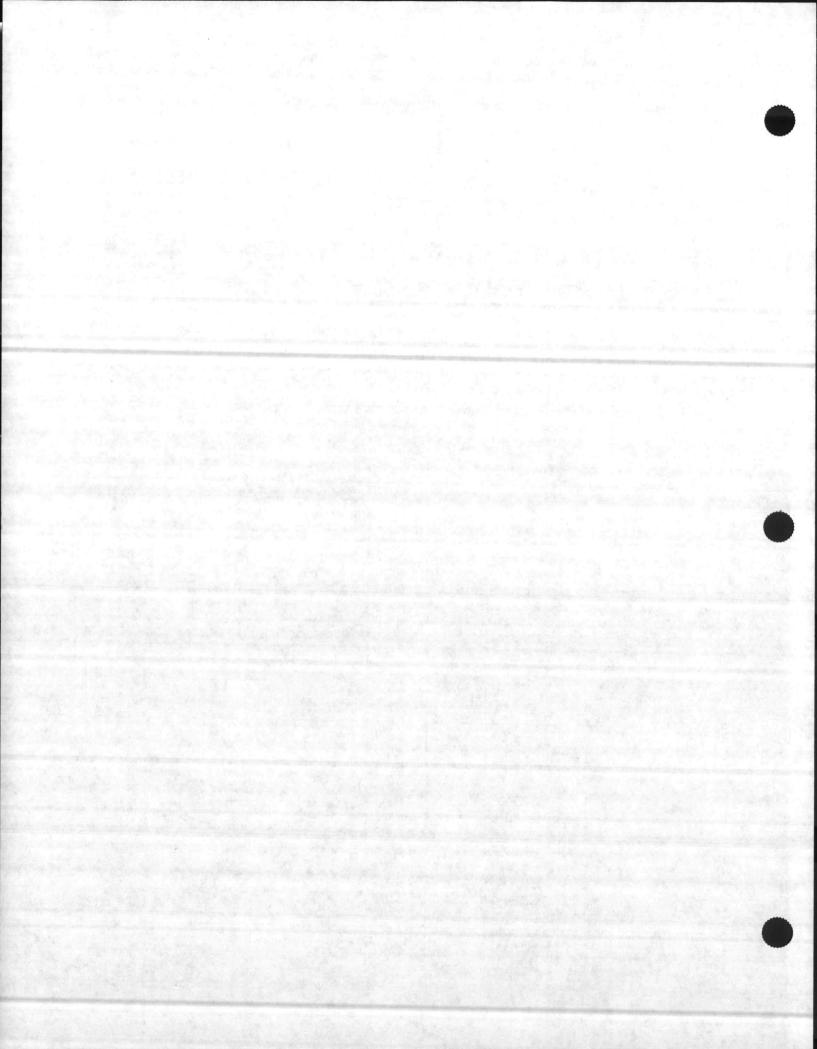
	WELL NUMBER	
TIME	RW-1	P-2
(MIN)	SWL (FEET)	SWL (FEET)
2290.0000	16.970	6.734
2300.0000	16.919	6.734
2310.0000	16.900	6.722
2320.0000	16.894	6.734
2330.0000	16.887	6.734
2340.0000	16.970	6.734
2350.0000	17.039	6.734
2360.0000	17.096	6.734
2370.0000	17.134	6.741
2380.0000	17.172	6.728
2390.0000	17.217	6.734
2400.0000	17.261	6.728
2410.0000	17.077	6.728
2420.0000	16.717	6.734
2430.0000	16.286	6.734
2440.0000	16.052	6.734
2450.0000	15.912	6.728
2460.0000	15.849	6.728
2470.0000	15.792	6.728
2480.0000	15.767	6.728
2490.0000	15.748	6.722
2500.0000	15.355	6.722
2510.0000	15.038	6.715
2520.0000	14.848	6.715
2530.0000	14.652	6.703
2540.0000	14.519	6.696
2550.0000	14.462	6.690
2560.0000	14.392	6.684
2570.0000	14.367	6.677
2580.0000	14.335	6.677
2590.0000	14.323	6.677
2600.0000	14.297	6.665
2610.0000	14.285	6.665
2620.0000	14.329	6.658
2630.0000	14.354	6.658
2640.0000	14.361	6.658
2650.0000	14.342	6.652
2660.0000	14.342	6.652
2670.0000	14.361	6.652
2680.0000	14.443	6.652
2690.0000	14.494	6.652



	WELL NUMBER	
TIME	RW-1	P-2
(MIN)	SWL (FEET)	SWL (FEET)
2700 0000	14.525	6.652
2700.0000 2710.0000	14.525	6.652
2720.0000	14.531	6.658
2730.0000	14.557	6.652
2740.0000	14.570	6.658
2750.0000	14.608	6.658
2760.0000	14.646	6.665
2770.0000	14.671	6.671
2780.0000	14.671	6.671
2790.0000	14.703	6.677
2800.0000	14.709	6.684
2810.0000	15.995	6.684
2820.0000	16.292	6.696
2830.0000	16.292	6.703
2840.0000	16.210	6.709
2850.0000	16.185	6.728
2860.0000	16.185	6.728
2870.0000	16.223	6.741
2880.0000	16.292	6.747
2890.0000	16.330	6.753
2900.0000	16.375	6.760
2910.0000	16.413	6.779
2920.0000	16.432	6.785
2930.0000	16.463	6.785
2940.0000	16.508	6.791
2950.0000	16.539	6.791
2960.0000	16.546	6.798
2970.0000	16.571	6.791
2980.0000	16.584	6.791
2990.0000	16.552	6.798
3000.0000	16.571	6.804
3010.0000	16.571	6.798
3020.0000	16.571	6.791
3030.0000	16.571	6.811
3040.0000	16.577	6.798
3050.0000	16.577	6.804
3060.0000	16.565	6.791
3070.0000	16.558	6.798
3080.0000	16.546	6.804
3090.0000	16.590	6.791
3100.0000	16.609	6.798

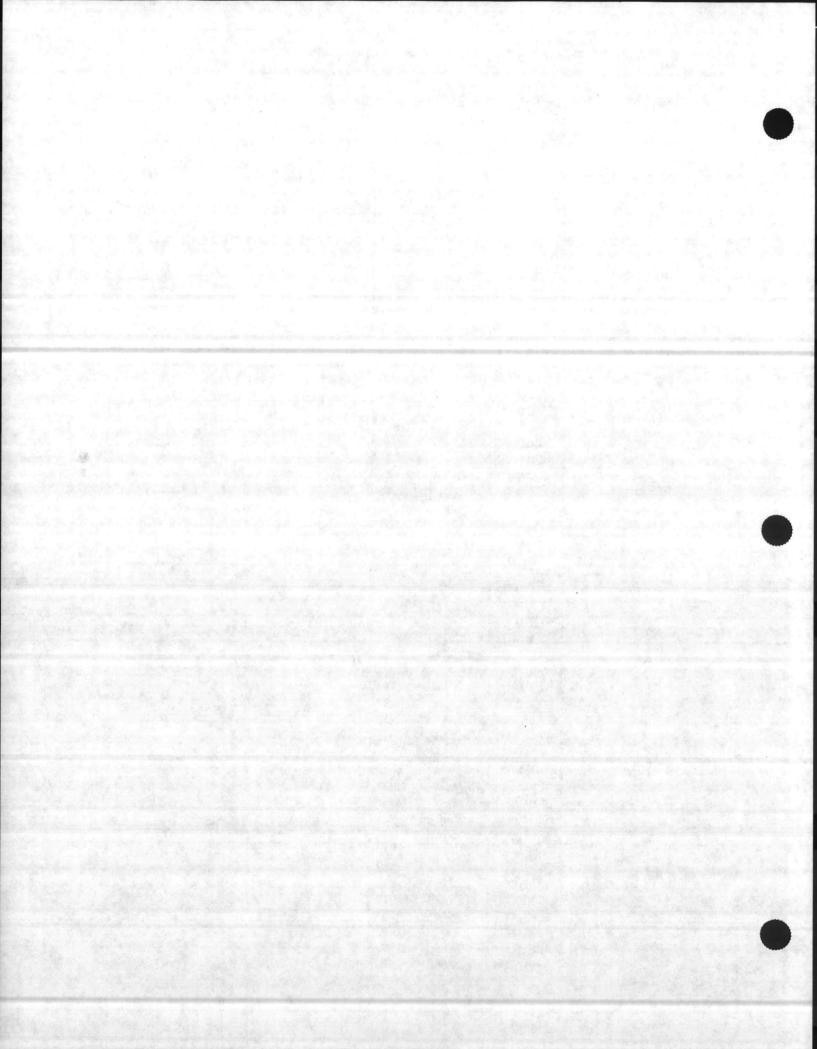


The second secon	WELL NUMBER	
TIME	RW-1	P-2
(MIN)	SWL (FEET)	SWL (FEET)
3110.0000	16.653	6.804
3120.0000	16.691	6.804
3130.0000	16.729	6.804
3140.0000	16.729	6.811
3150.0000	16.729	6.791
3160.0000	16.723	6.804
3170.0000	16.742	6.817
3180.0000	16.641	6.811
3190.0000	16.419	6.817
3200.0000	16.292	6.811
3210.0000	16.229	6.817
3220.0000	16.178	6.817
3230.0000	16.147	6.823
3240.0000	16.140	6.830
3250.0000	16.128	6.830
3260.0000	16.128	6.823
3270.0000	16.147	6.830
3280.0000	16.159	6.836
3290.0000	17.995	6.842
3300.0000	17.128	6.849
3310.0000	16.641	6.855
3320.0000	16.736	6.861
3330.0000	16.995	6.861
3340.0000	17.413	6.868
3350.0000	17.666	6.874
3360.0000	17.983	6.887
3370.0000	18.305	6.893
3380.0000	18.634	6.899
3390.0000	18.818	6.906
3400.0000	19.096	6.912
3410.0000	19.198	6.912
3420.0000	19.254	6.918
3430.0000	19.444	6.918
3440.0000	19.710	6.925
3450.0000	19.944	6.931
3460.0000	20.229	6.931
3470.0000	20.463	6.931
3480.0000	20.659	6.937
3490.0000	21.449	6.937
3500.0000	19.134	6.937
3510.0000	16.919	6.944



TEST: CONSTANT RATE DRAWDOWN

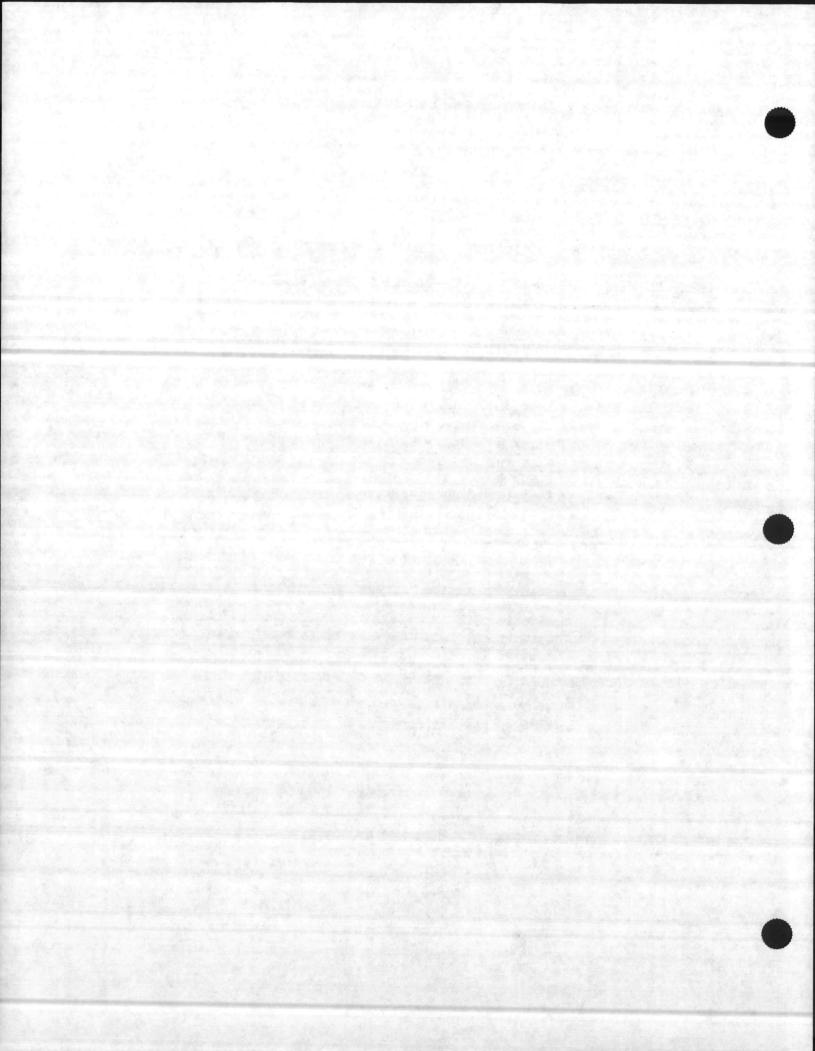
	WELL NUMBER	
TIME	RW-1	P-2
(MIN)	SWL (FEET)	SWL (FEET)
3520.0000	16.083	6.937
3530.0000	16.596	6.937
3540.0000	16.780	6.944
3550.0000	16.868	6.944
3560.0000	16.938	6.944
3570.0000	17.027	6.944
3580.0000	17.096	6.950
3590.0000	17.166	6.950
3600.0000	17.248	6.950
3610.0000	17.305	6.956
3620.0000	17.305	6.956
3630.0000	17.001	6.956
3640.0000	16.849	6.963
3650.0000	16.736	6.963
3660.0000	16.647	6.963
3670.0000	16.470	6.963
3680.0000	16.330	6.963
3690.0000	16.223	6.963
3700.0000	16.153	6.956
3710.0000	16.096	6.956
3720.0000	16.077	6.950
3730.0000	16.064	6.944
3740.0000	16.058	6.944
3750.0000	16.039	6.937
3760,0000	16.330	6.937
3770.0000	17.533	6.937
3780.0000	18.388	6.931
3790.0000	18.337	6.925
3800.0000	17.679	6.925
3810.0000	17.065	6.931
3820.0000	16.590	6.931
3830.0000	16.210	6.925
3840.0000	15.976	6.925
3850.0000	15.862	6.918
3860.0000	15.811	6.912
3870.0000	15.741	6.912
3880.0000	15.722	6.912
3890.0000	15.634	6.906
3900.0000	15.539	6.899
3910.0000	15.488	6.899
3920.0000	15.456	6.899



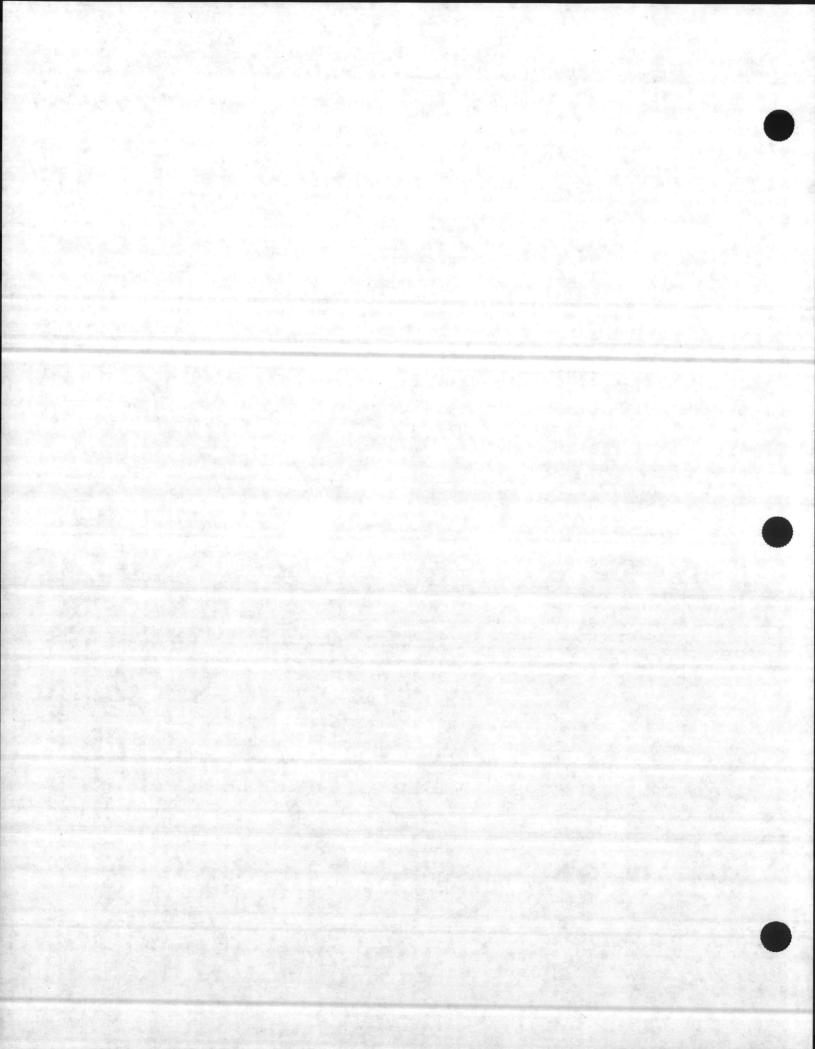
CONTRACT TASK ORDER: 0017 SITE I.D.: CAMP LEJEUNE, HPIA

TEST: CONSTANT RATE DRAWDOWN

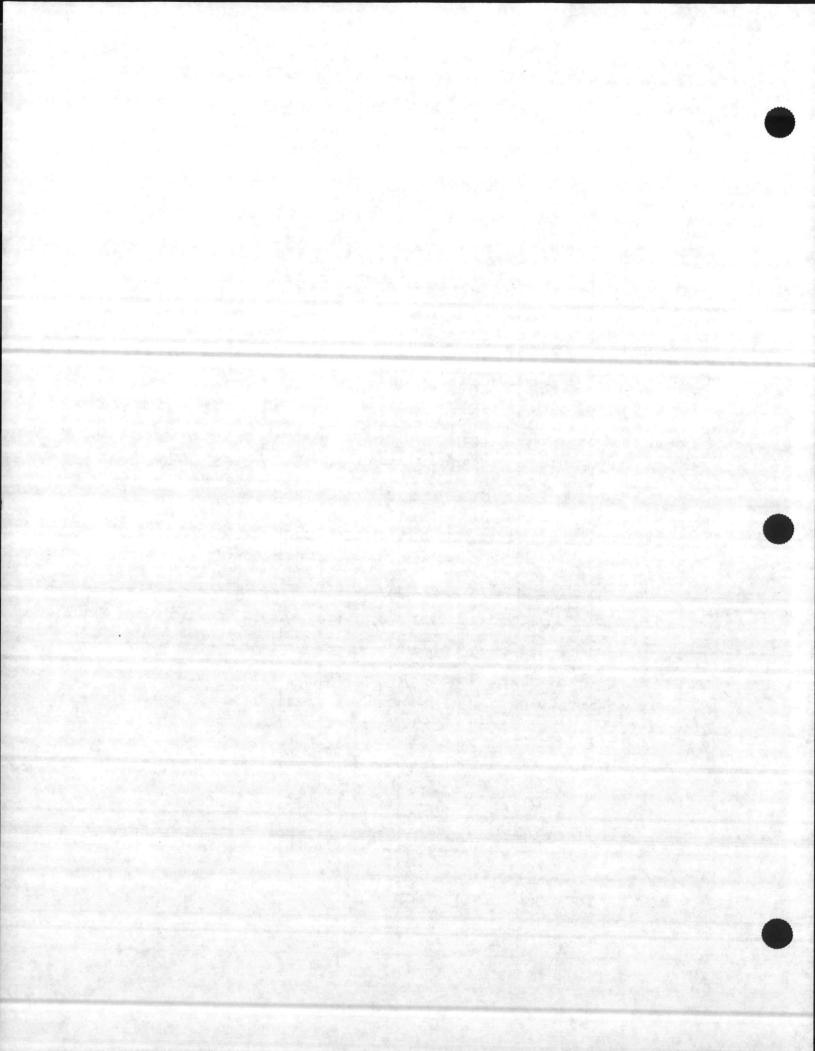
	WELL NUMBER			
TIME	RW-1	P-2		
A	SWL	SWL		
(MIN)	(FEET)	(FEET)		
3930.0000	15.437	6.893		
3940.0000	18.831	6.887		
3950.0000	22.353	6.893		
3960.0000	24.022	6.893		
3970.0000	25.582	6.893		
3980.0000	26.044	6.899		
3990.0000	26.094	6.899		
4000.0000	26.163	6.899		
4010.0000	25.949	6.906		
4020.0000	25.980	6.906		
4030.0000	25.873	6.912		
4040.0000	25.804	6.912		
4050.0000	25.677	6.918		
4060.0000	25.513	6.912		
4070.0000	24.685	6.918		
4080.0000	21.108	6.918		
4090.0000	17.128	6.925		
4100.0000	15.171	6.925		
4110.0000	14.253	6.918		
4120.0000	16.324	6.912		
4130.0000	17.748	6.912		
4140.0000	18.565	6.912		
4150.0000	19.406	6.912		
4160.0000	20.001	6.912		
4170.0000	20.678	6.918		
4180.0000	21.114	6.925		
4190.0000	21.386	6.931		
4200.0000	21.304	6.925		
4210.0000	21.266	6.937		
4220.0000	21.057	6.937		
4230.0000	20.785	6.944		
4240.0000	20.488	6.950		
4250.0000	20.248	6.956		
4260.0000	20.153	6.950		
4270.0000	20.482	6.950		
4280.0000	20.108	6.956		
4290.0000	20.279	6.956		
4300.0000	20.501	6.950		
4310.0000	20.608	6.963		
4320.0000	20.741	6.950		
4330.0000	20.899	6.956		



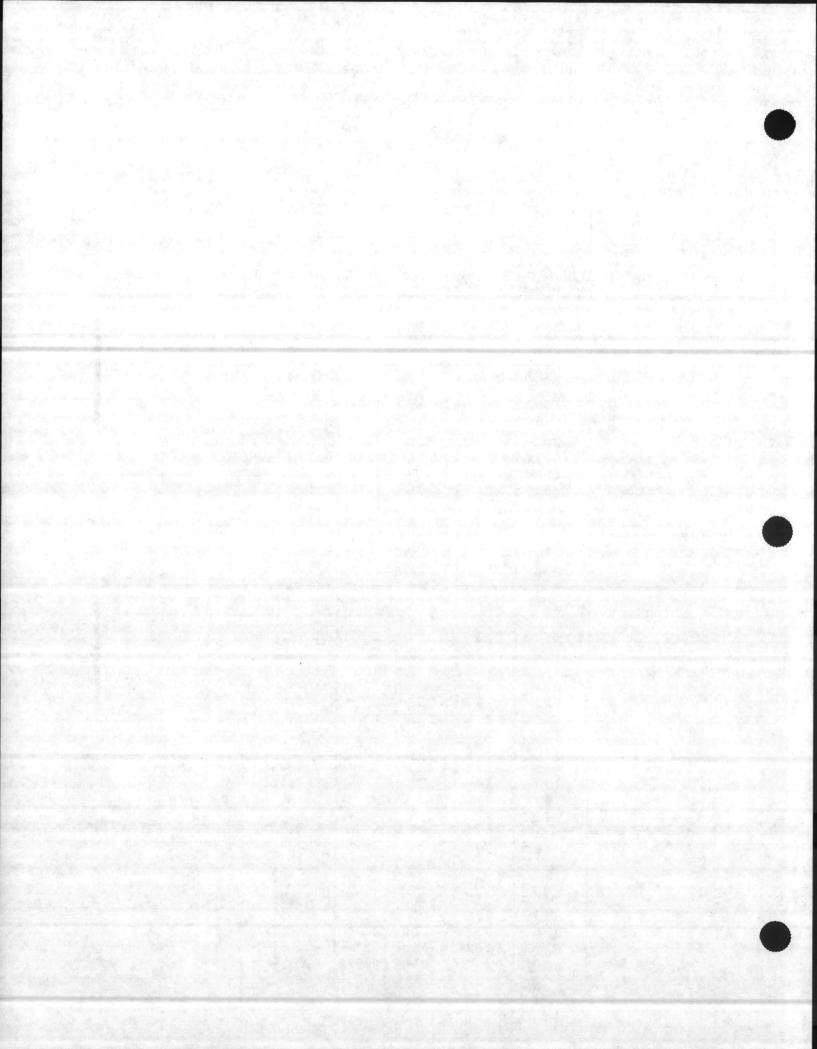
	WELL NUMBER		
TIME	RW-1	P-2	
(MIN)	SWL (FEET)	SWL (FEET)	
4340.0000	20.912	6.963	
4350.0000	20.874	6.956	



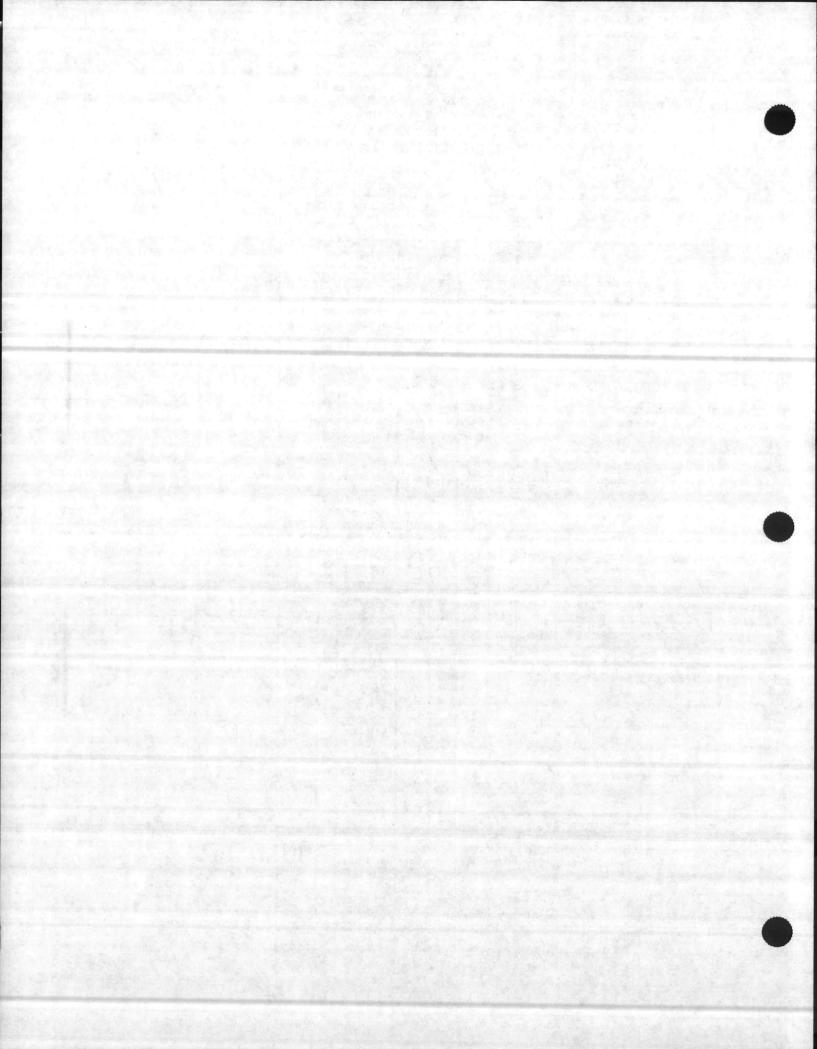
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
0.0000	7.343	7.281	12.734	12.968
0.0083	7.343	7.281	12.734	12.968
0.0166	7.343	7.281	12.734	12.968
0.0250	7.350	7.281	12.734	12.968
0.0333	7.343	7.281	12.734	12.968
0.0416	7.343	7.281	12.734	12.968
0.0500	7.343	7.281	12.734	12.968
0.0583	7.343	7.281	12.734	12.968
0.0666	7.350	7.281	12.734	12.968
0.0750	7.350	7.281	12.734	12.968
0.0833	7.343	7.287	12.734	12.968
0.0916	7.343	7.281	12.734	12.968
0.1000	7.350	7.281	12.734	12.968
0.1083	7.343	7.281	12.734	12.968
0.1166	7.343	7.281	12.734	12.968
0.1250	7.343	7.281	12.734	12.968
0.1333	7.350	7.287	12.734	12.968
0.1416	7.343	7.281	12.750	12.968
0.1500	7.343	7.281	12.734	12.968
0.1583	7.350	7.287	12.734	12.968
0.1666	7.350	7.281	12.734	12.984
0.1750	7.350	7.287	12.734	12.968
0.1833	7.350	7.281	12.734	12.968
0.1916	7.350	7.287	12.734	12.968
0.2000	7.343	7.287	12.734	12.968
0.2083	7.350	7.281	12.750	12.984
0.2166	7.350	7.287	12.734	12.968
0.2250	7.350	7.287	12.750	12.968
0.2333	7.350	7.287	12.734	12.968
0.2416	7.350	7.287	12.750	12.984
0.2500	7.350	7.281	12.734	12.968
0.2583	7.350	7.287	12.750	12.968
0.2666	7.350	7.287	12.750	12.968
0.2750	7.350	7.287	12.734	12.968
0.2833	7.350	7.287	12.734	12.968
0.2916	7.350	7.287	12.734	12.968
0.3000	7.343	7.287	12.734	12.968
0.3083	7.343	7.287	12.750	12.968
0.3065	7.350	7.287	12.750	12.968
0.3150	7.350	7.287	12.750	12.968
0.3230	7.343	7.287	12.734	12.984



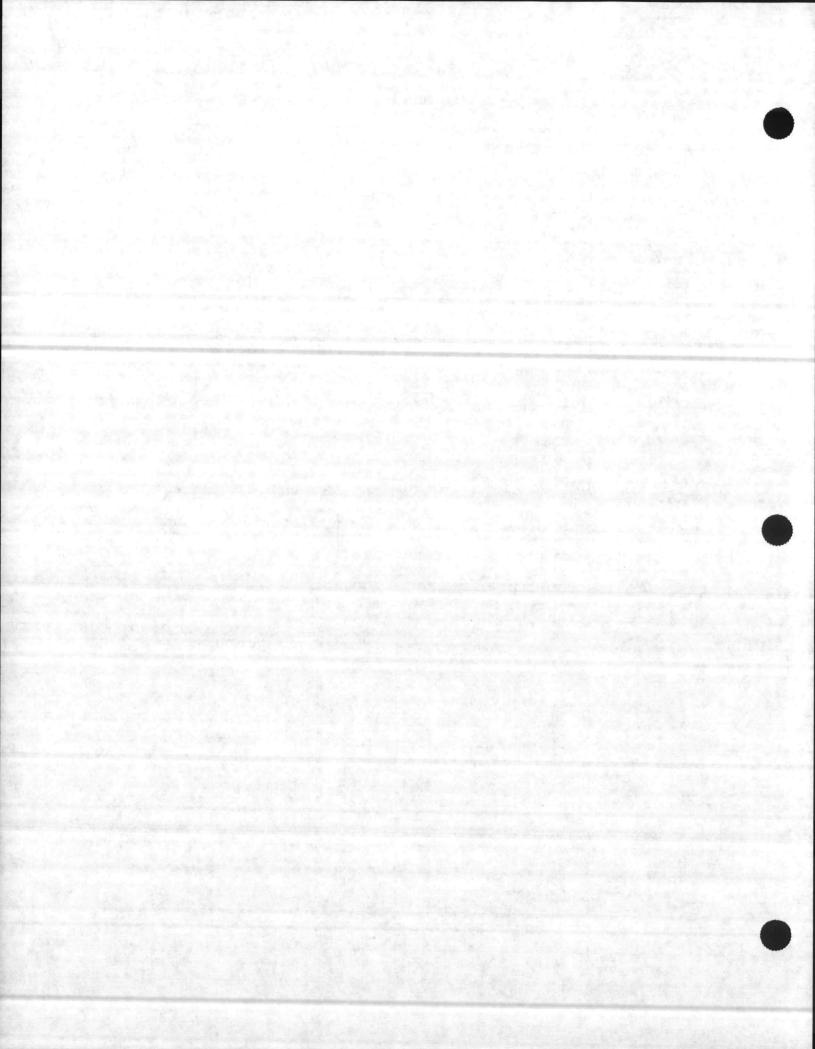
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
0.3500	7.343	7.281	12.750	12.968
0.3666	7.337	7.281	12.750	12.968
0.3833	7.343	7.281	12.750	12.968
0.4000	7.337	7.281	12.734	12.984
0.4166	7.343	7.281	12.734	12.968
0.4333	7.343	7.287	12.734	12.968
0.4500	7.343	7.287	12.734	12.984
0.4666	7.343	7.287	12.734	12.968
0.4833	7.343	7.281	12.750	12.968
0.5000	7.343	7.287	12.734	12.984
0.5166	7.343	7.274	12.734	12.968
0.5333	7.343	7.281	12.734	12.968
0.5500	7.343	7.281	12.734	12.984
0.5666	7.343	7.281	12.734	12.968
0.5833	7.343	7.287	12.734	12.984
0.6000	7.343	7.287	12.734	12.968
0.6166	7.350	7.287	12.734	12.984
0.6333	7.343	7.287	12.734	12.968
0.6500	7.350	7.287	12.750	12.984
0.6666	7.350	7.287	12.750	12.984
0.6833	7.350	7.287	12.750	12.984
0.7000	7.350	7.287	12.750	12.984
0.7166	7.350	7.287	12.750	12.984
0.7333	7.350	7.287	12.750	12.984
0.7500	7.350	7.287	12.750	12.984
0.7666	7.343	7.287	12.750	12.984
0.7833	7.350	7.287	12.750	12.984
0.8000	7.343	7.287	12.734	12.984
0.8166	7.350	7.287	12.750	12.984
0.8333	7.350	7.287	12.750	12.968
0.8500	7.350	7.287	12.750	12.968
0.8666	7.350	7.287	12.734	12.984
0.8833	7.350	7.287	12.734	12.984
0.9000	7.343	7.287	12.734	12.984
0.9166	7.350	7.287	12.734	12.968
0.9333	7.343	7.287	12.750	12.968
0.9500	7.350	7.287	12.750	12.968
0.9666	7.343	7.287	12.750	12.968
0.9833	7.343	7.287	12.734	12.968
1.0000	7.343	7.281	12.734	12.968
1.2000	7.343	7.281	12.734	12.968



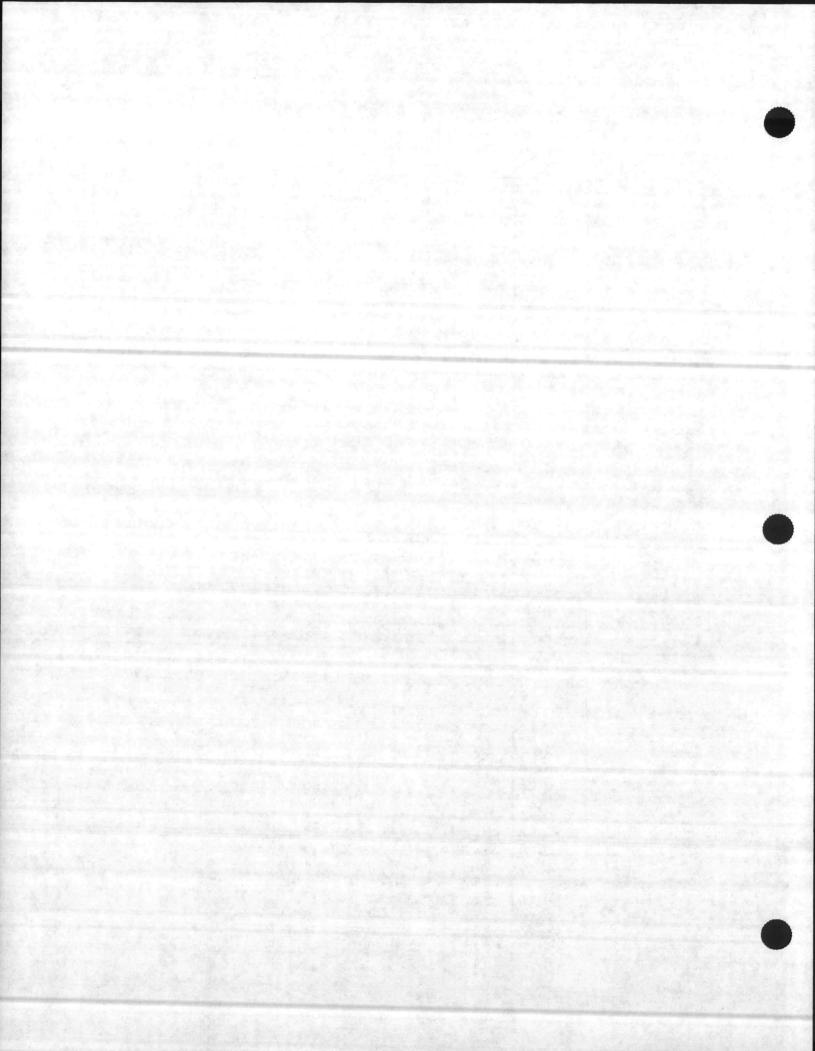
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
0.000	SWL	SWL	SWL	SWL
(MIN)	(FEET)	(FEET)	(FEET)	(FEET)
1.4000	7.343	7.287	12.734	12.968
1.6000	7.343	7.281	12.718	12.968
1.8000	7.343	7.287	12.734	12.968
2.0000	7.350	7.287	12,734	12.968
2.2000	7.343	7.281	12.718	12.968
2.4000	7.350	7.281	12.734	12.968
2,6000	7.337	7.281	12.718	12.968
2.8000	7.350	7.293	12.734	12.968
3.0000	7.350	7.281	12.734	12.968
3.2000	7.350	7.293	12.734	12.968
3.4000	7.350	7.287	12.734	12.984
3.6000	7.343	7.287	12.734	12.968
3.8000	7.350	7.287	12.750	12.968
4.0000	7.343	7.287	12.734	12.968
4.2000	7.350	7.281	12.734	12.968
4.4000	7.350	7.287	12.734	12.968
4.6000	7.343	7.287	12.734	12.968
4.8000	7.343	7.281	12.734	12,968
5.0000	7.343	7.287	12.734	12.984
5.2000	7.350	7.287	12.750	12.984
5.4000	7.350	7.287	12.734	12.968
5.6000	7.343	7.287	12.734	12.968
5.8000	7.350	7.287	12.734	12.968
6.0000	7.343	7.287	12.734	12.968
6.2000	7.350	7.287	12.734	12.968
6.4000	7.343	7.287	12.734	12.968
6.6000	7.343	7.281	12.734	12.968
6.8000	7.350	7.287	12.734	12.968
7.0000	7.350	7.287	12.734	12.968
7.2000	7.350	7.287	12.734	12.968
7.4000	7.350	7.287	12.734	12.968
7.6000	7.350	7.287	12.734	12.968
7.8000	7.343	7.287	12.734	12.968
8.0000	7.343	7.287	12.734	12.968
8.2000	7.350	7.287	12.734	12.968
8.4000	7.350	7.293	12.750	12.968
8.6000	7.350	7.287	12.734	12.984
8.8000	7.350	7.287	12.734	12.984
9.0000	7.350	7.293	12.734	12.968
9.2000	7.343	7.287	12.734	12.968
9.4000	7.343	7.287	12.734	12.968



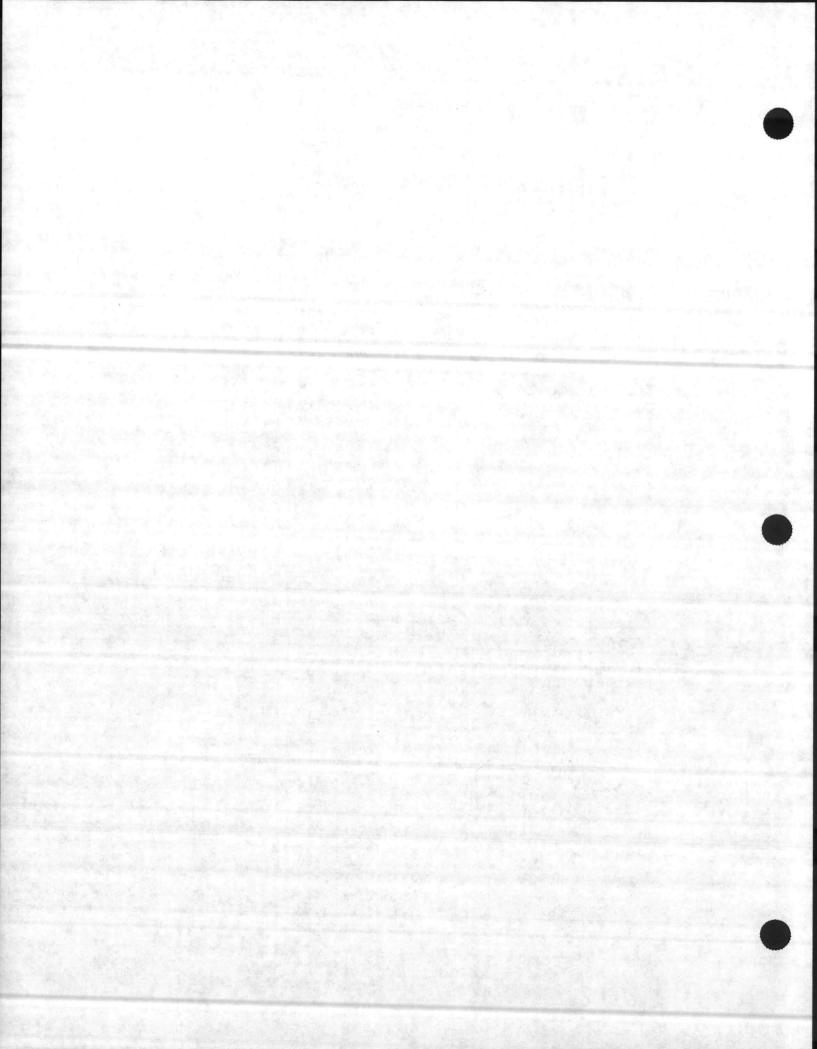
ELAPSED	W S	WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
9.6000	7.350	7.287	12.734	12.984
9.8000	7.356	7.293	12.734	12.968
10.0000	7.343	7.293	12.750	12.984
12.0000	7.350	7.293	12.750	12.984
14.0000	7.350	7.287	12.750	12.984
16.0000	7.350	7.287	12.750	13.000
18.0000	7.356	7.293	12.750	12.984
20.0000	7.356	7.300	12.750	12.984
22.0000	7.356	7.293	12.750	13.000
24.0000	7.356	7.293	12.734	12.984
26.0000	7.356	7.300	12.750	12.984
28.0000	7.356	7.300	12.750	12.984
30.0000	7.356	7.300	12.734	12.968
32.0000	7.356	7.300	12.750	12.984
34.0000	7.362	7.300	12.750	12.984
36.0000	7.356	7.300	12.750	13.000
38.0000	7.362	7.300	12.750	12.984
40.0000	7.369	7.312	12.750	12.984
42.0000	7.362	7.306	12.750	12.984
44.0000	7.356	7.306	12.734	12.984
46.0000	7.362	7.306	12.765	13.000
48.0000	7.369	7.306	12.750	12.984
50.0000	7.356	7.306	12.750	12.984
52.0000	7.362	7.306	12.750	12.984
54.0000	7.362	7.312	12.750	12.984
56.0000	7.369	7.312	12.750	13.000
58.0000	7.375	7.312	12.750	12.984
60.0000	7.375	7.318	12.750	13.000
62.0000	7.369	7.312	12.750	12.984
64.0000	7.382	7.318	12.750	13.000
66.0000	7.375	7.312	12.750	13.000
68.0000	7.382	7.318	12.750	12.984
70.0000	7.382	7.312	12.750	13.000
72.0000	7.375	7.312	12.750	12.984
74.0000	7.388	7.325	12.750	13.000
76.0000	7.382	7.318	12.750	13.000
78.0000	7.375	7.325	12.750	12.984
80.0000	7.382	7.318	12.750	13.000
82.0000	7.382	7.318	12.750	13.000
84.0000	7.382	7.318	12.750	13.000
86.0000	7.388	7.331	12.750	13.015



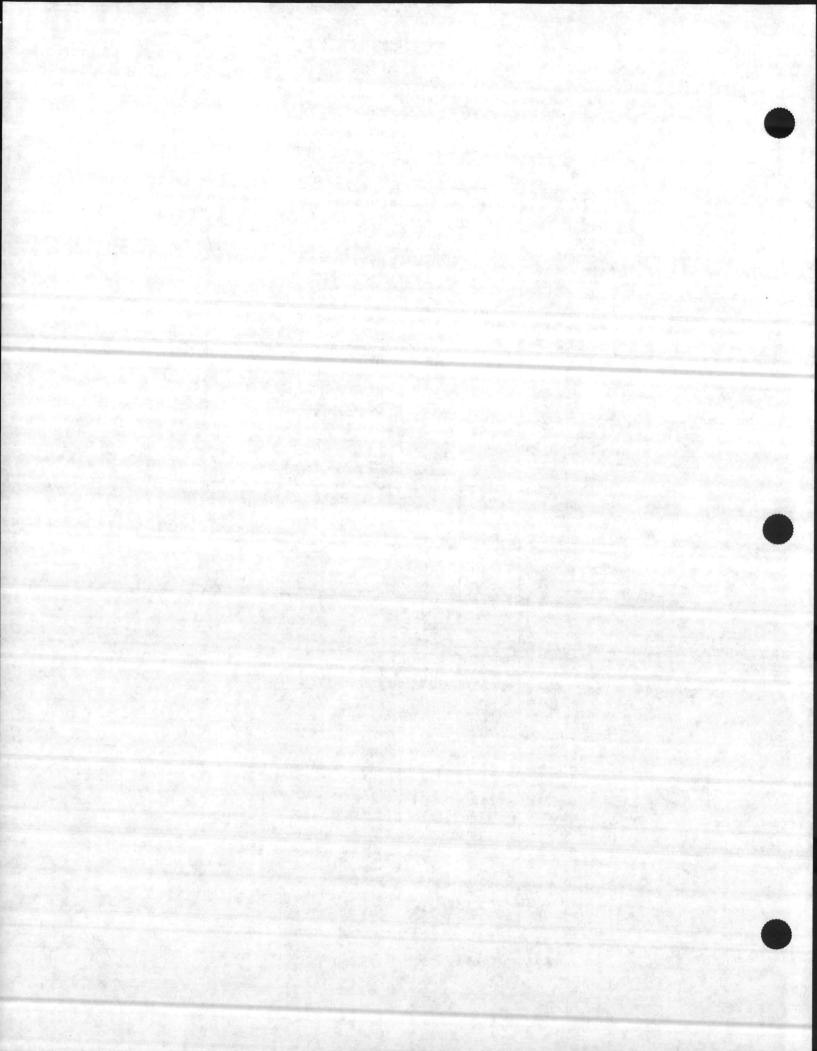
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
	SWL	SWL	SWL	SWL
(MIN)	(FEET)	(FEET)	(FEET)	(FEET)
88.0000	7.388	7.331	12.750	13.000
90.0000	7.388	7.331	12.750	13.000
92.0000	7.394	7.331	12.765	13.000
94.0000	7.388	7.337	12.765	13.000
96.0000	7.394	7.331	12.765	13.000
98.0000	7.394	7.337	12.750	13.000
100.0000	7.394	7.331	12.750	13.000
105.0000	7.407	7.344	12.750	13.000
110.0000	7.401	7.337	12.750	13.000
115.0000	7.401	7.331	12.750	13.000
120.0000	7.407	7.337	12.750	13.000
125.0000	7.407	7.344	12.750	12.984
130.0000	7.407	7.344	12.750	13.000
135.0000	7.407	7.350	12.750	13.000
140.0000	7.414	7.356	12.750	13.000
145.0000	7.414	7.350	12.750	13.000
150.0000	7.414	7.356	12.750	13.000
		7.356	12.750	13.000
155.0000	7.420		12.750	13.000
160.0000	7.426	7.356	12.750	13.000
165.0000	7.426	7.363		13.000
170.0000	7.426	7.369	12.750	
175.0000	7.433	7.369	12.750	13.015
180.0000	7.433	7.381	12.750	13.000
185.0000	7.439	7.381	12.734	12.984
190.0000	7.433	7.381	12.750	13.015
195.0000	7.439	7.388	12.765	13.000
200.0000	7.439	7.394	12.765	13.000
205.0000	7.446	7.394	12.765	13.000
210.0000	7.452	7.400	12.765	13.015
215.0000	7.452	7.407	12.750	13.015
220.0000	7.458	7.413	12.750	13.015
225.0000	7.452	7.407	12.750	13.000
230.0000	7.452	7.407	12.765	13.015
235.0000	7.458	7.413	12.750	13.000
240.0000	7.465	7.419	12.765	13.000
245.0000	7.465	7.426	12.765	13.000
250.0000	7.465	7.438	12.750	13.015
255.0000	7.465	7.445	12.765	13.015
260.0000	7.471	7.438	12.765	13.015
265.0000	7.471	7.445	12.765	13.015
270.0000	7.478	7.457	12.765	13.015



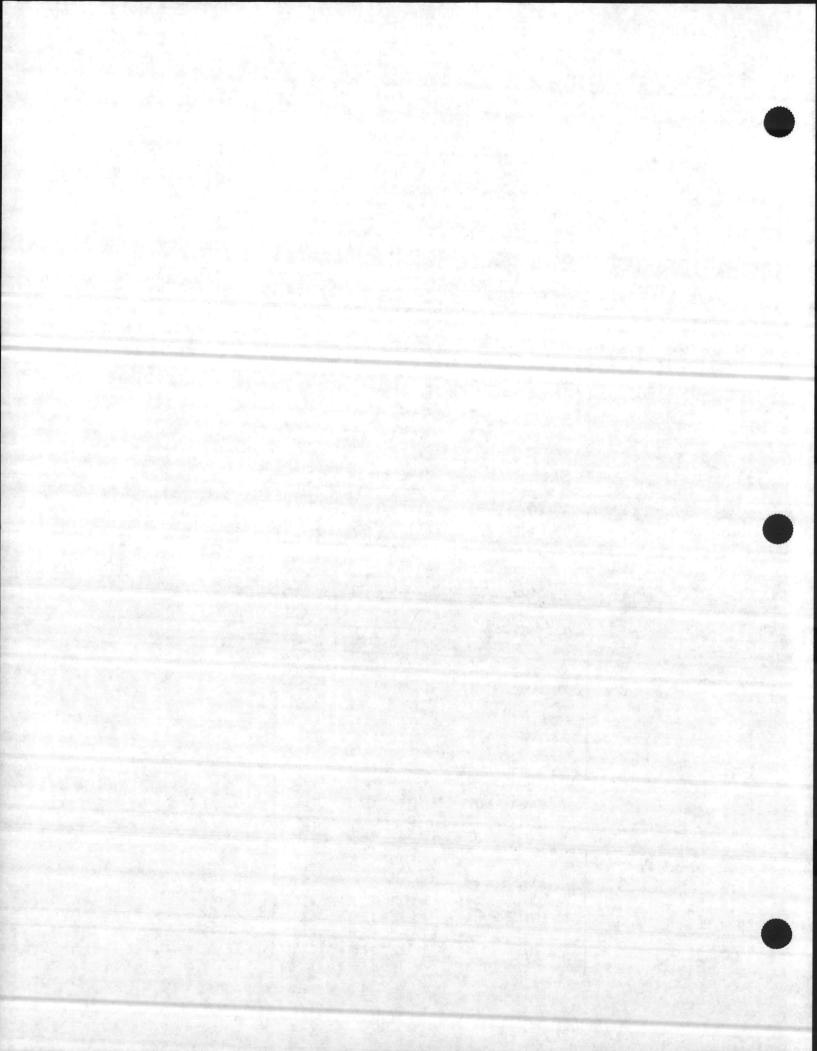
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
275.0000	7.478	7.457	12.765	13.015
280.0000	7.484	7.463	12.765	13.031
285.0000	7.484	7.463	12.765	13.031
290.0000	7.490	7.470	12.750	13.031
295.0000	7.497	7.470	12.781	13.000
300.0000	7.490	7.482	12.765	13.031
305.0000	7.497	7.482	12.765	13.015
310.0000	7.497	7.482	12.750	13.015
315.0000	7.497	7.482	12.765	13.015
320.0000	7.510	7.495	12.765	13.015
325.0000	7.503	7.495	12.765	13.015
330.0000	7.516	7.501	12.765	13.015
335.0000	7.516	7.508	12.765	13.031
340.0000	7.516	7.514	12.765	13.031
345.0000	7.522	7.520	12.765	13.031
350.0000	7.522	7.520	12.781	13.031
355.0000	7.529	7.533	12.781	13.031
360.0000	7.529	7.533	12.765	13.031
365.0000	7.529	7.533	12.781	13.031
370.0000	7.535	7.539	12.781	13.031
375.0000	7.535	7.545	12.765	13.031
380.0000	7.542	7.552	12.781	13.031
385.0000	7.548	7.558	12.781	13.031
390.0000	7.548	7.564	12.781	13.031
395.0000	7.554	7.571	12.781	13.046
400.0000	7.554	7.577	12.781	13.046
405.0000	7.554	7.577	12.781	13.031
410.0000	7.561	7.583	12.781	13.031
415.0000	7.567	7.583	12.781	13.046
420.0000	7.567	7.596	12.781	13.046
425.0000	7.567	7.602	12.796	13.046
430.0000	7.574	7.602	12.781	13.046
435.0000	7.586	7.615	12.781	13.046
440.0000	7.580	7.615	12.796	13.046
445.0000	7.586	7.621	12.796	13.046
450.0000	7.586	7.621	12.781	13.046
455.0000	7.593	7.627	12.796	13.046
460.0000	7.599	7.634	12.781	13.046
465.0000	7.599	7.640	12.781	13.046
470.0000	7.599	7.646	12.796	13.046
475.0000	7.606	7.646	12.781	13.046



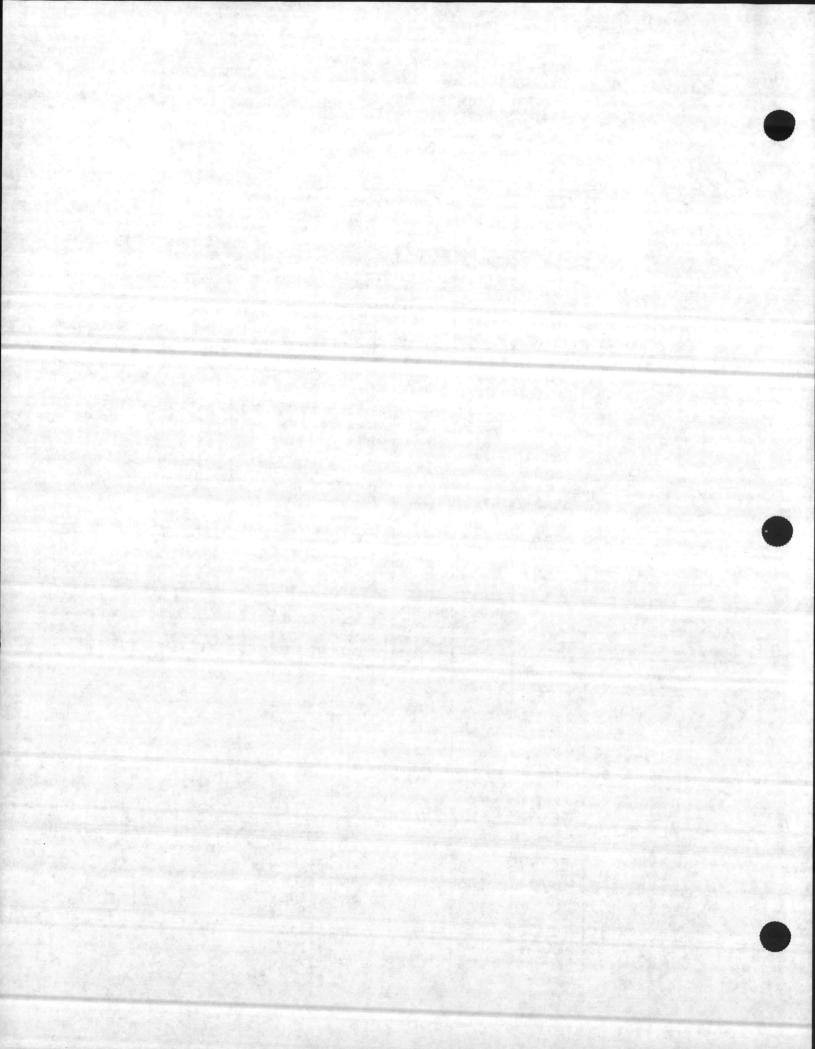
ELAPSED	WELL NUMBER			
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
(IVIIIV)	(PEET)	(ILLI)	(ILLI)	(I LLI)
480.0000	7.606	7.646	12.781	13.062
485.0000	7.606	7.653	12.796	13.046
490.0000	7.612	7.659	12.796	13.062
495.0000	7.618	7.659	12.796	13.046
500.0000	7.618	7.659	12.796	13.046
505.0000	7.618	7.659	12.781	13.046
510.0000	7.625	7.665	12.796	13.046
515.0000	7.625	7.672	12.796	13.046
520.0000	7.625	7.672	12.796	13.046
525.0000	7.631	7.684	12.796	13.062
530.0000	7.631	7.691	12.796	13.062
535.0000	7.638	7.697	12.796	13.062
540.0000	7.638	7.697	12.796	13.062
545.0000	7.644	7.703	12.796	13.046
550.0000	7.644	7.697	12.796	13.062
555.0000	7.644	7.703	12.796	13.062
560.0000	7.650	7.709	12.796	13.062
565.0000	7.650	7.716	12.812	13.046
570.0000	7.650	7.716	12.796	13.062
575.0000	7.657	7.722	12.796	13.062
580.0000	7.650	7.722	12.796	13.062
585.0000	7.657	7.722	12.796	13.046
590.0000	7.657	7.728	12.796	13.062
595.0000	7.663	7.728	12.812	13.062
600.0000	7.663	7.728	12.796	13.062
605.0000	7.670	7.735	12.796	13.062
610.0000	7.670	7.735	12.796	13.062
615.0000	7.670	7.741	12.796	13.062
620.0000	7.670	7.741	12.796	13.062
625.0000	7.676	7.747	12.796	13.062
630.0000	7.676	7.747	12.796	13.062
635.0000	7.676	7.754	12.812	13.062
640.0000	7.676	7.754	12.796	13.062
645.0000	7.683	7.760	12.812	13.046
650.0000	7.683	7.760	12.812	13.062
655.0000	7.689	7.766	12.812	13.062
660.0000	7.689	7.772	12.812	13.062
665.0000	7.689	7.772	12.812	13.062
670.0000	7.689	7.779	12.812	13.062
675.0000	7.695	7.772	12.812	13.062
680.0000	7.695	7.772	12.812	13.062



ELAPSED	WELL NUMBER			
TIME	P-1	24-1	24-2	24-3
	SWL	SWL	SWL	SWL
(MIN)	(FEET)	(FEET)	(FEET)	(FEET)
685.0000	7.695	7.772	12.812	13.078
690,0000	7.702	7.779	12.812	13.062
695,0000	7.695	7.779	12.812	13.062
700.0000	7.702	7.785	12.812	13.078
705.0000	7.702	7.785	12.812	13.062
710.0000	7.695	7.791	12.812	13.062
715.0000	7.708	7.785	12.812	13.062
720.0000	7.708	7.785	12.812	13.078
725.0000	7.702	7.791	12.812	13.078
730.0000	7.708	7.791	12.812	13.078
735.0000	7.708	7.798	12.812	13.078
740.0000	7.715	7.798	12.828	13.078
745.0000	7.715	7.798	12.812	13.078
750,0000	7.715	7.804	12.812	13.078
755.0000	7.721	7.804	12.812	13.078
760.0000	7.721	7.810	12.812	13.078
765.0000	7.715	7.810	12.812	13.078
770.0000	7.721	7.810	12.828	13.078
775.0000	7.721	7.810	12.828	13.078
780.0000	7.721	7.810	12.812	13.078
785.0000	7.721	7.810	12.812	13.078
790.0000	7.727	7.810	12.812	13.078
795.0000	7.727	7.817	12.812	13.078
800.0000	7.727	7.817	12.812	13.078
805.0000	7.721	7.817	12.812	13.078
810.0000	7.727	7.817	12.812	13.078
815.0000	7.727	7.817	12.812	13.078
820.0000	7.727	7.817	12.828	13.078
825.0000	7.727	7.817	12.812	13.078
830.0000	7.727	7.817	12.828	13.078
835.0000	7.727	7.817	12.828	13.078
840.0000	7.727	7.823	12.828	13.078
845.0000	7.727	7.823	12.828	13.078
850.0000	7.727	7.823	12.812	13.078
855.0000	7.734	7.823	12.828	13.078
860.0000	7.734	7.823	12.828	13.078
865.0000	7.727	7.823	12.812	13.078
870.0000	7.734	7.823	12.812	13.078
875.0000	7.734	7.823	12.812	13.078
880.0000	7.734	7.823	12.812	13.078
885.0000	7.734	7.823	12.812	13.078



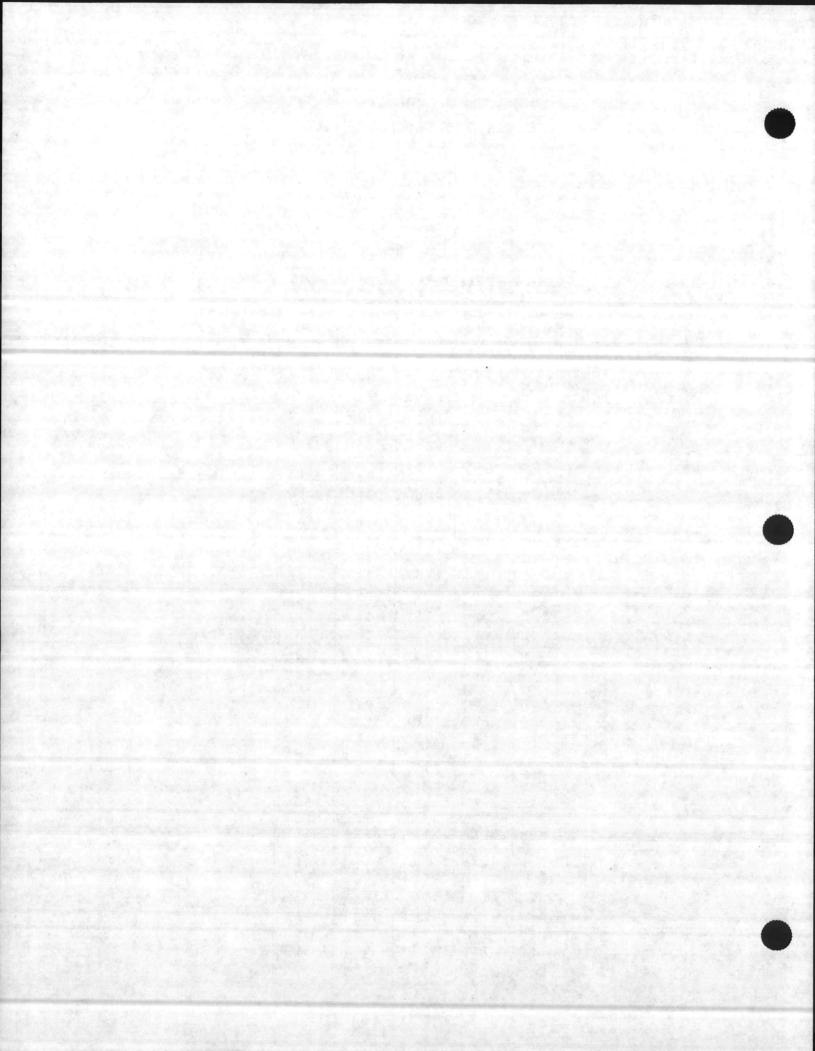
ELAPSED		WELL N	JMBER	Arm.
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
(IVIII t)	(1221)	(1221)	( )	
890.0000	7.734	7.823	12.812	13.078
895.0000	7.734	7.823	12.812	13.078
900.0000	7.734	7.823	12.828	13.078
905.0000	7.734	7.829	12.812	13.078
910.0000	7.734	7.829	12.812	13.062
915.0000	7.734	7.836	12.812	13.078
920.0000	7.734	7.836	12.828	13.078
925.0000	7.740	7.836	12.828	13.062
930.0000	7.740	7.836	12.812	13.078
935.0000	7.740	7.836	12.812	13.078
940.0000	7.740	7.842	12.812	13.078
945.0000	7.740	7.842	12.812	13.078
950.0000	7.740	7.836	12.812	13.078
955.0000	7.740	7.848	12.812	13.078
960.0000	7.740	7.842	12.812	13.078
965.0000	7.747	7.848	12.812	13.078
970.0000	7.747	7.848	12.828	13.078
975.0000	7.747	7.848	12.828	13.078
980.0000	7.747	7.861	12.812	13.078
985.0000	7.747	7.854	12.828	13.078
990.0000	7.747	7.854	12.812	13.078
995.0000	7.747	7.861	12.812	13.078
1000.0000	7.747	7.861	12.828	13.078
1005.0000	7.753	7.861	12.828	13.078
1010.0000	7.753	7.854	12.812	13.078
1015.0000	7.753	7.867	12.812	13.078
1020.0000	7.753	7.867	12.812	13.078
1025.0000	7.753	7.867	12.812	13.078
1030.0000	7.753	7.873	12.828	13.078
1035.0000	7.759	7.867	12.828	13.078
1040.0000	7.759	7.867	12.828	13.078
1045.0000	7.759	7.867	12.812	13.078
1050.0000	7.753	7.867	12.812	13.078
1055.0000	7.759	7.867	12.812	13.078
1060.0000	7.753	7.861	12.812	13.078
1065.0000	7.753	7.861	12.812	13.078
1070.0000	7.753	7.861	12.812	13.078
1075.0000	7.759	7.867	12.812	13.078
1080.0000	7.759	7.867	12.812	13.078
1085.0000	7.759	7.861	12.812	13.062
1090.0000	7.759	7.861	12.812	13.078



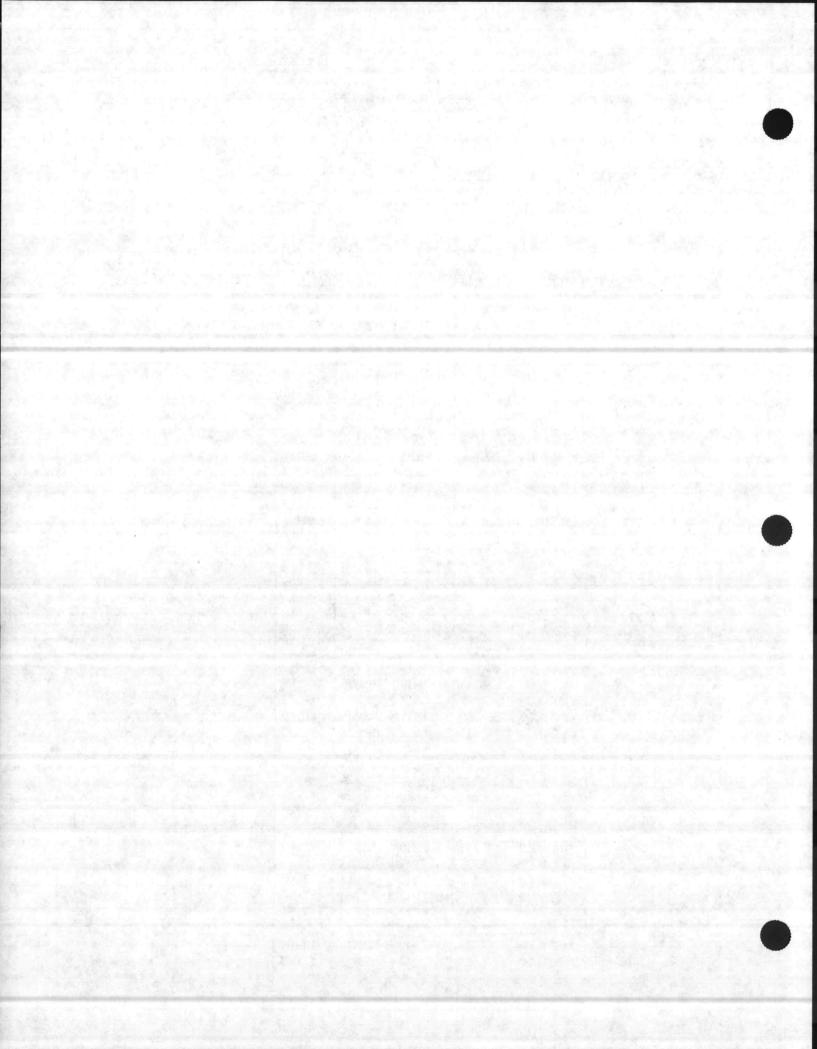
CONTRACT TASK ORDER: 0017 SITE I.D.: CAMP LEJEUNE, HPIA

TEST: CONSTANT RATE DRAWDOWN

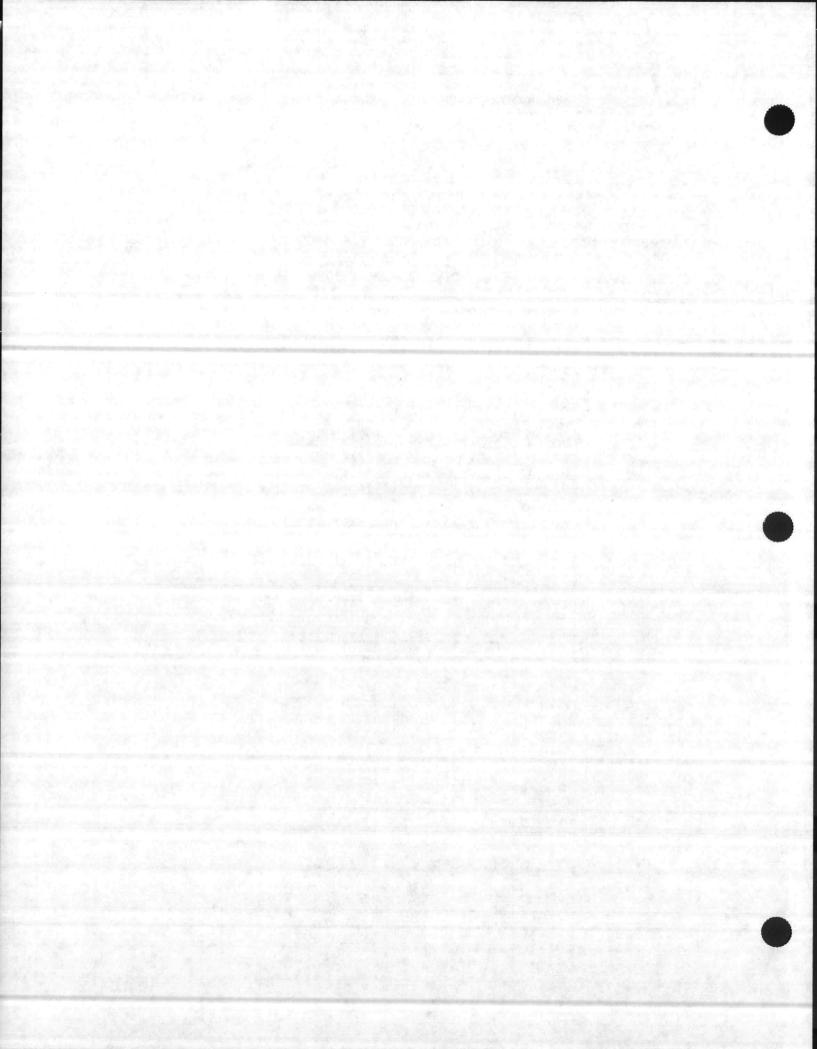
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
1095.0000	7.759	7.861	12.812	13.078
1100.0000	7.759	7.867	12.828	13.078
1105.0000	7.759	7.867	12.812	13.078
1110.0000	7.753	7.867	12.812	13.078
1115.0000	7.759	7.861	12.828	13.078
1120.0000	7.759	7.867	12.828	13.078
1125.0000	7.759	7.867	12.812	13.078
1130.0000	7.759	7.867	12.812	13.078
1135.0000	7.759	7.873	12.812	13.078
1140.0000	7.759	7.873	12.812	13.078
1145.0000	7.759	7.873	12.812	13.078
1150.0000	7.759	7.873	12.812	13.078
1155.0000	7.759	7.873	12.828	13.078
1160.0000	7.766	7.873	12.828	13.078
1165.0000	7.766	7.880	12.812	13.078
1170.0000	7.759	7.880	12.812	13.093
1175.0000	7.766	7.886	12.812	13.078
1180.0000	7.766	7.886	12.812	13.078
1185.0000	7.766	7.880	12.812	13.078
1190.0000	7.766	7.880	12.812	13.078
1195.0000	7.766	7.886	12.812	13.078
1200.0000	7.766	7.892	12.812	13.078
1205.0000	7.766	7.892	12.828	13.078
1210.0000	7.766	7.892	12.812	13.078
1215.0000	7.772	7.892	12.812	13.078
1220.0000	7.772	7.892	12.812	13.078
1225.0000	7.772	7.899	12.828	13.078
1230.0000	7.772	7.899	12.812	13.078
1235.0000	7.772	7.899	12.812	13.078
1240.0000	7.772	7.905	12.812	13.078
1245.0000	7.779	7.905	12.828	13.078
1250.0000	7.779	7.905	12.812	13.078
1255.0000	7.779	7.911	12.812	13.078
1260.0000	7.779	7.911	12.812	13.078
1265.0000	7.779	7.911	12.828	13.093
1270.0000	7.779	7.911	12.828	13.093
1275.0000	7.779	7.918	12.812	13.078
1280.0000	7.779	7.918	12.828	13.078
1285.0000	7.779	7.918	12.828	13.078
1290.0000	7.785	7.918	12.828	13.093
1295.0000	7.785	7.918	12.828	13.078



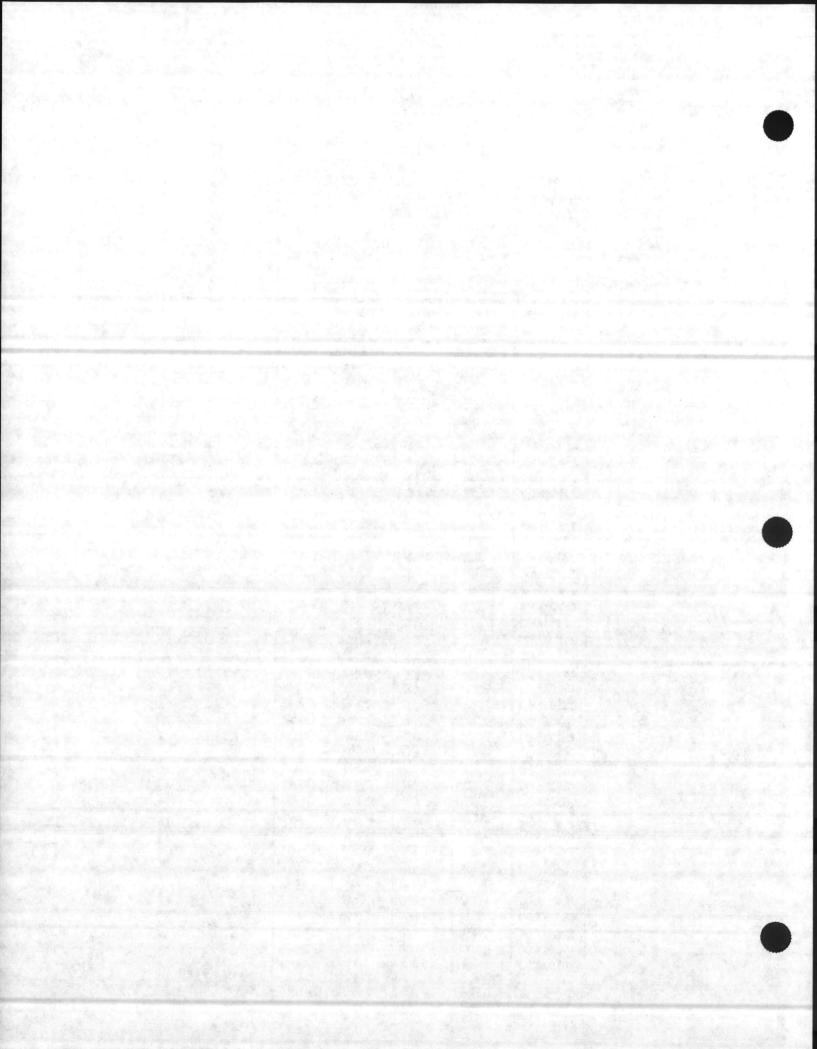
ELAPSED	WELL NUMBER			
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
1300.0000	7.785	7.924	12.812	13.093
1305.0000	7.785	7.924	12.828	13.078
1310.0000	7.785	7.924	12.812	13.093
1315.0000	7.785	7.924	12.828	13.093
1320.0000	7.785	7.924	12.812	13.078
1325.0000	7.791	7.930	12.828	13.078
1330.0000	7.779	7.930	12.828	13.093
1335.0000	7.785	7.930	12.828	13.093
1340.0000	7.785	7.930	12.828	13.078
1345.0000	7.785	7.936	12.828	13.093
1350.0000	7.785	7.930	12.828	13.093
1355.0000	7.785	7.930	12.828	13.093
1360.0000	7.785	7.930	12.828	13.093
1365.0000	7.785	7.930	12.828	13.093
1370.0000	7.785	7.930	12.828	13.093
1375.0000	7.779	7.930	12.828	13.093
1380.0000	7.785	7.936	12.828	13.093
1385.0000	7.785	7.936	12.828	13.093
1390.0000	7.785	7.936	12.828	13.093
1395.0000	7.785	7.936	12.828	13.093
1400.0000	7.785	7.943	12.843	13.109
1405.0000	7.785	7.943	12.828	13.093
1410.0000	7.785	7.943	12.828	13.093
1415.0000	7.785	7.943	12.828	13.109
1420.0000	7.785	7.943	12.843	13.093
1425.0000	7.785	7.949	12.843	13.109
1430.0000	7.785	7.943	12.828	13.093
1435.0000	7.785	7.943	12.828	13.093
1440.0000	7.785	7.943	12.843	13.093
1445.0000	7.785	7.949	12.843	13.093
1450.0000	7.785	7.949	12.843	13.093
1455.0000	7.785	7.949	12.843	13.093
1460.0000	7.785	7.949	12.843	13.093
1465.0000	7.785	7.949	12.828	13.093
1470.0000	7.785	7.949	12.843	13.093
1475.0000	7.785	7.943	12.843	13.093
1480.0000	7.785	7.943	12.843	13.093
1485.0000	7.785	7.943	12.843	13.109
1490.0000	7.785	7.943	12.843	13.109
1495.0000	7.785	7.949	12.843	13.109
1500.0000	7.785	7.943	12.843	13.093



ELAPSED	WELL NUMBER			
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
1505 0000	7 705	7.943	12.828	13.109
1505.0000 1510.0000	7.785 7.785	7.943	12.843	13.109
1515.0000	7.785	7.943	12.843	13.109
1520.0000	7.785	7.943	12.843	13.109
1525.0000	7.785	7.936	12.843	13.093
1530.0000	7.779	7.943	12.843	13.109
1535.0000	7.785	7.936	12.843	13.109
1540.0000	7.779	7.930	12.843	13.109
1545.0000	7.779	7.936	12.843	13.109
1550.0000	7.779	7.924	12.843	13.109
1555.0000	7.772	7.924	12.843	13.109
1560.0000	7.772	7.924	12.828	13.109
1565.0000	7.772	7.924	12.843	13.093
1570.0000	7.779	7.918	12.843	13.109
1575.0000	7.772	7.924	12.843	13.109
1580.0000	7.772	7.911	12.843	13.109
1585.0000	7.772	7.918	12.843	13.109
1590.0000	7.766	7.911	12.843	13.109
1595.0000	7.766	7.911	12.843	13.109
1600.0000	7.766	7.905	12.843	13.093
1605.0000	7.766	7.899	12.828	13.093
1610.0000	7.766	7.899	12.828	13.093
1615.0000	7.759	7.899	12.828	13.093
1620.0000	7.759	7.892	12.828	13.093
1625.0000	7.753	7.886	12.828	13.093
1630.0000	7.759	7.886	12.828	13.093
1635.0000	7.753	7.886	12.828	13.093
1640.0000	7.753	7.886	12.828	13.109
1645.0000	7.753	7.886	12.828	13.109
1650.0000	7.747	7.880	12.828	13.093
1655.0000	7.747	7.880	12.828	13.093
1660.0000	7.747	7.880	12.828	13.093
1665.0000	7.747	7.880	12.828	13.093
1670.0000	7.740	7.873	12.828	13.093
1675.0000	7.747	7.873	12.828	13.093
1680.0000	7.740	7.873	12.828	13.093
1685.0000	7.740	7.873	12.828	13.093
1690.0000	7.734	7.867	12.812	13.093
1695.0000	7.740	7.867	12.828	13.093
1700.0000	7.740	7.867	12.828	13.093
1705.0000	7.734	7.861	12.812	13.078



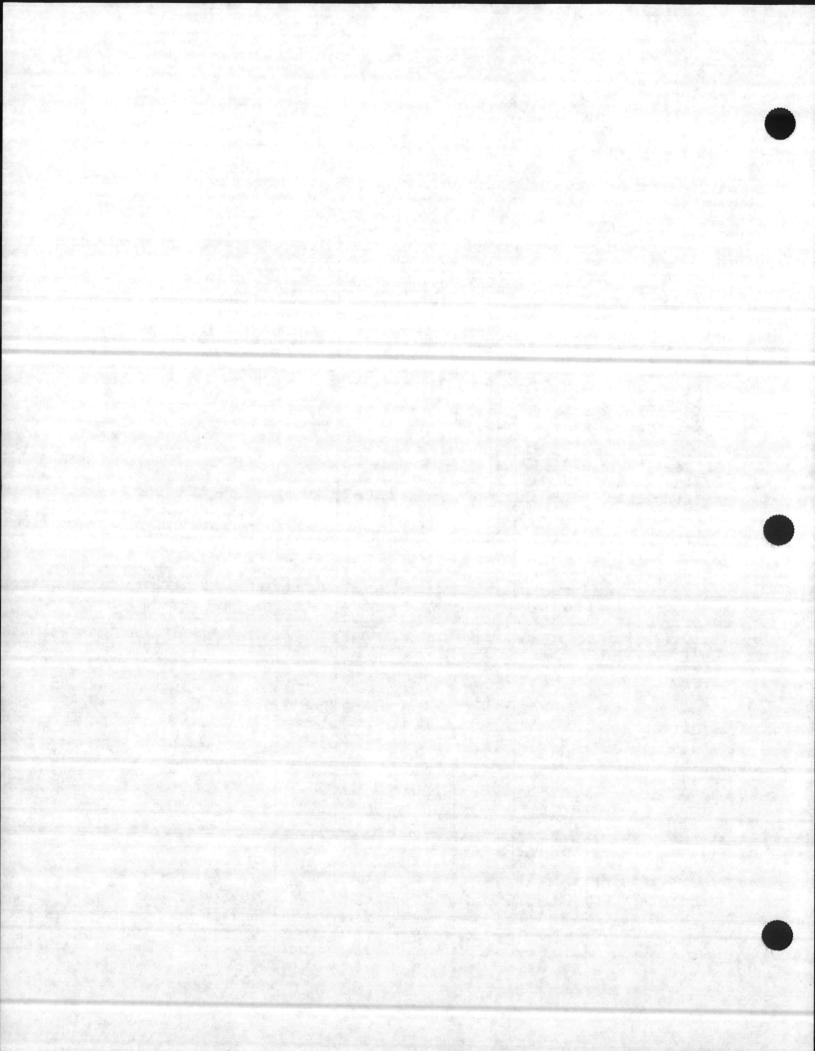
ELAPSED TIME (MIN)	WELL NUMBER			
	P-1	24-1 SWL (FEET)	24-2 SWL (FEET)	24-3 SWL (FEET)
	SWL (FEET)			
1710.0000	7.734	7.861	12.828	13.093
1715.0000	7.734	7.861	12.828	13.093
1713.0000	7.734	7.861	12.823	13.093
1725.0000	7.727	7.854	12.812	13.078
1730.0000	7.727	7.854	12.812	13.078
1735.0000	7.727	7.854	12.812	13.078
1740.0000	7.727	7.854	12.812	13.093
1745.0000	7.727	7.854	12.812	13.078
1750.0000	7.727	7.854	12.812	13.093
1755.0000	7.727	7.854	12.812	13.093
1760.0000	7.727	7.861	12.812	13.093
1765.0000	7.727	7.861	12.812	13.093
1770.0000	7.727	7.861	12.812	13.093
1775.0000	7.727	7.861	12.812	13.093
1780.0000	7.727	7.861	12.828	13.078
1785.0000	7.727	7.861	12.812	13.093
1790.0000	7.727	7.861	12.812	13.078
1795.0000	7.727	7.861	12.812	13.078
1800.0000	7.727	7.861	12.828	13.093
1805.0000	7.727	7.867	12.828	13.093
1810.0000	7.727	7.867	12.812	13.093
1815.0000	7.727	7.867	12.812	13.093
1820.0000	7.727	7.861	12.812	13.093
1825.0000	7.727	7.867	12.812	13.093
1830.0000	7.727	7.867	12.812	13.093
1835.0000	7.727	7.867	12.812	13.093
1840.0000	7.734	7.873	12.828	13.093
1845.0000	7.727	7.873	12.828	13.093
1850.0000	7.727	7.873	12.812	13.093
1855.0000	7.727	7.873	12.812	13.093
1860.0000	7.734	7.880	12.828	13.093
1865.0000	7.734	7.880	12.812	13.093
1870.0000	7.734	7.880	12.812	13.078
1875.0000	7.734	7.880	12.828	13.093
1880.0000	7.734	7.880	12.812	13.093
1885.0000	7.734	7.880	12.812	13.093
1890.0000	7.734	7.886	12.812	13.093
1895.0000	7.734	7.880	12.796	13.078
1900.0000	7.734	7.880	12.730	13.093
1905.0000	7.734	7.886	12.812	13.078
1910.0000	7.740	7.886	12.812	13.093



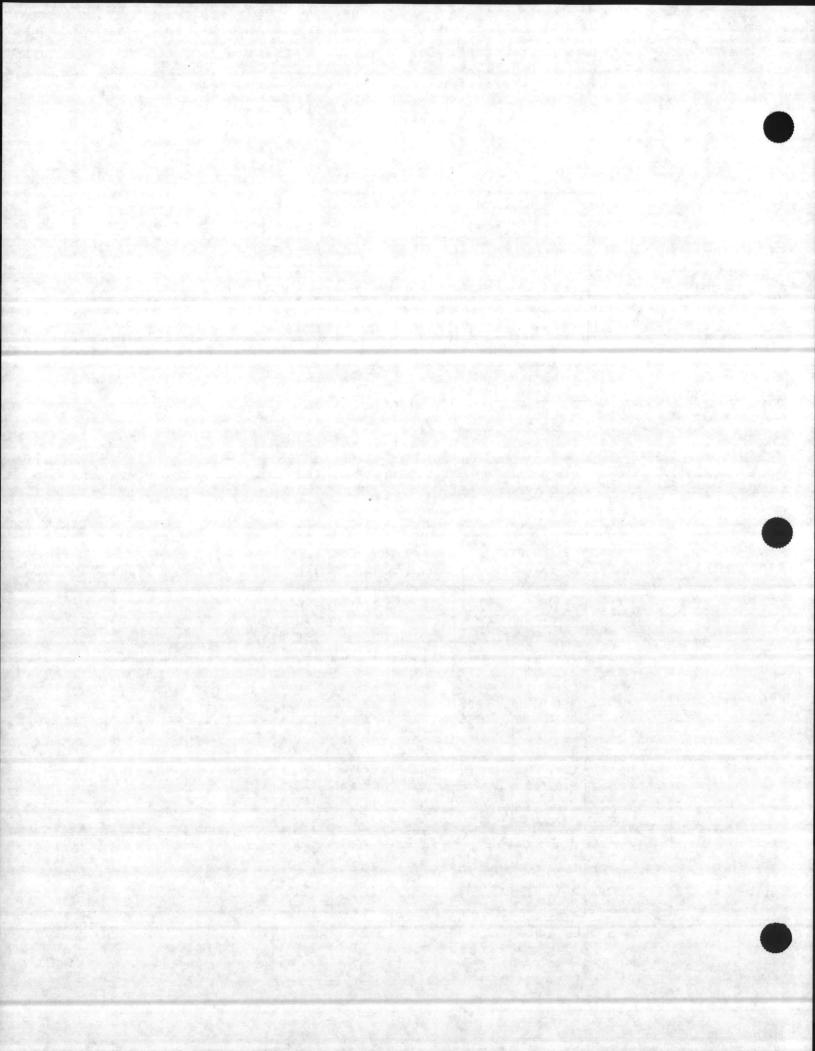
CONTRACT TASK ORDER: 0017 SITE I.D.: CAMP LEJEUNE, HPIA

TEST: CONSTANT RATE DRAWDOWN

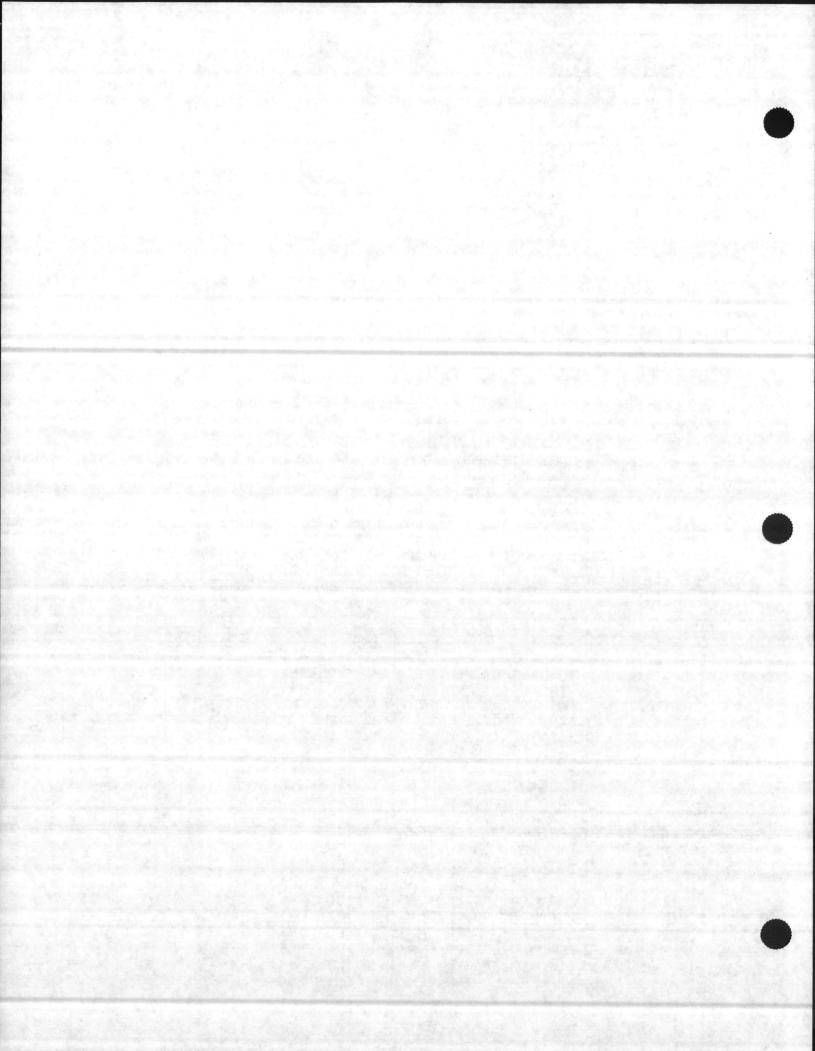
ELAPSED	WELL NUMBER			
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
1915.0000	7.740	7.892	12.812	13.093
1920.0000	7.740	7.892	12.812	13.078
1925.0000	7.740	7.899	12.812	13.093
1930.0000	7.747	7.899	12.812	13.093
1935.0000	7.747	7.899	12.812	13.078
1940.0000	7.747	7.905	12.812	13.093
1945.0000	7.747	7.905	12.812	13.093
1950.0000	7.747	7.911	12.812	13.093
1955.0000	7.747	7.905	12.812	13.093
1960.0000	7.747	7.911	12.812	13.093
1965.0000	7.747	7.911	12.812	13.093
1970.0000	7.753	7.911	12.812	13.093
1975.0000	7.753	7.911	12.812	13.093
1980.0000	7.753	7.911	12.812	13.078
1985.0000	7.753	7.911	12.812	13.078
1990.0000	7.753	7.918	12.812	13.093
1995.0000	7.753	7.911	12.812	13.078
2000.0000	7.753	7.918	12.812	13.078
2005.0000	7.753	7.918	12.812	13.078
2010.0000	7.753	7.924	12.812	13.093
2015.0000	7.753	7.918	12.812	13.078
2020.0000	7.759	7.918	12.812	13.078
2025.0000	7.759	7.918	12.812	13.078
2030.0000	7.759	7.918	12.812	13.093
2035.0000	7.759	7.924	12.812	13.093
2040.0000	7.759	7.918	12.812	13.093
2045.0000	7.759	7.924	12.812	13.093
2050.0000	7.759	7.924	12.812	13.078
2055.0000	7.766	7.924	12.812	13.078
2060.0000	7.759	7.924	12.812	13.078
2065.0000	7.766	7.924	12.812	13.07
2070.0000	7.766	7.924	12.812	13.093
2075.0000	7.766	7.924	12.812	13.093
2080.0000	7.766	7.924	12.812	13.09
2085.0000	7.766	7.924	12.812	13.07
2090.0000	7.766	7.924	12.812	13.07
2095.0000	7.766	7.930	12.812	13.07
2100.0000	7.766	7.924	12.812	13.07
2105.0000	7.766	7.924	12.812	13.07
2110.0000	7.766	7.924	12.812	13.078
2115.0000	7.766	7.924	12.812	13.078



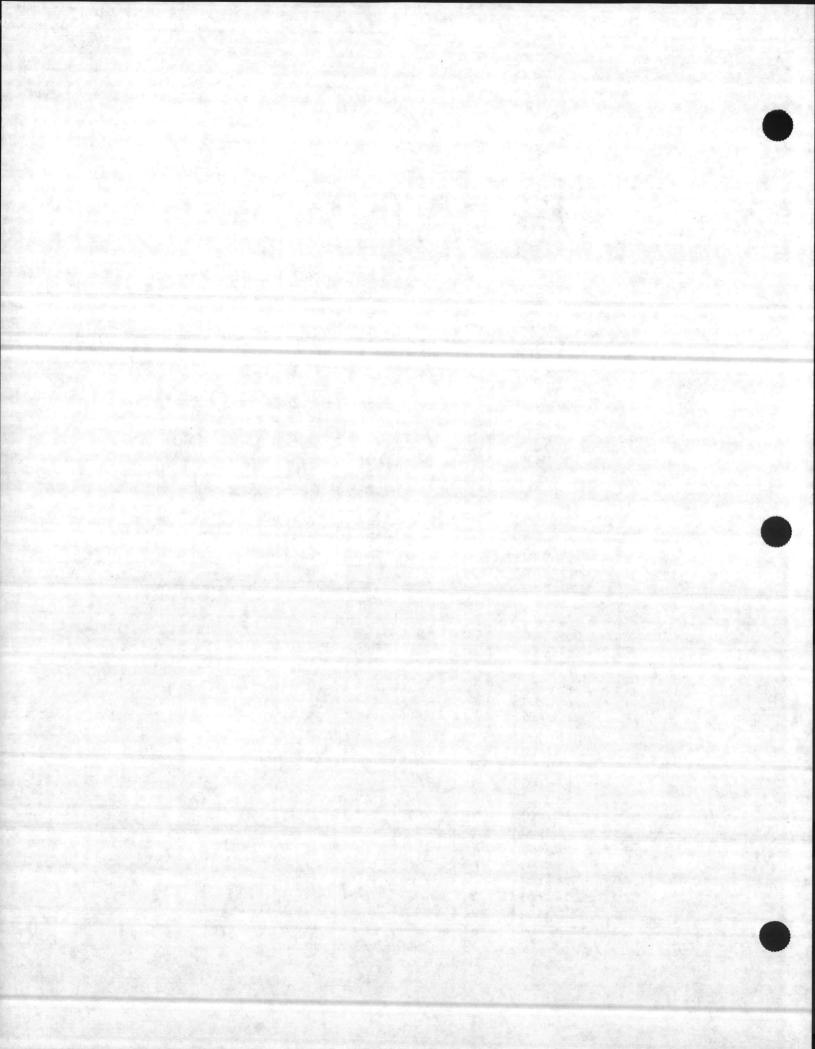
ELAPSED TIME (MIN)	WELL NUMBER			
	P-1	24-1 SWL (FEET)	24-2 SWL (FEET)	24-3 SWL (FEET)
	SWL (FEET)			
F / No Falls	la la gran travalla di sa		real second	10.000
2120.0000	7.766	7.924	12.812	13.093
2125.0000	7.766	7.924	12.812	13.078
2130.0000	7.766	7.924	12.812	13.078
2135.0000	7.766	7.930	12.812	13.093 13.078
2140.0000	7.766	7.924	12.796	13.078
2145.0000	7.766	7.930	12.812	13.078
2150.0000	7.766	7.924	12.796 12.796	13.078
2155.0000	7.766	7.924 7.930	12.790	13.078
2160.0000	7.766		12.812	13.078
2165.0000	7.766	7.930 7.924	12.812	13.078
2170.0000	7.766 7.766	7.924	12.812	13.078
2175.0000	7.772	7.930	12.796	13.078
2180.0000	7.766	7.930	12.790	13.078
2185.0000 2190.0000	7.766	7.930	12.812	13.078
2195.0000	7.766	7.930	12.796	13.078
2200.0000	7.766	7.930	12.790	13.078
2205.0000	7.772	7.930	12.812	13.078
2210.0000	7.772	7.930	12.812	13.078
2215.0000	7.772	7.930	12.812	13.078
2220.0000	7.772	7.930	12.812	13.078
2225.0000	7.772	7.930	12.812	13.078
2230.0000	7.772	7.930	12.812	13.078
2235.0000	7.766	7.930	12.812	13.078
2240.0000	7.766	7.924	12.812	13.078
2245.0000	7.766	7.924	12.796	13.078
2250.0000	7.766	7.924	12.812	13.078
2255.0000	7.766	7.924	12.796	13.078
2260.0000	7.766	7.924	12.796	13.078
2265.0000	7.766	7.924	12.796	13.078
2270.0000	7.766	7.924	12.796	13.062
2275.0000	7.766	7.924	12.796	13.062
2280.0000	7.766	7.924	12.796	13.062
2285.0000	7.766	7.924	12.796	13.078
2290.0000	7.766	7.930	12.796	13.078
2295.0000	7.766	7.924	12.796	13.078
2300.0000	7.766	7.924	12.796	13.078
2305.0000	7.766	7.924	12.796	13.062
2310.0000	7.766	7.924	12.796	13.078
2315.0000	7.766	7.930	12.796	13.062
2320.0000	7.766	7.930	12.796	13.078



ELAPSED	WELL NUMBER			
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
			THE PROPERTY.	
2325.0000	7.766	7.924	12.796	13.078
2330.0000	7.766	7.930	12.796	13.062
2335.0000	7.766	7.930	12.796	13.062
2340.0000	7.766	7.930	12.796	13.078
2345.0000	7.766	7.924	12.796	13.078
2350.0000	7.766	7.924	12.796	13.062
2355.0000	7.766	7.924	12.796	13.078
2360.0000	7.766	7.924	12.796	13.062
2365.0000	7.766	7.924	12.781	13.062
2370.0000	7.759	7.918	12.781	13.062
2375.0000	7.759	7.918	12.796	13.062
2380.0000	7.759	7.918	12.781	13.062
2385.0000	7.759	7.918	12.781	13.062
2390.0000	7.759	7.918	12.781	13.062
2395.0000	7.759	7.918	12.781	13.062
2400.0000	7.759	7.918	12.781	13.062
2405.0000	7.766	7.924	12.796	13.062
2410.0000	7.759	7.918	12.781	13.046
2415.0000	7.759	7.918	12.796	13.062
2420.0000	7.759	7.924	12.781	13.062
2425.0000	7.759	7.924	12.796	13.062
2430.0000	7.759	7.924	12.796	13.062
2435.0000	7.766	7.930	12.796	13.062
2440.0000	7.759	7.930	12.781	13.062
2445.0000	7.759	7.924	12.781	13.062
2450.0000	7.759	7.930	12.781	13.062
2455.0000	7.759	7.930	12.781	13.062
2460.0000	7.759	7.930	12.781	13.046
2465.0000	7.759	7.930	12.781	13.062
2470.0000	7.759	7.936	12.781	13.062
2475.0000	7.759	7.930	12.781	13.062
2480.0000	7.759	7.930	12.781	13.046
2485.0000	7.759	7.936	12.781	13.046
2490.0000	7.766	7.936	12.781	13.062
2495.0000	7.759	7.936	12.781	13.062
2500.0000	7.766	7.936	12.781	13.046
2505.0000	7.759	7.936	12.781	13.040
2510.0000	7.766	7.936	12.781	13.046
2515.0000	7.766	7.943	12.781	13.062
2520.0000	7.766	7.943	12.781	13.046
2525.0000	7.766	7.936	12.781	13.062



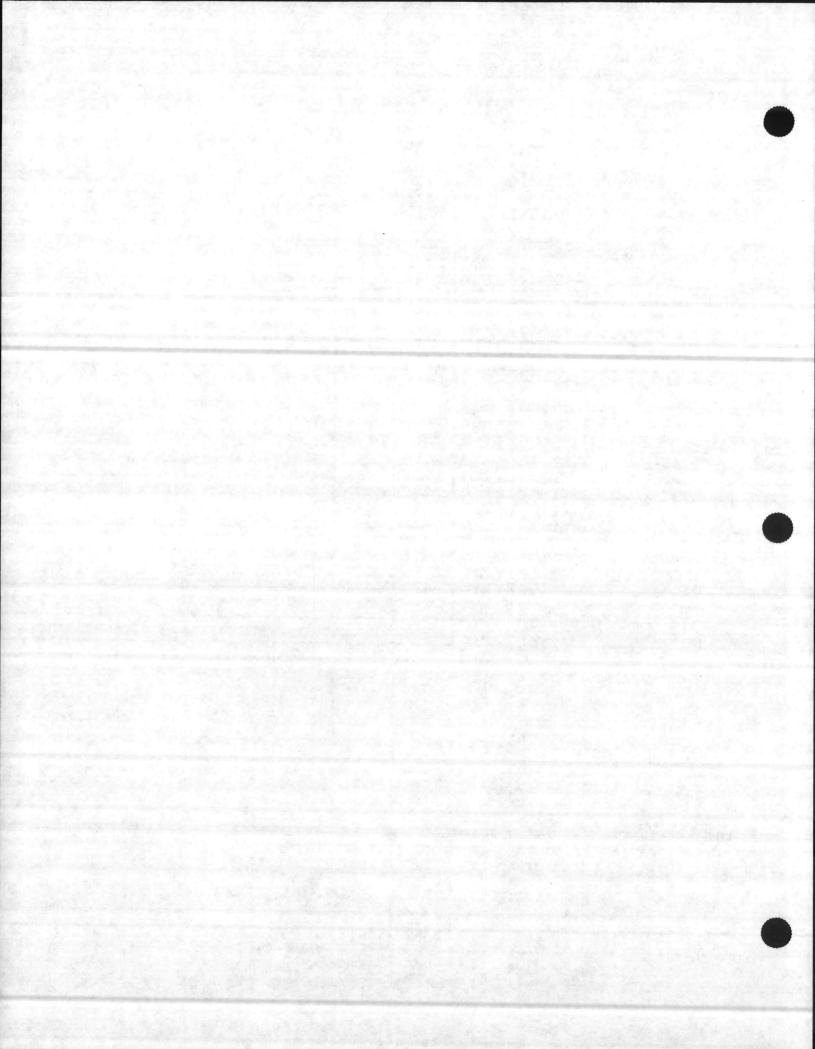
ELAPSED	WELL NUMBER					
TIME	P-1	24-1	24-2	24-3		
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)		
2530.0000	7.766	7.936	12.781	13.046		
2535.0000	7.759	7.936	12.781	13.062		
2540.0000	7.759	7.936	12.781	13.062		
2545.0000	7.759	7.936	12.781	13.046		
2550.0000	7.759	7.943	12.781	13.046		
2555.0000	7.766	7.943	12.781	13.046		
2560.0000	7.759	7.943	12.781	13.046		
2565.0000	7.759	7.943	12.781	13.046		
2570.0000	7.759	7.943	12.781	13.046		
2575.0000	7.759	7.943	12.781	13.046		
2580.0000	7.759	7.943	12.765	13.046		
2585.0000	7.759	7.949	12.781	13.046		
2590.0000	7.766	7.955	12.781	13.046		
2595.0000	7.766	7.949	12.781	13.062		
2600.0000	7.766	7.949	12.781	13.046		
2605.0000	7.766	7.949	12.781	13.046		
2610.0000	7.766	7.949	12.781	13.046		
2615.0000	7.766	7.955	12.781	13.046		
2620.0000	7.759	7.955	12.781	13.046		
2625.0000	7.766	7.955	12.781	13.046		
2630.0000	7.759	7.955	12.765	13.046		
2635.0000	7.766	7.955	12.781	13.046		
2640.0000	7.766	7.955	12.781	13.046		
2645.0000	7.766	7.955	12.781	13.046		
2650.0000	7.766	7.955	12.781	13.046		
2655.0000	7.759	7.949	12.781	13.046		
2660.0000	7.766	7.949	12.781	13.046		
2665.0000	7.766	7.955	12.781	13.046		
2670.0000	7.759	7.949	12.781	13.046		
2675.0000	7.766	7.955	12.781	13.046		
2680.0000	7.766	7.962	12.781	13.046		
2685.0000	7.766	7.962	12.781	13.046		
2690.0000	7.766	7.962	12.765	13.046		
2695.0000	7.766	7.968	12.781	13.046		
2700.0000	7.766	7.968	12.781	13.046		
2705.0000	7.766	7.968	12.781	13.046		
2710.0000	7.766	7.968	12.781	13.046		
2715.0000	7.766	7.968	12.781	13.046		
2720.0000	7.766	7.968	12.781	13.046		
2725.0000	7.766	7.968	12.781	13.046		
2730.0000	7.772	7.968	12.781	13.046		



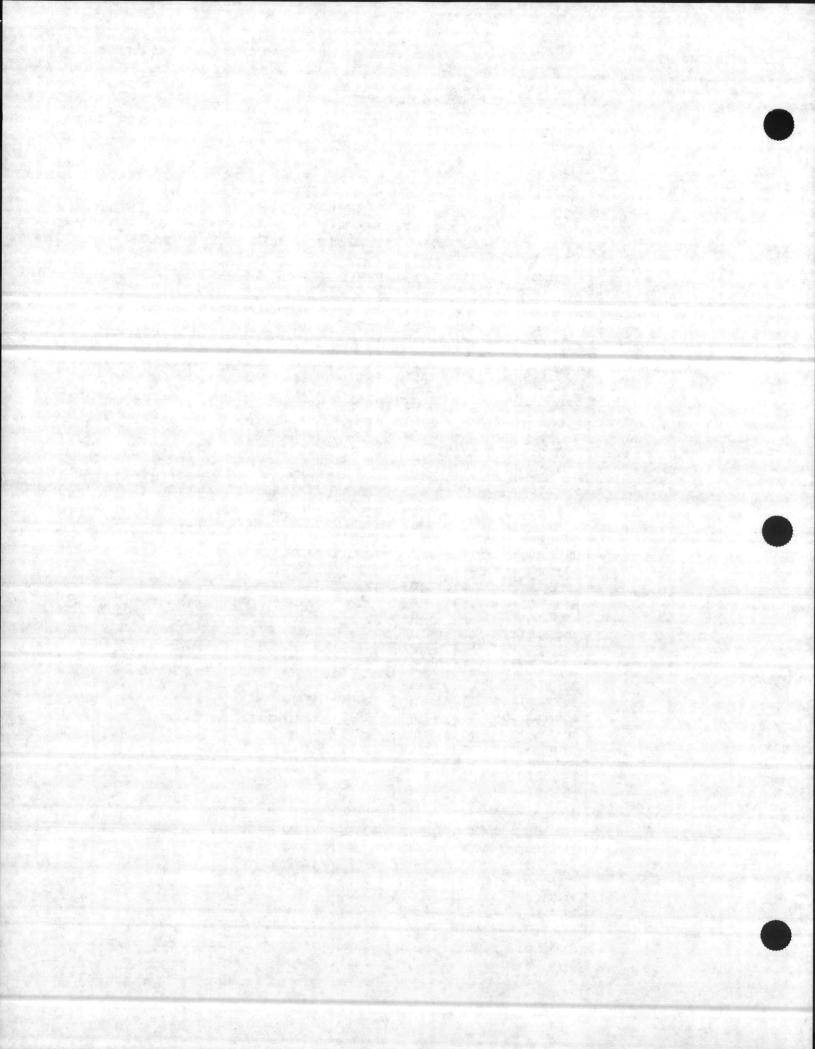
CONTRACT TASK ORDER: 0017 SITE I.D.: CAMP LEJEUNE, HPIA

TEST: CONSTANT RATE DRAWDOWN FLOW RATE: 1.5 GPM

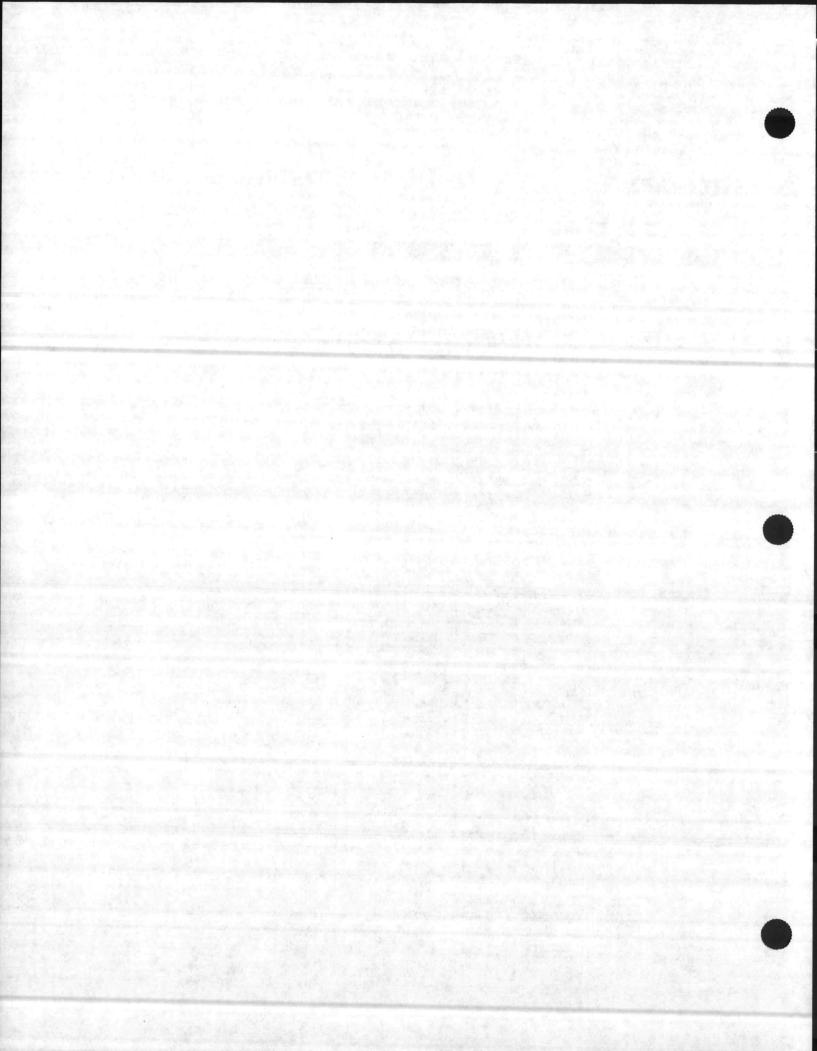
ELAPSED	WELL NUMBER					
TIME	P-1	24-1	24-2	24-3		
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)		
			KATON TAN			
2735.0000	7.766	7.968	12.781	13.046		
2740.0000	7.772	7.974	12.781	13.046		
2745.0000	7.772	7.974	12.781	13.046		
2750.0000	7.772	7.981	12.781	13.046		
2755.0000	7.772	7.981	12.781	13.046		
2760.0000	7.772	7.987	12.781	13.062		
2765.0000	7.772	7.987	12.781	13.046		
2770.0000	7.779	7.987	12.781	13.062		
2775.0000	7.772	7.987	12.781	13.062		
2780.0000	7.779	7.987	12.781	13.062		
2785.0000	7.772	7.987	12.781	13.046		
2790.0000	7.772	7.987	12.781	13.046		
2795.0000	7.779	7.993	12.781	13.062		
2800.0000	7.779	7.987	12.781	13.046		
2805.0000	7.772	7.993	12.781	13.046		
2810.0000	7.779	8.000	12.781	13.062		
2815.0000	7.779	7.993	12.796	13.062		
2820.0000	7.779	7.993	12.781	13.062		
2825.0000	7.779	8.000	12.796	13.062		
2830.0000	7.779	7.993	12.796	13.062		
2835.0000	7.779	7.993	12.796	13.062		
2840.0000	7.779	8.000	12.796	13.062		
2845.0000	7.779	8.000	12.796	13.062		
2850.0000	7.779	8.000	12.796	13.062		
2855.0000	7.779	8.000	12.796	13.062		
2860.0000	7.779	8.000	12.796	13.062		
2865.0000	7.779	8.006	12.796	13.062		
2870.0000	7.779	8.012	12.796	13.062		
2875.0000	7.785	8.012	12.796	13.078		
2880.0000	7.785	8.025	12.796	13.078		
2885.0000	7.791	8.018	12.796	13.078		
2890.0000	7.791	8.025	12.796	13.062		
2895.0000	7.791	8.025	12.812	13.078		
2900.0000	7.791	8.025	12.812	13.078		
2905.0000	7.791	8.031	12.796	13.078		
2910.0000	7.791	8.031	12.812	13.078		
2915.0000	7.791	8.031	12.812	13.062		
2920.0000	7.798	8.025	12.812	13.078		
2925.0000	7.798	8.031	12.812	13.078		
2930.0000 2935.0000	7.798 7.798	8.031 8.031	12.812 12.812	13.078		



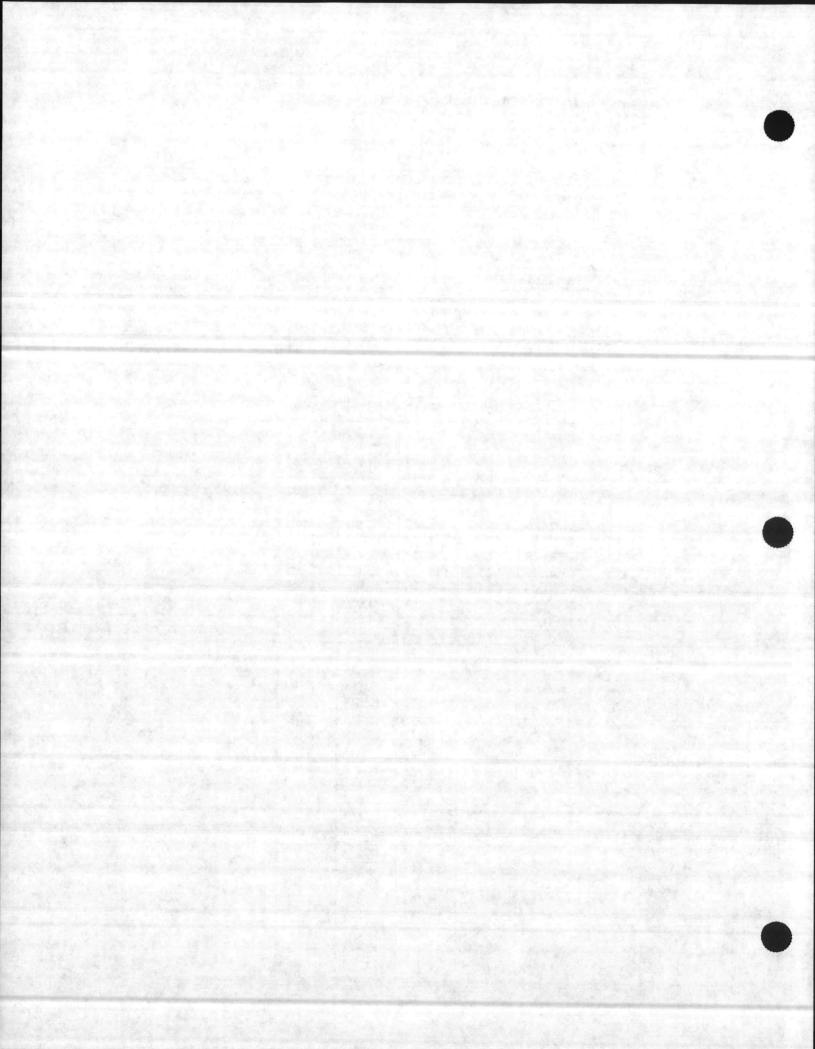
ELAPSED	WELL NUMBER					
TIME	P-1	24-1	24-2	24-3		
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)		
Andrew State		0.005	10.704	12.070		
2940.0000	7.791	8.025	12.796	13.078		
2945.0000	7.798	8.031	12.812	13.078		
2950.0000	7.798	8.037	12.812	13.078		
2955.0000	7.798	8.031	12.796	13.062		
2960.0000	7.798	8.025	12.796	13.062		
2965.0000	7.798	8.031	12.796	13.062		
2970.0000	7.798	8.031	12.796	13.078		
2975.0000	7.798	8.031	12.796	13.062		
2980.0000	7.791	8.018	12.796	13.062		
2985.0000	7.798	8.025	12.796	13.062		
2990.0000	7.791	8.025	12.796	13.062		
2995.0000	7.798	8.025	12.796	13.062		
3000.0000	7.798	8.025	12.796	13.062		
3005.0000	7.798	8.025	12.796	13.062		
3010.0000	7.798	8.031	12.812	13.062		
3015.0000	7.798	8.025	12.796	13.062		
3020.0000	7.798	8.025	12.812	13.062		
3025.0000	7.791	8.025	12.796	13.078		
3030.0000	7.791	8.018	12.796	13.062		
3035.0000	7.791	8.018	12.812	13.062		
3040.0000	7.791	8.018	12.812	13.062		
3045.0000	7.798	8.025	12.812	13.062		
3050.0000	7.791	8.018	12.796	13.062		
3055.0000	7.785	8.012	12.796	13.062		
3060.0000	7.791	8.018	12.796	13.062		
3065.0000	7.791	8.012	12.796	13.078		
3070.0000	7.785	8.012	12.796	13.046		
3075.0000	7.785	8.012	12.796	13.062		
3080.0000	7.785	8.012	12.796	13.062		
3085.0000	7.785	8.000	12.796	13.031		
3090.0000	7.785	8.018	12.765	13.046		
3095.0000	7.785	8.012	12.796	13.046		
3100.0000	7.785	8.018	12.796	13.062		
3105.0000	7.785	8.012	12.796	13.062		
3110.0000	7.785	8.012	12.796	13.062		
3115.0000	7.785	8.000	12.796	13.046		
3120.0000	7.791	8.018	12.796	13.062		
3125.0000	7.785	8.012	12.796	13.062		
3130.0000	7.785	8.000	12.843	13.062		
3135.0000	7.791	8.025	12.796	13.078		
3140.0000	7.785	8.018	12.796	13.062		



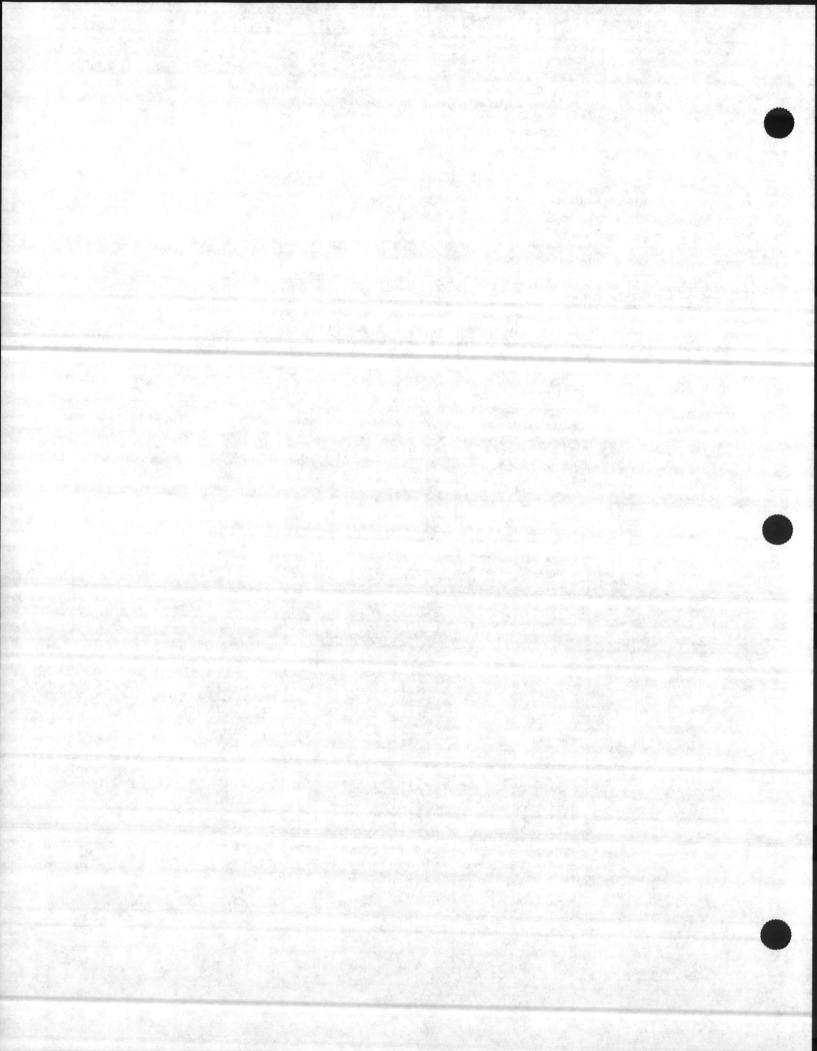
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
(MIIIV)	(ILLI)	(ILLI)	(LEDI)	(I BBI)
3145.0000	7.791	8.018	12.812	13.062
3150.0000	7.798	8.018	12.781	13.062
3155.0000	7.785	8.018	12.781	13.062
3160.0000	7.791	8.025	12.812	13.062
3165.0000	7.791	8.025	12.812	13.062
3170.0000	7.785	8.025	12.796	13.062
3175.0000	7.798	8.031	12.796	13.062
3180.0000	7.798	8.031	12.812	13.078
3185.0000	7.798	8.031	12.812	13.078
3190.0000	7.791	8.031	12.796	13.078
3195.0000	7.798	8.037	12.812	13.078
3200.0000	7.798	8.037	12.812	13.078
3205.0000	7.798	8.031	12.812	13.078
3210.0000	7.798	8.037	12.812	13.078
3215.0000	7.798	8.044	12.812	13.078
3220.0000	7.798	8.044	12.812	13.078
3225.0000	7.798	8.044	12.812	13.078
3230.0000	7.804	8.044	12.812	13.078
3235.0000	7.804	8.050	12.812	13.078
3240.0000	7.804	8.050	12.812	13.078
3245.0000	7.804	8.056	12.812	13.078
3250.0000	7.804	8.056	12.812	13.078
3255.0000	7.811	8.056	12.812	13.093
3260.0000	7.811	8.063	12.812	13.078
3265.0000	7.811	8.063	12.812	13.078
3270.0000	7.811	8.069	12.812	13.078
3275.0000	7.817	8.069	12.812	13.078
3280.0000	7.817	8.075	12.828	13.093
3285.0000	7.823	8.075	12.828	13.093
3290.0000	7.823	8.075	12.812	13.093
3295.0000	7.823	8.075	12.828	13.093
3300.0000	7.823	8.081	12.828	13.078
3305.0000	7.823	8.081	12.828	13.093
3310.0000	7.823	8.088	12.828	13.093
3315.0000	7.830	8.088	12.828	13.093
3320.0000	7.830	8.088	12.828	13.093
3325.0000	7.830	8.088	12.828	13.078
3330.0000	7.830	8.094	12.828	13.078
3335.0000	7.836	8.094	12.828	13.093
3340.0000	7.836	8.100	12.828	13.078
3345.0000	7.836	8.100	12.828	13.093



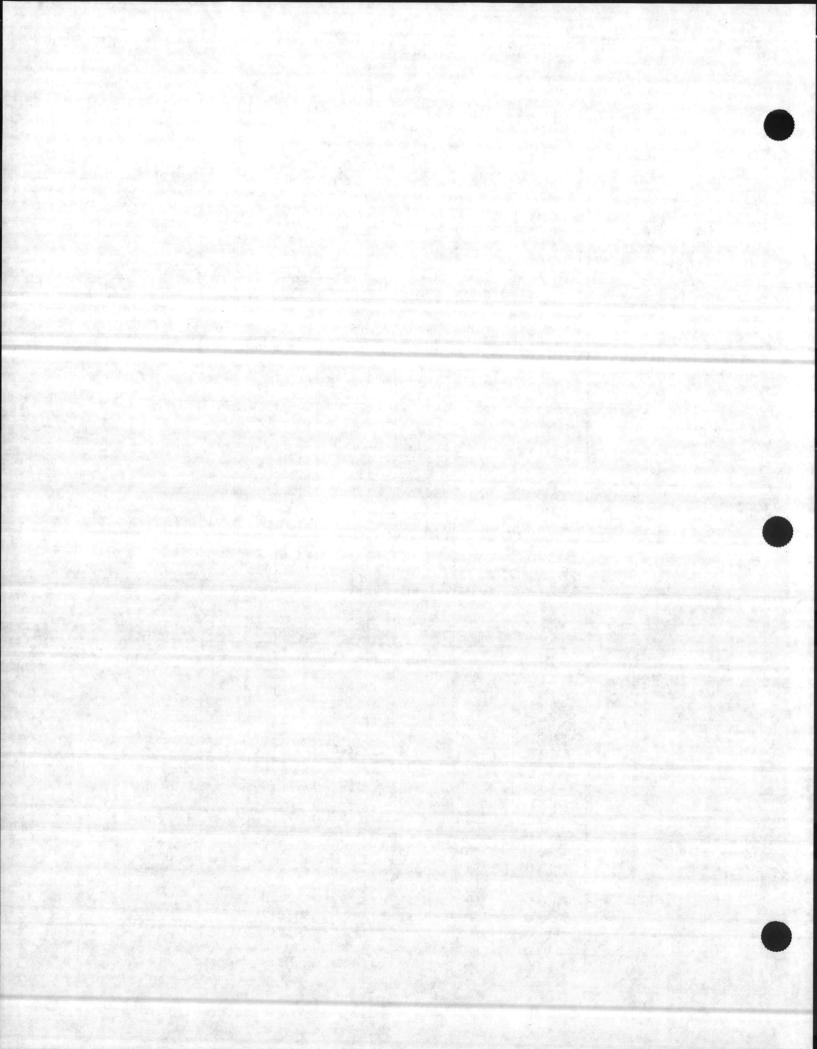
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
	()			
3350.0000	7.836	8.100	12.828	13.093
3355.0000	7.843	8.107	12.828	13.093
3360.0000	7.843	8.113	12.828	13.093
3365.0000	7.843	8.113	12.828	13.093
3370.0000	7.843	8.119	12.828	13.093
3375.0000	7.849	8.119	12.828	13.093
3380.0000	7.849	8.119	12.828	13.093
3385.0000	7.855	8.126	12.828	13.093
3390.0000	7.855	8.126	12.828	13.093
3395.0000	7.855	8.132	12.843	13.093
3400.0000	7.862	8.138	12.828	13.093
3405.0000	7.862	8.132	12.828	13.093
3410.0000	7.868	8.138	12.843	13.093
3415.0000	7.862	8.138	12.828	13.093
3420.0000	7.862	8.138	12.828	13.093
3425.0000	7.868	8.138	12.843	13.093
3430.0000	7.868	8.138	12.843	13.093
3435.0000	7.875	8.145	12.828	13.093
3440.0000	7.875	8.145	12.843	13.093
3445.0000	7.875	8.138	12.843	13.093
3450.0000	7.875	8.145	12.843	13.093
3455.0000	7.875	8.145	12.843	13.093
3460.0000	7.875	8.145	12.843	13.093
3465.0000	7.881	8.145	12.843	13.109
3470.0000	7.881	8.151	12.828	13.093
3475.0000	7.881	8.151	12.843	13.109
3480.0000	7.887	8.157	12.843	13.109
3485.0000	7.887	8.157	12.843	13.093
3490.0000	7.887	8.157	12.843	13.109
3495.0000	7.887	8.157	12.843	13.093
3500.0000	7.887	8.157	12.843	13.109
3505.0000	7.887	8.157	12.843	13.109
3510.0000	7.887	8.157	12.843	13.093
3515.0000	7.887	8.157	12.843	13.109
3520.0000	7.894	8.157	12.843	13.109
3525.0000	7.894	8.157	12.843	13.109
3530.0000	7.894	8.163	12.843	13.093
3535.0000	7.894	8.157	12.843	13.109
3540.0000	7.894	8.163	12.843	13.109
3545.0000	7.894	8.157	12.843	13.109
3550.0000	7.894	8.157	12.843	13.109



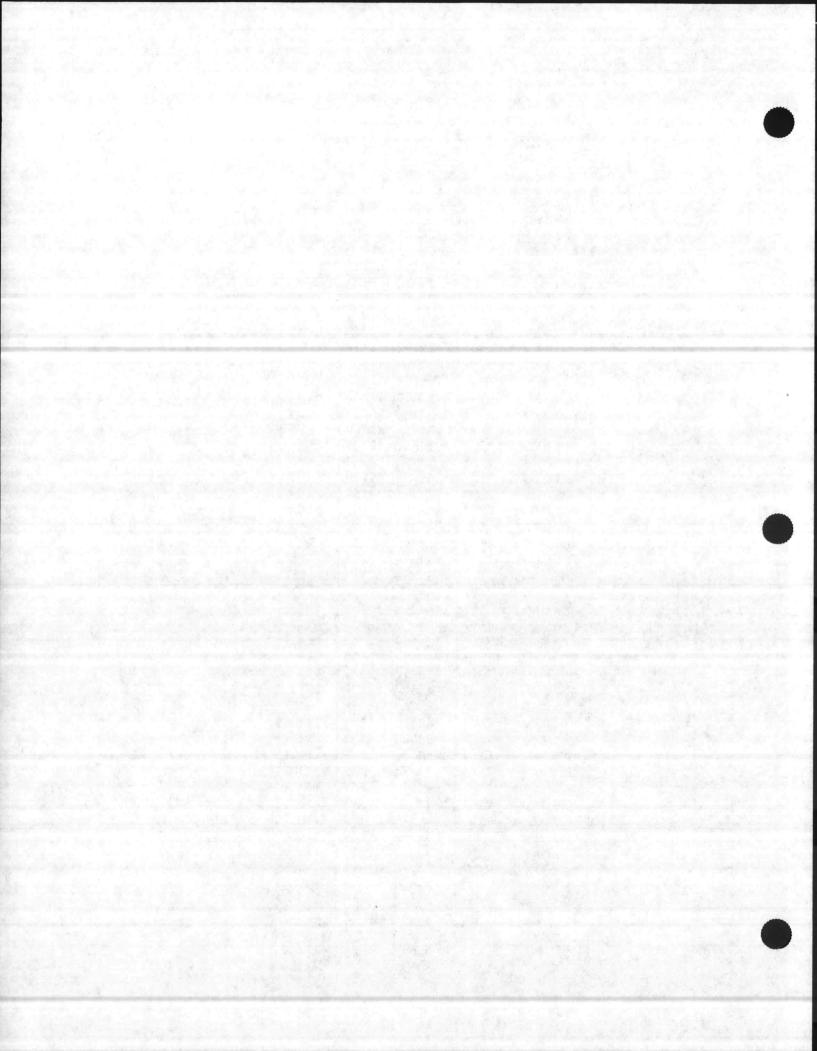
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
3555.0000	7.894	8.157	12.843	13.109
3560.0000	7.900	8.163	12.843	13.109
3565,0000	7.900	8.163	12.843	13.109
3570.0000	7.900	8.163	12.843	13.109
3575.0000	7.900	8.163	12.859	13.109
3580.0000	7.900	8.163	12.859	13.109
3585.0000	7.907	8.157	12.843	13.109
3590.0000	7.907	8.170	12.859	13.109
3595.0000	7.907	8.163	12.859	13.109
3600.0000	7.907	8.163	12.859	13.109
3605.0000	7.907	8.163	12.859	13.109
3610.0000	7.907	8.170	12.859	13.124
3615.0000	7.907	8.163	12.859	13.109
3620.0000	7.907	8.163	12.859	13.109
3625.0000	7.913	8.170	12.859	13.124
3630.0000	7.913	8.170	12.859	13.109
3635.0000	7.913	8.170	12.859	13.109
3640.0000	7.913	8.170	12.859	13.124
3645.0000	7.913	8.170	12.859	13.124
3650.0000	7.913	8.170	12.859	13.109
3655.0000	7.913	8.170	12.859	13.109
3660.0000	7.913	8.170	12.875	13.109
3665.0000	7.919	8.170	12.859	13.124
3670.0000	7.919	8.170	12.859	13.124
3675.0000	7.919	8.170	12.859	13.124
3680.0000	7.919	8.170	12.859	13.124
3685.0000	7.919	8.170	12.859	13.124
3690.0000	7.919	8.170	12.875	13.124
3695.0000	7.919	8.170	12.875	13.124
3700.0000	7.919	8.170	12.859	13.124
3705.0000	7.919	8.170	12.859	13.124
3710.0000	7.919	8.170	12.875	13.124
3715.0000	7.919	8.170	12.875	13.124
3720.0000	7.919	8.170	12.859	13.124
3725.0000	7.926	8.170	12.859	13.124
3730.0000	7.919	8.170	12.859	13.124
3735.0000	7.919	8.170	12.875	13.124
3740.0000	7.919	8.170	12.859	13.124
3745.0000	7.919	8.163	12.859	13.124
3750.0000	7.919	8.163	12.859	13.124
3755.0000	7.919	8.170	12.875	13.124



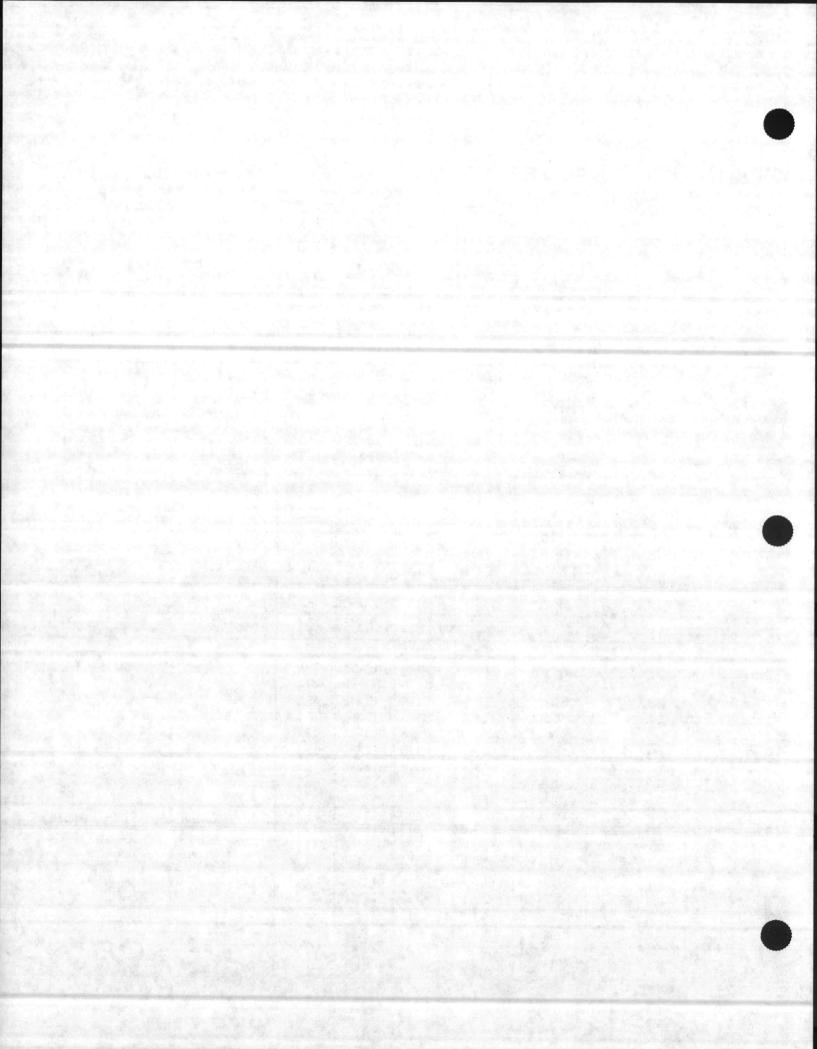
ELAPSED	WELL NUMBER					
TIME	P-1	24-1	24-2	24-3		
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)		
(MIN)	(LEET)	(LDDI)	(1221)	(-22-)		
3760.0000	7.919	8.170	12.875	13.109		
3765.0000	7.919	8.170	12.859	13.124		
3770.0000	7.919	8.163	12.859	13.124		
3775.0000	7.913	8.170	12.859	13.124		
3780.0000	7.913	8.170	12.859	13.124		
3785.0000	7.913	8.163	12.859	13.124		
3790.0000	7.913	8.163	12.859	13.124		
3795.0000	7.913	8.170	12.859	13.124		
3800.0000	7.913	8.163	12.859	13.124		
3805.0000	7.913	8.163	12.859	13.124		
3810.0000	7.913	8.170	12.859	13.124		
3815.0000	7.913	8.163	12.859	13.124		
3820.0000	7.913	8.157	12.859	13.109		
3825.0000	7.907	8.151	12.859	13.124		
3830.0000	7.913	8.151	12.859	13.109		
3835.0000	7.907	8.163	12.875	13.124		
3840.0000	7.907	8.163	12.859	13.109		
3845.0000	7.907	8.163	12.859	13.109		
3850.0000	7.907	8.163	12.859	13.109		
3855.0000	7.913	8.163	12.859	13.109		
3860.0000	7.907	8.163	12.859	13.124		
3865.0000	7.907	8.163	12.859	13.124		
3870.0000	7.913	8.163	12.859	13.124		
3875.0000	7.907	8.163	12.875	13.124		
3880.0000	7.907	8.170	12.859	13.109		
3885.0000	7.907	8.170	12.859	13.109		
3890.0000	7.907	8.176	12.859	13.124		
3895.0000	7.907	8.170	12.859	13.109		
3900.0000	7.907	8.176	12.859	13.124		
3905.0000	7.907	8.170	12.859	13.124		
3910.0000	7.907	8.170	12.859	13.124		
3915.0000	7.907	8.163	12.859	13.124		
3920.0000	7.907	8.163	12.859	13.124		
3925.0000	7.907	8.163	12.859	13.109		
3930.0000	7.907	8.157	12.859	13.109		
3935.0000	7.907	8.151	12.859	13.109		
3940.0000	7.900	8.151	12.859	13.109		
3945.0000	7.900	8.151	12.859	13.124		
3950.0000	7.900	8.138	12.859	13.124		
3955.0000	7.900	8.138	12.859	13.109		
3960.0000	7.900	8.138	12.859	13.109		



ELAPSED	WELL NUMBER					
TIME	P-1	24-1	24-2	24-3		
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)		
2065 0000	7,000	0 120	12.859	13.109		
3965.0000	7.900	8.138	12.859	13.109		
3970.0000	7.900	8.138 8.132	12.859	13.109		
3975.0000 3980.0000	7.900 7.900	8.138	12.859	13.109		
3985.0000	7.900	8.138	12.859	13.109		
3990.0000	7.900	8.138	12.859	13.124		
3995.0000	7.900	8.138	12.859	13.124		
4000.0000	7.900	8.145	12.859	13.109		
4005.0000	7.900	8.138	12.875	13.109		
4010.0000	7.900	8.138	12.859	13.109		
4015.0000	7.907	8.138	12.859	13.109		
4020.0000	7.900	8.145	12.859	13.124		
4025.0000	7.900	8.138	12.859	13.124		
4030.0000	7.900	8.138	12.859	13.124		
4035.0000	7.900	8.138	12.859	13.124		
4040.0000	7.907	8.138	12.843	13.124		
4045.0000	7.900	8.138	12.859	13.124		
4050.0000	7.907	8.138	12.859	13.124		
4055.0000	7.907	8.145	12.859	13.124		
4060.0000	7.907	8.145	12.859	13.109		
4065.0000	7.907	8.145	12.859	13.109		
4070.0000	7.907	8.145	12.859	13.109		
4075.0000	7.900	8.145	12.859	13.109		
4080.0000	7.907	8.151	12.859	13.109		
4085.0000	7,907	8.151	12.859	13.109		
4090.0000	7.907	8.151	12.859	13.109		
4095.0000	7,907	8.157	12.859	13.124		
4100.0000	7.907	8.157	12.859	13.124		
4105.0000	7.907	8.157	12.859	13.109		
4110.0000	7.907	8.157	12.859	13.124		
4115.0000	7.907	8.151	12.875	13.12		
4120.0000	7.907	8.151	12.859	13.12		
4125.0000	7.907	8.151	12.859	13.12		
4130.0000	7.907	8.151	12.859	13.10		
4135.0000	7.907	8.151	12.843	13.12		
4140.0000	7.907	8.151	12.859	13.109		
4145.0000	7.907	8.145	12.859	13.10		
4150.0000	7.900	8.145	12.859	13.10		
4155.0000	7.907	8.145	12.859	13.109		
4160.0000	7.907	8.151	12.859	13.109		
4165.0000	7.907	8.151	12.859	13.124		



ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
4170.0000	7.907	8.151	12.859	13.109
4175.0000	7.907	8.157	12.859	13.124
4180.0000	7.913	8.157	12.859	13.124
4185.0000	7.907	8.151	12.859	13.124
4190.0000	7.907	8.157	12.859	13.124
4195.0000	7.907	8.163	12.859	13.124
4200.0000	7.907	8.163	12.859	13.124
4205.0000	7.907	8.163	12.859	13.124
4210.0000	7.907	8.163	12.859	13.124
4215.0000	7.913	8.163	12.859	13.124
4220.0000	7.907	8.163	12.859	13.124
4225.0000	7.913	8.163	12.875	13.124
4230.0000	7.913	8.170	12.875	13.124
4235.0000	7.913	8.170	12.875	13.140
4240.0000	7.913	8.170	12.875	13.140
4245.0000	7.913	8.176	12.875	13.140
4250.0000	7.919	8.170	12.875	13.140
4255.0000	7.919	8.176	12.875	13.140
4260.0000	7.913	8.176	12.890	13.140
4265.0000	7.913	8.176	12.875	13.140
4270.0000	7.919	8.176	12.890	13.140
4275.0000	7.913	8.176	12.890	13.156
4280.0000	7.919	8.176	12.875	13.156
4285.0000	7.913	8.176	12.890	13.156
4290.0000	7.919	8.176	12.875	13.140
4295,0000	7.919	8.176	12.890	13.140
4300.0000	7.919	8.176	12.875	13.140
4305.0000	7.919	8.176	12.875	13.140
4310.0000	7.919	8.176	12.890	13.140
4315.0000	7.919	8.176	12.890	13.156
4320.0000	7.919	8.176	12.890	13.140
4325.0000	7.919	8.176	12.890	13.156
4330.0000	7.919	8.176	12.890	13.156
4335.0000	7.919	8.176	12.890	13.140
4340.0000	7.919	8.176	12.890	13.140
4345.0000	7.919	8.176	12.890	13.140
4350.0000	7.919	8.176	12.890	13.140
4355.0000	7.919	8.170	12.890	13.156

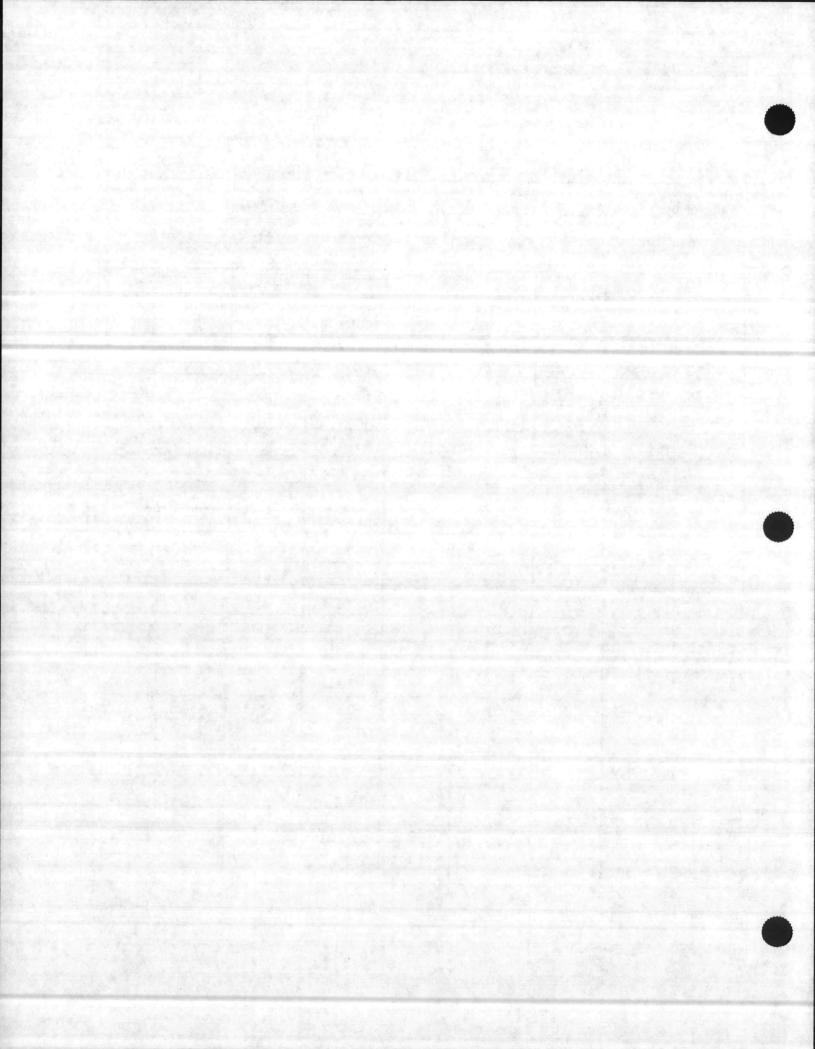




Phase: Drawdown	X	
Recovery		Initial Static W.L. Below M.P. (ft.)
Project		M.P. Elevation (ft., NGVD)
Well Number	ai (HPGWZI)	Initial W.L. Elevation (ft., NGVD)
Distance to Pumped Well	ft.	Test Start Date/Time 2-2-73/10:05

Date	Time	Elapsed Time (min.)	Foot Mark Held at M.P. (ft.)	Wetted Tape (ft.)	Water Level Below M.P. (ft.)	Elev. of Water Surface (ft.)	Draw- down	Obtained By
2-2-93	9120	Initial			10.7			DABAL
2-2-93	15:31	326			10.7			MOS
2-3-93	8:48	1363			10.7			MDS
2-3-93	16:50	1785			10.64			DOM
2/1/43	0650	2685			10.68			RPD
2-4-93	11:12	1			10.70			MOS
2-4-93	18:55				10.72			MOS
0658	06 58				10.70			RAD
7-6-93	10:01			4,2	10.66			MOS
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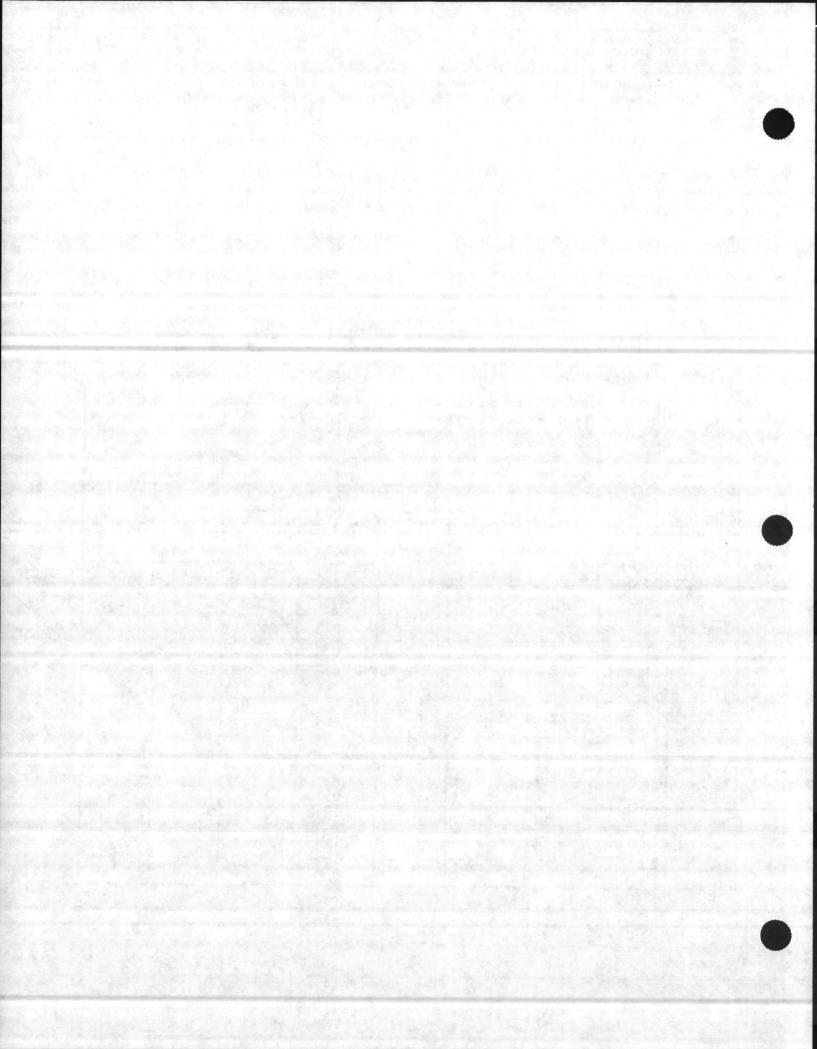




Phase: Drawdown _	×			
Recovery _			Initial Static W.L. Below M.P. (ft.)	
Project			M.P. Elevation (ft., NGVD)	
Well Number	22		Initial W.L. Elevation (ft., NGVD)	- 1
Distance to Pumped We	an	ft.	Test Start Date/Time 2-2-73/10:05	5

Date	Time	Elapsed Time (min.)	Foot Mark Held at M.P. (ft.)	Wetted Tape (ft.)	Water Level Below M.P. (ft.)	Elev. of Water Surface (ft.)	Draw- down	Obtained By
a-2-93	9:07	INIBIAL			7.00			DABAL
2-2-93		313			7.10			MDS
2-3-93	8:42	135.7			7.16			MOS
2-3-93	15:40	1775			7.12			257
2/4/43	0655	2750			7.18			RPD
22-4-93	11:07				7.22			MOS
2-4-93	16:46	1.07			7.27			MOS
2.5-43	0700				7.30			RAD
2-5-6	0946				7.16			MOS
	A. A.							
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			A 70					
- V		319.3	A-A					1 2
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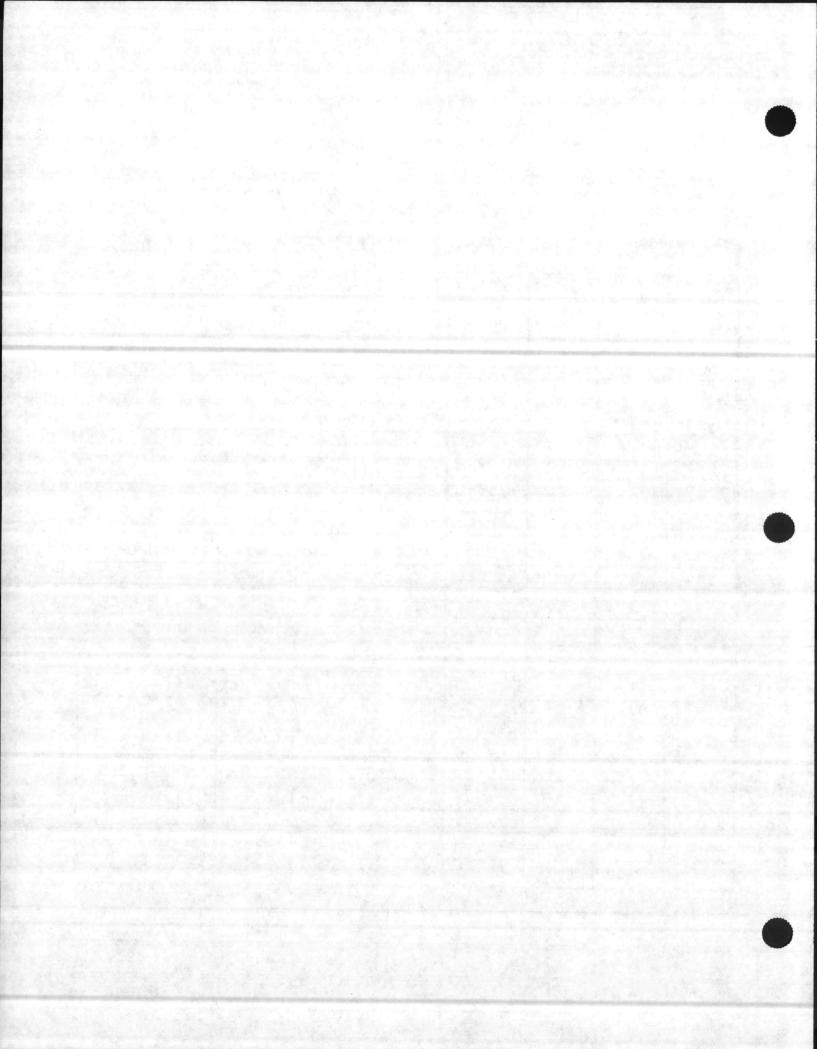




Phase: Drawdown	Χ		
Recovery		Initial Static W.L. Below M.P. (ft.) 9.	59
Project		M.P. Elevation (ft., NGVD)	
Well Number	22-1 (HPGW22-1)	Initial W.L. Elevation (ft., NGVD)	
Distance to Pumped Well	ft.	Test Start Date/Time 2-2-93 /10:	05

Date	Time	Elapsed Time (min.)	Foot Mark Held at M.P. (ft.)	Wetted Tape (ft.)	Water Level Below M.P. (ft.)	Elev. of Water Surface (ft.)	Draw- down	Obtained By
2-2-93	9:31	INITIAL			9.59			DAGAL
2-2-93	15:49	344			9.56			MOS
2-3-93	8:57	1372			9.60			MOS
2-3-93	15:56	1791			9.46			DJM
2/11/13	0645	2672			9.49			RPD
2-4-93	11:19	19			9.56			MOS
24-93	19'07				9.56 9.05 chil			MDS
	0653				9:56			RPO
2.5-93	W:08			19	9.42			MOS
							K.	
			1672	16.52.2.3				
	dia di di			16	respective states			
			1902			1.75 1.7	The said	
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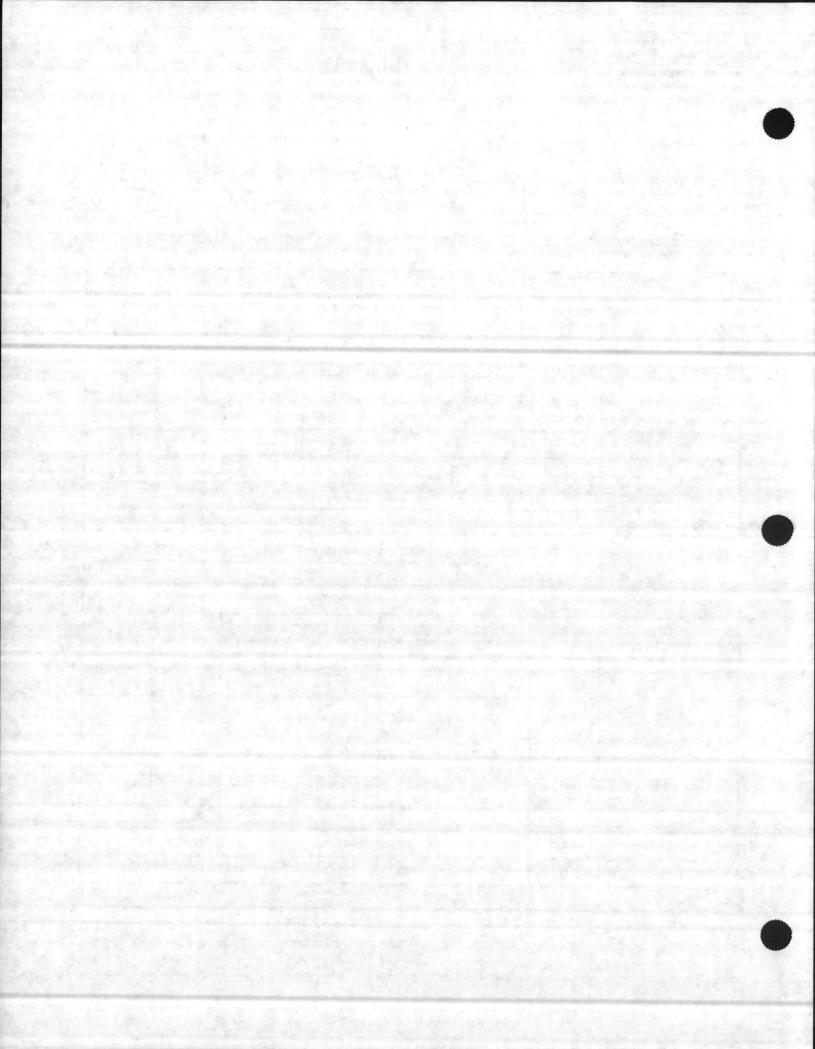




Phase: I	Orawdown	*		
I	Recovery		Initial Static W.L. Below M.P. (ft.)	8. 47
Project _			M.P. Elevation (ft., NGVD)	
Well Num	iber	22-2(HPGMW)	Initial W.L. Elevation (ft., NGVD)	
Distance t	to Pumped Well	ft.	Test Start Date/Time 2-2-73	110:05

Date	Time	Elapsed Time (min.)	Foot Mark Held at M.P. (ft.)	Wetted Tape (ft.)	Water Level Below M.P. (ft.)	Elev. of Water Surface (ft.)	Draw- down	Obtained By
2-2-13	9:40	Instant			8.47		1	DARAL
2-2-93	15:56	351			8.52			MOS
2-7-93	9:03	137.8			8.52			MOS
2-3-93	15:58	1793			8.42			DIM
2/4/43	0640	2665	100 mg		8.46			RIP
2/4/93	11:23				8.50			mo s
2/4/93	1906				8.56	1 - 1 - 1 - 1 - 1		MDS
2-543	0650			2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	8.56			RAD
1-5-93	1012				8.46			MPS
						1. 4.		
							1	
	1 1 2 2 2 2 2			destruction				

Comments:	omments.							
		4.198			_ entire_ more in		- I conduct on a	
	5 L. J. S.							

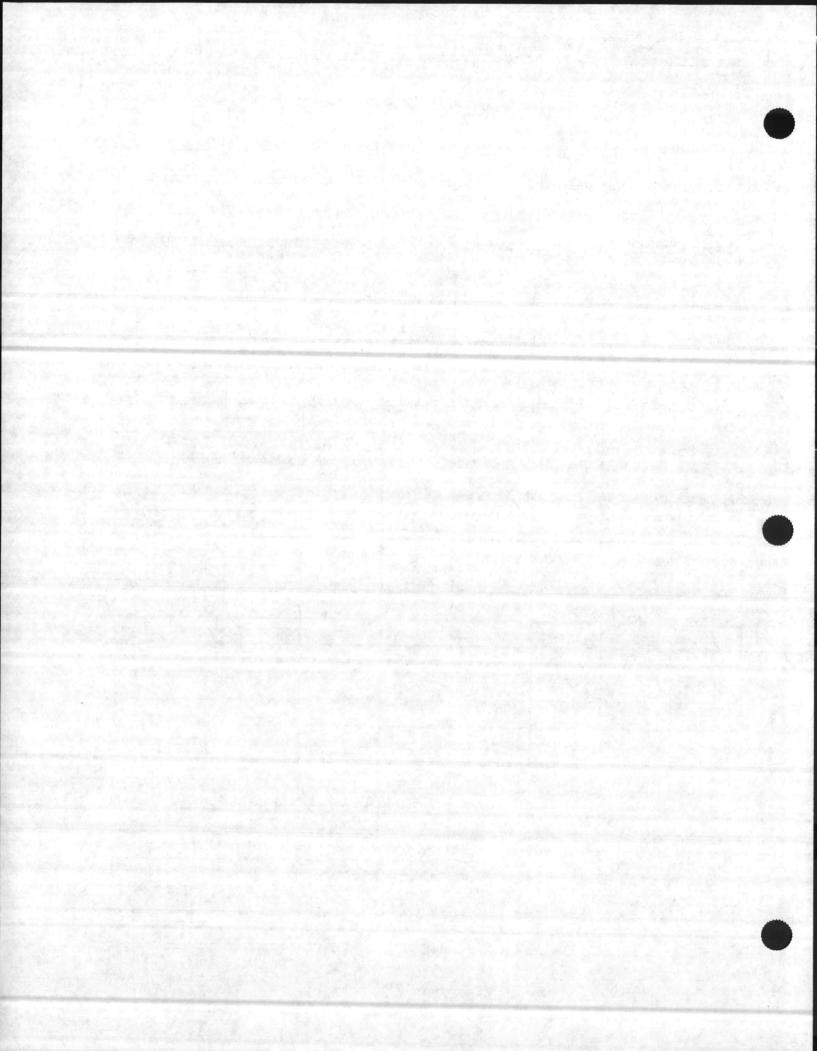




Phase:	Drawdown	×			
	Recovery _		The Way of the	Initial Static W.L. Below M.P. (ft.) 9.75	
Project				M.P. Elevation (ft., NGVD)	_
Well Nu	mber	23		Initial W.L. Elevation (ft., NGVD)	
Distance	e to Pumped Wel	1	ft.	Test Start Date/Time 2-2-93 / 10:05	

Date	Time	Elapsed Time (min.)	Foot Mark Held at M.P. (ft.)	Wetted Tape (ft.)	Water Level Below M.P. (ft.)	Elev. of Water Surface (ft.)	Draw- down	Obtained By
2-2-93	8:55	Jackins			9.75		<b>L</b>	DABAL
2-2-93	-16:06	341		The state of the s	9.70			MDS
2-3-93	9:10	1385			9.84			MOS
2-3-93	15:43	1778			9.71			75m
2.4.93	0700	2625			9.73'			RID
2-4-93	10:52				9.79			MAS
2-4-93	18:19				9.82			MOS
2.5.93	0706				9.86			RAD
1-5-93	9:38			20 Cm	9.72			MOS
	3 and 245				45			7
	Car Service							1
	on the co		to a second				P 7 (4.5)	
						The state of the s		

Comments.			este de la companya d
	- Charles		T. North



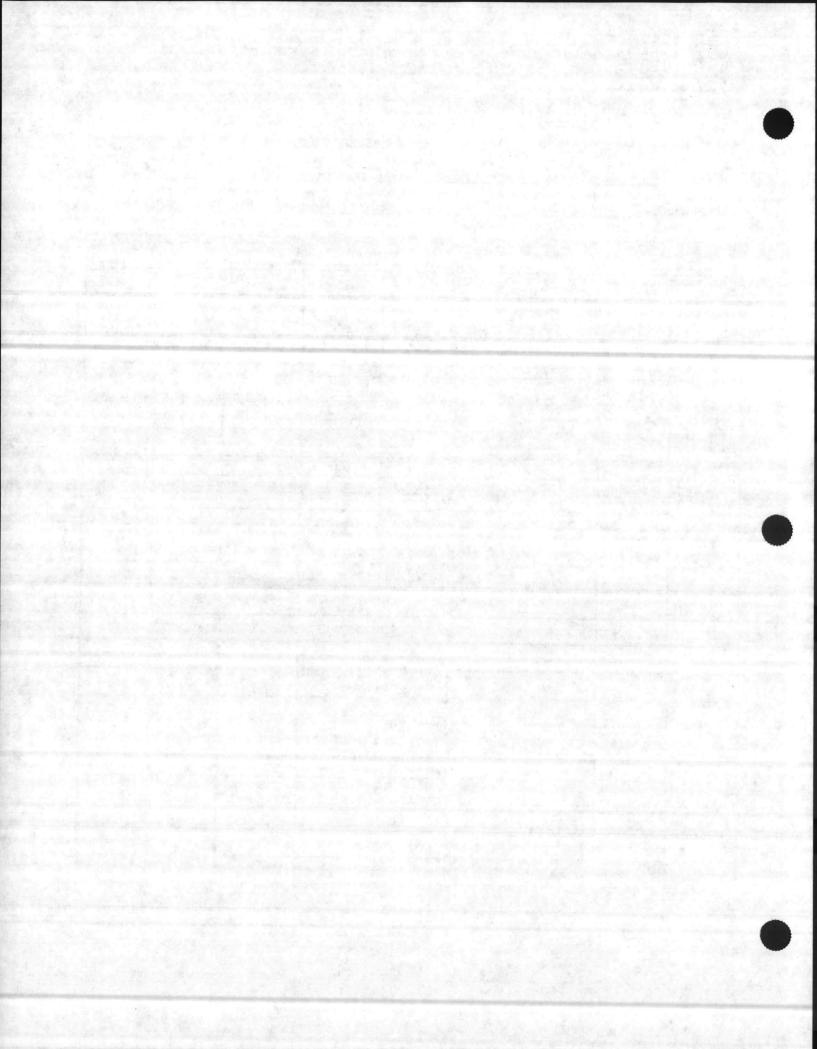
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Page	of	
a upo	O.	



Phase: Drawdown X		
Recovery		Initial Static W.L. Below M.P. (ft.) 7.08
Project Hadnot Point Ind. Acea		M.P. Elevation (ft., NGVD)
Well Number 25		Initial W.L. Elevation (ft., NGVD)
Distance to Pumped Well	ft.	Test Start Date/Time 2-2-13 /10:05

Date	Time	Elapsed Time (min.)	Foot Mark Held at M.P. (ft.)	Wetted Tape (ft.)	Water Level Below M.P. (ft.)	Elev. of Water Surface (ft.)	Draw- down	Obtained By
2-2-93	15:04	initial			7.08	The second second		MO S
2-3-93	8:29	1344			7.20	19 July 19		MOS
2-3-93	15:36	סררו			7.12	17.48		DJM
2.3.43	2225	2180			1.15			RIO
2-4-43	00235	2430			7.15		1	RPD
2/4-93	0725	3020	4,78° a		7.2			RPO
2/4/93		3233			7.26			mos
2/4/93	18:25				7.30			· mps
2.543		Mar				100		
2.5.93					7.34		+ 100 100	RAD
2-6-43					9.6			MOS
			Marie Control					
		194	773L					
		English Com						
							1	
Marin Company								
		A. F. VILLEY		and the second				
							de la company	
	The second							

Comments:	and the second second second		de la lace
	and the second second	and the second s	

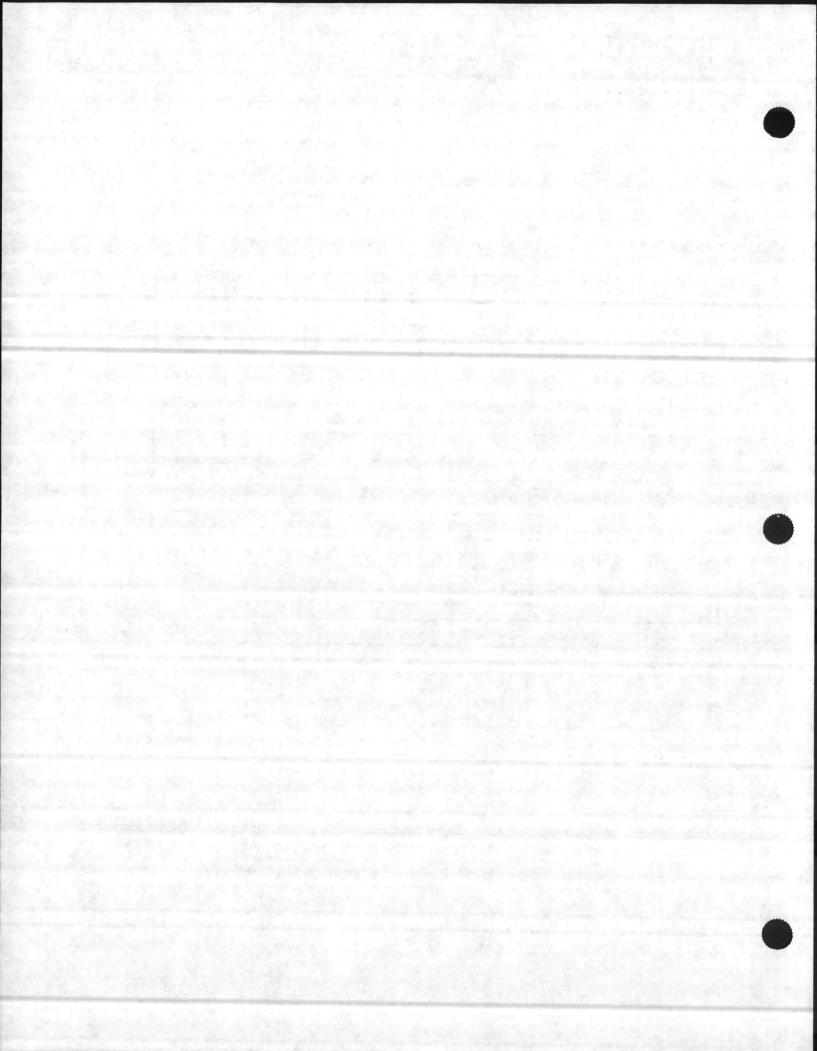




Phase:	Drawdown	×	<u> </u>		
	Recovery			Initial Static W.L. Below M.P. (ft.)	9.55
Project	Hadnot	Point Ind. A	reA	M.P. Elevation (ft., NGVD)	
Well No	ımber	30-2		Initial W.L. Elevation (ft., NGVD)	
Distanc	e to Pumped	Well	ft.	Test Start Date/Time 2-2-95	3/10:05

Date	Time	Elapsed Time (min.)	Foot Mark Held at M.P. (ft.)	Wetted Tape (ft.)	Water Level Below M.P. (ft.)	Elev. of Water Surface (ft.)	Draw- down	Obtained By
2-2-13	10:05	INITIAL			9.55			DABAL
2-2-93	12:30	145			9.68			MD 3
2-2-93	14:43	278			9.60			MOS
2-2-93	19:03	478			9.61			DIM
2-3-93	9: 24	1399			9.68			NOS
23-93	12:38	1593	200		9.68		1.00	MOS
2-3-93	15:30	1765			9.64			MAMAS
2-3-23	18:03	1918			9.909.64			MAMPOSE
2-3-43	2215	2330			9.64			RPO
2-4-43	0235	2540			9.6	and the		RID
2-4-43	0720	3175			9.6			RPD
2-4-93	10:44	3379			9.62			MOS
2-4-93	18:11	3826		1000	9.64	12.00		m03
2-5-43	8027	4202		Company of the state	9.70			KPD
2.5.93	0715	4610.			9.68		1,4	RPD
2-6-93	0930	4745	A principle of the second	11 11 11 11 11 11 11 11 11 11 11 11 11	9.60			MOS
						7.5		
				Michael Control				

Comments:	Although the control of the control

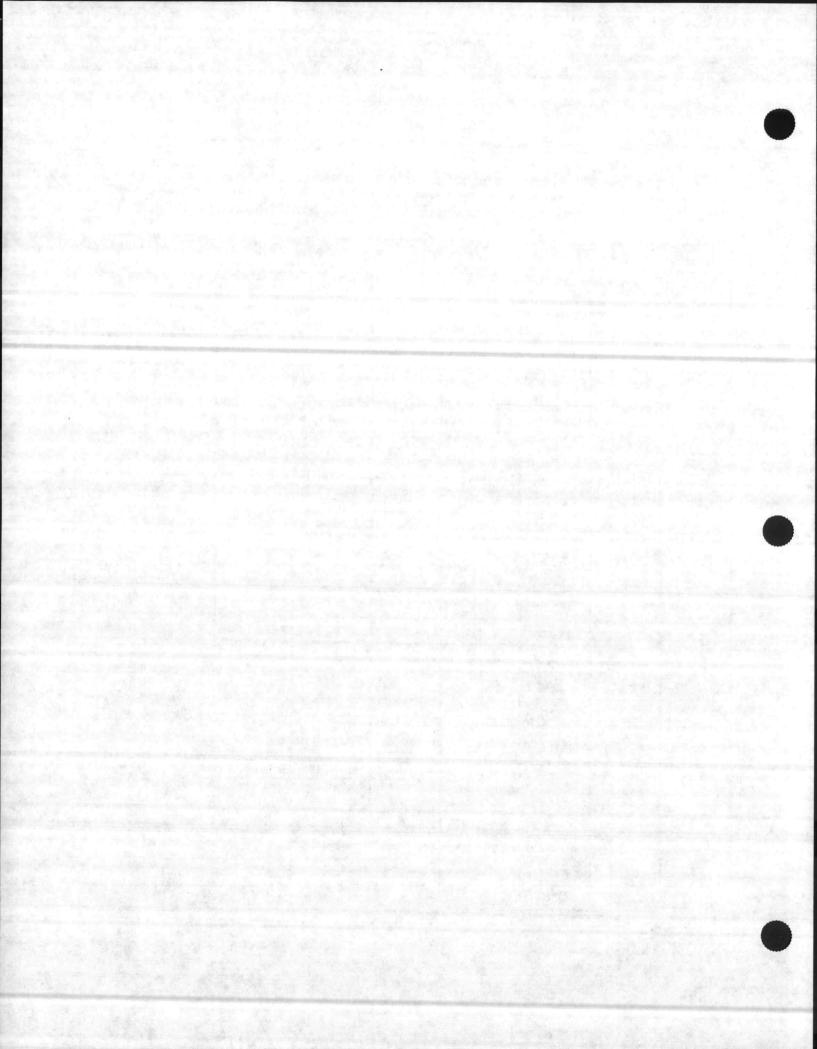


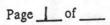


Phase:	Drawdown	X			
	Recovery			Initial Static W.L. Below M.P. (ft.)	9.60
Project	HAN Not	Point Ind.	Area	M.P. Elevation (ft., NGVD)	
Well N	umber	30-3		Initial W.L. Elevation (ft., NGVD)	
Distanc	e to Pumped	Well	ft.	Test Start Date/Time 2-2-93/	10:05

Date	Time	Elapsed Time (min.)	Foot Mark Held at M.P. (ft.)	Wetted Tape (ft.)	Water Level Below M.P. (ft.)	Elev. of Water Surface (ft.)	Draw- down	Obtained By
2-2-93	8:19	INITIAL			9.60			DABAL
2-2-93	12:27	142			9.6458			MD 5
2-2-93	14:47	282	-X-12		9.66			MDS
2-2-2	18:00	475			9.67			AMAMA
2-3-93	09:20	1395			9.74			MDS
2-3-93	12:36	1591			9.72			MOS
2-3-93	15:28	1743			9.70			D. Marie
2-3-93	18:00	1915			9.70			DIMANA
2-3-43	2210	2105			9.70			RPD
2 . 4 . 43	0235	2370			9.66			RPD
2/+143	0715	2850			9.66			RPD
14/93	1041	3056			9,66			MDS
2/4/93	1809	4K3504			9.70			mos
2.5/43	0020	3875			9.74			RPD
2.5.43	and the second second	4329			9.44			RPD
2-6-93	0900	4465			9.64			MDS
	Maria de la compansión de	S. Bernell	M 4 5 5			471 A 471 BB	10	
And the second					4 4	The state	W W	
				Language Co.				

Comments:	



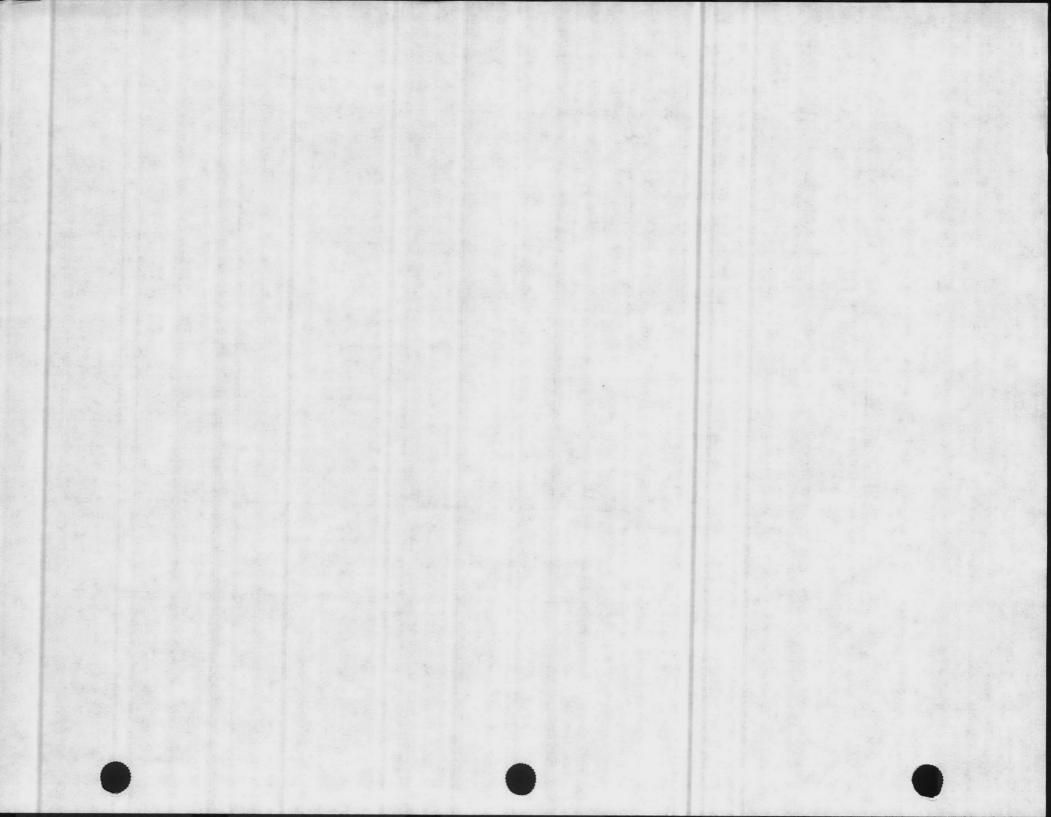




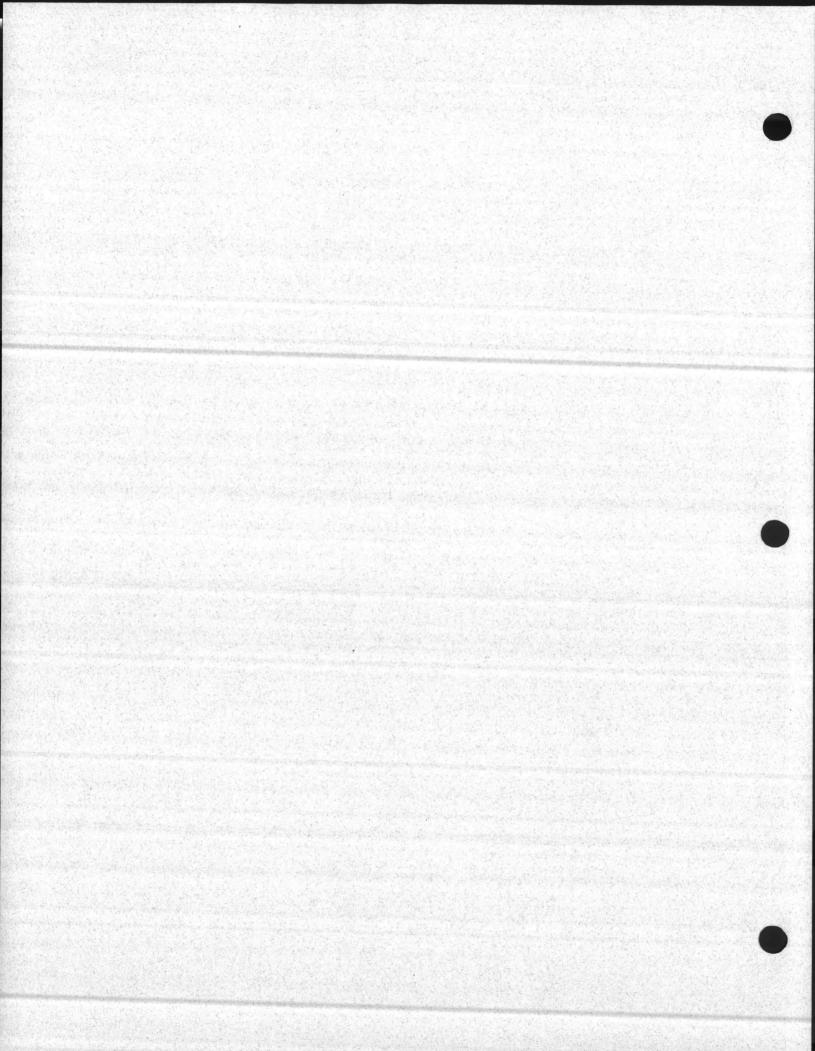
# FLUID LEVEL MEASUREMENTS

Project Hadnot Point	CTO Number
10 Joe	[2012]

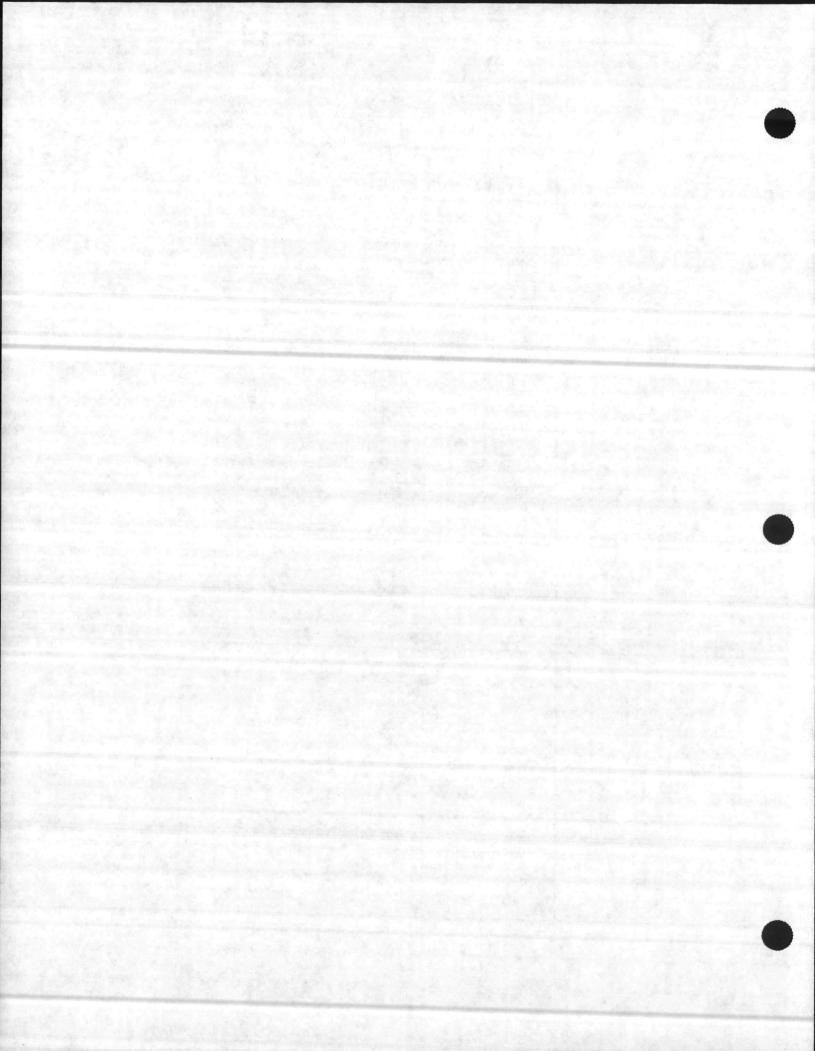
Date	Time	Well Number	Top of Casing Elevation (feet above MSL)	Depth to Product (feet below top of casing)	Depth to Groundwater (feet below top of casing)	Product Thickness (feet)	Product Elevation (feet above MSL)	Groundwater Botton Elevation (feet above MSL)	Obtained by
1/40		RWI			7.46′	- 10 - 1		27.3'	APO/mos
2/2/93	750				7			24.75	RPD/MES
2/2/93	751	P2			5.10			24 65'	KPP
2/2/93	755	PI			7.35	-		27.25	RPD/MOS
2/2/93	759	HPGW 24-1			7.30			77.80	RPD/
2/2/93	807	24-2			12.75			11. 1	RPD/mo.
2/2/93	812	24-3			13.00'			101.3 to 1100	1mm
	0839				9.60			101. 3 not ton	A STATE OF THE STA
	0845				9.55			76.15	RPD
					9.75			27.35	RPO
The second secon	0855							27.70	RPD
PRINTED TO A STATE OF THE PARTY	0907	The second secon			7.0			27.60	RPD
	0920				9.59			17.64	RPD
2/2/2	0931	20-1						2315	300
2/2/2	0290	22.2			8.47				1
1	1					1		-	+
	1			_					



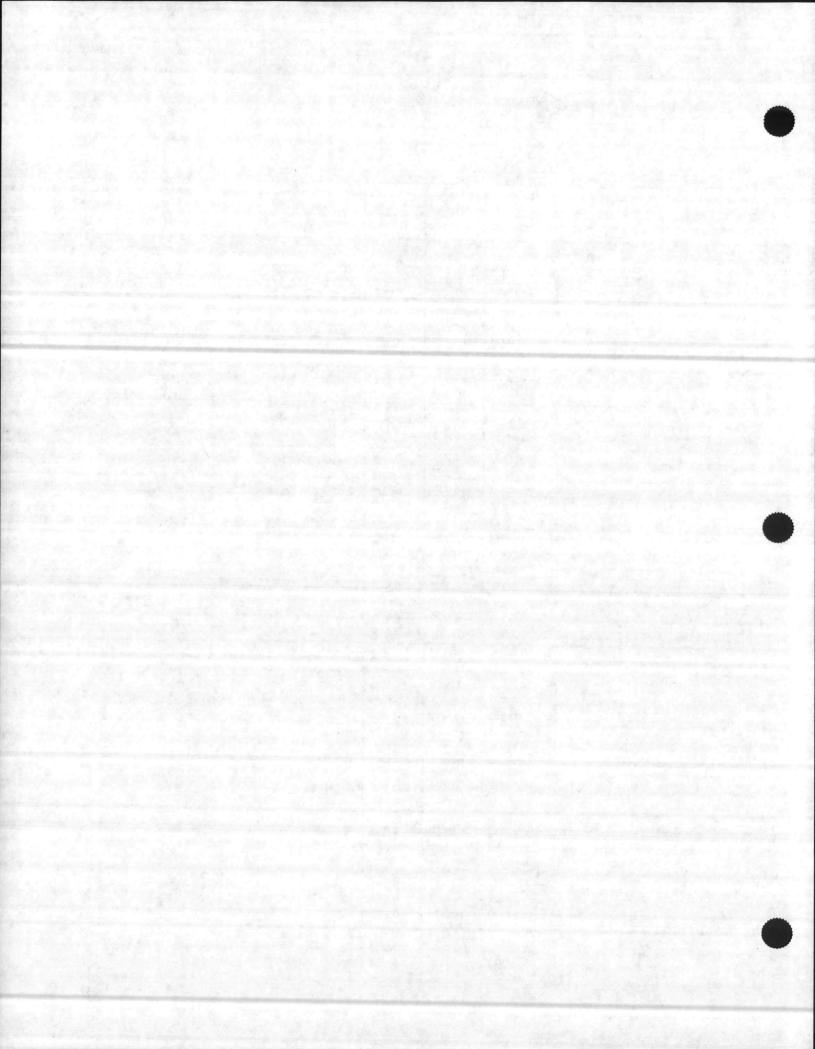
APPENDIX D AQUIFER TEST DATA - RECOVERY PHASE



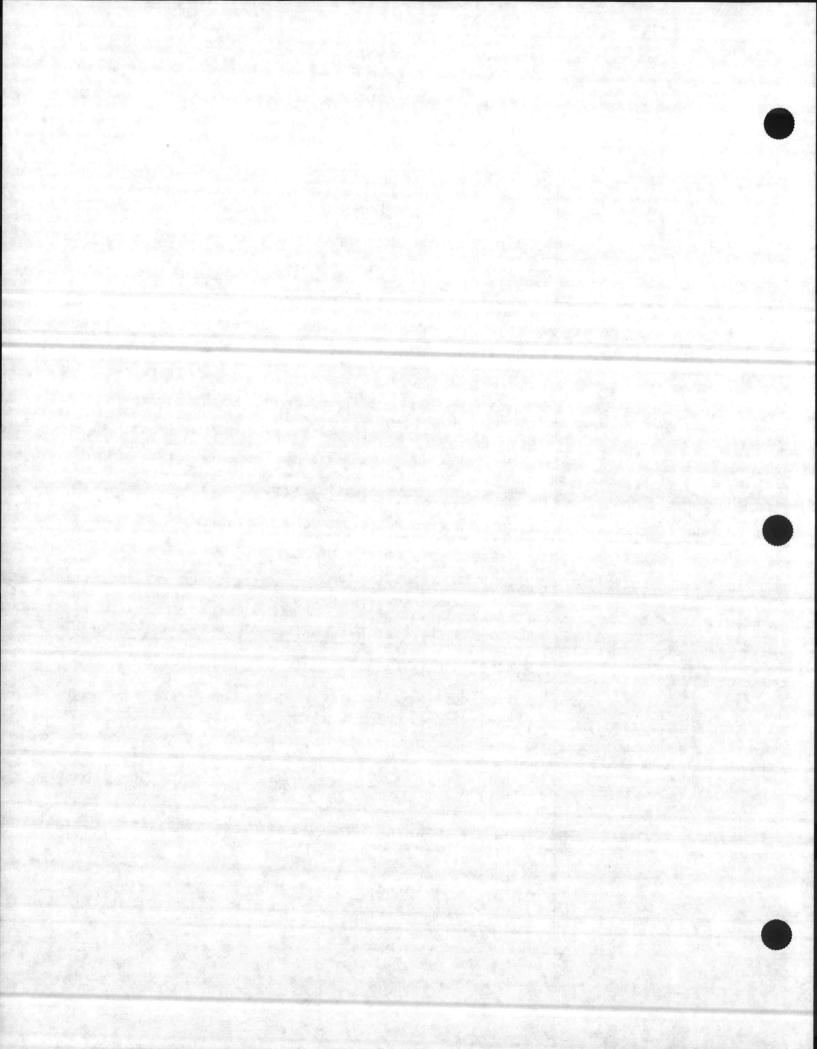
	WELL NUMBER			
TIME	RW-1	P-2		
(MIN)	SWL (FEET)	SWL (FEET)		
0.0000	20.412	6.956		
0.0000	20.412	6.963		
0.0033	20.399	6.963		
0.0000	20.416	6.963		
0.0100	20.399	6.963		
0.0166	20.399	6.963		
0.0200	20.399	6.963		
0.0233	20.393	6.963		
0.0255	20.406	6.963		
0.0300	20.418	6.963		
0.0333	20.393	6.963		
0.0500	20.387	6.963		
0.0666	20.374	6.963		
0.0833	20.362	6.963		
0.1000	20.349	6.963		
0.1166	20.336	6.963		
0.1333	20.324	6.963		
0.1500	20.311	6.963		
0.1666	20.298	6.963		
0.1833	20.286	6.963		
0.2000	20.273	6.963		
0.2166	20.260	6.963		
0.2333	20.248	6.963		
0.2500	20.235	6.963		
0.2666	20.222	6.963		
0.2833	20.210	6.969		
0.3000	20.197	6.969		
0.3166	20.191	6.969		
0.3333	20.178	6.969		
0.4166	20.115	6.963		
0.5000	20.058	6.963		
0.5833	19.995	6.969		
0.6666	19.938	6.969		
0.7500	19.881	6.969		
0.8333	19.817	6.969		
0.9166	19.754	6.969		
1.0000	19.691	6.969		
1.0833	19.628	6.963		
1.1666	19.577	6.969		
1.2500	19.520	6.969		
1.3333	19.470	6.969		
1.4166	19.413	6.969		



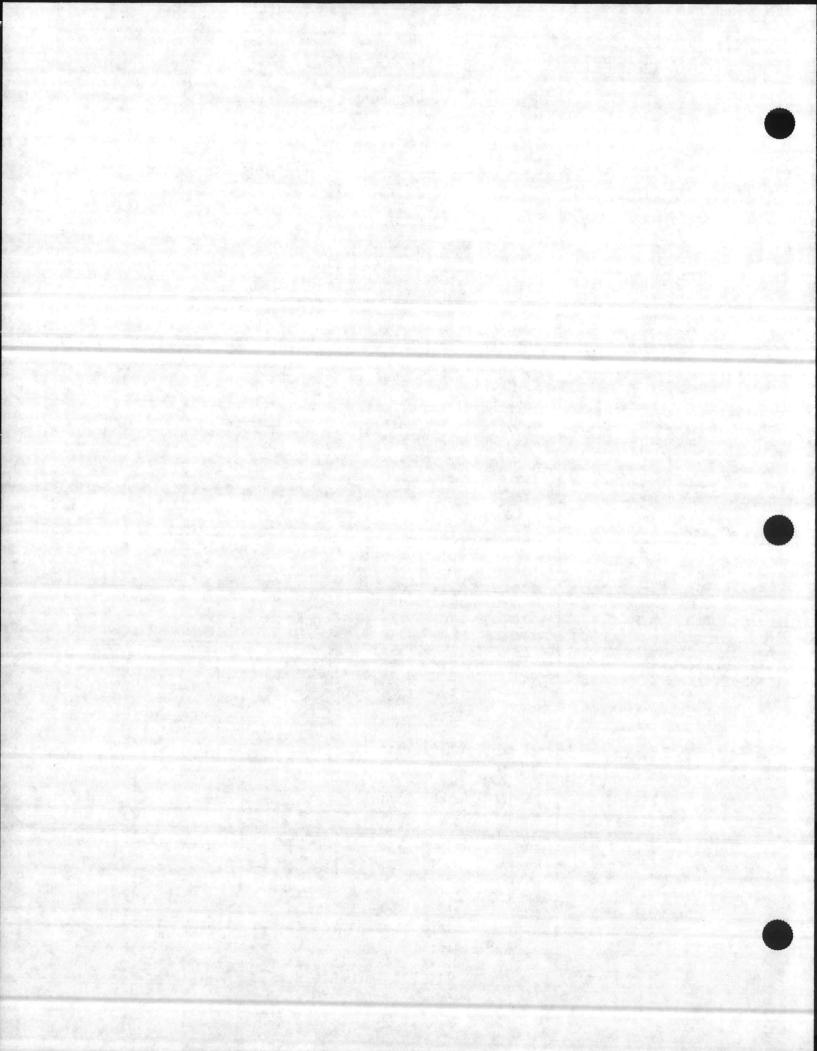
	WELL NUMBER			
TIME	RW-1	P-2		
	SWL	SWL		
(MIN)	(FEET)	(FEET)		
1.5000	19.356	6.969		
1.5833	19.292	6.963		
1.6666	19.229	6.969		
1.7500	19.172	6.969		
1.8333	19.109	6.969		
1.9166	19.046	6.969		
2.0000	18.982	6.969		
2.5000	18.622	6.975		
3.0000	18.248	6.969		
3.5000	17.881	6.963		
4.0000	17.514	6.956		
4.5000	17.153	6.963		
5.0000	16.818	6.963		
5.5000	16.495	6.969		
6.0000	16.197	6.975		
6.5000	15.919	6.975		
7.0000	15.640	6,969		
7.5000	15.387	6,969		
8.0000	15.152	6,969		
8.5000	14.937	6.963		
9.0000	14.722	6.963		
9.5000	14.506	6.956		
10.0000	14.304	6.956		
12.0000	13.581	6.956		
14.0000	12.910	6.956		
16.0000	12.301	6.95		
18.0000	11.832	6.944		
20.0000	11.484	6.937		
22.0000	11.211	6.937		
24.0000	10.983	6.931		
26.0000	10.793	6.918		
28.0000	10.628	6.912		
30.0000	10.482	6.899		
32,0000	10.380	6.893		
34.0000	10.279	6.887		
36.0000	10.203	6.88		
38.0000	10.127	6.868		
40.0000	10.051	6.861		
42.0000	10.006	6.849		
44.0000	9.949	6.849		
46.0000	9.905	6.836		
48.0000	9.860	6.823		



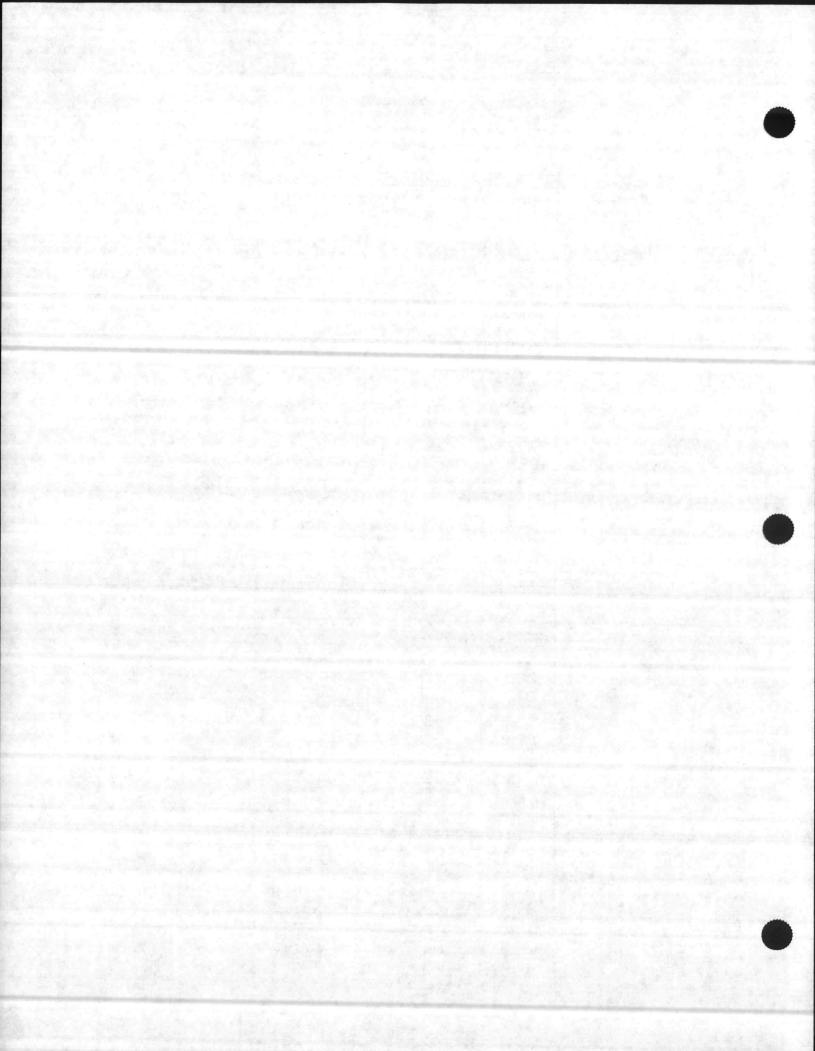
ELAPSED	JMBER	
TIME	RW-1	P-2
	SWL	SWL
(MIN)	(FEET)	(FEET)
50,0000	0.014	2011
50.0000	9.816	6.811
52.0000	9.778	6.804
54.0000	9.746	6.798
56.0000	9.714	6.798
58.0000	9.676	6.779
60.0000	9.651	6.772
62.0000	9.619	6.766
64.0000	9.594 9.569	6.76 6.747
66.0000	9.569	6.747
68.0000	9.537	6.734
70.0000 72.0000	9.518	6.728
74.0000	9.303	6.722
76.0000	9.473	6.709
78.0000	9.442	6.703
80.0000	9.442	6.69
82.0000	9.397	6.677
84.0000	9.385	6.671
86.0000	9.372	6.665
88.0000	9.353	6.665
90.0000	9.347	6.658
92.0000	9.328	6.646
94.0000	9.315	6.639
96.0000	9.296	6.627
98.0000	9.277	6.62
100.0000	9.270	6.608
110.0000	9.207	6.57
120.0000	9.150	6.544
130.0000	9.106	6.513
140.0000	9.061	6.487
150.0000	9.010	6.456
160.0000	8.979	6.437
170.0000	8.941	6.405
180.0000	8.903	6.38
190.0000	8.871	6.354
200.0000	8.833	6.335
210.0000	8.807	6.316
220.0000	8.776	6.291
230.0000	8.750	6.272
240.0000	8.719	6.253
250.0000	8.693	6.24
260.0000	8.661	6.221

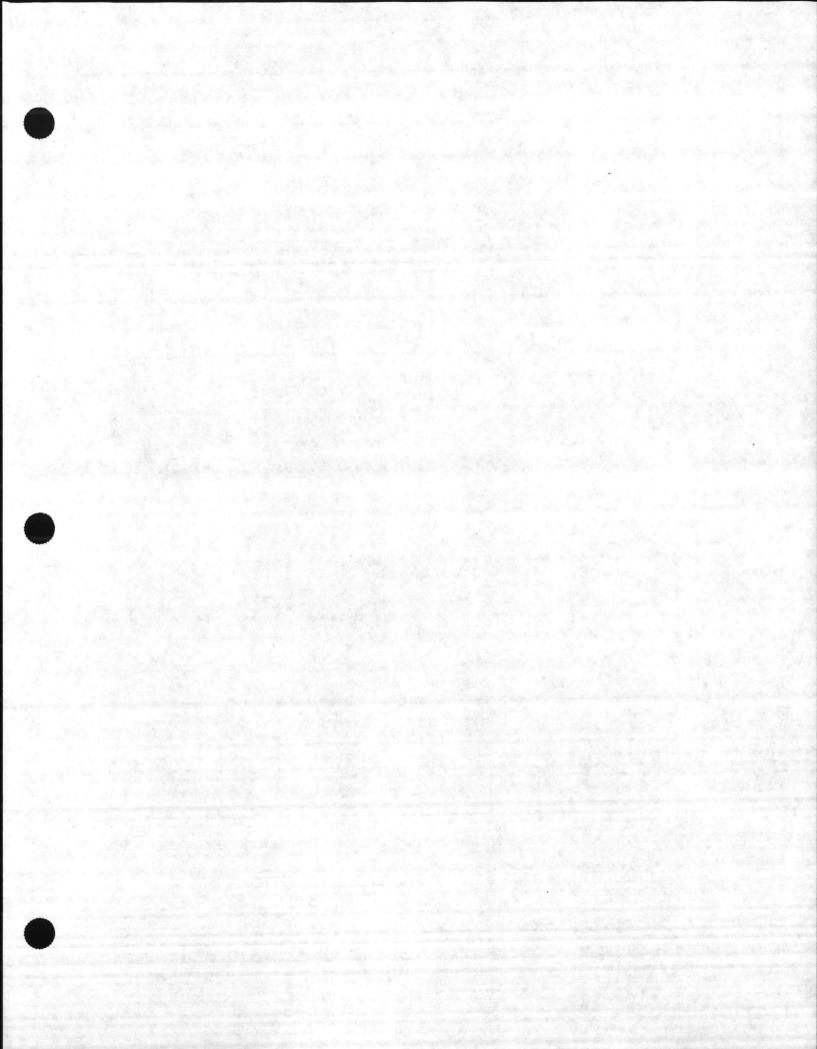


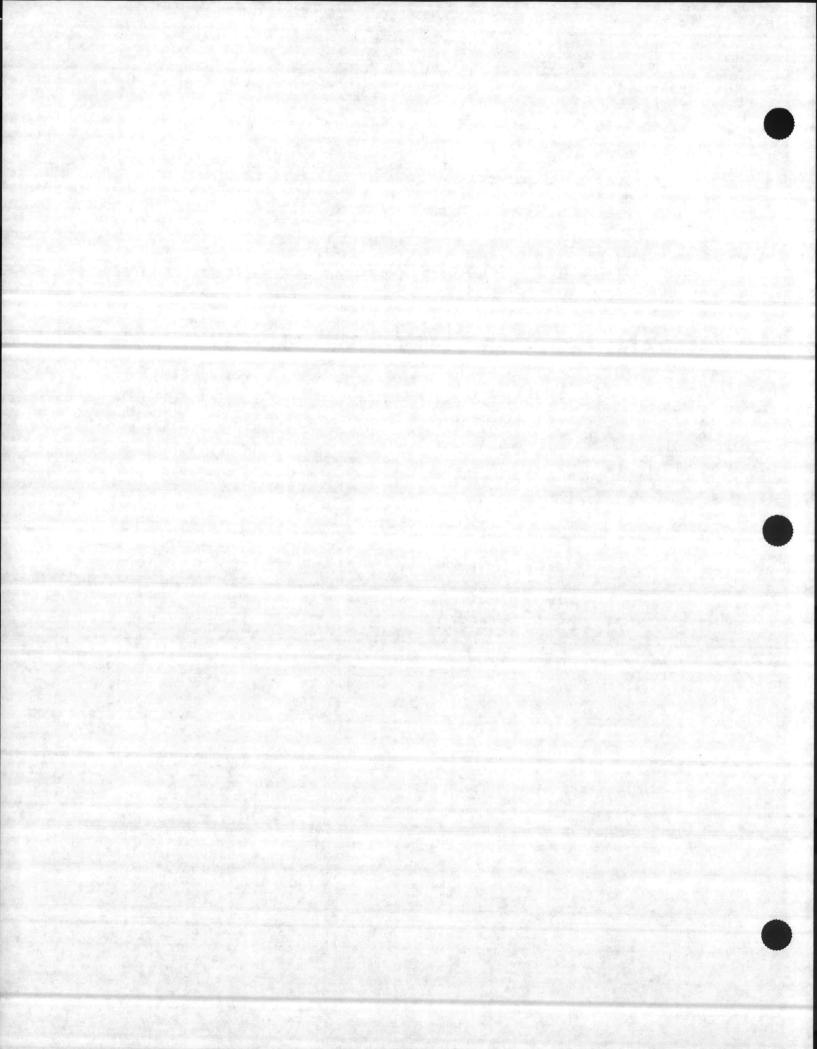
ELAPSED WELL NUMBER TIME				
TIME	RW-1	P-2		
(MIN)	SWL (FEET)	SWL (FEET)		
270.0000	8.642	6.202		
280.0000	8.617	6.183		
290.0000	8.592	6.171		
300.0000	8.560	6.152		
310.0000	8.541	6.133		
320.0000	8.522	6.12		
330.0000	8.496	6.107		
340.0000	8.477	6.088		
350.0000	8.458	6.069		
360.0000	8.439	6.057		
370.0000	8.414	6.044		
380.0000	8.395	6.025		
390.0000	8.376	6.012		
400.0000	8.357	5.993		
410.0000	8.338	5.98		
420.0000	8.332	5.974		
430.0000	8.313	5.961		
440.0000	8.300	5.949		
450.0000	8.287	5.936		
460.0000	8.274	5.923		
470.0000	8.262	5.917		
480.0000	8.249	5.904		
490.0000	8.236	5.898		
500.0000	8.230	5.885		
510.0000	8.217	5.879		
520.0000	8.205	5.866		
530.0000	8.192	5.854		
540.0000	8.179	5.847		
550.0000	8.173	5.841		
560.0000	8.167	5.835		
570.0000	8.154	5.822		
580.0000	8.148	5.816		
590.0000	8.135	5.809		
600.0000	8.129	5.803		
610.0000	8.122	5.797		
620.0000	8.109	5.784		
630.0000	8.103	5.778		
640.0000	8.097	5.771		
650.0000	8.084	5.759		
660.0000	8.071	5.746		
670.0000	8.065	5.74		
680.0000	8.059	5.733		



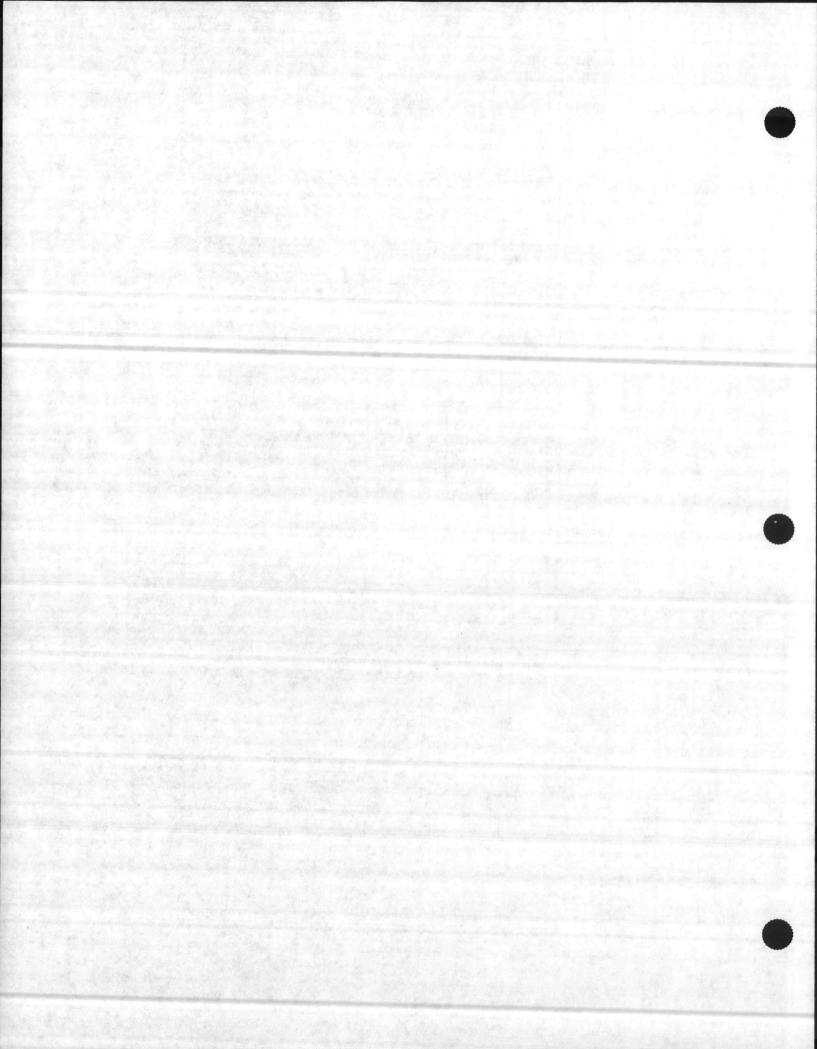
	WELL NUMBER				
TIME	RW-1	P-2			
(MIN)	SWL (FEET)	SWL (FEET)			
(141114)	(I DDI)	(1221)			
690.0000	8.052	5.727			
700.0000	8.046	5.721			
710.0000	8.033	5.708			
720.0000	8.021	5.702			
730.0000	8.014	5.702			
740.0000	8.008	5.689			
750.0000	8.002	5.683			
760.0000	8.002	5.676			
770.0000	7.995	5.67			
780.0000	7.983	5.664			
790.0000	7.976	5.657			
800.0000	7.970	5.651			
810.0000	7.957	5.632			
820.0000	7.951	5.632			
830.0000	7.945	5.626			
840.0000	7.938	5.607			
850.0000	7.925	5.613			
860.0000	7.925	5.6			
870.0000	7.913	5.594			
880.0000	7.906	5.588			
890.0000	7.900	5.581			
900.0000	7.894	5.575			
910.0000	7.887	5.569			
920.0000	7.881	5.55			
930.0000	7.875	5.562			
940.0000	7.875	5.556			
950.0000	7.868	5.55			
960,0000	7.862	5.537			
970.0000	7.856	5.537			
980.0000	7.849	5.524			
990.0000	7.843	5.524			
1000.0000	7.837	5.518			
1010.0000	7.830	5.518			
1020.0000	7.824	5.505			
1030.0000	7.818	5.499			
1040.0000	7.818	5,499			
1050.0000	7.818	5.499			
1060.0000	7.818	5.486			
1070.0000	7.818	5.493			
1080.0000	7.811	5.486			
1090.0000	7.805	5.48			
1100.0000	7.792	5.48			





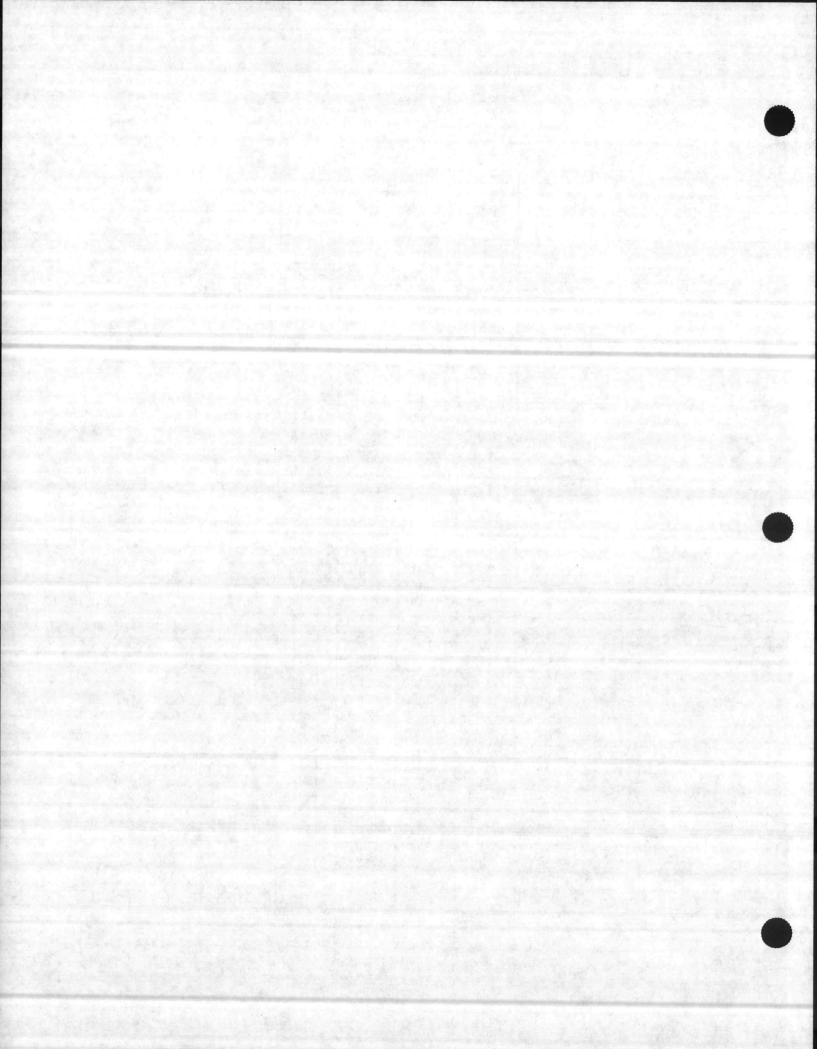


ELAPSED	WELL N	JMBER
TIME	RW-1	P-2
(MIN)	SWL (FEET)	SWL (FEET)
1110.0000	7.792	5.473
1120.0000	7.799	5.473
1130.0000	7.799	5.48
1140.0000	7.805	5.48
1150.0000	7.805	5.48
1160.0000	7.799	5.473
1170.0000	7.799	5.467
1180.0000	7.799	5.48
1190.0000	7.799	5.473
1200.0000	7.799	5.473
1210.0000	7.792	5.473
1220.0000	7.780	5.454
1230.0000	7.786	5.461
1240.0000	7.786	5.454
1250.0000	7.780	5.454

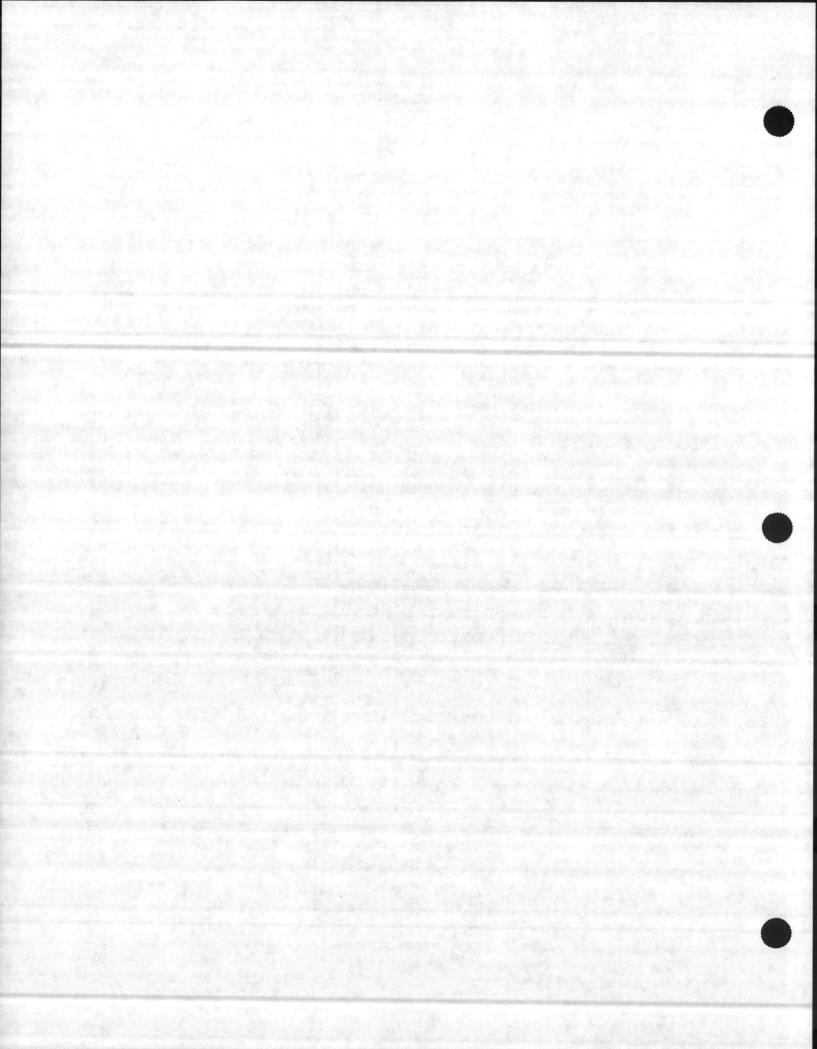


CONTRACT TASK ORDER: 0017 SITE I.D.: CAMP LEJEUNE, HPIA TEST: RECOVERY

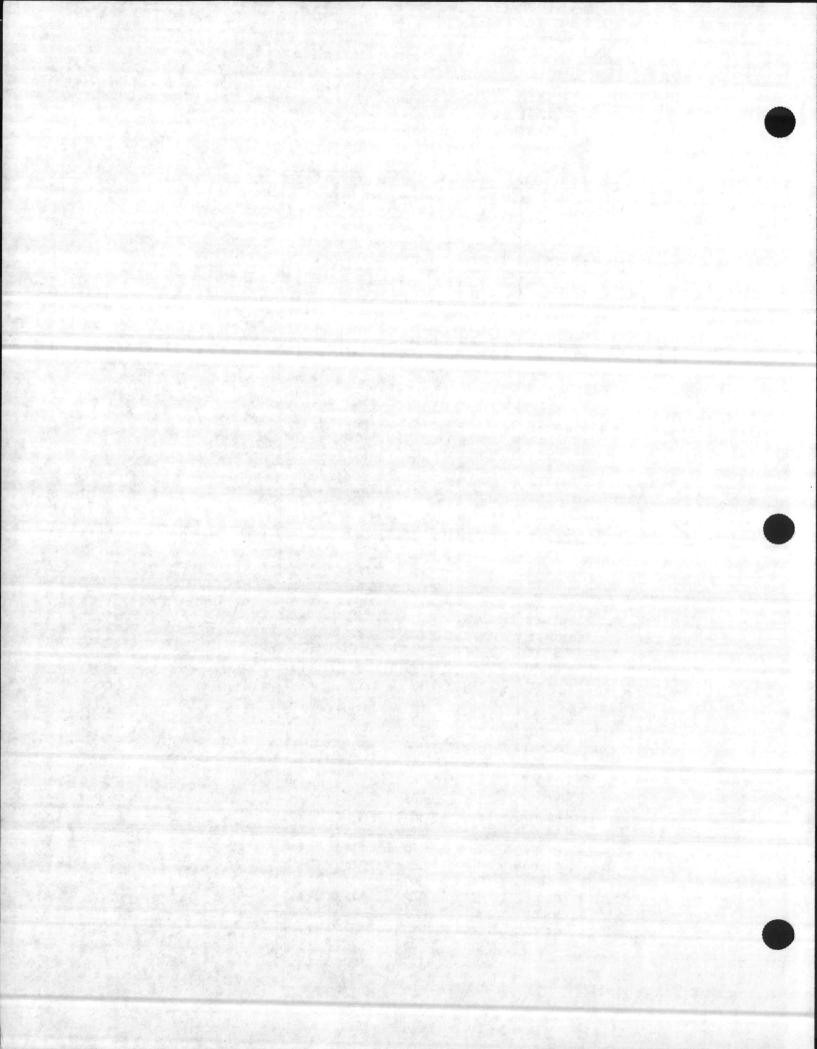
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
0.0000	7.010	0 162	12.875	13.124
0.0000	7.919	8.163	12.890	13.140
0.0083	7.913	8.163		13.140
0.0166	7.913	8.163	12.890 12.875	13.140
0.0250	7.913 7.913	8.163 8.163	12.875	13.140
0.0333	7.913	8.163	12.890	13.140
0.0416		8.163	12.890	13.140
0.0500	7.913	8.170	12.890	13.140
0.0583	7.913			13.140
0.0666	7.913	8.163	12.875	13.140
0.0750	7.919	8.163	12.875	13.140
0.0833	7.913	8.170	12.890	
0.0916	7.919	8.163	12.890	13.140
0.1000	7.913	8.163	12.875	13.140
0.1083	7.913	8.163	12.890	13.140
0.1166	7.913	8.170	12.890	13.140
0.1250	7.913	8.163	12.875	13.140
0.1333	7.913	8.170	12.875	13.140
0.1416	7.919	8.170	12.875	13.140
0.1500	7.919	8.163	12.890	13.140
0.1583	7.919	8.163	12.875	13.140
0.1666	7.919	8.163	12.890	13.140
0.1750	7.913	8.163	12.890	13.140
0.1833	7.913	8.163	12.890	13.140
0.1916	7.913	8.170	12.875	13.140
0.2000	7.919	8.170	12.890	13.140
0.2083	7.919	8.170	12.875	13.140
0.2166	7.919	8.170	12.890	13.140
0.2250	7.913	8.163	12.875	13.140
0.2333	7.913	8.163	12.890	13.140
0.2416	7.913	8.163	12.875	13.140
0.2500	7.913	8.163	12.875	13.140
0.2583	7.919	8.170	12.875	13.140
0.2666	7.913	8.163	12.875	13.140
0.2750	7.913	8.170	12.875	13.140
0.2833	7.919	8.170	12.875	13.140
0.2916	7.919	8.170	12.875	13.156
0.3000	7.913	8.170	12.875	13.140
0.3083	7.913	8.170	12.890	13.140
0.3166	7.919	8.170	12.890	13.140
0.3250	7.913	8.170	12.875	13.140
0.3333	7.919	8.163	12.875	13.140
0.3500	7.919	8.170	12.875	13.140



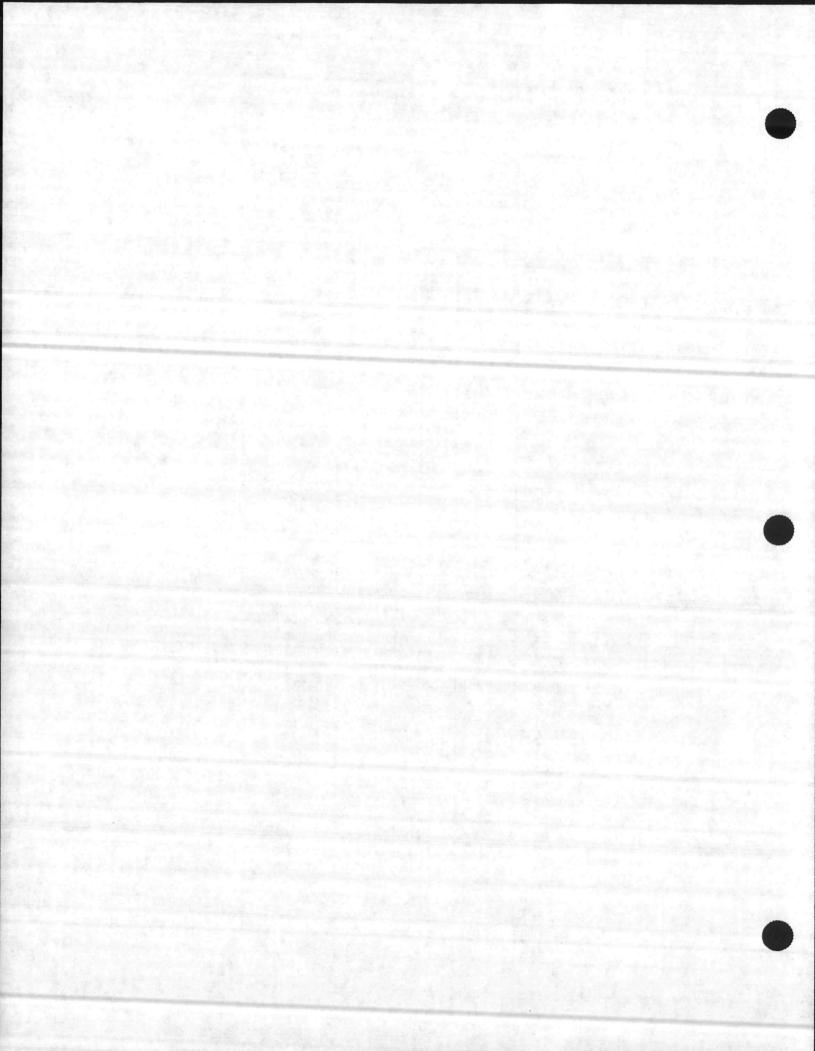
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
0.2000	7.010	0 162	12 900	13.140
0.3666	7.919	8.163	12.890	13.140
0.3833	7.919	8.163 8.170	12.890 12.890	13.140
0.4000	7.919 7.919	8.163	12.875	13.140
0.4166 0.4333	7.919	8.170	12.875	13.140
0.4500	7.919	8.163	12.875	13.140
0.4666	7.919	8.170	12.875	13.140
0.4833	7.913	8.170	12.875	13.140
0.5000	7.919	8.163	12.875	13.140
0.5166	7.919	8.163	12.890	13.140
0.5333	7.919	8.163	12.875	13.140
0.5500	7.919	8.163	12.875	13.140
0.5666	7.919	8.163	12.875	13.140
0.5833	7.919	8.163	12.875	13.140
0.6000	7.919	8.170	12.875	13.140
0.6166	7.919	8.170	12.890	13.140
0.6333	7.919	8.170	12.890	13.140
0.6500	7.919	8.170	12.890	13.140
0.6666	7.913	8.170	12.875	13.140
0.6833	7.919	8.163	12.890	13.140
0.7000	7.913	8.170	12.875	13.140
0.7166	7.919	8.170	12.890	13.140
0.7333	7.919	8.170	12.875	13.140
0.7500	7.919	8.163	12.875	13.140
0.7666	7.913	8.170	12.890	13.140
0.7833	7.919	8.163	12.875	13.140
0.8000	7.919	8.163	12.890	13.140
0.8166	7.919	8.170	12.875	13.140
0.8333	7.919	8.170	12.875	13.140
0.8500	7.919	8.163	12.875	13.140
0.8666	7.919	8.170	12.890	13.140
0.8833	7.919	8.163	12.875	13.140
0.9000	7.919	8.163	12.890	13.140
0.9166	7.919	8.163	12.890	13.140
0.9333	7.919	8.170	12.875	13.140
0.9500	7.919	8.170	12.875	13.140
0.9666	7.919	8.163	12.890	13.140
0.9833	7.919	8.163	12.875	13.140
1.0000	7.919	8.163	12.890	13.140
1.2000	7.919	8.163	12.875	13.140
1.4000	7.919	8.170	12.875	13.140
1.6000	7.919	8.163	12.875	13.140



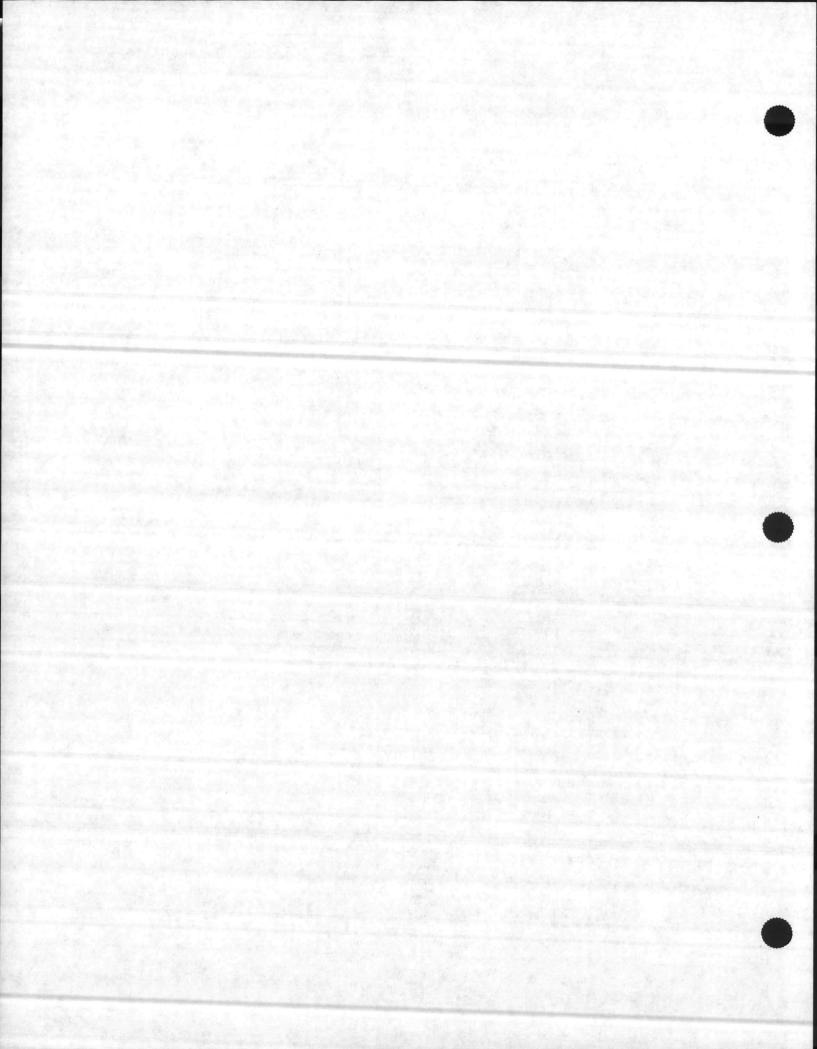
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
1.8000	7.919	8.163	12.875	13.124
2.0000	7.913	8.163	12.875	13.140
2.2000	7.919	8.170	12.875	13.140
2.4000	7.913	8.163	12.875	13.140
2.6000	7.913	8.163	12.875	13.140
2.8000	7.913	8.163	12.890	13.140
3.0000	7.913	8.163	12.875	13.140
3.2000	7.913	8.163	12.875	13.140
3.4000	7.913	8.163	12.890	13.140
3.6000	7.913	8.163	12.875	13.140
3.8000	7.913	8.163	12.875	13.140
4.0000	7.913	8.163	12.890	13.140
4.2000	7.913	8.163	12.875	13.140
4.4000	7.913	8.163	12.890	13.140
4.6000	7.913	8.163	12.875	13.140
4.8000	7.913	8.163	12.875	13.140
5.0000	7.913	8.163	12.875	13.140
5.2000	7.919	8.163	12.875	13.140
5.4000	7.913	8.163	12.875	13.140
5.6000	7.913	8.163	12.875	13.140
5.8000	7.913	8.163	12.875	13.140
6.0000	7.913	8.163	12.875	13.140
6.2000	7.919	8.163	12.875	13.140
6.4000	7.913	8.163	12.875	13.140
6.6000	7.913	8.163	12.875	13.140
6.8000	7.913	8.163	12.875	13.140
7.0000	7.919	8.163	12.875	13.140
7.2000	7.913	8.163	12.875	13.140
7.4000	7.913	8.170	12.875	13.140
7.6000	7.913	8.163	12.875	13.140
7.8000	7.913	8.163	12.875	13.140
8.0000	7.913	8.163	12.875	13.140
8.2000	7.913	8.163	12.875	13.124
8.4000	7.913	8.170	12.875	13.140
8.6000	7.919	8.170	12.875	13.140
8.8000	7.913	8.163	12.875	13.140
9.0000	7.919	8.163	12.875	13.140
9.2000	7.913	8.163	12.875	13.140
9.4000	7.913	8.163	12.875	13.140
9.6000	7.919	8.170	12.890	13.140
9.8000	7.919	8.170	12.890	13.140
10.0000	7.919	8.170	12.890	13.156



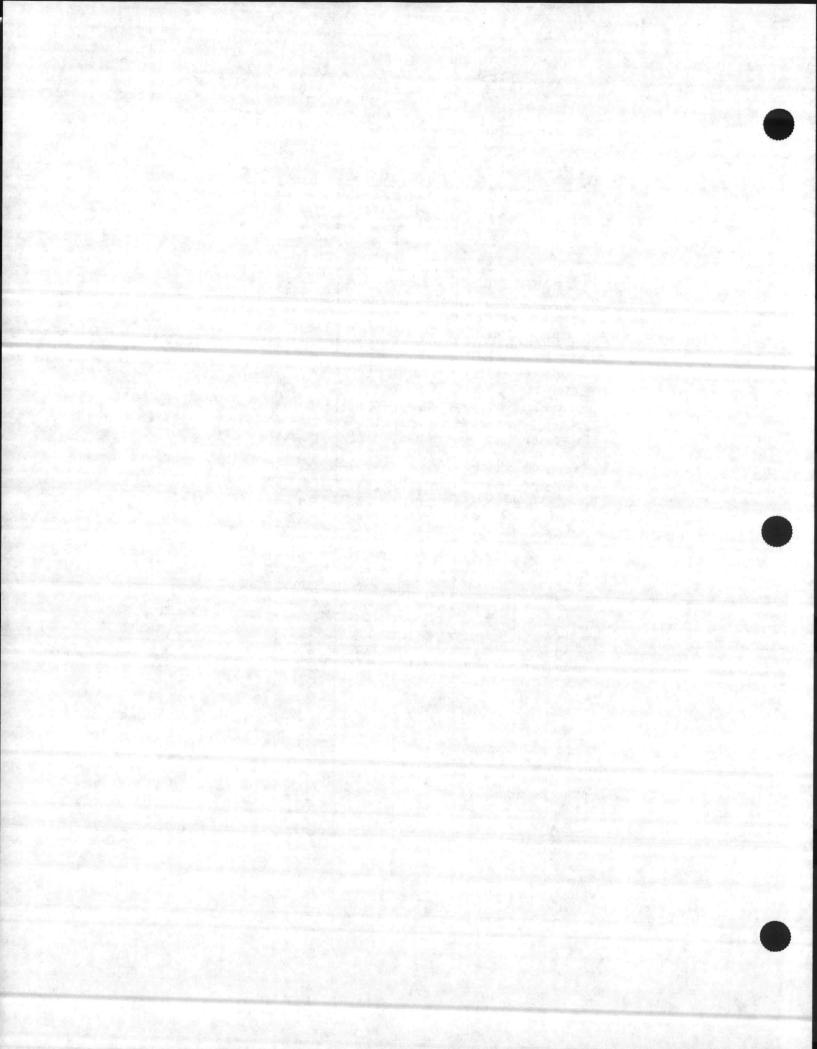
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
12.0000	7.919	8.170	12.890	13.156
14.0000	7.919	8.163	12.890	13.156
16.0000	7.913	8.170	12.890	13.156
18.0000	7.913	8.163	12.890	13.156
20.0000	7.919	8.163	12.890	13.156
22.0000	7.913	8.163	12.890	13.156
24.0000	7.913	8.163	12.890	13.156
26.0000	7.913	8.163	12.890	13.156
28.0000	7.913	8.163	12.890	13.140
30.0000	7.913	8.163	12.890	13.156
32.0000	7.913	8.163	12.890	13.140
34.0000	7.907	8.163	12.890	13.140
36.0000	7.907	8.163	12.890	13.156
38.0000	7.907	8.163	12.890	13,156
40.0000	7.907	8.170	12.890	13.156
42.0000	7.907	8.163	12.890	13.156
44.0000	7.907	8.163	12.890	13.156
46.0000	7.907	8.163	12.890	13.140
48.0000	7.907	8.157	12.890	13.156
50.0000	7.907	8.157	12.890	13.156
52.0000	7.900	8.157	12.890	13.156
54.0000	7.900	8.151	12.890	13.140
56.0000	7.900	8.151	12.890	13.156
58.0000	7.900	8.151	12.890	13.156
60.0000	7.894	8.145	12.890	13.156
62.0000	7.900	8.145	12.890	13.156
64.0000	7.894	8.145	12.890	13.156
66.0000	7.894	8.138	12.890	13.156
68.0000	7.894	8.138	12.890	13.156
70.0000	7.894	8.138	12.890	13.156
72.0000	7.887	8.132	12.890	13.156
74.0000	7.887	8.126	12.890	13.140
76.0000	7.887	8.119	12.890	13.156
78.0000	7.881	8.119	12.890	13.140
80.0000	7.881	8.113	12.875	13.156
82.0000	7.881	8.113	12.890	13.156
	7.875	8.113	12.890	13.156
84.0000	7.881	8.113	12.890	13.140
86.0000	THE PERSON NAMED OF THE PE	The state of the s	12.890	13.156
88.0000	7.875	8.107	A CONTRACTOR OF THE PARTY OF TH	13.156
90.0000	7.875	8.100	12.890	13.130
92.0000 94.0000	7.875 7.875	8.100 8.094	12.890 12.890	13.140



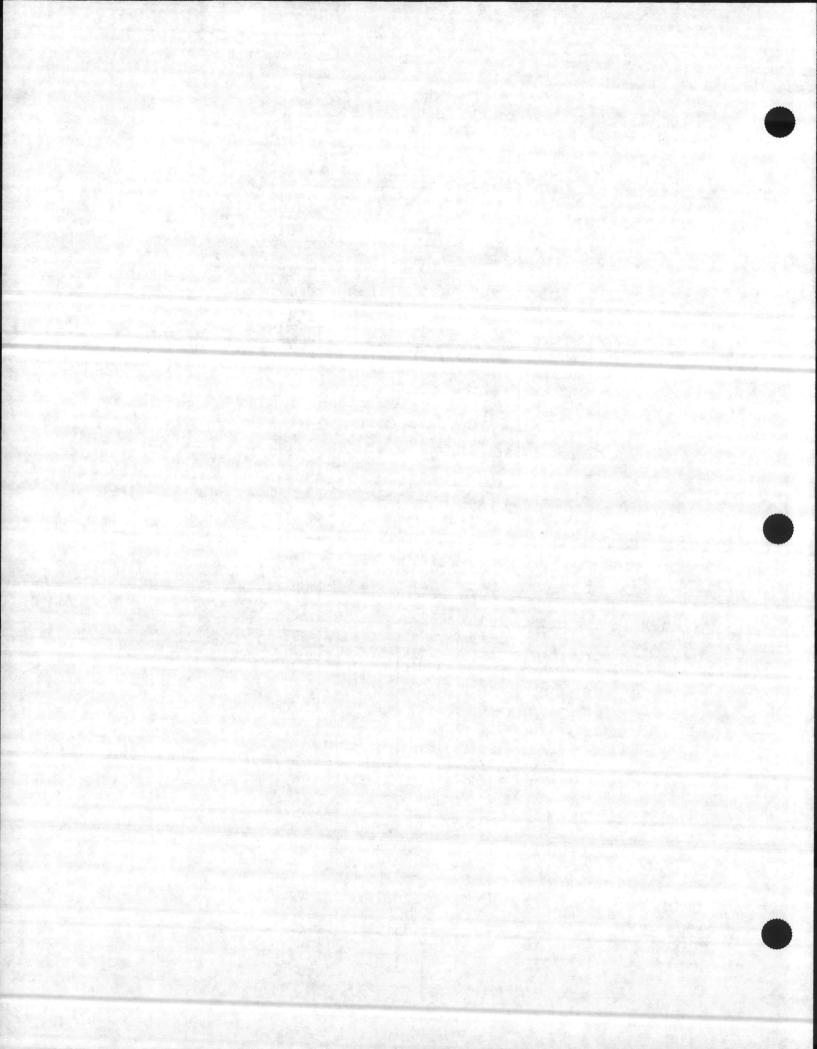
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(MIN)	SWL (FEET)	SWL (FEET)	SWL (FEET)	SWL (FEET)
(MIN)	(FEEI)	(PEEI)	(FEET)	(PEEI)
96.0000	7.868	8.094	12.890	13.140
98.0000	7.868	8.088	12.890	13.140
100.0000	7.862	8.088	12.890	13.140
105.0000	7.862	8.081	12.890	13.140
110.0000	7.855	8.075	12.875	13.140
115.0000	7.849	8.075	12.875	13.140
120.0000	7.849	8.069	12.875	13.140
125.0000	7.843	8.069	12.875	13.140
130.0000	7.836	8.069	12.875	13.140
135.0000	7.836	8.056	12.875	13.140
140.0000	7.830	8.056	12.875	13.140
145.0000	7.823	8.050	12.875	13.124
150.0000	7.823	8.044	12.875	13.124
155.0000	7.817	8.037	12.875	13.124
160.0000	7.817	8.031	12.875	13.140
165.0000	7.811	8.025	12.875	13.140
170.0000	7.811	8.025	12.875	13.140
175.0000	7.804	8.018	12.875	13.140
180.0000	7.798	8.012	12.859	13.140
185.0000	7.798	8.006	12.875	13.140
190.0000	7.791	8.006	12.859	13.124
195.0000	7.791	8.000	12.859	13.140
200.0000	7.791	8.000	12.859	13.140
205.0000	7.785	7.993	12.859	13.140
210.0000	7.785	7.987	12.875	13.140
215.0000	7.779	7.987	12.859	13.124
220.0000	7.779	7.981	12.859	13.124
225.0000	7.772	7.981	12.875	13.124
230.0000	7.766	7.974	12.859	13.124
235.0000	7.766	7.968	12.859	13.140
240.0000	7.766	7.962	12.859	13.124
245.0000	7.759	7.962	12.859	13.140
250.0000	7.759	7.962	12.859	13.140
255.0000	7.753	7.955	12.859	13.140
260.0000	7.753	7.949	12.859	13.140
265.0000	7.747	7.949	12.859	13.124
270.0000	7.747	7.943	12.859	13.124
275.0000	7.740	7.943	12.859	13.124
280.0000	7.740	7.936	12.859	13.140
285.0000	7.740	7.930	12.859	13.124
290.0000	7.734	7.924	12.859	13.124
295.0000	7.734	7.918	12.859	13.124



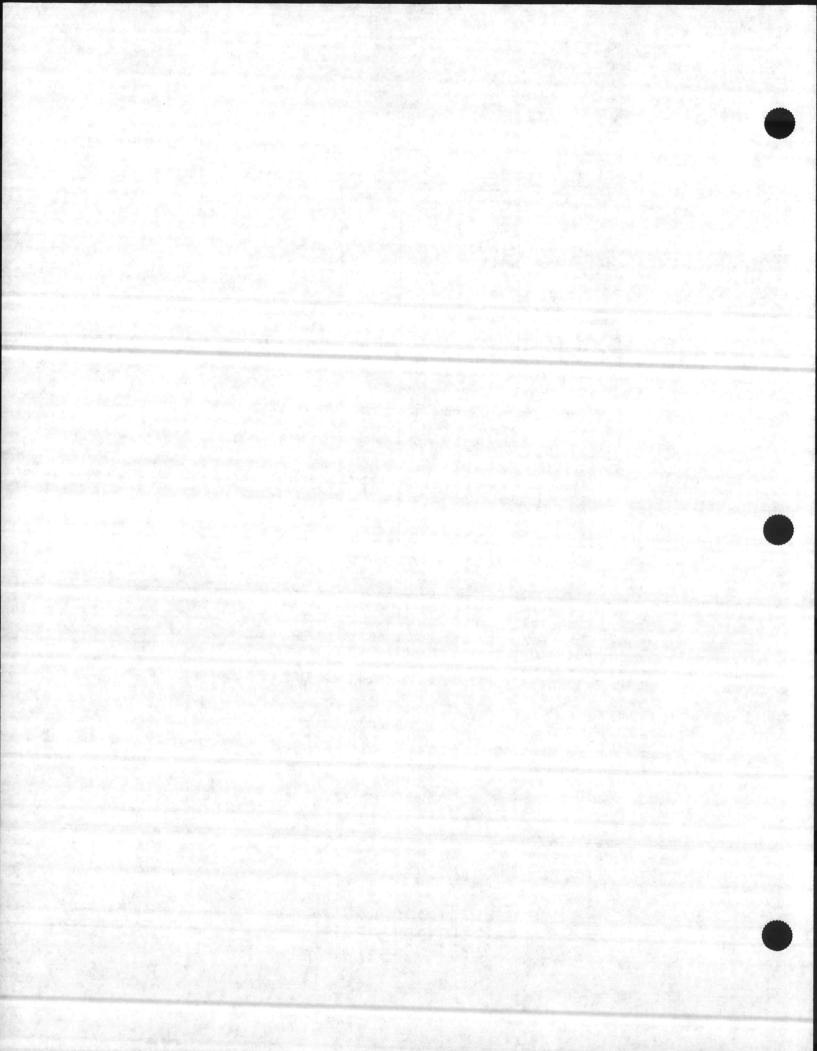
ELAPSED		WELL N	JMBER	
TIME	P-1	24-1	24-2	24-3
(ACD)	SWL (FEET)	SWL	SWL (FEET)	SWL (FEET)
(MIN)	(FEEI)	(FEET)	(FEEI)	(PEET)
300.0000	7.727	7.918	12.859	13.124
305.0000	7.727	7.911	12.859	13.124
310.0000	7.721	7.905	12.859	13.124
315.0000	7.721	7.905	12.859	13.124
320.0000	7.721	7.905	12.859	13.124
325.0000	7.721	7.899	12.859	13.124
330.0000	7.715	7.899	12.843	13.124
335.0000	7.715	7.892	12.859	13.124
340.0000	7.708	7.886	12.859	13.124
345.0000	7.708	7.886	12.859	13.124
350,0000	7.702	7.880	12.843	13.124
355.0000	7.702	7.873	12.843	13.124
360.0000	7.702	7.873	12.843	13.124
365.0000	7.695	7.861	12.843	13.124
370.0000	7.695	7.861	12.843	13.124
375.0000	7.695	7.861	12.843	13.124
380.0000	7.689	7.854	12.843	13.124
385.0000	7.689	7.854	12.843	13.109
390.0000	7.683	7.848	12.843	13.109
395.0000	7.683	7.848	12.843	13.109
400.0000	7.683	7.842	12.843	13.109
405.0000	7.676	7.842	12.843	13.109
410.0000	7.676	7.836	12.843	13.109
415.0000	7.676	7.836	12.843	13.109
420.0000	7.676	7.829	12.843	13.109
425.0000	7.670	7.829	12.843	13.109
430.0000	7.670	7.823	12.843	13.109
435.0000	7.670	7.823	12.843	13.109
440.0000	7.663	7.823	12.843	13.109
445.0000	7.663	7.817	12.828	13.109
450.0000	7.663	7.817	12.828	13.109
455.0000	7.663	7.817	12.828	13.109
460.0000	7.657	7.810	12.828	13.109
465.0000	7.657	7.810	12.843	13.109
470.0000	7.657	7.810	12.843	13.109
475.0000	7.657	7.804	12.828	13.109
480.0000	7.657	7.804	12.828	13.093
485.0000	7.650	7.804	12.828	13.109
490.0000	7.650	7.798	12.828	13.109
495.0000	7.650	7.798	12.828	13.109
500.0000	7.650	7.798	12.828	13.109
505.0000	7.650	7.791	12.828	13.109



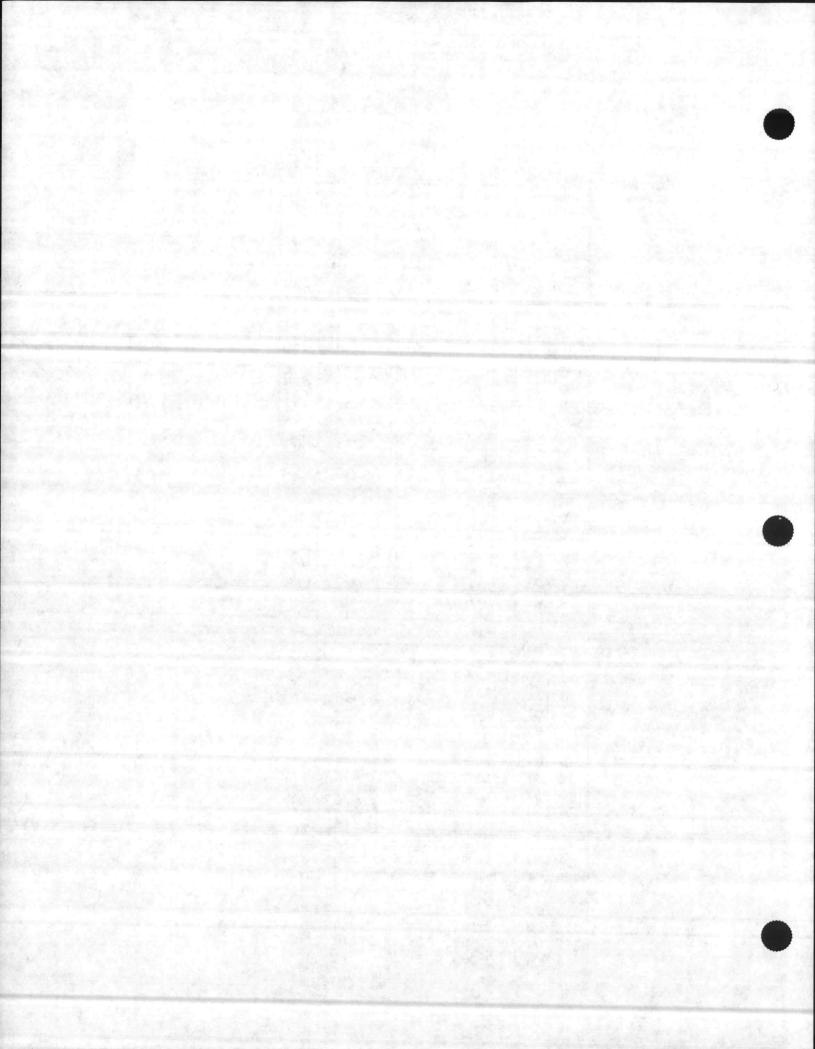
ELAPSED TIME	WELL NUMBER				
	P-1	24-1	24-2	24-3	
	SWL	SWL	SWL	SWL	
(MIN)	(FEET)	(FEET)	(FEET)	(FEET)	
(MIII4)	(PEET)	(I LLI)	(I LLI)	(I EEI)	
510.0000	7.644	7.785	12.828	13.109	
515.0000	7.644	7.785	12.828	13.109	
520.0000	7.644	7.785	12.828	13.093	
525.0000	7.638	7.779	12.843	13.109	
530.0000	7.638	7.779	12.828	13.093	
535.0000	7.638	7.779	12.828	13.093	
540.0000	7.638	7.779	12.828	13.109	
545.0000	7.638	7.772	12.828	13.109	
550.0000	7.631	7.766	12.828	13.093	
555.0000	7.631	7.772	12.828	13.109	
560.0000	7.631	7.772	12.828	13.109	
565.0000	7.631	7.766	12.828	13.109	
570.0000	7.631	7.766	12.828	13.109	
575.0000	7.625	7.760	12.828	13.109	
580.0000	7.625	7.760	12.828	13.109	
585.0000	7.631	7.760	12.828	13.093	
590.0000	7.625	7.760	12.828	13.109	
595.0000	7.625	7.754	12.828	13.109	
600.0000	7.625	7.754	12.828	13.109	
605.0000	7.618	7.747	12.828	13.109	
610.0000	7.618	7.747	12.828	13.093	
615.0000	7.618	7.747	12.828	13.109	
620.0000	7.618	7.741	12.828	13.109	
625.0000	7.612	7.741	12.828	13.093	
630.0000	7.612	7.735	12.828	13.109	
635.0000	7.612	7.735	12.828	13.093	
640.0000	7.612	7.735	12.828	13.109	
645.0000	7.612	7.728	12.828	13.109	
650.0000	7.612	7.722	12.828	13.093	
655.0000	7.606	7.722	12.828	13.093	
660.0000	7.606	7.716	12.828	13.093	
665.0000	7.599	7.716	12.828	13.093	
670.0000	7.599	7.709	12.812	13.093	
675.0000	7.606	7.709	12.828	13.093	
680.0000	7.599	7.709	12.828	13.109	
685.0000	7.599	7.709	12.828	13.093	
690.0000	7.599	7.709	12.828	13.093	
695.0000	7.599	7.703	12.828	13.093	
700.0000	7.593	7.703	12.828	13.093	
705.0000	7.593	7.703	12.828	13.093	
710.0000	7.593	7.697	12.812	13.093	
715.0000	7.593	7.691	12.828	13.093	



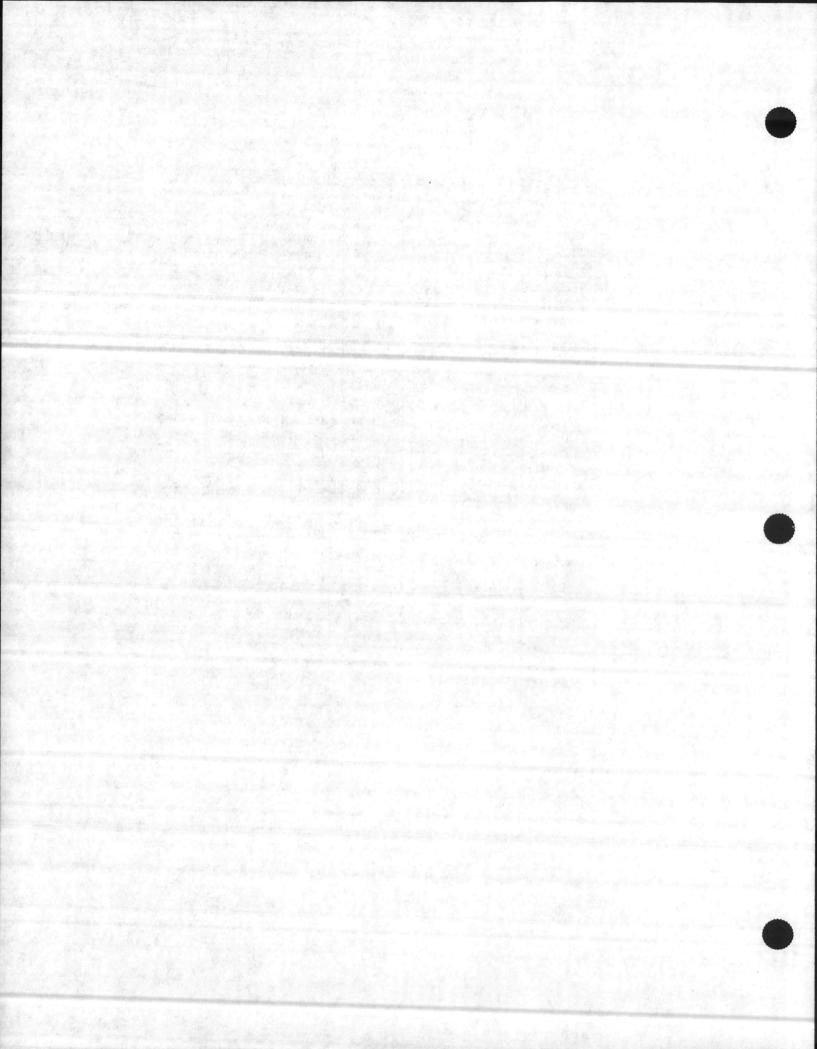
ELAPSED	WELL NUMBER				
TIME	P-1	24-1	24-2	24-3	
	SWL	SWL	SWL	SWL	
(MIN)	(FEET)	(FEET)	(FEET)	(FEET)	
<b>720 0000</b>	7.504	7.001	12.000	12 002	
720.0000	7.586	7.691	12.828	13.093	
725.0000	7.586	7.691	12.812	13.093	
730.0000	7.586	7.691	12.828	13.093	
735.0000	7.586	7.684	12.828	13.093 13.093	
740.0000	7.586	7.678	12.812		
745.0000	7.586	7.678	12.812	13.093	
750.0000	7.580	7.672	12.812	13.093	
755.0000	7.580	7.678	12.812	13.093	
760.0000	7.580	7.678	12.812	13.093	
765.0000	7.580	7.672	12.812	13.093	
770.0000	7.574	7.672	12.812	13.093	
775.0000	7.574	7.672	12.812	13.093	
780.0000	7.574	7.665	12.812	13.093	
785.0000	7.574	7.665	12.828	13.093	
790.0000	7.574	7.659	12.812	13.093	
795.0000	7.567	7.653	12.828	13.093	
800.0000	7.567	7.646	12.828	13.093	
805.0000	7.567	7.646	12.812	13.093	
810.0000	7.561	7.646	12.812	13.078	
815.0000	7.561	7.640	12.812	13.093	
820.0000	7.561	7.640	12.812	13.093	
825.0000	7.561	7.640	12.812	13.093	
830.0000	7.554	7.634	12.812	13.093	
835.0000	7.554	7.627	12.812	13.093	
840.0000	7.554	7.627	12.812	13.078	
845.0000	7.548	7.627	12.812	13.093	
850.0000	7.548	7.621	12.812	13.078	
855.0000	7.548	7.621	12.812	13.078	
860.0000	7.548	7.621	12.812	13.078	
865.0000	7.548	7.615	12.796	13.093	
870.0000	7.542	7.615	12.796	13.078	
875.0000	7.542	7.615	12.796	13.078	
880.0000	7.542	7.615	12.796	13.078	
885.0000	7.542	7.609	12.796	13.078	
890.0000	7.535	7.609	12.796	13.093	
895.0000	7.535	7.609	12.796	13.078	
900.0000	7.535	7.602	12.796	13.078	
905.0000	7.535	7.596	12.812	13.078	
910.0000	7.529	7.596	12.796	13.078	
915.0000	7.529	7.596	12.796	13.078	
920.0000	7.529	7.590	12.796	13.078	
925.0000	7.529	7.590	12.796	13.078	



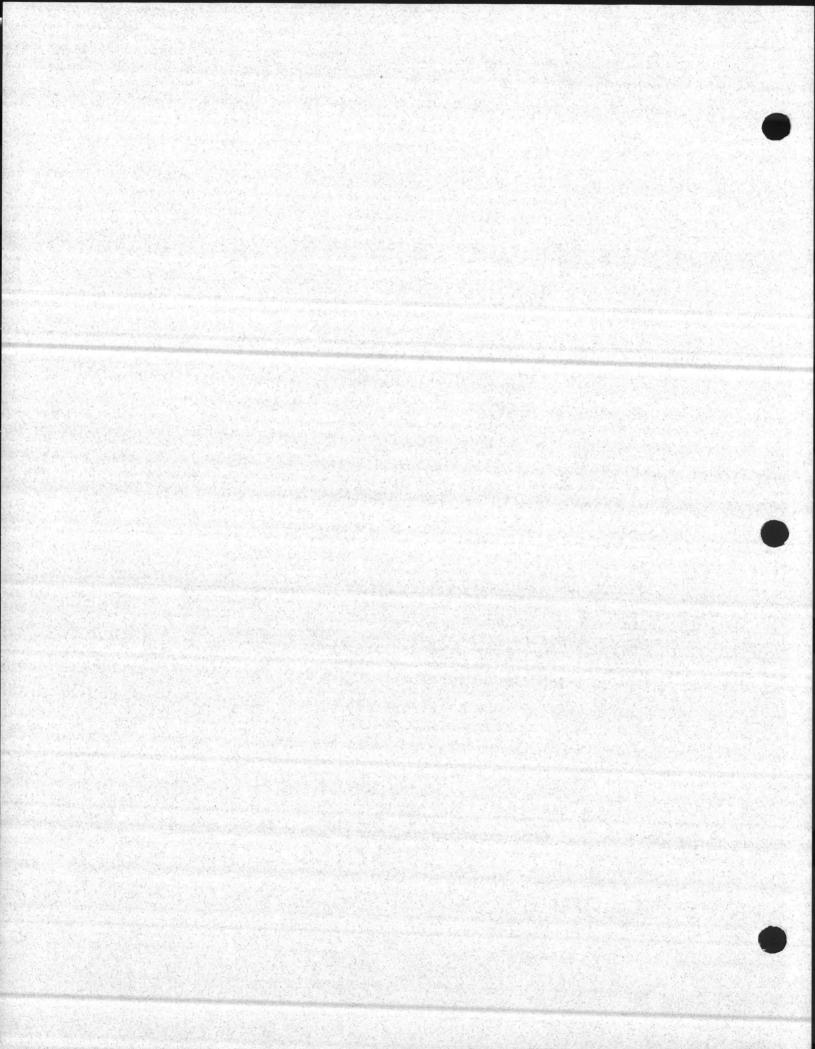
ELAPSED	WELL NUMBER			
TIME (MIN)	P-1	24-1 SWL (FEET)	24-2 SWL (FEET)	24-3 SWL (FEET)
	SWL (FEET)			
(141114)	(I DDI)	(I DDI)	(LDD1)	(LBB1)
930.0000	7.529	7.596	12.796	13.078
935.0000	7.529	7.596	12.796	13.078
940.0000	7.529	7.590	12.796	13.078
945.0000	7.522	7.590	12.796	13.078
950.0000	7.522	7.583	12.796	13.078
955.0000	7.522	7.583	12.796	13.078
960.0000	7.522	7.583	12.796	13.078
965.0000	7.522	7.583	12.796	13.078
970.0000	7.516	7.577	12.796	13.078
975.0000	7.516	7.577	12.796	13.078
980.0000	7.516	7.571	12.781	13.062
985.0000	7.516	7.571	12.796	13.062
990.0000	7.510	7.564	12.781	13.062
995.0000	7.510	7.571	12.796	13.062
1000.0000	7.510	7.564	12.796	13.062
1005.0000	7.510	7.564	12.796	13.078
1010.0000	7.503	7.558	12.796	13.062
1015.0000	7.503	7.558	12.781	13.062
1020.0000	7.503	7.558	12.781	13.062
1025.0000	7.497	7.552	12.781	13.062
1030.0000	7.497	7.552	12.781	13.062
1035.0000	7.497	7.552	12.781	13.062
1040.0000	7.497	7.552	12.781	13.062
1045.0000	7.497	7.552	12.781	13.046
1050.0000	7.497	7.552	12.781	13.062
1055.0000	7.497	7.558	12.781	13.062
1060.0000	7.497	7.552	12.781	13.062
1065.0000	7.497	7.558	12.781	13.046
1070.0000	7.497	7.558	12.781	13.062
1075.0000	7.497	7.552	12.781	13.062
			12.781	13.062
1080.0000 1085.0000	7.497	7.545 7.539	12.781	13.046
	7.490	Land to the state of the state of	12.781	13.040
1090.0000	7.490	7.545		13.062
1095.0000	7.490	7.539	12.781	13.062
1100.0000	7.490	7.539	12.781	13.046
1105.0000	7.490	7.539	12.781	13.046
1110.0000	7.490	7.539	12.781	13.046
1115.0000	7.484	7.539	12.781	
1120.0000	7.490	7.552	12.781	13.046
1125.0000	7.490	7.558	12.781	13.062
1130.0000	7.490	7.552	12.781	13.046
1135.0000	7.490	7.558	12.781	13.062



ELAPSED TIME (MIN)	WELL NUMBER			
	P-1 SWL (FEET)	24-1 SWL (FEET)	24-2 SWL (FEET)	24-3 SWL (FEET)
1145.0000	7.490	7.558	12.781	13.046
1150.0000	7,490	7.552	12.781	13.062
1155.0000	7.490	7.552	12.781	13.046
1160.0000	7.490	7.552	12.781	13.062
1165.0000	7.490	7.558	12.781	13.062
1170.0000	7.497	7.558	12.781	13.062
1175.0000	7.490	7.558	12.781	13.062
1180.0000	7.490	7.552	12.781	13.046
1185.0000	7.490	7.558	12.781	13.046
1190.0000	7.490	7.552	12.781	13.046
1195.0000	7.490	7.552	12.781	13.046
1200.0000	7.490	7.552	12.781	13.062
1205.0000	7.490	7.552	12.781	13.062
1210.0000	7.490	7.552	12.781	13.046
1215.0000	7.484	7.545	12.781	13.046
1220.0000	7.490	7.545	12.781	13.046
1225.0000	7.484	7.539	12.781	13.046
1230.0000	7.484	7.539	12.781	13.046
1235.0000	7.484	7.545	12.781	13.046
1240.0000	7.484	7.539	12.765	13.046
1245.0000	7.484	7.539	12.781	13.046
1250.0000	7.484	7.539	12.781	13.046
1255.0000	7.484	7.539	12.781	13.046
1260.0000	7.478	7.533	12.765	13.046



APPENDIX E BENCH-SCALE TREATABILITY STUDY ANALYTICAL RESULTS - GROUNDWATER CHARACTERIZATION



1600 0005

55830



January 20, 1993 Report No.: 00013053 Section A Page 1

NUS CLIENT NO:

WORK ORDER NO:

VENDOR NO:

### LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENCIRONMENTAL, INC./NAVY CLEAN

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: HP1A-GW-24-1

NUS SAMPLE NO: P0221928

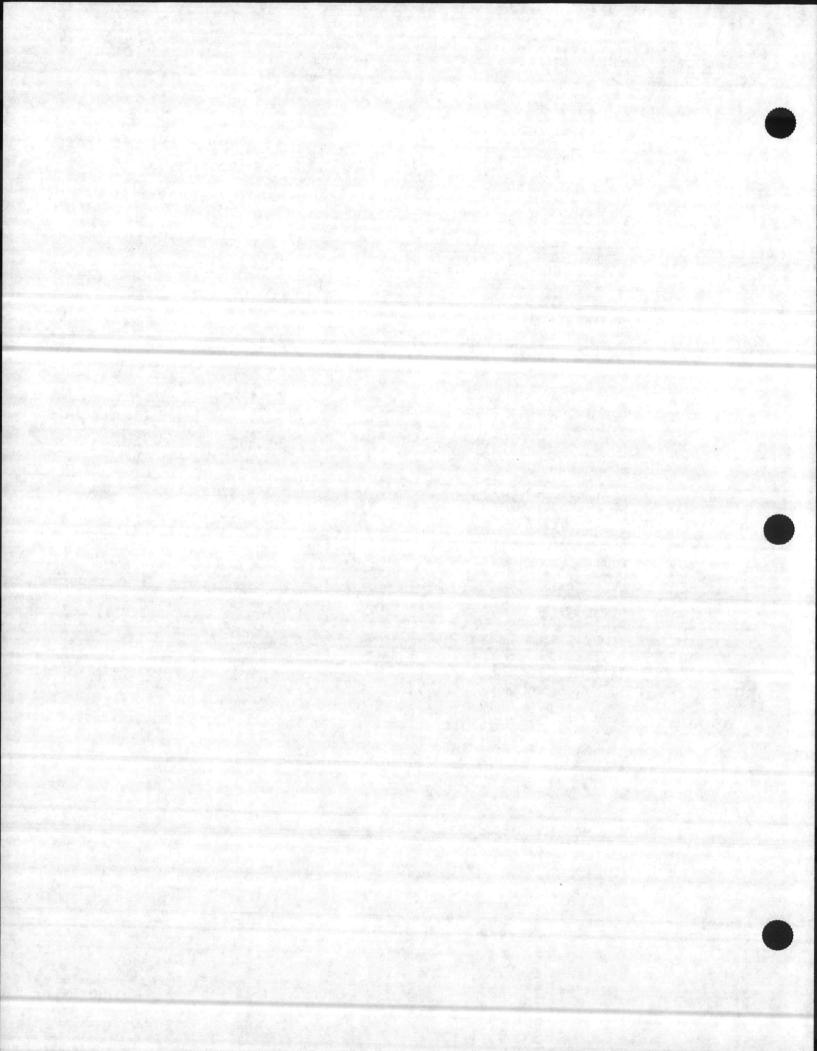
P.O. NO .:

DATE SAMPLED: 29-DEC-92

DATE RECEIVED: 31-DEC-92

APPROVED BY: Joanne Simanic

LN	CODE	DETERMINATION	RESULT	UNIT
1	1030	Ammonia (N), Direct		Total April
		Ammonia (as N), Direct	0.8	mg/L
2	1020	Alkalinity, Pht (as CaCO3)	0	mg/L
3	1023	Alkalinity, Total (as CaCO3)	35	mg/L
4	1024	Alkalinity, Bicarbonate (as CaCO3)	35	mg/L
5	1026	Alkalinity, Carbonate (as CaCO3)	0	mg/L
6	I130	Chloride (as C1)	22	mg/L
7	1320	Hardness, Total (as CaCO3)	65	mg/L
8	1391	Nitrate/Nitrite	< 0.1	mg/L
9	1410	Nitrite (as N)	< 0.02	mg/L
10	1590	Solids, Dissolved at 180C	110	mg/L
11	1610	Solids, Suspended at 103C	910	mg/L
12	1680	Oil and Grease, Gravimetric	6	mg/L
13	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
14	DPACK	CLP Data Package Deliverable	DONE	





January 20, 1993 Report No.: 00013053 Section A Page 3

#### LABORATORY ANALYSIS REPORT

CLIENT NAME:

BAKER ENCIRONMENTAL, INC./NAVY CLEAN

ADDRESS:

420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION:

MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: HP1A-GW-24-1-D

NUS SAMPLE NO: P0221930

P.O. NO .:

NUS CLIENT NO:

1600 0005

WORK ORDER NO: 55830

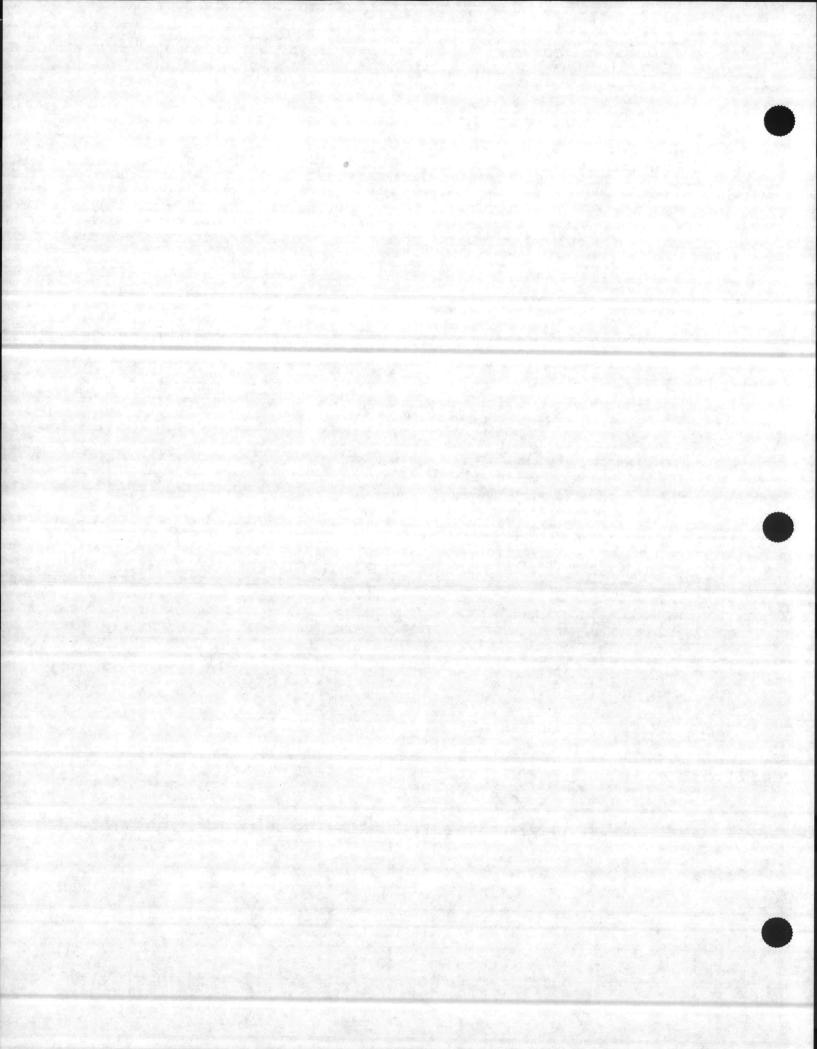
**VENDOR NO:** 

DATE SAMPLED: 29-DEC-92 DATE RECEIVED: 31-DEC-92

APPROVED BY:

Joanne Simanic

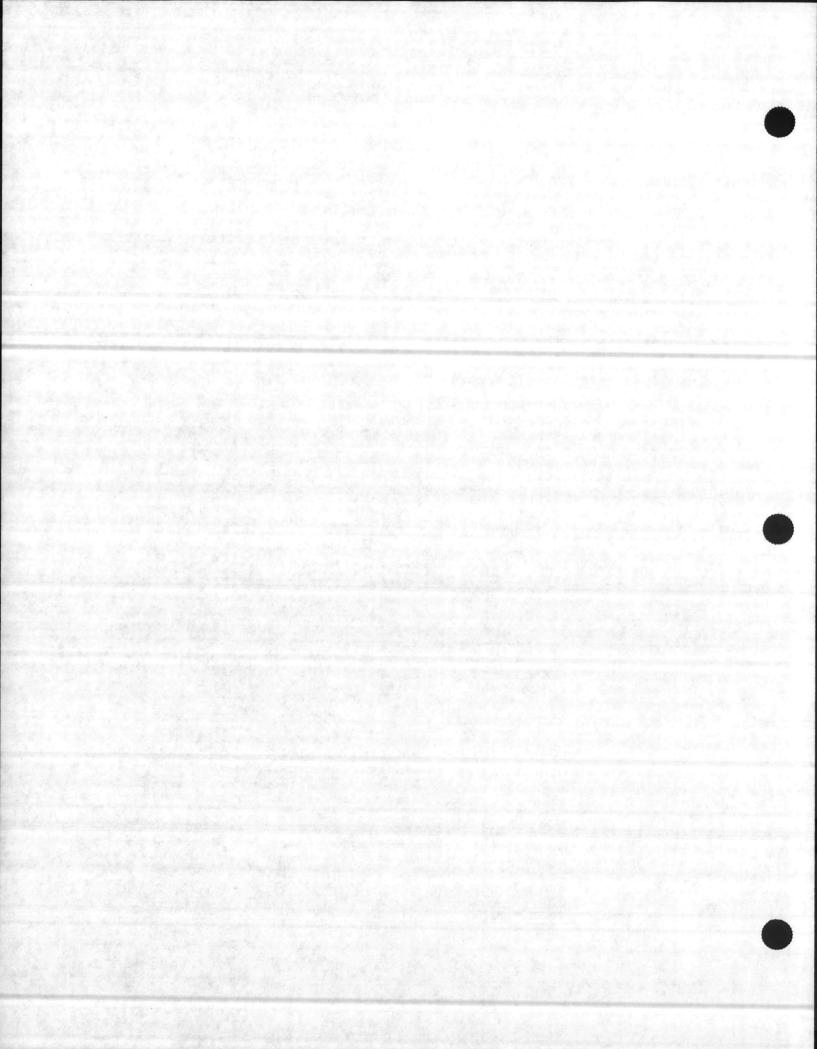
 LN	CODE	DETERMINATION	RESULT	UNITS
12	1680	Oil and Grease, Gravimetric	6	mg/L
13	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
14	DPACK	CLP Data Package Deliverable	DONE	



# U.S. EPA - CLP

				221928
			Contract:	
b Code: HNUS	Ca	se No.: BKHD	SAS No.:	SDG No.: PKG1
trix (soil/w	ater): WATE	R	Lab S	ample ID: P221928
evel (low/med	): LOW_	_	Date	Received: 12/29/92
Solids:	0.	0		
			an mother day wain	ht): UG/L
Co	ncentration	Units (ug/L	or mg/kg dry weig	
	:	1	11	
	ICAS No.	Analyte  C	oncentration C  Q	
	17429-90-5	Aluminum	259001_1	IP_I
	17440-36-0	!Antimony i	20.0:0:	
	17440-38-2	!Arsenic :	7./iBi	11-1
	17440-39-3	! Barium :	/8. UIBI	
	17440-41-7	!Bervllium;	1.0;B;	
	17440-43-9	: Cadmium i	3.0.0.	
	17440-70-2	:Calcium :	18600:_i	
	17440-47-3	!Chromium	32.0i_i_*	
	17440-48-4	!Cobalt :	8.0:0:	
	17440-50-8	Copper	14.0;B;	(F(
	17439-89-6	!Tron	264001	
	17439-92-1	!Lead :	22.41_1_	15_1
	17439-95-4	!Maonesium:	3100;B;	(
	17439-96-5	!Manoanese:	84.01_1	1 - 1
	17439-97-6	!Mercury :	0.20.01_1	4
	17440-02-0	Nickel	22.01B1	!P_!
	17440-09-7	(Potassium)	2330(B)	IF_I
	17782-49-2	!Selenium !	1.5(B)(	NiF_i
	17440-22-4	Silver		
	17440-23-5	!Sodium !	86201_1_	
	17440-28-0	(Thallium )	2.0(0)	; F;
	17440-62-2	[Vanadium_]	73.01_1	
		Zinc		IP_I
			1_1_	!NR!
			1_1_	II
olor Before:	TAN	Clarit	y Before: OFAQUE	Texture:
			The second secon	A
olor After:	COLORLESS	Clarit	y After: CLEAR_	Artifacts: _
omments:				
a manner i la esta				

FORM I - IN

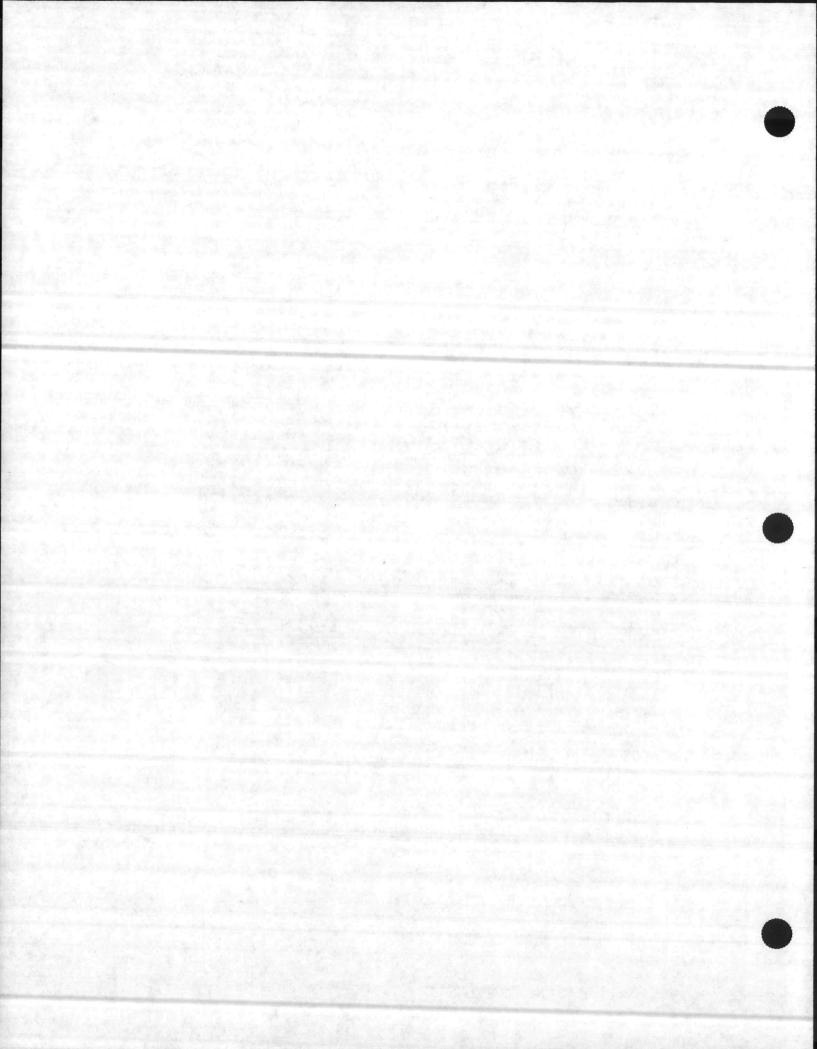


			U.S.	EPA - CLP			
		·	NORGANIC A	1 NALYSES DA	ra shee		EPA SAMPLE NO.
			MONOMINE				221929
ab Name:	HALLI	BURTON_NUS_		Contract			
.ab Code:	HNUS_	Cas	e No.: BKH	ID SAS I	No.:		SDG No.: PKG1
		ter): WATER			Lab	Samp	le ID: P221929
_evel (lo	w/med)	: LOW_			Dat	e Rec	eived: 12/29/92
% Solids:		0.0					
. Solius.		41 15 10 16 16 16 16 16 16 16 16 16 16 16 16 16				1	
	Cor	ncentration	Units (ug	/L or mg/kg	dry we	ight)	: UG/L_
		1		1			
		CAS No.	Analyte	:Concentrat	ion(C)	LA	iri i
		1 1 17429-90-5		!	!=!-		-15-1
		17429-90-5	Aluminum_	13	5.01B1_		-!!
		17/1//	' ABTIMODY				
		17440-30-2	'Arsenic		2.0101		
		17440-30-3	Bartum		THOID!		
		17/1/0-/11-7	! Pary 1 111m		1.0101		
		C TARACT	Cadmille	A	3.0101		
		17/1/0-70-7	(Calerium	1 10	10001 1		
		17110-17-3	! Checomitim		O. OIOI		
200		17110-1	'Cobalt		0.0101		
		17/1/0-50-8	!Cooper		2.0101		
		17/70-00-4	1 1000	1	77		
		17470-07-1	!! oad	A CONTRACTOR OF THE PARTY OF TH	1.0101		
		17470-05-4	Mannestum		1330101		
		17470-04-5	MADDAMESE		24. 101		
		17170 07-4	1 Marration 1	. 그 이 시시 하면서 그 아니는 생각이 그 사람들이 모르는 것	J. 20101	14	
		17440-07-0	Mickel		20.0101		
		17440-02-0	(Potassium	1 i	000101		
		17782-49-2	Selenium_	1	1.0:0:		_(F_(
		17440-22-4		1	_3.0:U:		_!P_!
		17440-23-5	Sodium		99101_		_!F_!
		17440-28-0	:Thallium_	Land the second	_2.0:0:		_[[-]
		17440-62-2		- (	4.0101		_!P_!
		17440-66-6	:Zinc	_1	57.01_		!P_!
		15955-70-0	[Cyanide_	-1			!NR!
			1	_1			
Color Be	fore:	COLORLESS	Clar	ity Before:	CLEAR_		Texture:
Color Af	ter:	COLORLESS	Clar	ity After:	CLEAR_		Artifacts:

FORM I - IN

Comments:

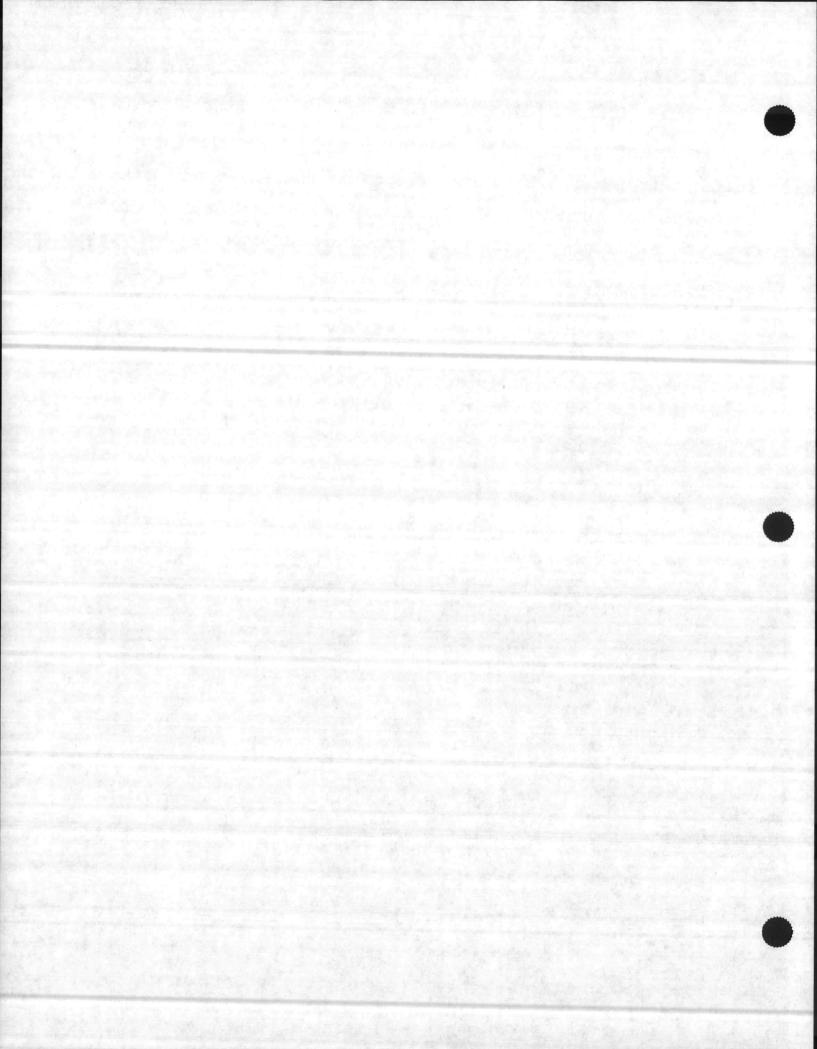
HPIA-GW-24-1\_DISSOLVED



#### U.S. EPA - CLF

	I	NORGANIC ANA	LYSES DATA SHEET	
	PURTON NUS		Contract:	221930 I
Name: HALL	BOK 1014-1409-			CDC No . PVG1
Code: HNUS	Cas	e No.: BKHD	SAS No.:	SDG No.: FKG1
trix (soil/wa	ater): WATER	3	Lab S	ample ID: P221930_
vel (low/med	): LOW_	46 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	Date	Received: 12/29/92
Solids:	0.0			
		11-it- /115/1	or mg/kg dry weig	ht): UG/L_
Co	ncentration	Units (ag/c		
	1	1	1 1	
	ICAS No.	Analyte  C	oncentration C	
	17420-90-5	Aluminum	382001_1_	1F_1
	17447-70-3	!Antimony !	20.0 U  21.6 _	{F_1
	17440-38-2	Arsenic	21.61_1_	!F_!
	17440-39-3	Barium	21.6 _  120 B	!P_!
	17/1/0 7/3-7	1 5 1 6 7 1 1 100	101001	
	7	Change III	04.01	The same of the sa
	1 - 7 4 5 40 4	(Cobolt	0.0,00	
		10	10.0101	
	17470 00 /	Thomas	303001	
	17470 07 1	11 0 3 0		
	I TO A TO OF A	INDESCRIPTION:	3020101	
	17782-49-2	Selenium_i		
	17440-22-4	isilver		
		Sodium		F I MARK TO THE REST
		{Thallium_{		IP I
		Vanadium_		
		Zinc		INRI
				1 1
	1	_11		
olor Before:	TAN	Clarit	y Before: OPAQUE	Texture:
olor After:	COLORLESS	Clarit	y After: CLEAR_	Artifacts:
	10.17			
Comments:				
HPIA-GW-24	-1-D			

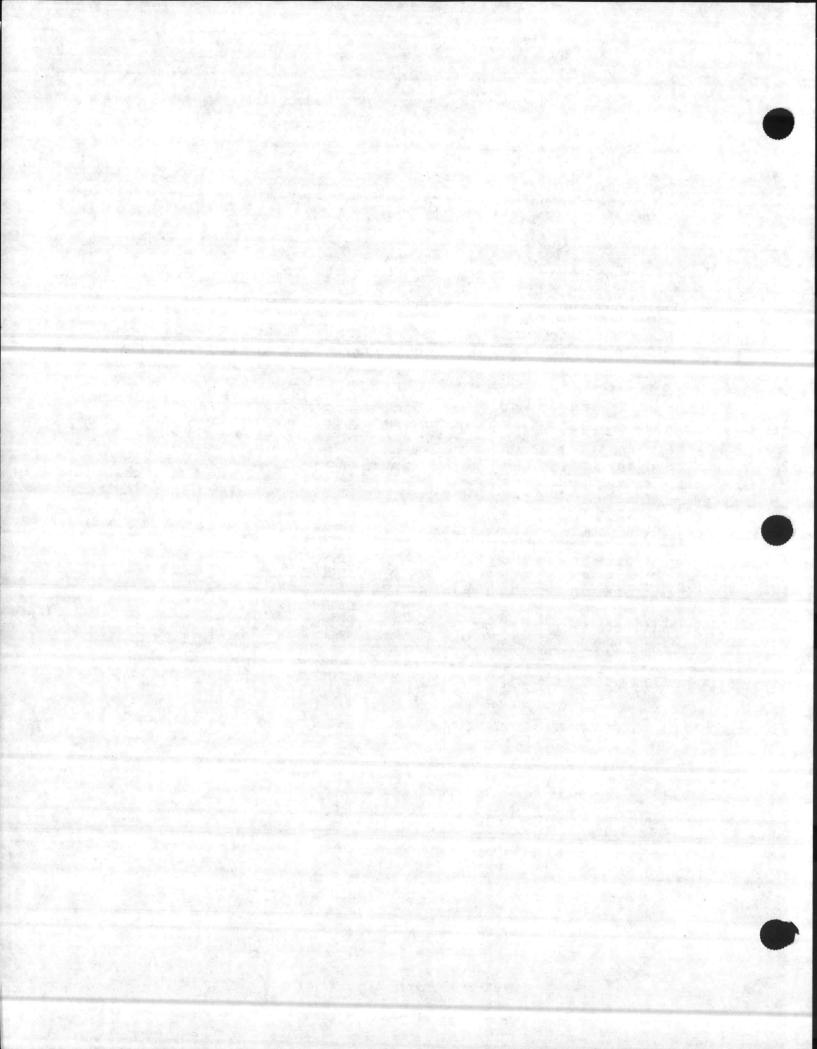
FORM I - IN



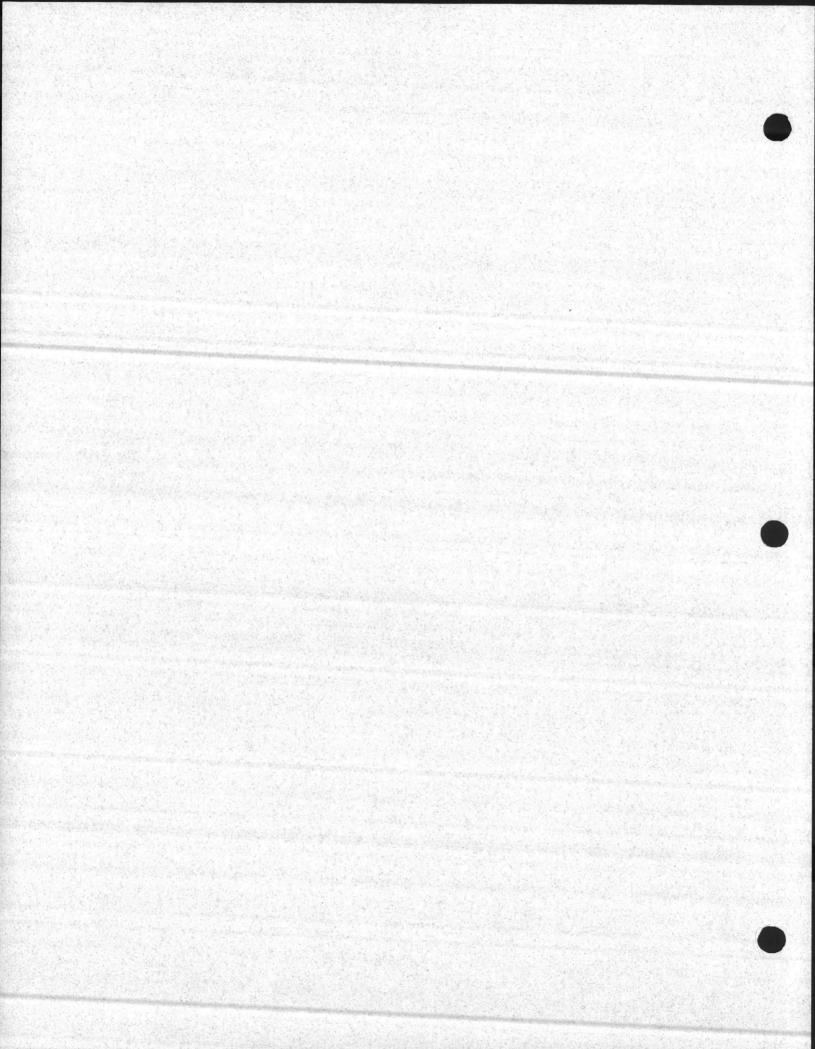
## U.S. EPA - CLP

	J	NORGANIC A	1 NALYSES DATA SHEET	
				221931
			Contract:	
b Code: HNUS	Cas	se No.: BKH	D_ SAS No.:	SDG No.: PKG1
trix (soil/w	ater): WATE	₹	Lab	Sample ID: F221931_
evel (low/med	): LOW_		Date	Received: 12/29/92
Solids:	0.0	0		
			u /ka day wai	obt): UG/L
Со			'L or mg/kg dry wei	
		1	1-1-	
	ICAS No.	: Analyte	Concentration   C	Q [M ] 
	17429-90-5	Aluminum_	40.01B1_	!E_!
	17440-36-0	Antimony_	20.0101_	[F]
	17440-38-2	Arsenic	2.0101_	
	17440-39-3	Barium	135!B!_	!P!
	17440-41-7	:Beryllium	1.0 U _	!P_
	17440-43-9	:Cadmium	5.0101_	IP_
	17440-70-2	Calcium	153001_1_ 10.01U1_ 8.01U1	IF
	17440-47-3	Chromium_	10.0101_	_*!F_!
	17440-48-4	:Cobalt	8.0 U  2.0 B  33.0 B	E P. Service
	17440-50-8	Copper	12.0 B _	
	17439-89-6	[Iron	33.0 B _	[P]
	17439-92-1	Lead	1.0 U _	F_I
	17439-95-4	: Magnesium	1.0 U _  1520 B _   26.0	
	17439-96-5	Manganese	26.01_1	
	17439-97-6	!Mercury_	0.20 U  20.0 U  820 B	_N:CV:
	17440-02-0	!Nickel	20.0101_	
	17440-09-7	Potassium	18201B1_	! <u>-</u> -
	17782-49-2	Selenium_	8201B1 1.01U1	_N
	17440-22-4	Silver	3.0:0:_	
	17440-23-5	Sodium	195101_1_	
	17440-28-0			
	17440-62-2	[Vanadium_	4.0101_	IP_
	17440-66-6	!Zinc	53.0 _	INE!
	15955-70-0	Cyanide_		
	1	1	THE RESIDENCE OF THE PROPERTY OF	
olor Before:	COLORLESS	Clari	ty Before: CLEAR_	Texture:
Color After:	COLORLESS	Clari	ty After: CLEAR_	Artifacts:
Comments:		IED		
LICA OLL SIA	-1-D DISSOL	VED	THE RESERVE THE PROPERTY OF THE PERSON OF TH	

FORM I - IN



APPENDIX F BENCH-SCALE TREATABILITY STUDY ANALYTICAL RESULTS - OIL/WATER SEPARATION





January 15, 1993 Report No.: 00012974 Section A Page 1

#### LABORATORY ANALYSIS REPORT

BAKER ENCIRONMENTAL, INC./NAVY CLEAN CLIENT NAME:

420 ROUSER ROAD ADDRESS:

CORAOPOLIS, PA 15108-

MR. JOHN LOVELY ATTENTION:

Carbon Copy:

SAMPLE ID: 930012

NUS CLIENT NO: 1600 0005

WORK ORDER NO:

DATE SAMPLED:

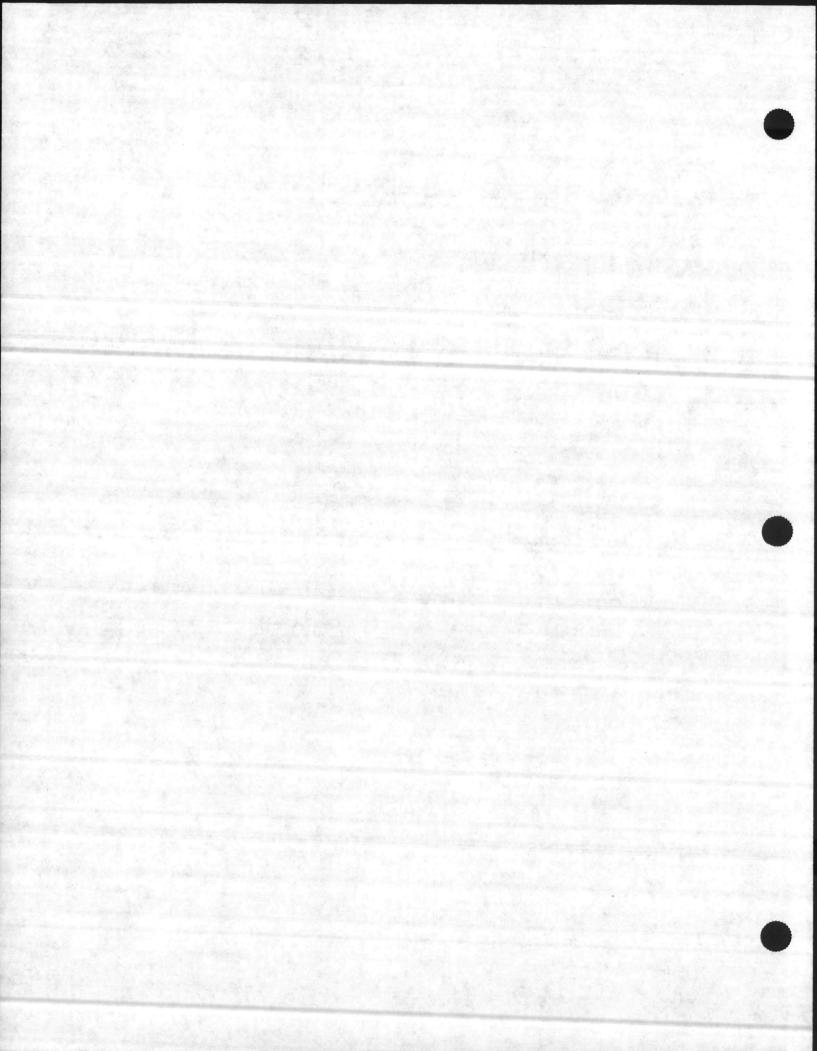
55830

05-JAN-93

VENDOR NO:

06-JAN-93 DATE RECEIVED: P0222131 NUS SAMPLE NO: Joanne Simanic APPROVED BY: P.O. NO .: CTO # 17

TEST UNIT RESULT DETERMINATION LN CODE mg/L < 3 Oil and Grease, Gravimetric **I680** 1





January 15, 1993 Report No.: 00012974

LABORATORY ANALYSIS REPORT

DETERMINATION

BAKER ENCIRONMENTAL, INC./NAVY CLEAN CLIENT NAME:

420 ROUSER ROAD ADDRESS:

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

NUS SAMPLE NO: P0222132

Section A Page 2

WORK ORDER NO:

NUS CLIENT NO: 1600 0005 55830

**VENDOR NO:** 

SAMPLE ID: 930013

P.O. NO .: CTO # 17

DATE SAMPLED: 05-JAN-93 DATE RECEIVED:

06-JAN-93

APPROVED BY:

Joanne Simanic

TEST CODE LN

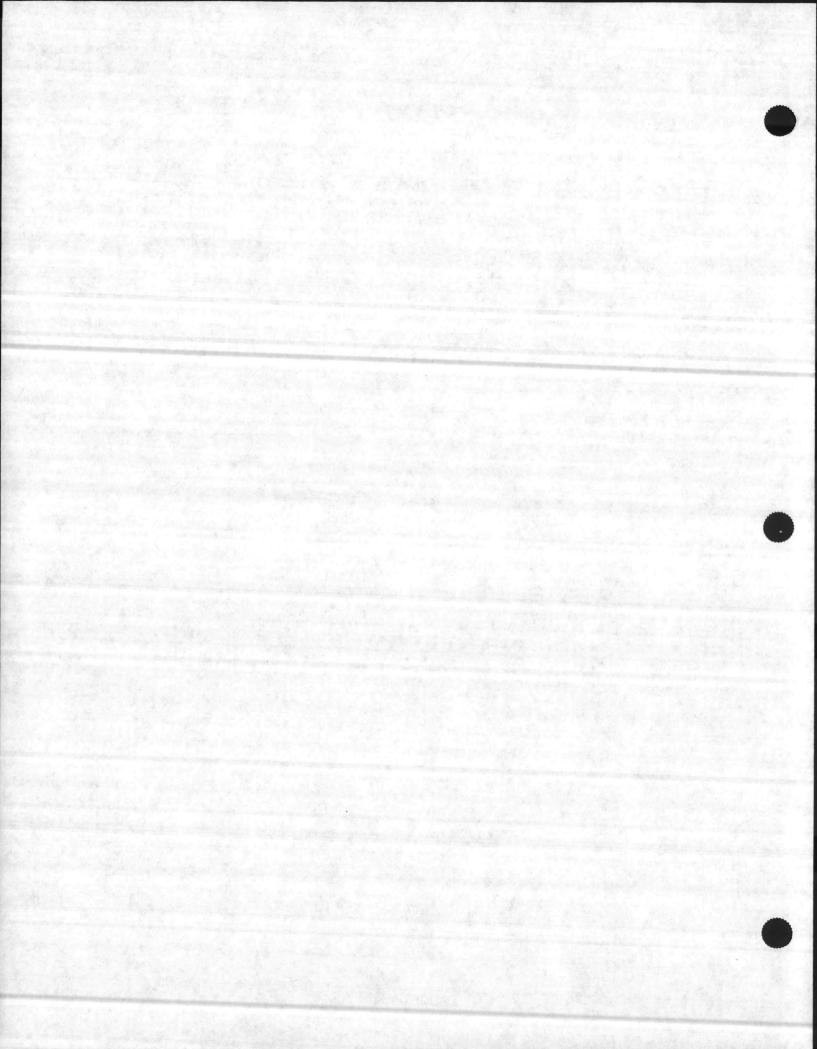
RESULT

UNITS

1680 1

Oil and Grease, Gravimetric

mg/L





January 15, 1993 Report No.: 00012974 Section A Page 3

NUS CLIENT NO: 1600 0005

55830

WORK ORDER NO:

VENDOR NO:

RESULT

< 3

LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENCIRONMENTAL, INC./NAVY CLEAN

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: 930014 NUS SAMPLE NO: P0222133

P.O. NO .: CTO # 17

DATE SAMPLED: 05-JAN-93

DATE RECEIVED: 06-JAN-93
APPROVED BY: Joanne Simanic

TEST

DETERMINATION

LN CODE

1680

Oil and Grease, Gravimetric

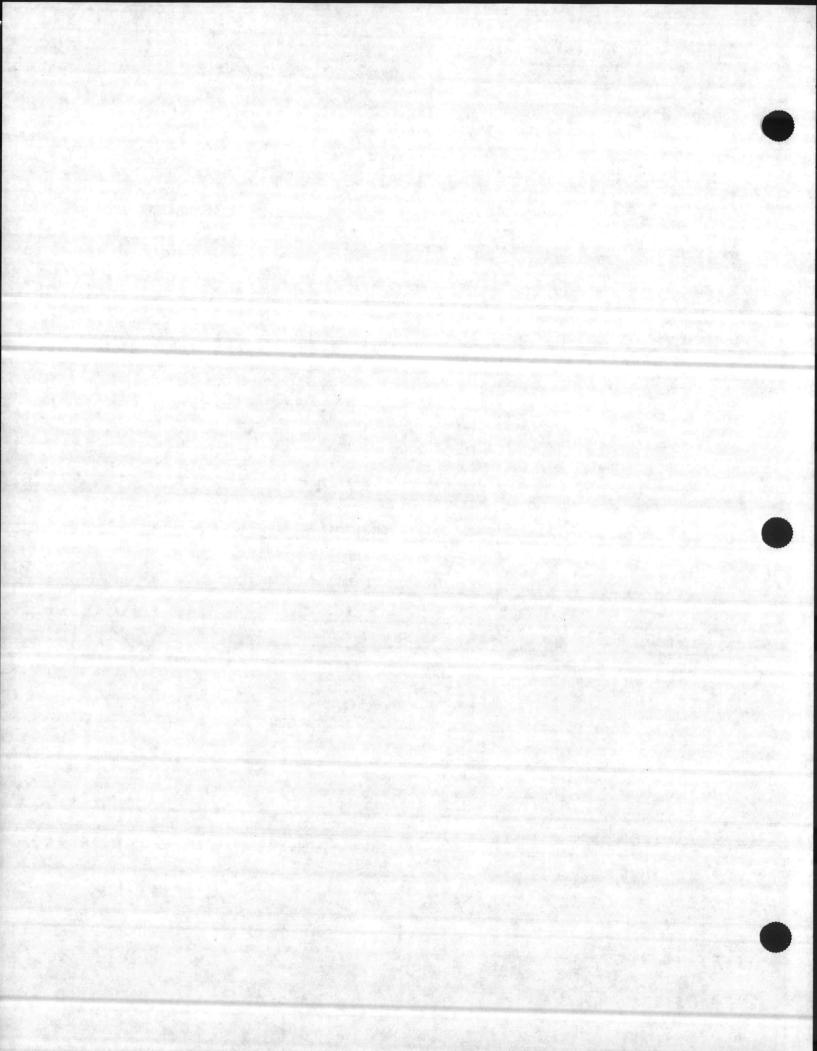
------

UNITS

mg/L

COMMENTS:

1





January 15, 1993 Report No.: 00012974 Section A Page 4

#### LABORATORY ANALYSIS REPORT

CLIENT NAME:

BAKER ENCIRONMENTAL, INC./NAVY CLEAN

ADDRESS:

420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION:

MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: 930015

NUS SAMPLE NO: P0222134

P.O. NO.: CTO # 17

NUS CLIENT NO: 1600 0005

WORK ORDER NO: 55830

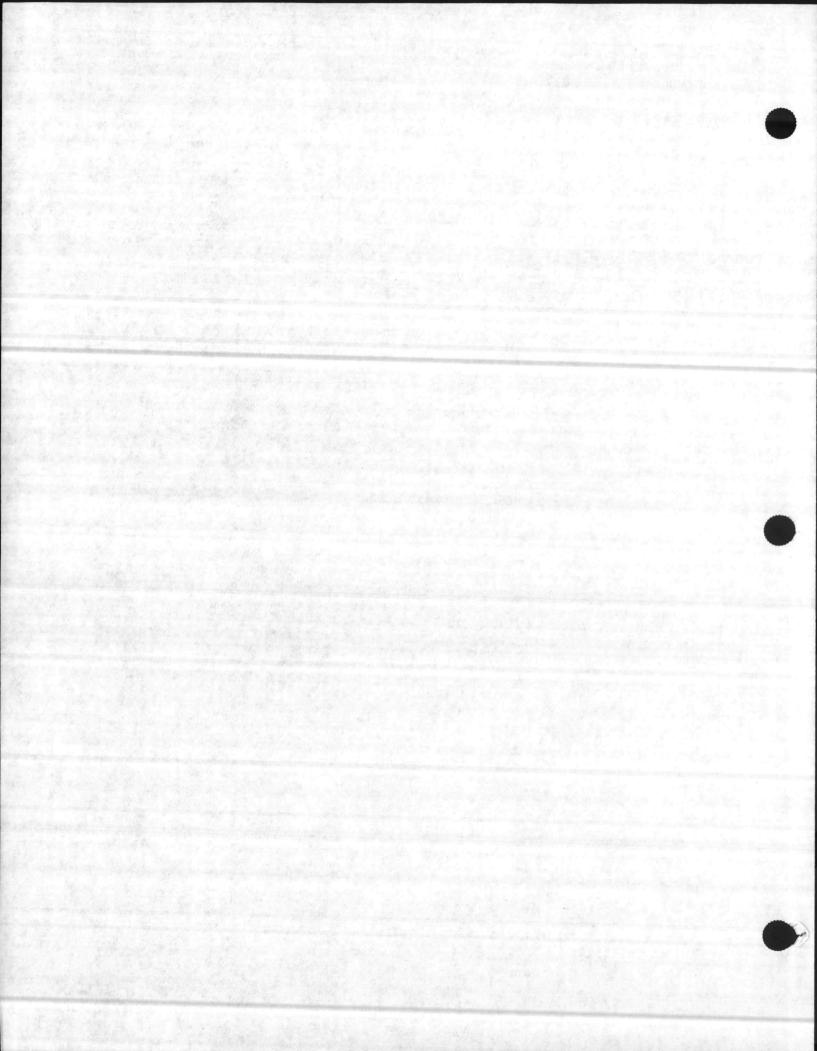
VENDOR NO:

DATE SAMPLED: 05-JAN-93
DATE RECEIVED: 06-JAN-93

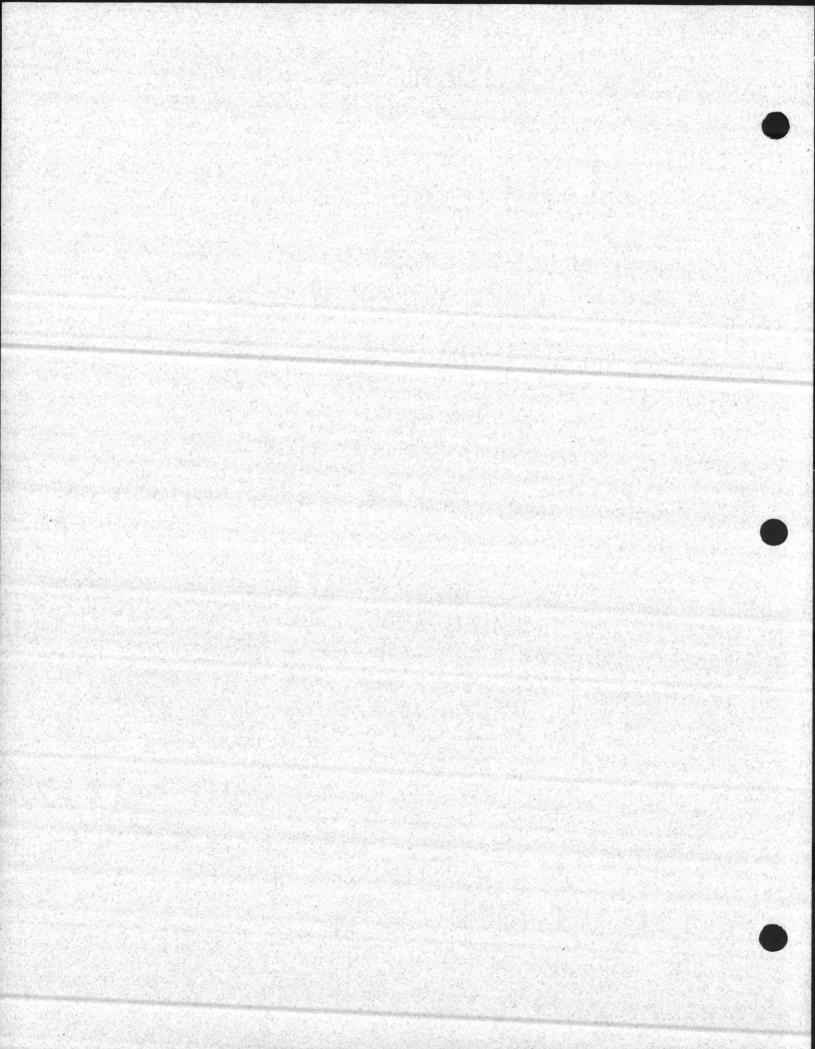
APPROVED BY:

Joanne Simanic

LN	TEST	DETERMINATION	RESULT	UNITS
 1	1680	Oil and Grease, Gravimetric	< 3	mg/L



APPENDIX G BENCH-SCALE TREATABILITY STUDY ANALYTICAL RESULTS - SOLIDS SETTLING





February 23, 1993 Report No.: 00013685 Section A Page 1

#### LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

Solids, Suspended at 103C

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: 930016 NUS SAMPLE NO: P0225090

P.O. NO .: CTO # 19017

NUS CLIENT NO: 1600 0006

05-FEB-93

05-FEB-93

mg/L

Joanne Simanic

WORK ORDER NO: 55830

VENDOR NO:

DATE SAMPLED:

DATE RECEIVED:

62

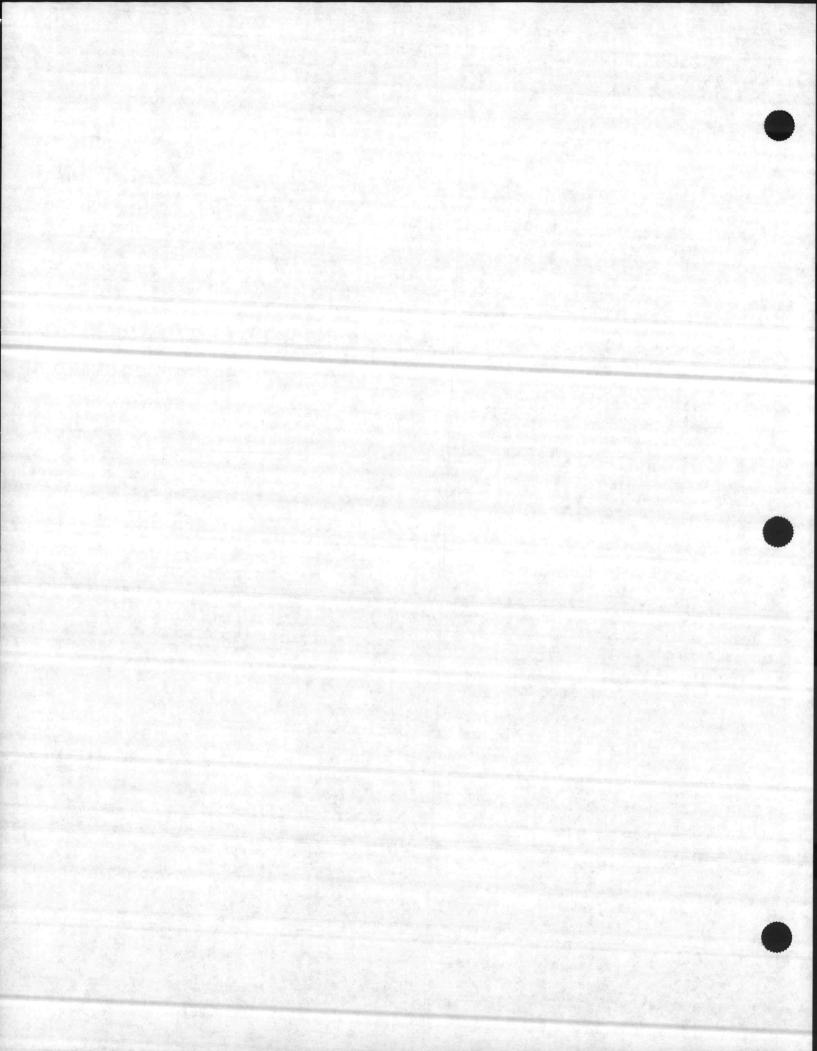
APPROVED BY:

TEST
LN CODE DETERMINATION RESULT UNIT

COMMENTS:

**I610** 

CLEVELAND (216) 891-4700 HOUSTON (713) 488-1810 PITTSBURGH (412) 747-2580





February 23, 1993 Report No.: 00013685 Section A Page 3

NUS CLIENT NO: 1600 0006

55830

WORK ORDER NO:

VENDOR NO:

#### LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

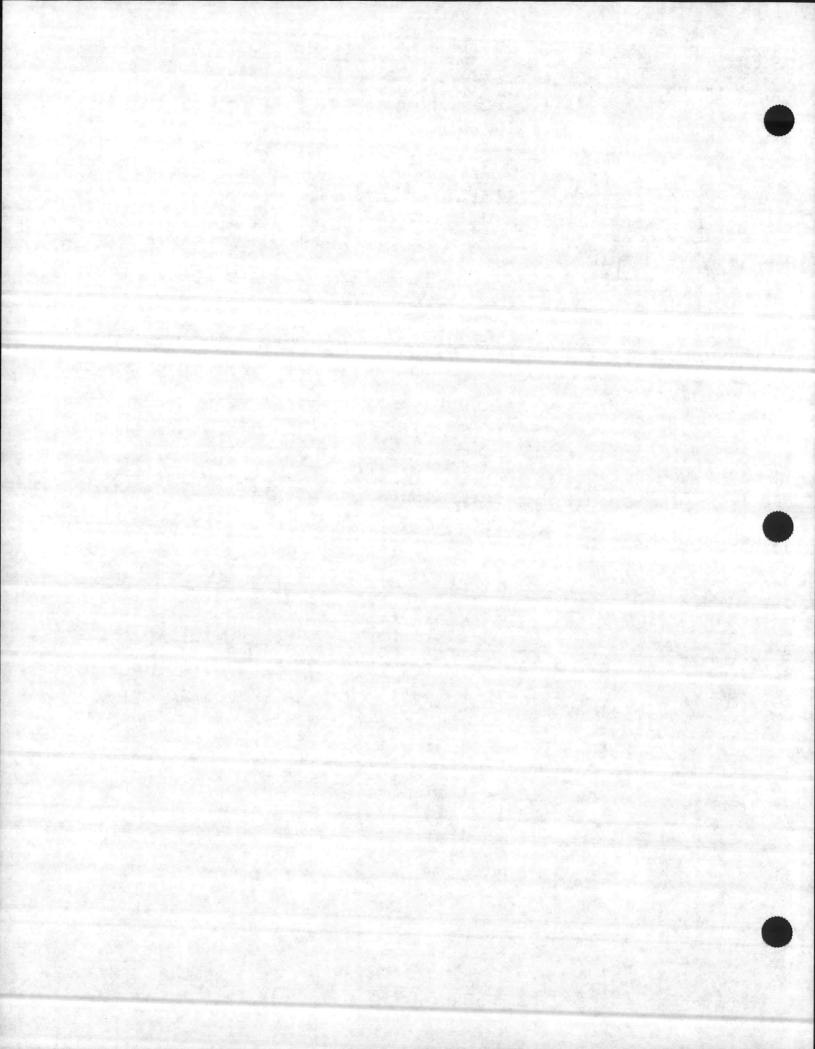
Carbon Copy:

SAMPLE ID: 930018

NUS SAMPLE NO: P0225092 P.O. NO.: CTO \* 19017 DATE SAMPLED: 05-FEB-93
DATE RECEIVED: 05-FEB-93

DATE RECEIVED: 05-FEB-93
APPROVED BY: Joanne Simanic

LN	TEST CODE	DETERMINATION	RESULT	UNITS
1	T610	Solids, Suspended at 103C	48	mg/L





February 23, 1993 Report No.: 00013685 Section A Page 4

#### LABORATORY ANALYSIS REPORT

CLIENT NAME:

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

NUS CLIENT NO:

1600 0006

WORK ORDER NO: 55830

VENDOR NO:

SAMPLE ID: 930019

NUS SAMPLE NO: P0225093

P.O. NO.: CTO # 19017

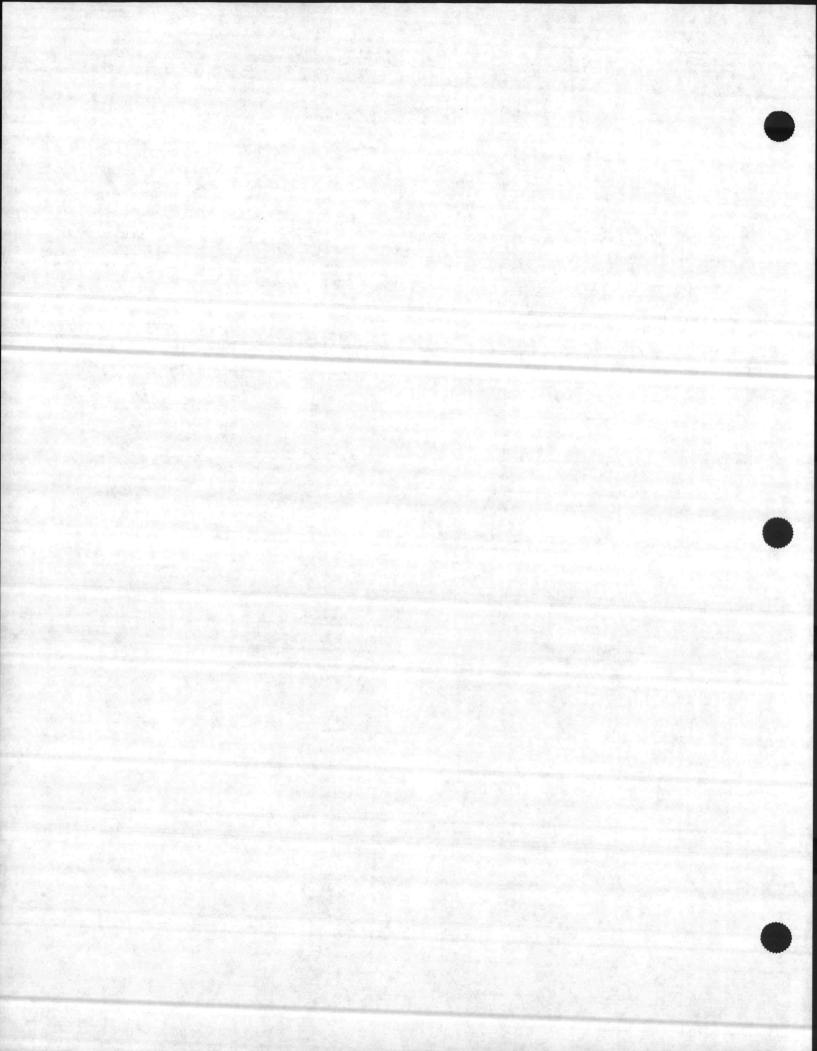
DATE SAMPLED: DATE RECEIVED:

05-FEB-93 05-FEB-93

APPROVED BY:

Joanne Simanic

LN	TEST CODE	DETERMINATION	RESULT	UNITS
	T610	Solids, Suspended at 1030	35	mg/L





February 23, 1993 Report No.: 00013685

#### LABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

MR. JOHN LOVELY ATTENTION:

Carbon Copy:

SAMPLE ID: 930020

NUS SAMPLE NO: P0225094

P.O. NO.: CTO # 19017

·Section A Page 5

NUS CLIENT NO: 1600 0006 WORK ORDER NO: 55830

VENDOR NO:

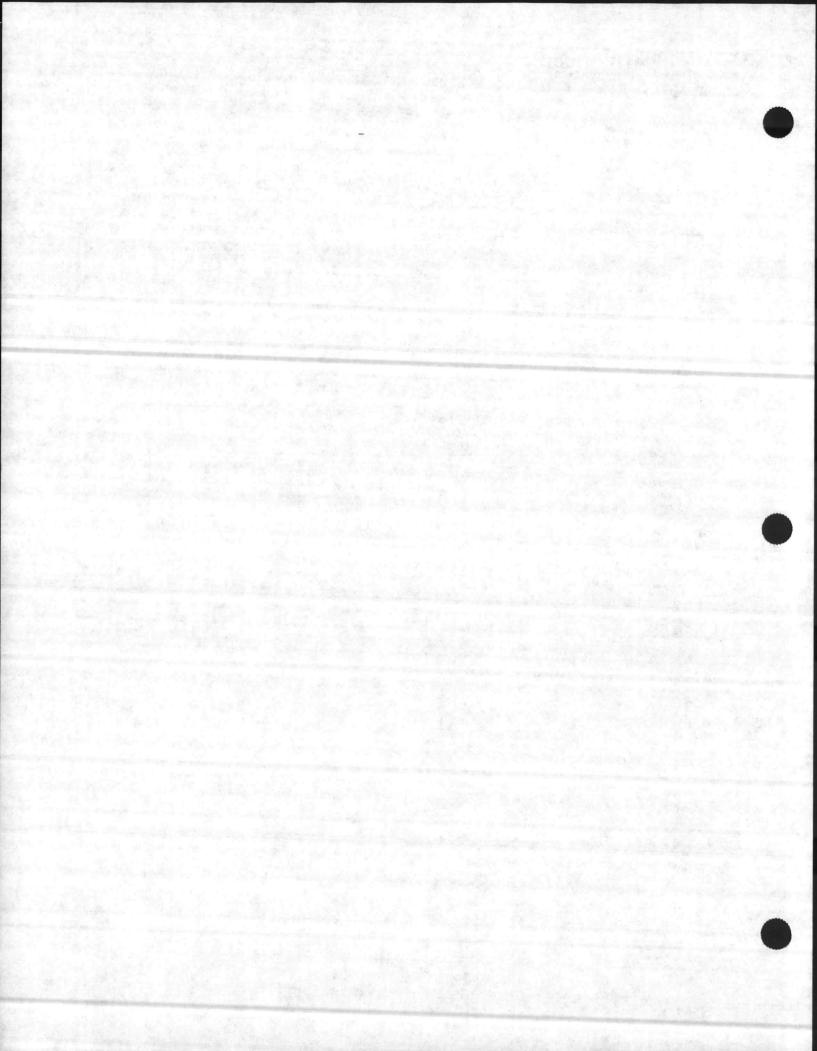
DATE SAMPLED: 05-FEB-93 DATE RECEIVED: 05-FEB-93 APPROVED BY: Joanne Simanic

TEST UNITS DETERMINATION RESULT CODE LN 32 mg/L Solids, Suspended at 103C

COMMENTS:

**I610** 

1





February 23, 1993 Report No.: 00013685 Section A Page 6

#### LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS:

420 ROUSER ROAD

ATTENTION: MR. JOHN LOVELY

CORAOPOLIS, PA 15108-

Carbon Copy:

SAMPLE ID:

930021

NUS SAMPLE NO: P0225095

P.O. NO.: CTO # 19017

NUS CLIENT NO: 1600 0006

WORK ORDER NO:

55830

VENDOR NO:

DATE SAMPLED:

05-FEB-93 05-FEB-93

DATE RECEIVED: APPROVED BY:

Joanne Simanic

TEST CODE LN

DETERMINATION

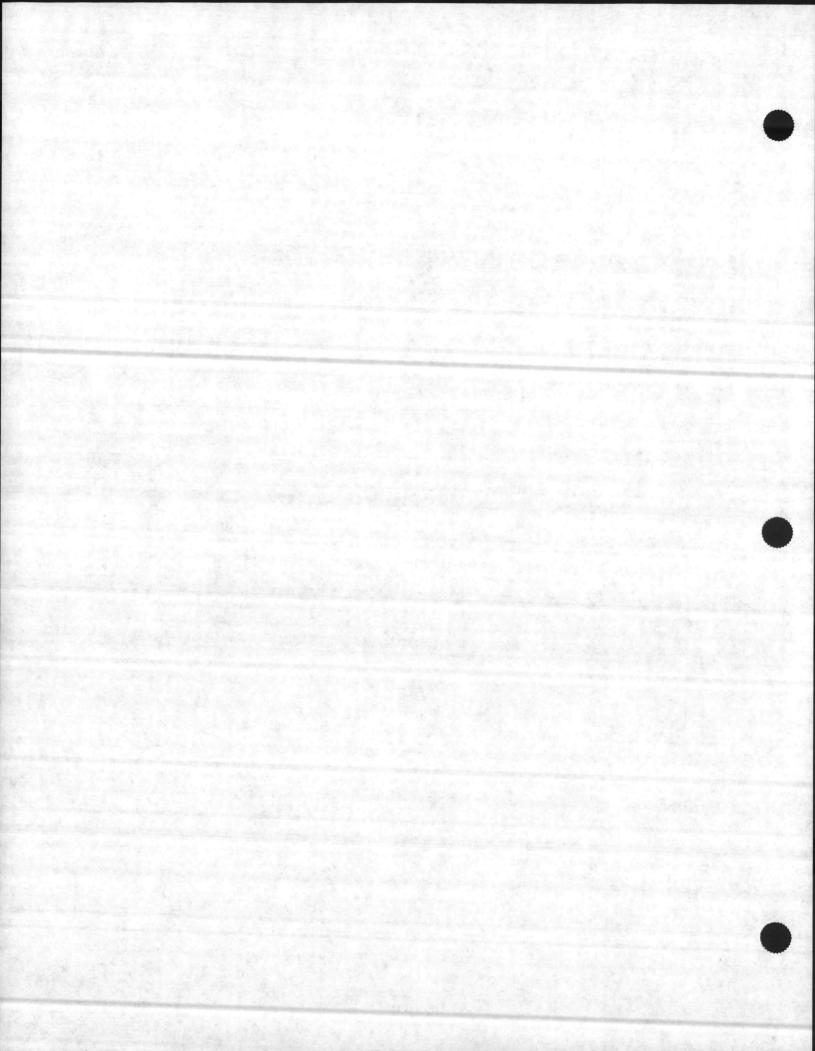
RESULT

UNITS

I610

Solids, Suspended at 103C

25 mg/L





February 23, 1993 Report No.: 00013685 Section A Page 8

## LABORATORY ANALYSIS REPORT

CLIENT NAME:

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS:

420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION:

JOHN LOVELY

Carbon Copy:

SAMPLE ID:

930023

NUS SAMPLE NO: P.O. NO .:

P0225097

CTO # 19017

NUS CLIENT NO: 1600 0006

WORK ORDER NO: 55830

VENDOR NO:

DATE SAMPLED: 05-FEB-93 DATE RECEIVED: 05-FEB-93

APPROVED BY:

Joanne Simanic

TEST CODE LN

DETERMINATION

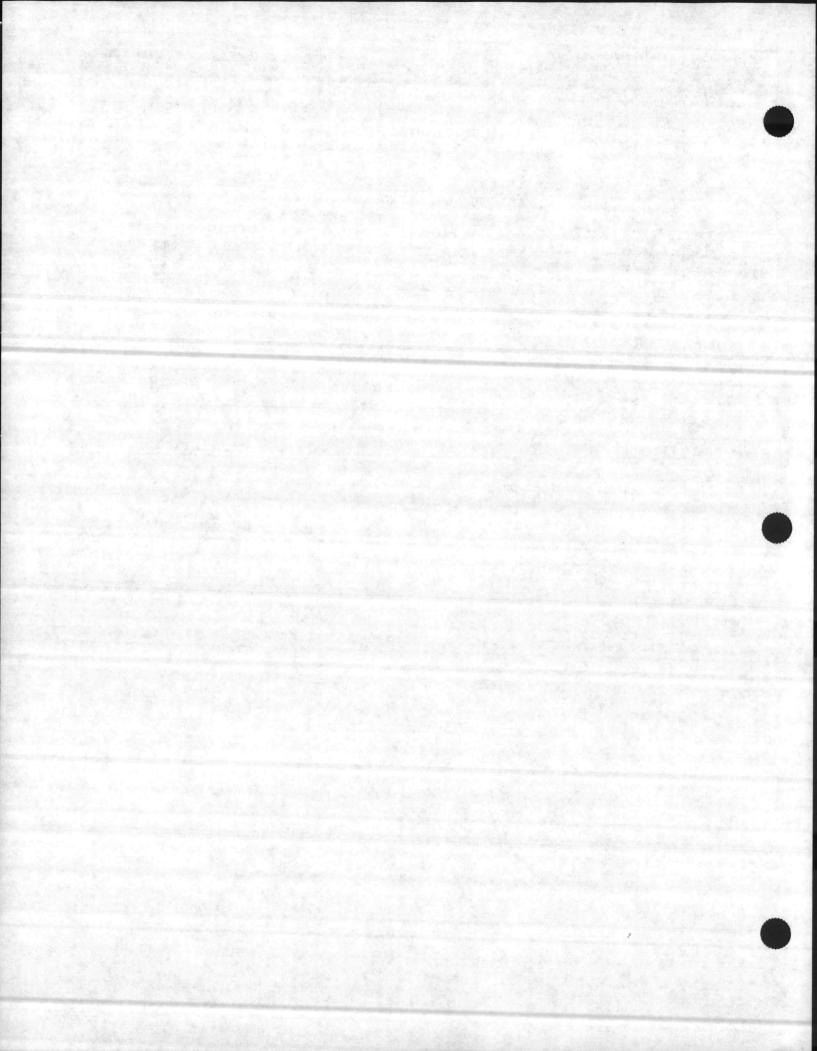
RESULT

UNITS

**I610** 

Solids, Suspended at 103C

mg/L 28





February 23, 1993 Report No.: 00013685 Section A Page 9

## LABORATORY ANALYSIS REPORT

CLIENT NAME:

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS:

420 ROUSER ROAD

ATTENTION: MR. JOHN LOVELY

CORAOPOLIS, PA 15108-

Carbon Copy:

**SAMPLE ID: 930024** 

NUS SAMPLE NO: P0225098

P.O. NO.: CTO # 19017

NUS CLIENT NO: 1600 0006

WORK ORDER NO: 55830

VENDOR NO:

DATE SAMPLED: 05-FEB-93 05-FEB-93 DATE RECEIVED:

APPROVED BY:

Joanne Simanic

TEST DETERMINATION LN CODE

**I610** 

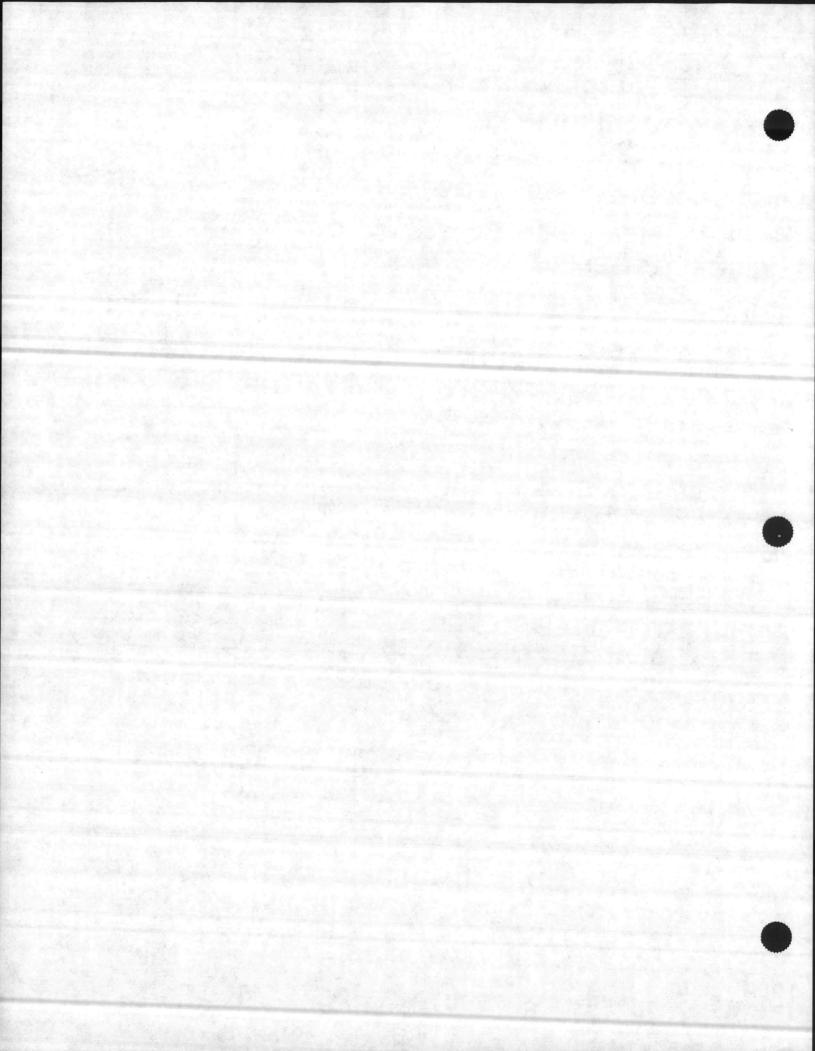
Solids, Suspended at 1030

27

RESULT

mg/L

UNITS





February 23, 1993 Report No.: 00013685 -Section A Page 10

## LABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

420 ROUSER ROAD ADDRESS:

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: 930025

NUS SAMPLE NO: P0225099

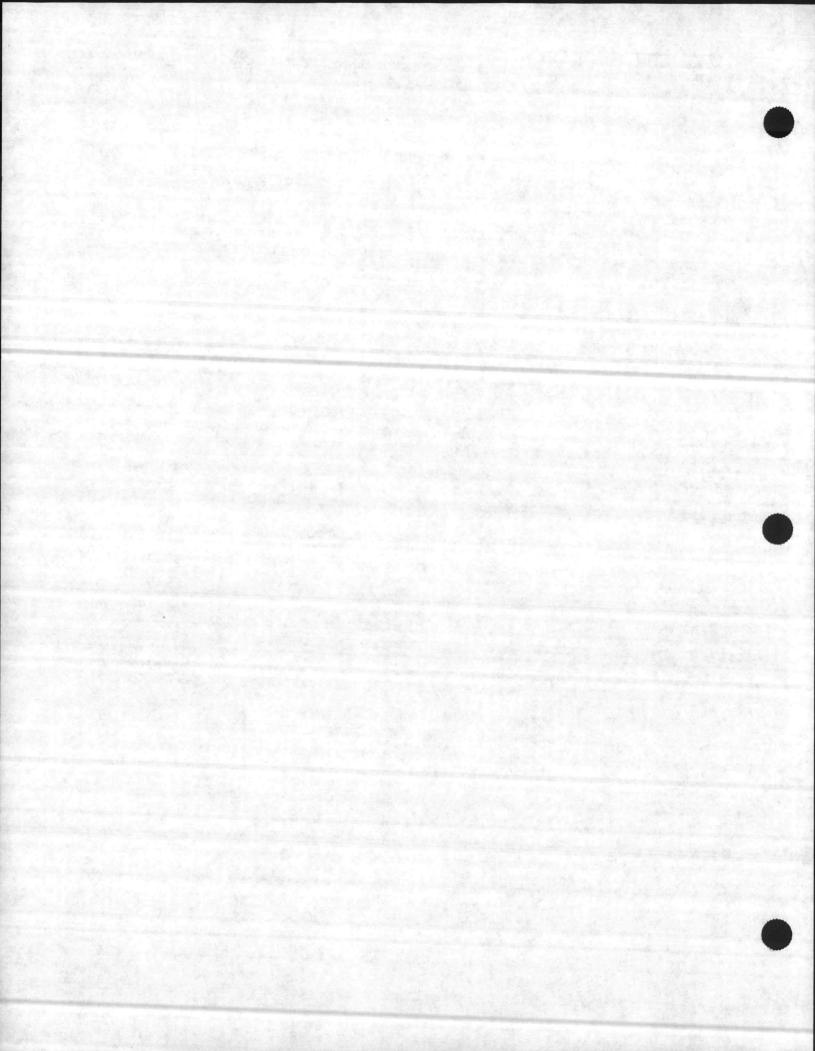
1600 0006 NUS CLIENT NO:

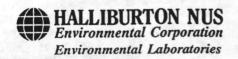
WORK ORDER NO: 55830

VENDOR NO:

DATE SAMPLED: 05-FEB-93 DATE RECEIVED: 05-FEB-93 Joanne Simanic APPROVED BY: P.O. NO.: CTO # 19017

TEST RESULT UNITS DETERMINATION CODE LN 20 mg/L Solids, Suspended at 103C **I610** 





February 23, 1993 Report No.: 00013685 -Section A Page 11

## LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS:

420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION:

MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID:

NUS SAMPLE NO:

P.O. NO.: CTO # 19017

NUS CLIENT NO: 1600 0006

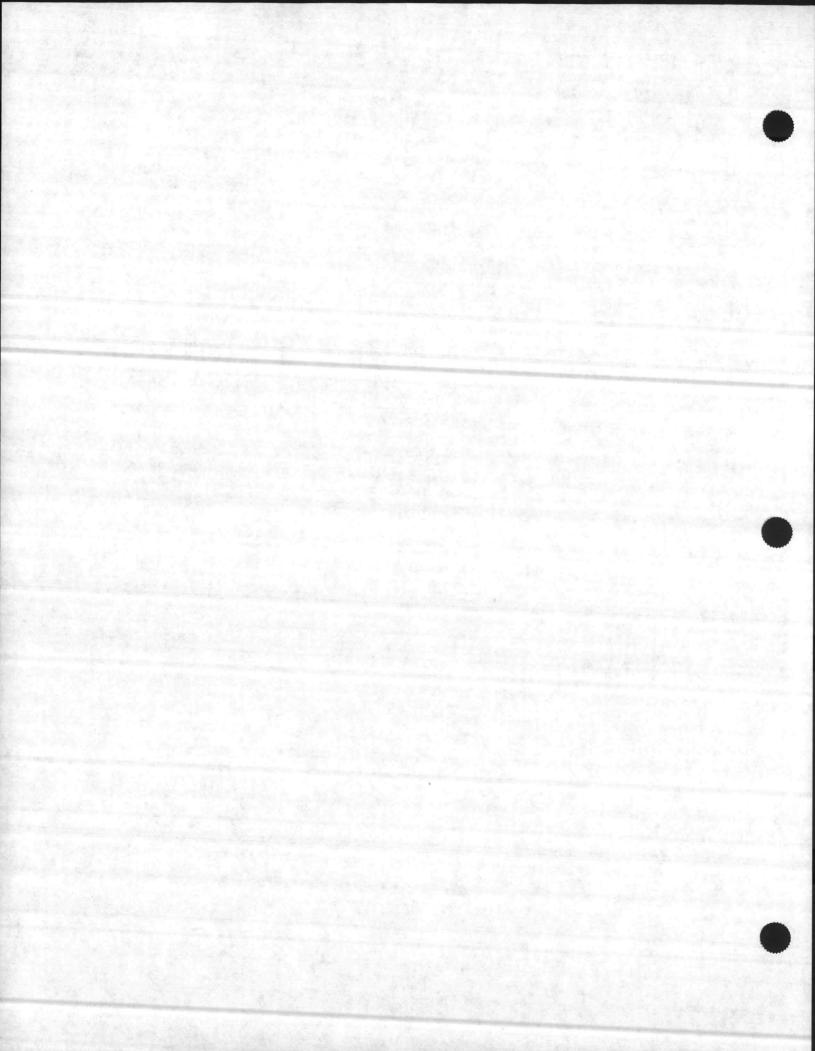
WORK ORDER NO:

55830

VENDOR NO:

05-FEB-93 DATE SAMPLED: 930026 05-FEB-93 DATE RECEIVED: P0225100 APPROVED BY: Joanne Simanic

TEST UNITS RESULT DETERMINATION CODE LN 16 mg/L Solids, Suspended at 103C **I610** 1





February 23, 1993 Report No.: 00013685

## LABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

420 ROUSER ROAD ADDRESS:

CORAOPOLIS, PA 15108-

MR. JOHN LOVELY ATTENTION:

Carbon Copy:

**SAMPLE ID: 930028** 

NUS SAMPLE NO: P0225102

P.O. NO .: CTO # 19017

Section A Page 13

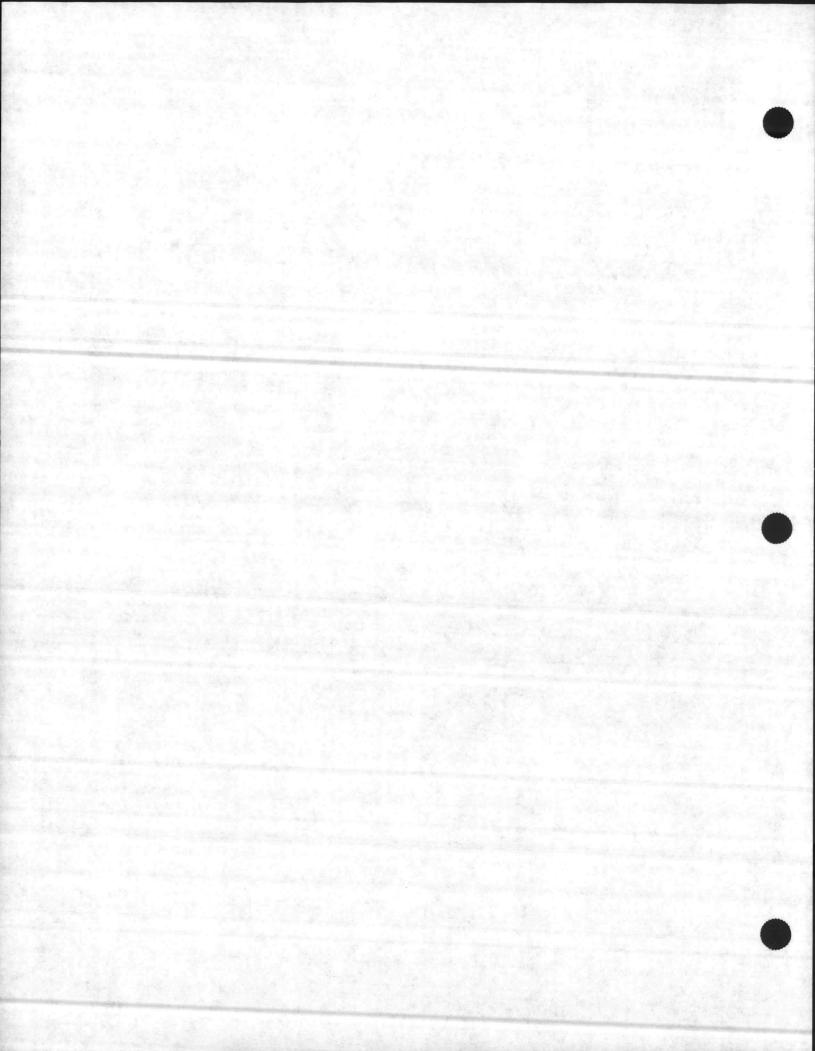
NUS CLIENT NO: 1600 0006 WORK ORDER NO: 55830

VENDOR NO:

DATE SAMPLED: 05-FEB-93 05-FEB-93 DATE RECEIVED:

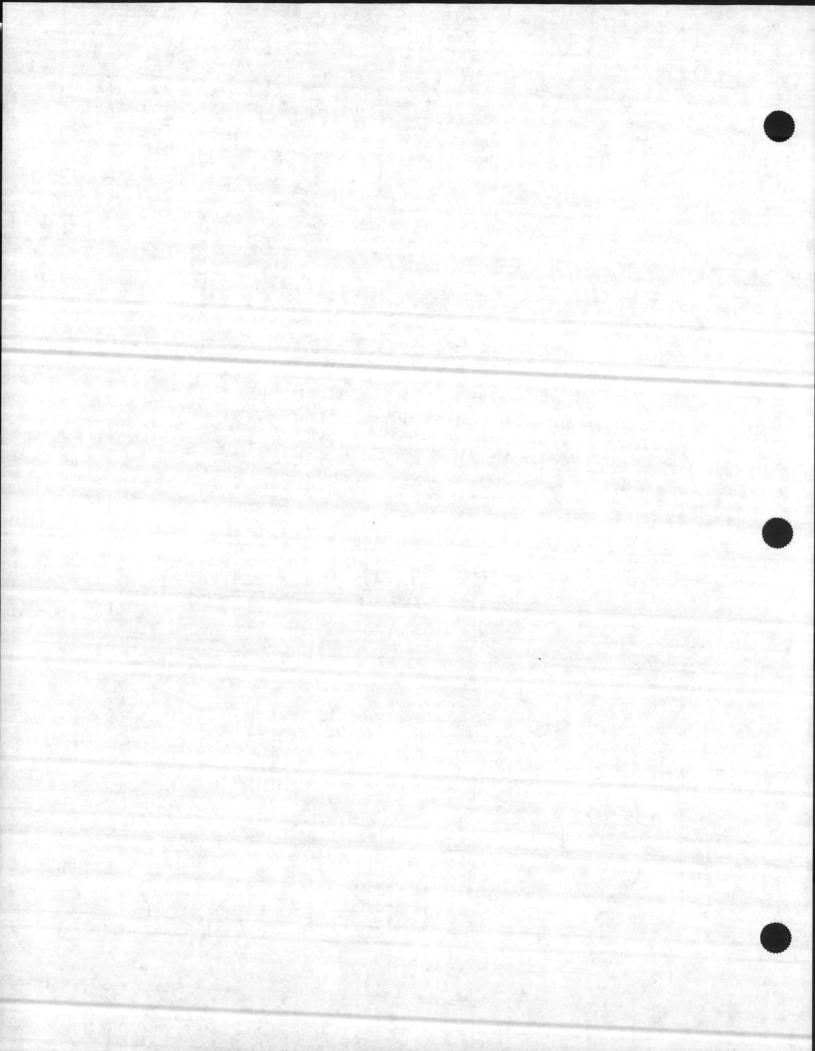
APPROVED BY: Joanne Simanic

LN	TEST CODE	DETERMINATION	RESULT	UNITS
	T610	Solids, Suspended at 103C	93	mg/L



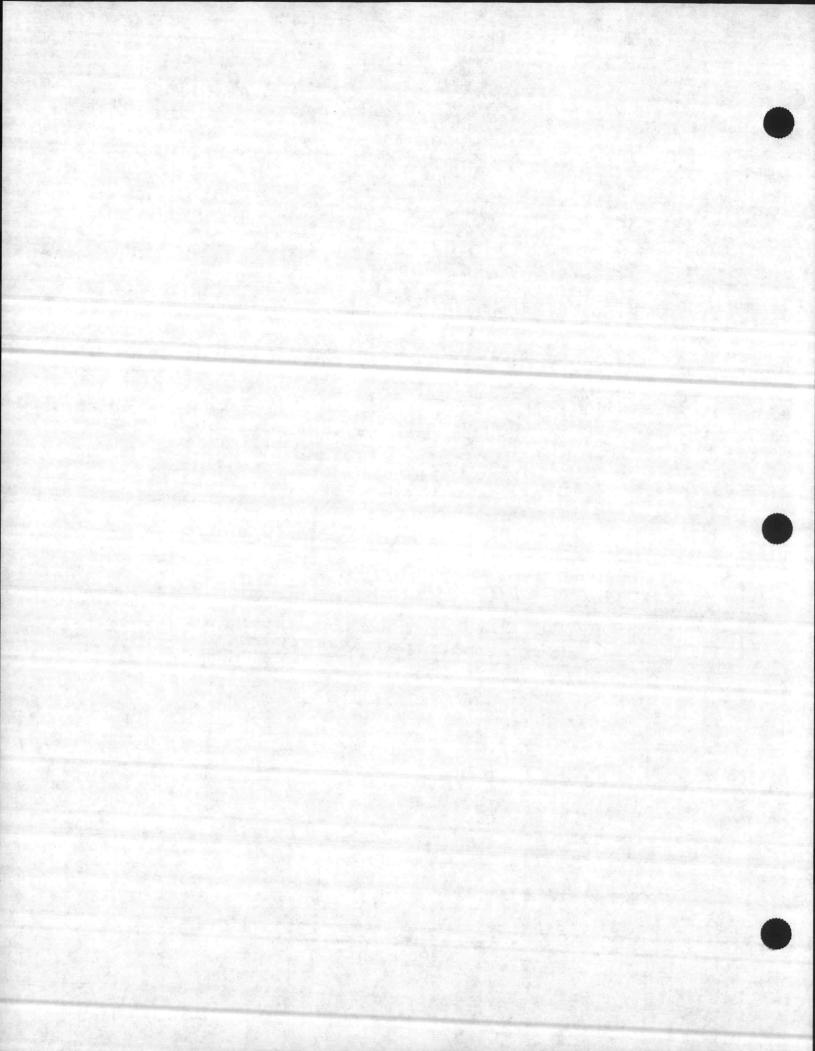
		INORGANIC AN	1 ALYSES DATA SHE		EPA SAMPLE NO.
					930017
Name: HALL	IBURTON_NUS		Contract:	1	
Code: HNUS	Ca	se No.: BKHD	SAS No.: _		SDG No.: PKG3
trix (soil/w	ater): WATE	R	La	b Sample	ID: P225091_
vel (low/med	): LOW_		Da	te Recei	ved: 02/05/93
Solids:		o			
Co	ncentration	Units (ug/L	or mg/kg dry w	eight):	UG/L_
			11		
	ICAS No.	: Analyte :C	oncentration C   _	11 D	1 [
	7429-90-5	:Aluminum :	27801_1	: F	
	17440-38-2	:Arsenic :	4.0101	: F	
	1/440-4/-3	ichromium_i_	20.01_1		
	17439-89-6	Iron	89301_1	UF	_1
	17439-92-1	Lead	4.41B1	: F	
	17439-97-6	!Mercury_!_	2.0 U	10	CVI
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lor Before:	GREY	Clarity	Before: OPAQUE		Texture:
lor After:	COLORLESS	Clarity	After: CLEAR		Artifacts:

FORM I - IN



### U.S. FPA - CLE

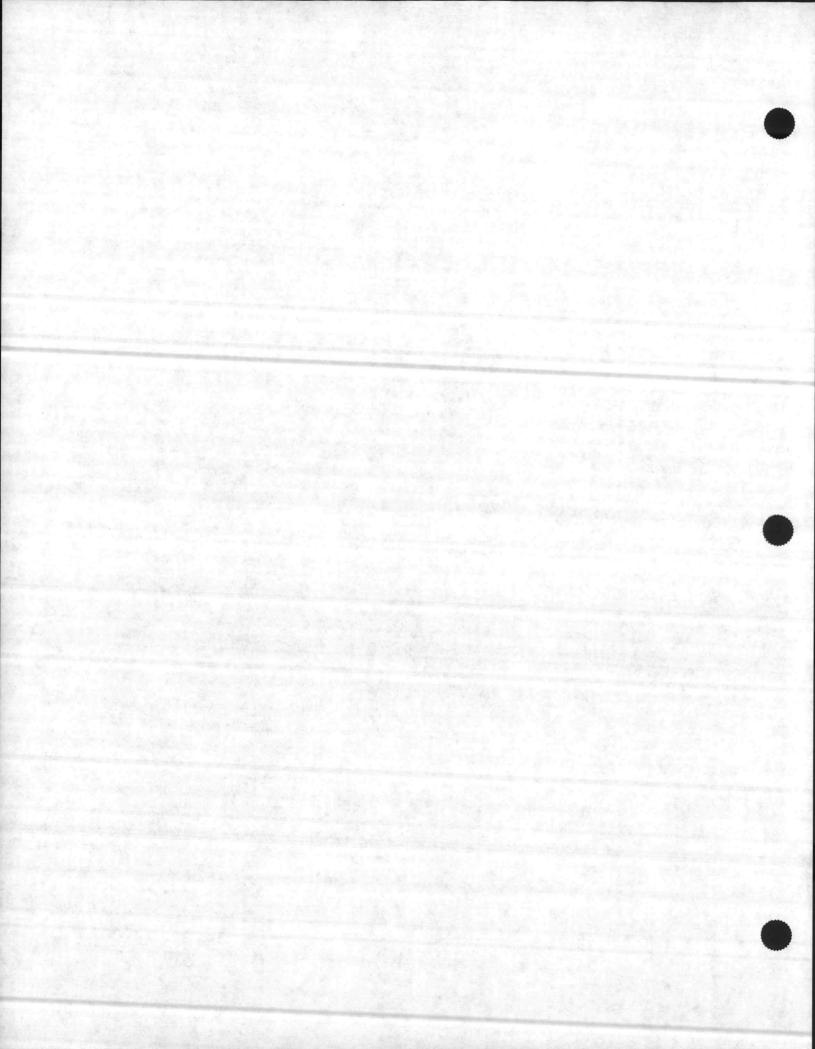
The second second second		INORGANIC	1 ANALYSES DATA S	SHEET	EPA SAMPLE NO.
					930022
b Name:	HALLIBURTON_NU	S	Contract: _		
b Code:	HNUS C	ase No.: BK	HD SAS No.:		SDG No.: PKG3
atrix (so	oil/water): WAT	ER		Lab San	nple ID: P225096_
evel (low	/med): LOW	_		Date Re	eceived: 02/05/93
Solids:	The second second	_0			
	Concentratio	n Units (ug	/L or mg/kg dry	weight	t): UG/L_
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	ICAS No.	! Analyte	Concentration	ici Q	[M ]
	7429-90-5	-i	12290	<u> -</u>	TIP i
	17440-38-2	Arsenic_	4.0 14.0 6400 3.2 2.0	101	IF_I
	17440-47-3	Chromium_	14.0	_	IP_I
	17439-89-6	!Iron	16400	1_1	IP_I
	17439-92-1	!Lead	13.2	(B)	!F_!
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			gy term i gylgan manifest fransi och myt en i säner		
olor Afte	er: COLORLESS	Clari	ity After: CLE	AR_	Artifacts:
omments:					



### U.S. EPA - CLP

		INURGANIC	ANALYSES DATA S	HEEI	
b Name: HAL	LIBURTON_NUS		Contract:		930027 
b Code: HNU	S Ca	se No.: BK	HD_ SAS No.:		SDG No.: PKG3_
trix (soil/	water): WATE	R		Lab Sam	aple ID: P225101
evel (low/me	d): LOW_	_		Date Re	eceived: 02/05/93
Solids:	And the second s	0			
C	oncentration	Units (ug	/L or mg/kg dry	weight	:): UG/L_
	1	:		T	
	CAS No.	Analyte	Concentration	C! Q	IM I
	17429-90-5	Aluminum	282	71-	TIP_I
	17440-38-2	Arsenic_	14.01	U:	iF_i
	17440-47-3	:Chromium_	10.01	U:	iF_i
	17439-89-6	!Iron	23101	_'	:P_:
	17439-92-1	!Lead	11.0	-!	!F_!
	17439-97-6	Mercury_	12.01	U!	
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olor Before:	GREY	Clar	ity Before: OFAG	QUE	Texture:
olor After:	COLORLESS	Clar	ity After: CLEA	AR_	Artifacts:
omments:					
Jumen cs:			200		

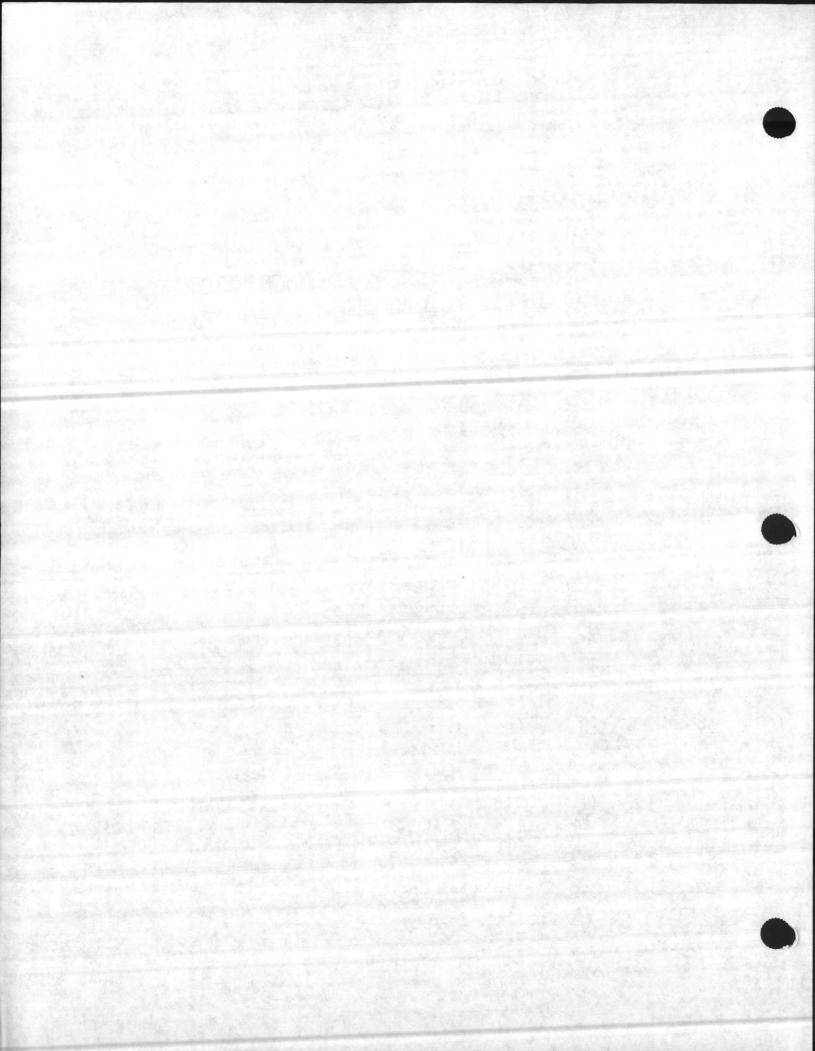
FORM I - IN



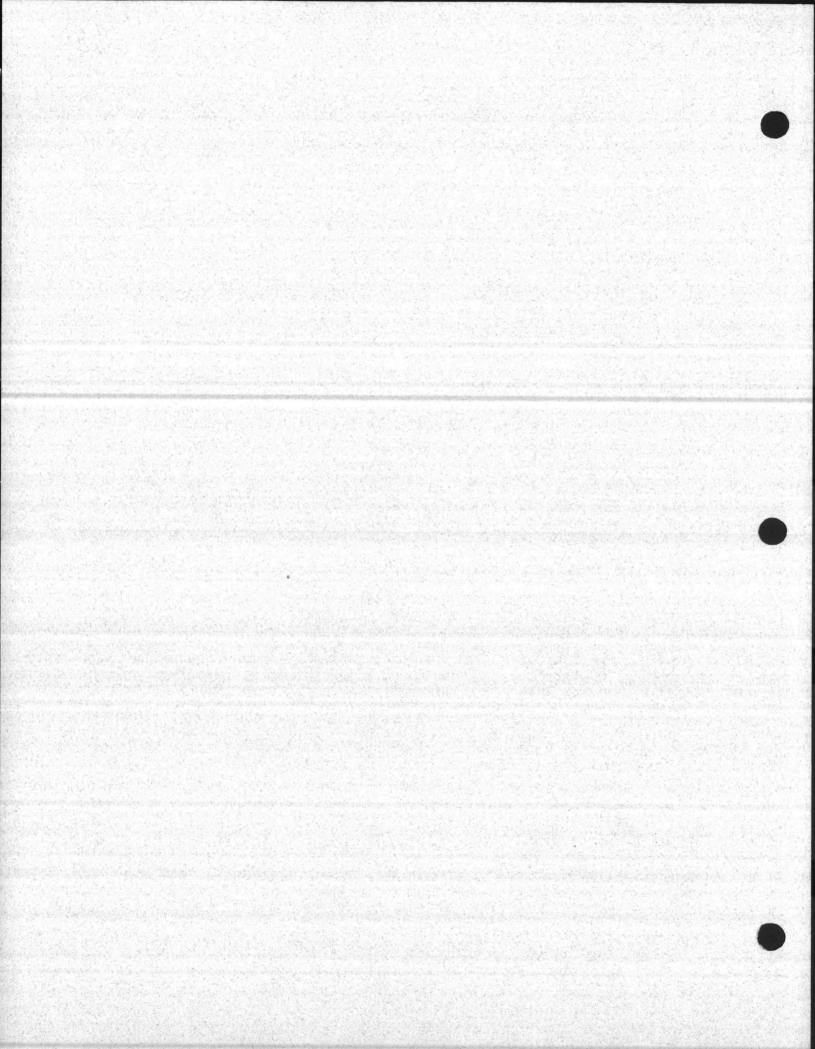
## U.S. EPA - CLF

			INDEGANIC A	1 NALYSES DATA S		EPA SAMPLE NO.
						930029
ab Na	me: HALL	IBURTON_NUS		Contract:		. 1
ь Са	de: HNUS	Ca	se No.: BKH	D_ SAS No.:		SDG No.: PKG3_
trix	(soil/w	ater): WATE	R		Lab Samp	le ID: P225103
vel	(low/med	): LOW_			Date Rec	eived: 02/05/93
Soli	ds:		0			
	Ca	ncentration	Units (ug/	L or mg/kg dry	/ weight)	: UG/L_
		1	1 1		414	T
				Concentration		
		17429-90-5	: Aluminum :	3640		ÎP.
				4.0		
		17440-47-3	Chromium_!	19.0		_1P_1
		17439-89-6	Iron	10200		_!P_!
		17439-92-1	Lead	6.2		_!F_!
				2.0		
				Property Commencer Commenc		
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lor	Before:	COLORLESS	Clarit	y Before: CLE	AR_	Texture:
lor	After:	COLORLESS	Clarit	y After: CLE	AR_	Artifacts:
mmer	its:					
Commer —	its:					

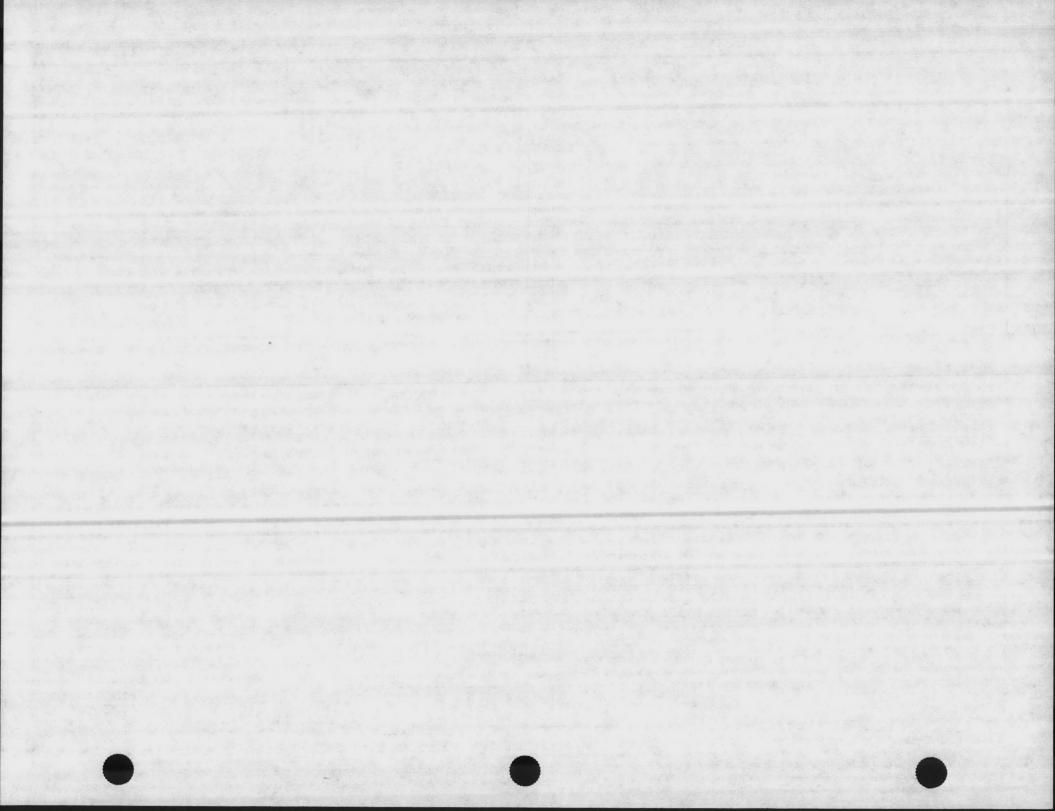
FORM I - IN



APPENDIX H
BENCH-SCALE TREATABILITY STUDY ANALYTICAL
RESULTS - QA/QC



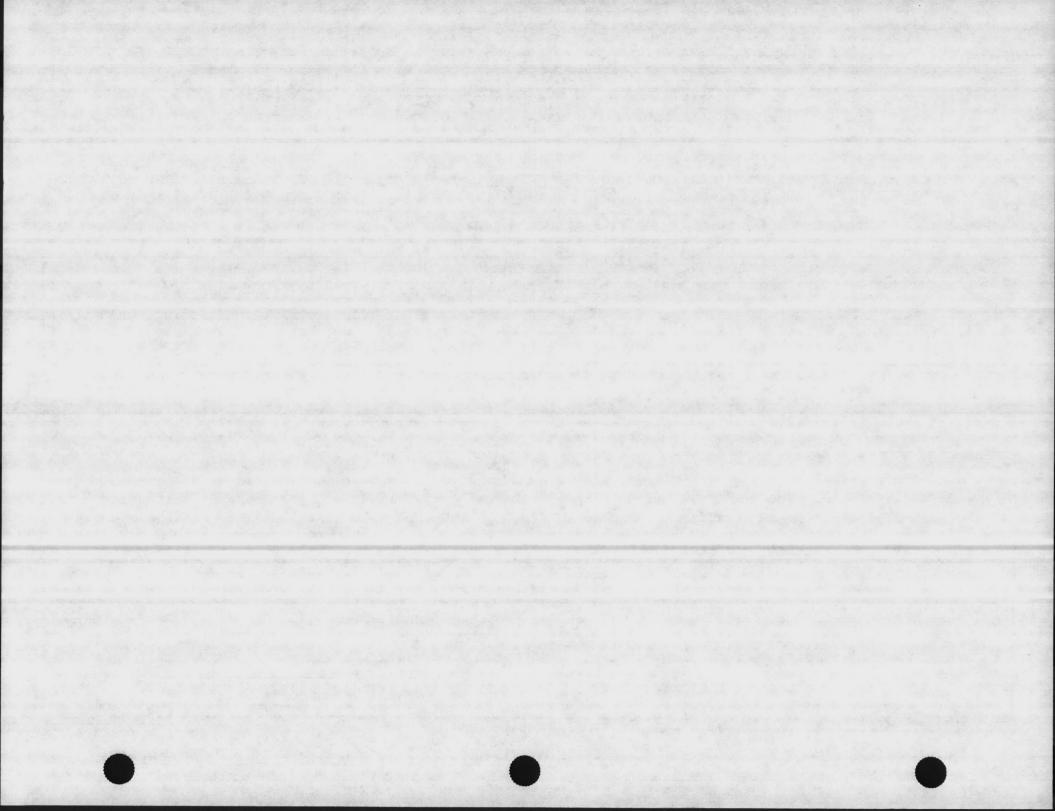
PROJECT					ENAME: 19017	-70-SRN	NO.		/5	2/200	X Any Chesse	25	× 250	/ X/		
SAMPLER	S (SIGNA		-				OF CON- TAINERS	1	A SE	2000	A Market	Ches outs	NA S	REMARKS		
STATION NO.	DATE	TIME	COMP	GRAB		STATION LOCATION		1/4	J'A'	0	1. A.	12	0			
	12/29/92	1515		X	HPIA-	SW-24-1	5	×	X	×	X	X	X	NEED	ETALS (DISSOLVED) SAMPLE  IS TO BE PROFERED FILTERED	
	12/29	1515		X	HPLA -	sw-24-1-D	3	*	*	*				NEEDS	ETALS (DISSOLVED) SAMPLE " TO DE FILTERED & PRESERVED	
	12/29	1515		×	HPIA-	Sw - 24-1				×				EXTRA	Volume	
	12/	1515	YEK.	×												
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	1															
							7									
	1:		100	175.0												
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Mark					BC94 1200	DECEMBED BY (CICALATURE)	DELIN	OUISH	ED BY	(SIGNA	TURE):		DAT	E/TIME:	RECEIVED BY(SIGNATURE):	
RELINQUI	SHED BY	(SIGNA	TURE):	0	ATE/TIME:	RECEIVED BY (SIGNATURE):		20.51						T		
RELINQUI	SHED BY	(SIGNA	TURE):	0	ATE/TIME:	RECEIVED FOR CABORATORY E	DA DA	TEITIN	AE: RI	EMARK	S:	54	MPLE	S PACE	KEO ON ICE	
En a comment Figures						1 Vortore	16/21	311	9005	AMPL	LES S	HIPP	EO V	CA FE	DERAL EXPRESS	



## HALLIBURTON NUS Environmental Corporation and Subsidiaries

CHAIN OF CUSTODY RECORD

PROJECT	10.:			4	ENAME: 19017 -	70 - SRN			/	/	Soll Maria	Wat .	1	12/	4
SAMPLER!			mto				NO. OF CON- TAINERS	1	HASOLIDE	W. S. S.	70 00	2/	/	Se Ville Vil	REMARKS
STATION NO.	DATE	TIME	COMP	GRAB		STATION LOCATION		10	14	1 5	2/2	//	10	/	
	12/29/92	1515		X	HPIA- 6	W-24-1	4	*	*	*	*				
		1515		×		w - 24-1	l		×					EXTR	A VOLUE
	12/29/92	1515		X	HPIA-G	w - 24-1	3						*	PRESE	veo w/ HNO3
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Mark					ATE/TIME:	RECEIVED BY JOHN TOREY.	ALLIN	40.01							
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RELINQUIS	HED BY	SIGNA	TURE):	D	PATE/TIME:	RECEIVED FOR LABORATORY BY (SIGNATURE)	/ 1	/							D ON ICE FEDGRAL EXPRESS





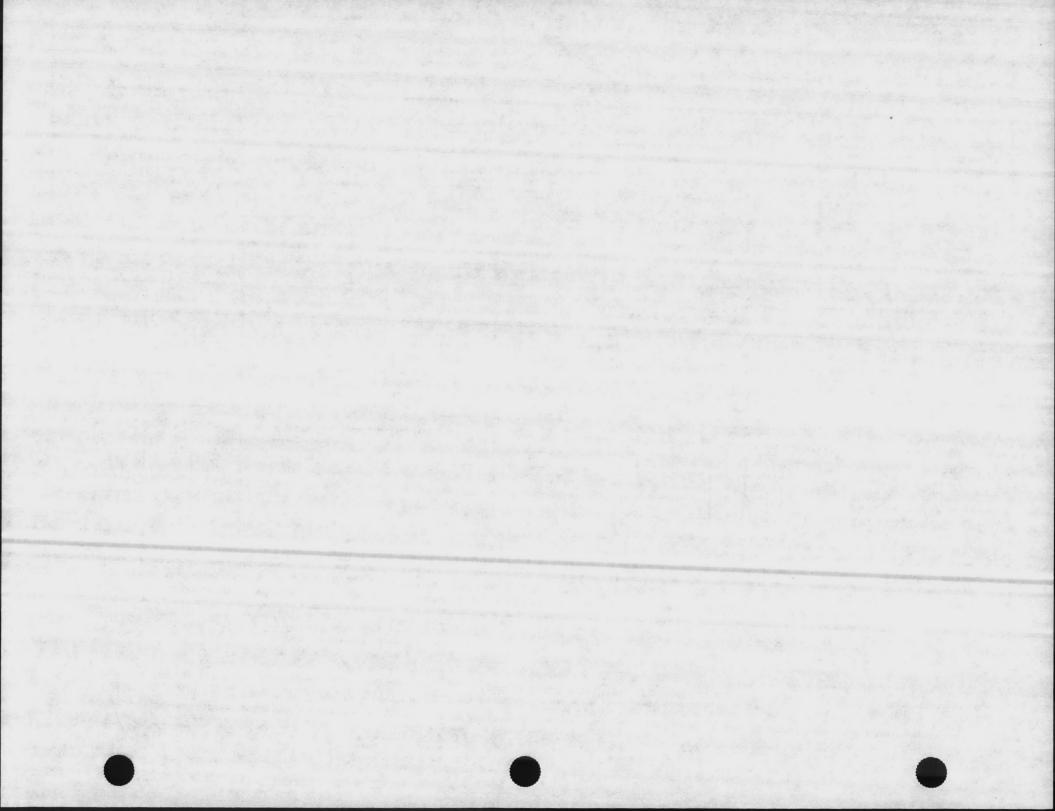
## Baker Environmental, Inc.

Airport Office Park, Bldg. 3 420 Rouser Road Coraopolis, PA 15108 412-269-6000

## **CHAIN-OF-CUSTODY RECORD**

Pg. 1 of 1

Baker Environmental,	Co 41	2-269-600	PA 15108 00				1000	Analy	sis Re	quested /	Preser	vative	Requi	red				
Service Order Project Name: Project Manag Field Team:	ger: Me.	Lejeune Féve	-57-S -Treabbilin Kretschi VA - Treab	nan	2/4	Oil ad Green				vpe of Co								
Sample			Sample Location	Ma Typ	trix e (1)	G	1											
Sample Number	Date	Time		(2)	(2)				N	umber of	Contai	ner(s)					Remarks	1.4
9300/2	1/5/93	2:15pm	Treatability	GW		1											* All GW samples coll	
930013	1/5/93	2:30	Treatability	GN		1											From Location HPIA-	6W-24
930014	1/5/93	-	Trestability	GW		1										-	for Treatability Tes	ting
93015	1/5/93		Treatability	GW		1		ing comm		50							Coil/wster Separat	m)
TOUIS	13/12	JIOOPI																
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Relinquished By Received By: Shipped by (che	1.	who me	w		Other [	Date:	1/5	193	Time:	4; 48m	- See Wo	ork Orde	dy seal round: er	on cool	er:	Yes Yes riority	No No Regular	□ <sub>NA</sub>
Relinquished By: Received By: Shipped by (ch					Other [	Date:			Time:			alysis Re Dispos		Re	turn to Archive	Baker until:	Lab Disposal	(date)
Relinquished By Received By: Shipped by (ch					Other (	Date:					(1)	A - A	roundy oring	vater	WP -	- Surfac - Waste - Wipe - Waste	water (3) P - Plasti	
COUR AMALYTI	CAL DECLI	TC AND C	HAIN OF CUST	ODY TO	PROI	CTMAN	VAGER.										G - Glass	





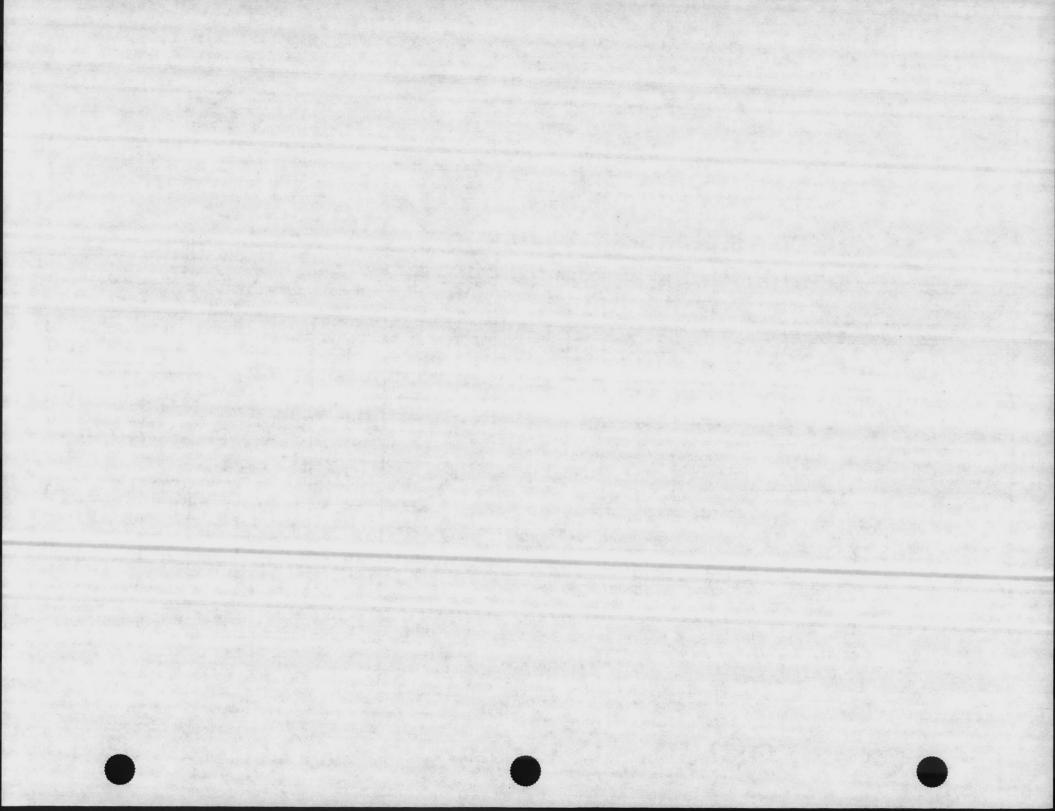
Baker Environmental, Inc.

Airport Office Park, Bldg. 3 420 Rouser Road Corappolis, PA 15108

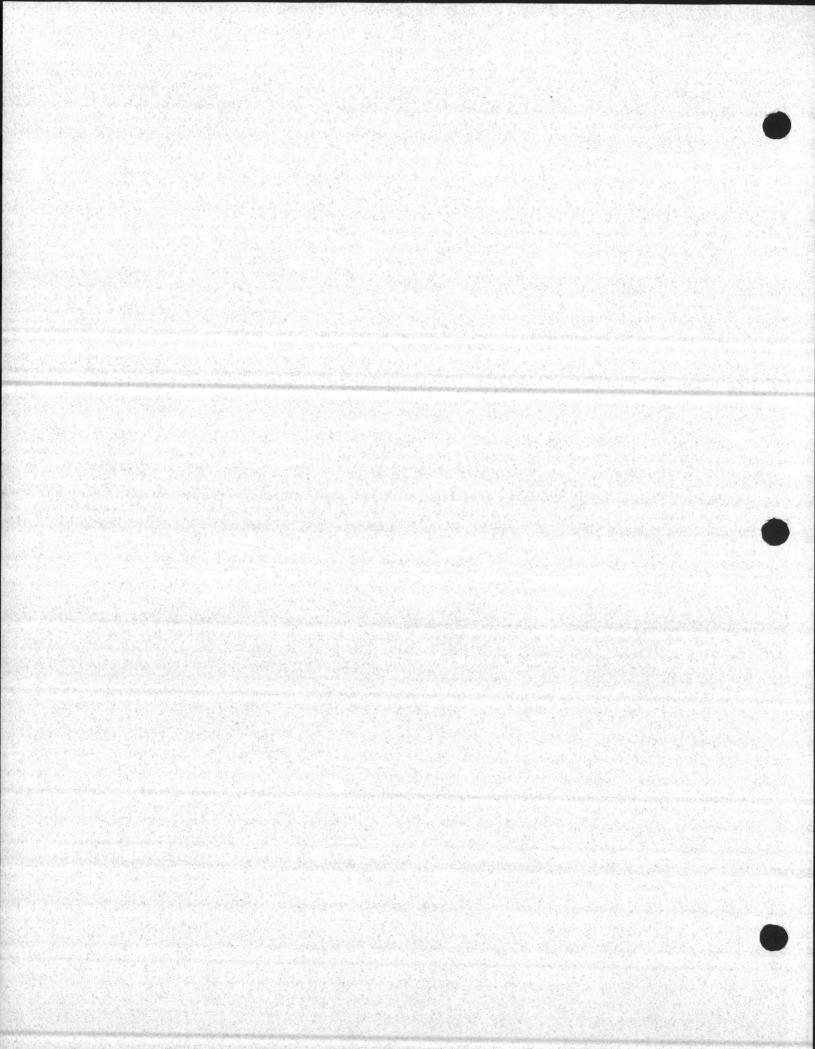
# CHAIN-OF-CUSTODY RECORD

Pg. 1 of 1

Baker Environmental, 1 c	41	2-269-600	00		1	1	Ana	lysis Requ	ested /	/ Preservative Required	
Service Order N Project Name: Project Manage Field Team:	lo.:	1900 Giner Organi	17-56.	-5R1 321/ 321/32	<u>U</u> <u>L</u> <u>11 ma</u>	1				Container(s) (3)	
Sample Number	Date	Time	Sample Location	Тур	trix e (1) COM.	-M	PPA			f Container(s) Remarks	
730016	11.	17:1		(GU)							-
700017		13:	BE WHILE	6 W			+ 1				
130018		134	94	60)		1					
42-017	-	ON:	M	(311)		1					
730020		. 01;	3 -	GW							
9-0021		Oli	Amini	600		1			-		
7: HODX		01:	4.3	EW					-		
430020		0)	19 d 3mi	(1	-						
150024		67.	8 3 1	J (	(11)				-		
18(0)35	-	011	1 1 113	1	11)						
4.(X)	- 2	(),)	12 13 6	1 1 6	111	7 15					or !
150071		100	10'00	5 6		100					
10000	7	7 17	5 600	10	U			Wale Ro			
Pallaquished By:	13	15 179	(1)()a			Date:	-/:/:	fime:		Sample Stored at 4°C:  Chain-of-custody seal on cooler:  Analysis turnaround:  See Work Order  See Analysis Reguest Form	VA
Relinquished By: Received By: Shipped by (chec						Date:		_ Time: _ Time:		Sample Disposal: Return to Baker Lab Disposal Archive until:	)
Relinquished By: Received By: Shipped by (che						Date:		_ Time: _		(1) A - Air SW - Surface water GW - Groundwater W - Waste COM - Composite WP - Wipe SO - Soil WW - Wastewater G - G - Glass	



APPENDIX I PILOT-SCALE TREATABILITY STUDY ANALYTICAL RESULTS - GROUNDWATER



900 Gemini Avenue Houston, TX 77058



February 23, 1993 Report No.: 00013686 Section A Page 1

NUS CLIENT NO: 1600 0006

55830

## LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS: 420 ROUSER ROAD WORK ORDER NO:

CORAOPOLIS, PA 15108- VENDOR NO:

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: 1-DL DATE SAMPLED: 02-FEB-93

BIS SAMPLE NO. P0225104

DATE RECEIVED: 06-FEB-93

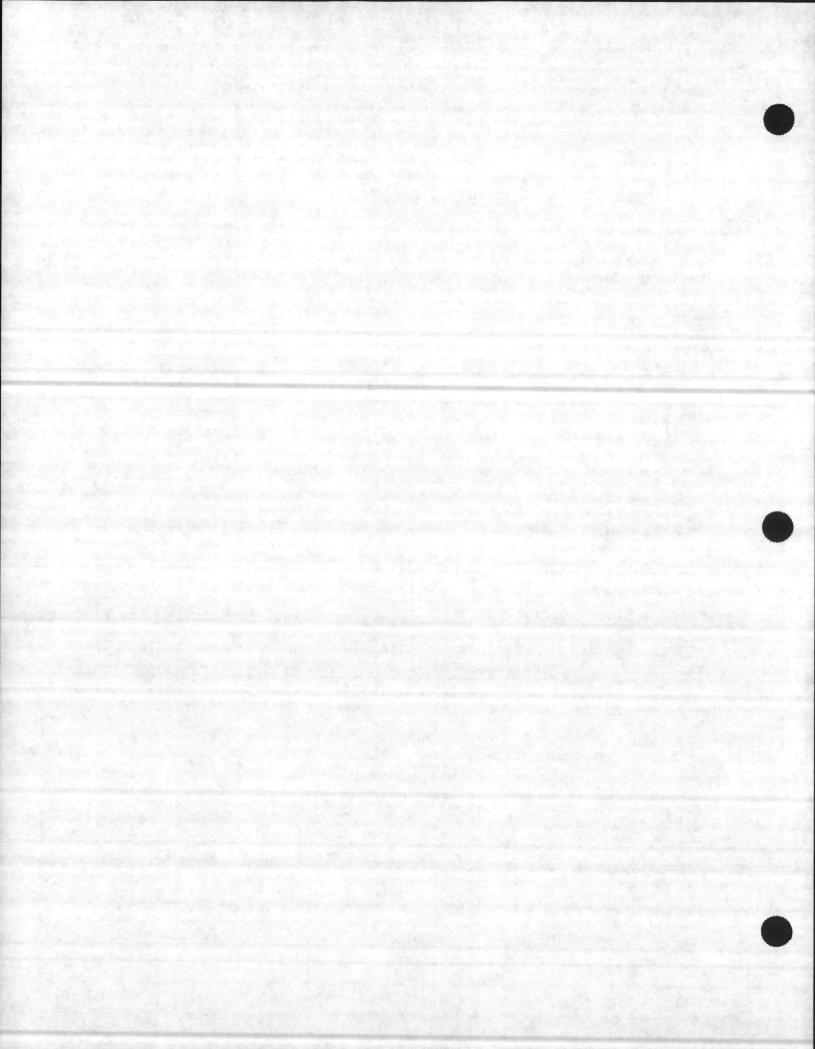
NUS SAMPLE NO: P0225104

P.O. NO.: CTO # 19017

DATE RECEIVED: 06-FEB-93

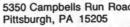
APPROVED BY: Ruth Volk

	TEST		DECUL T	UNIT
 LN	CODE	DETERMINATION	RESULT	
3	1680	Oil and Grease, Gravimetric	< 3	mg/L
4	I391	Nitrate/Nitrite	< 0.1	mg/L
5	1320	Hardness, Total (as CaCO3)	46	mg/L
6	1030	Ammonia (N), Direct		
		Ammonia (as N), Direct	0.4	mg/L
7	1020	Alkalinity, Pht (as CaCO3)	0	mg/L
8	1023	Alkalinity, Total (as CaCO3)	30	mg/L
9	1024	Alkalinity, Bicarbonate (as CaCO3)	30	mg/L
10	1026	Alkalinity, Carbonate (as CaCO3)	0	mg/L
11	I130	Chloride (as C1)	23	mg/L
12	1410	Nitrite (as N)	< 0.02	mg/L
13	I590	Solids, Dissolved at 180C	110	mg/L
14	1610	Solids, Suspended at 103C	< 10	mg/L



1600 0006

02-FEB-93



5350 Campbells Run Road

900 Gemini Avenue Houston, TX 77058

February 23, 1993 Report No.: 00013686 · Section A Page 2

## ABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

A HALLIBURTON NUS

Environmental Corporation **Environmental Laboratories** 

Carbon Copy:

SAMPLE ID: 1-0H

NUS SAMPLE NO: P0225105

WORK ORDER NO: 55830 **VENDOR NO:** 

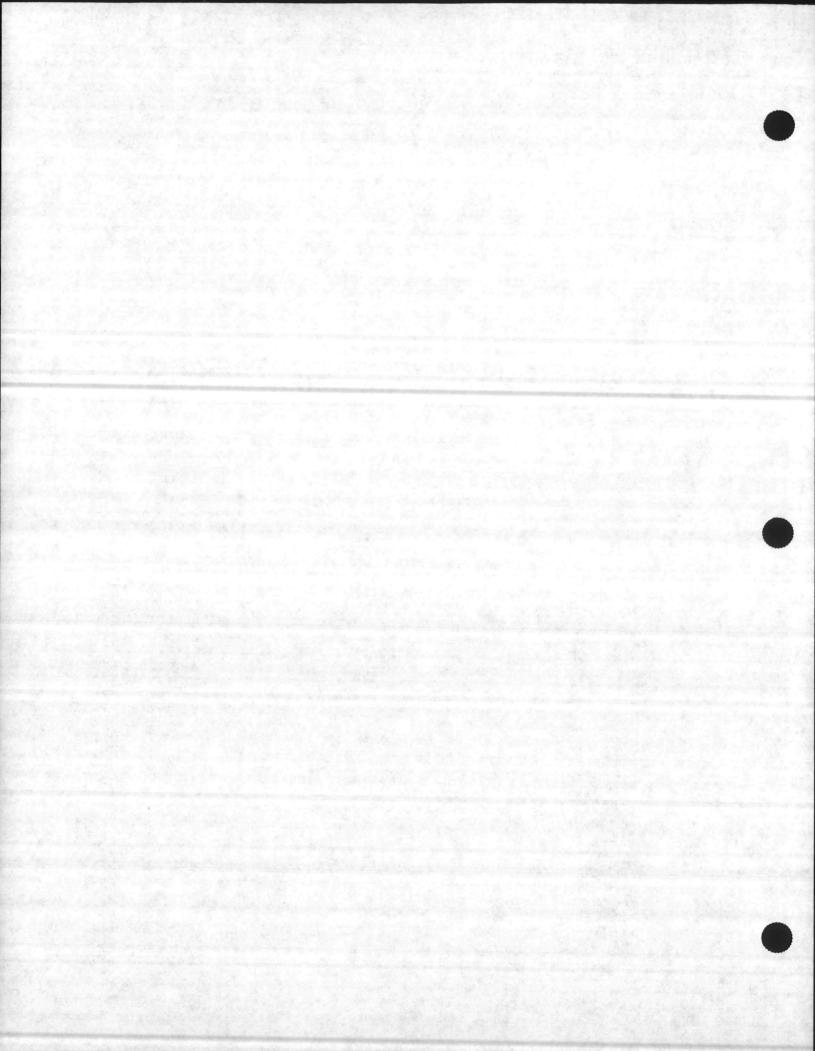
DATE SAMPLED:

NUS CLIENT NO:

DATE RECEIVED: 06-FEB-93 Joanne Simanic APPROVED BY:

P.O. NO.: CTO # 19017

<u>L</u>	N CODE		RESULT	UNITS
	401	W TAL METALS & CLP DATA PACKAGE	DONE	
1			DONE	
2		마이와 ():) 교육 (1985) : [1985] : [		
3	G107	1,2-dimethylbenzene [o-xylene]	3	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	8	ug/L
		benzene	4	ug/L
		ethylbenzene	4	ug/L
		methylbenzene [toluene]	5	ug/L
5	G100	등는 "INTELLIFE 프로마이아 그는 사람이 사람이 있다면 없는 중요 이 없습니다. 2015년 2015년 - "INTELLIFE" INTELLIFE		
	0100	1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1.1-dichloroethene [1.1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1.2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L



900 Gemini Avenue Houston, TX 77058



February 23, 1993 Report No .: 00013686 Section A Page 3

## LABORATORY ANALYSIS REPORT

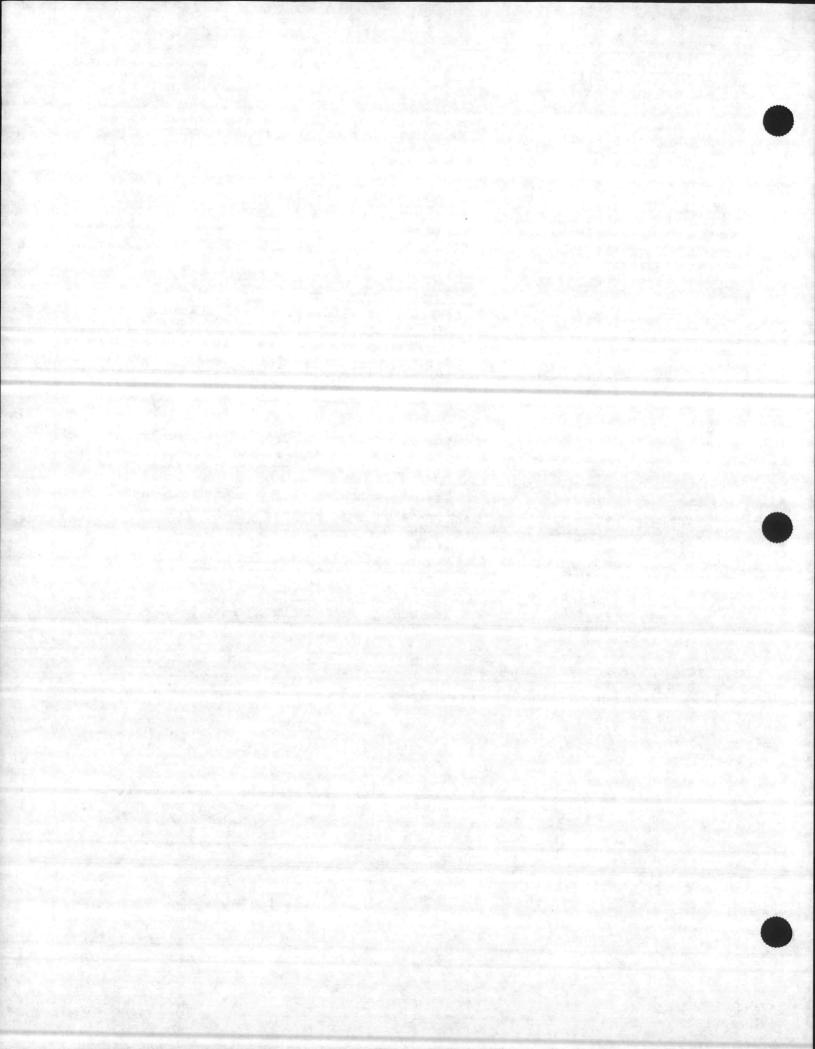
BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

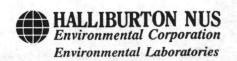
1-0W SAMPLE ID: NUS SAMPLE NO: P0225105

LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		_ trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 40 D	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		-trichloroethene [trichloroethylene]	150 D	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	270 D	ug/L
		Oil and Grease. Gravimetric	< 3	mg/L

In the BTEX analysis, m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.

Sample number P225105 exhibited high surrogate recoveries in both the primary and confirmational analyses. The high surrogate recoveries were due to a matrix interference. The matrix interference also interferred with the confirmation of benzene. The benzene result from the primary analysis is reported.





February 23, 1993 Report No.: 00013686 Section A Page 4

## ABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

MR. JOHN LOVELY ATTENTION:

Carbon Copy:

SAMPLE ID: 1-AS

P0225106 NUS SAMPLE NO:

P.O. NO.: CTO # 19017

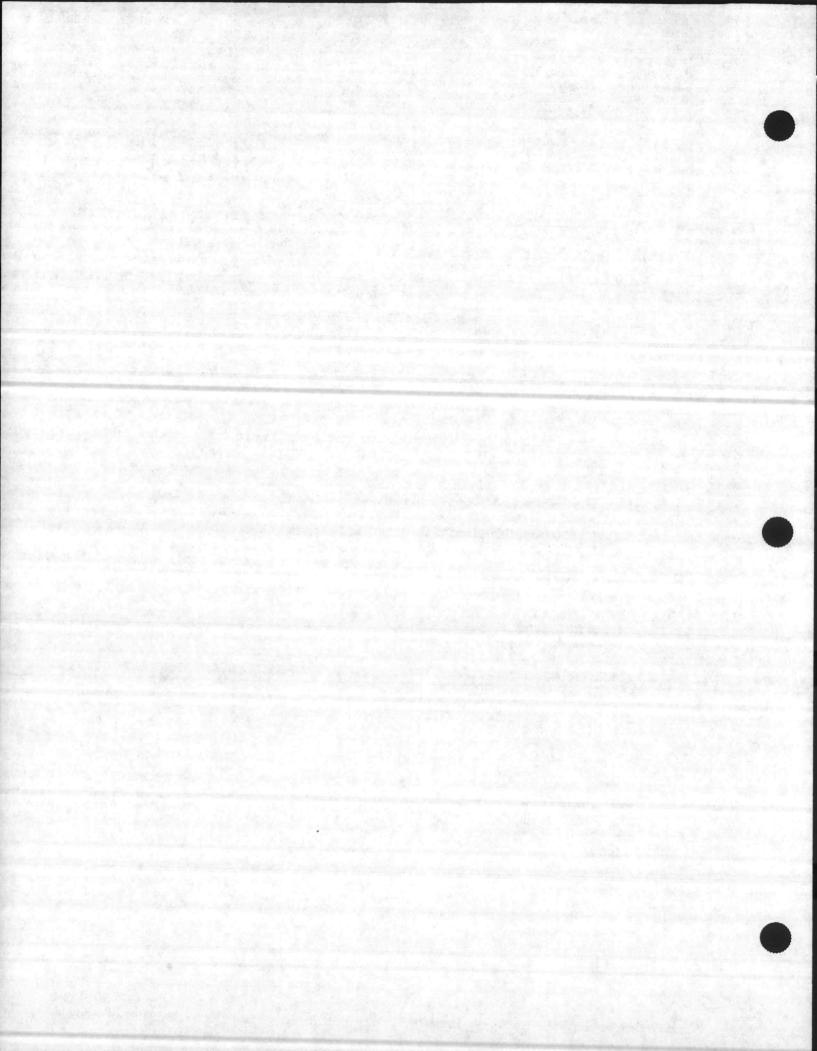
1600 0006 NUS CLIENT NO: WORK ORDER NO: 55830

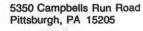
VENDOR NO:

DATE SAMPLED: 02-FEB-93 06-FEB-93 DATE RECEIVED:

Joanne Simanic APPROVED BY:

LN	CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
		1,2-dimethylbenzene [o-xylene]	9	ug/L
12. 12.		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	17	ug/L
		benzene	5	ug/L
		ethylbenzene	17	ug/L
		methylbenzene [toluene]	25	ug/L
5	G100W	PURGEABLE HALOCARBONS		
	010011	1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L







February 23, 1993 Report No.: 00013686 Section A Page 5

## LABORATORY ANALYSIS REPORT

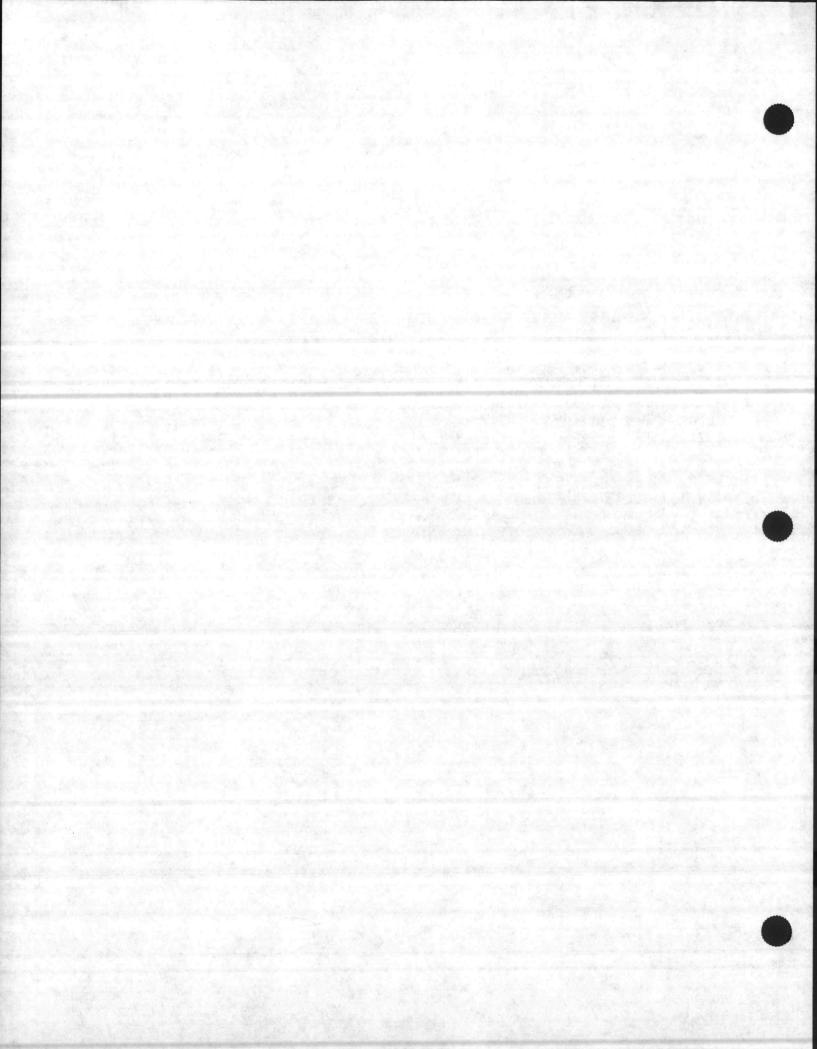
CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

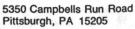
SAMPLE ID: 1-AS NUS SAMPLE NO: P0225106

LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	6	ug/L
		trans-1.3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		_trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column.

The concentration reported represents the sum of the two isomers.







February 23, 1993 Report No.: 00013686 · Section A Page 6

## LABORATORY ANALYSIS REPORT

CLIENT NAME:

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

NUS CLIENT NO:

1600 0006

ADDRESS:

420 ROUSER ROAD

WORK ORDER NO:

55830

MR. JOHN LOVELY

ATTENTION:

CORAOPOLIS, PA 15108-

VENDOR NO:

Carbon Copy:

SAMPLE ID: 1-AC

DATE SAMPLED:

02-FEB-93

NUS SAMPLE NO:

P0225107

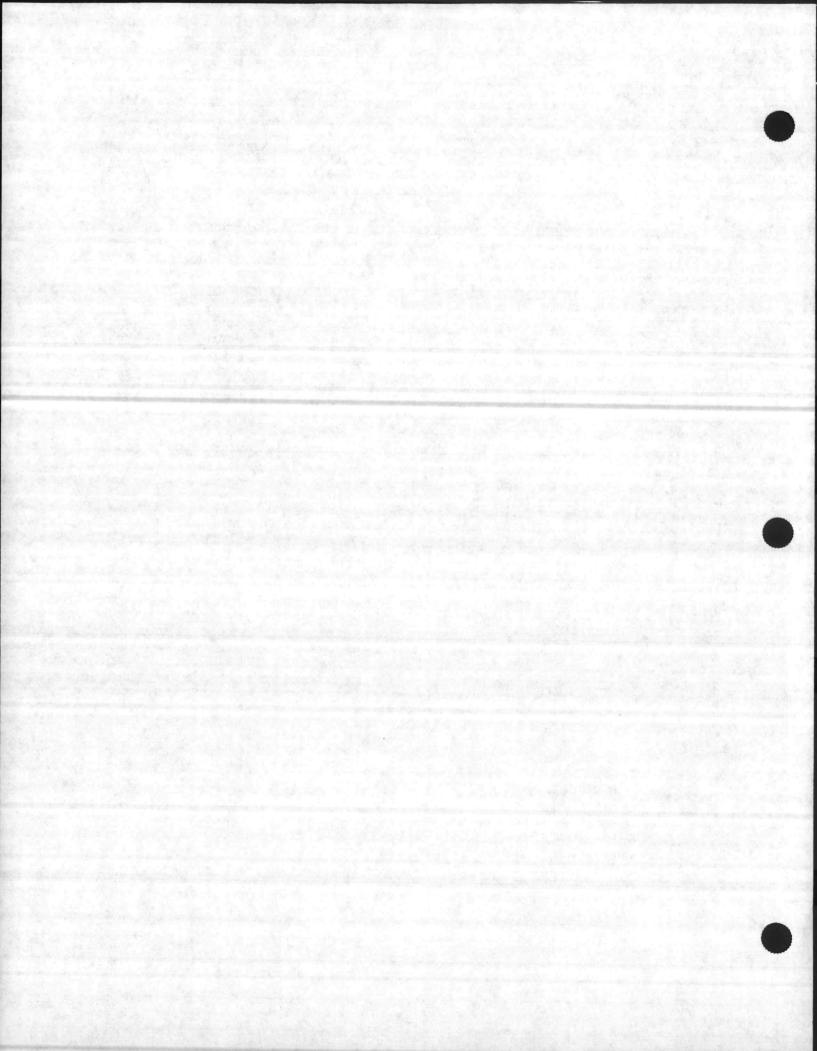
DATE RECEIVED:

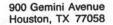
06-FEB-93

P.O. NO.: CTO # 19017

APPROVED BY:

LN	CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
	010/11	1,2-dimethylbenzene [o-xylene]	< 2	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	< 2	ug/L
		benzene	< 2	ug/L
		ethylbenzene	< 2	ug/L
		methylbenzene [toluene]	< 2	ug/L
5	G100W	PURGEABLE HALOCARBONS		
3	OTOON	1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1.2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
- 2		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L







February 23, 1993 Report No.: 00013686 Section A Page 7

#### LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

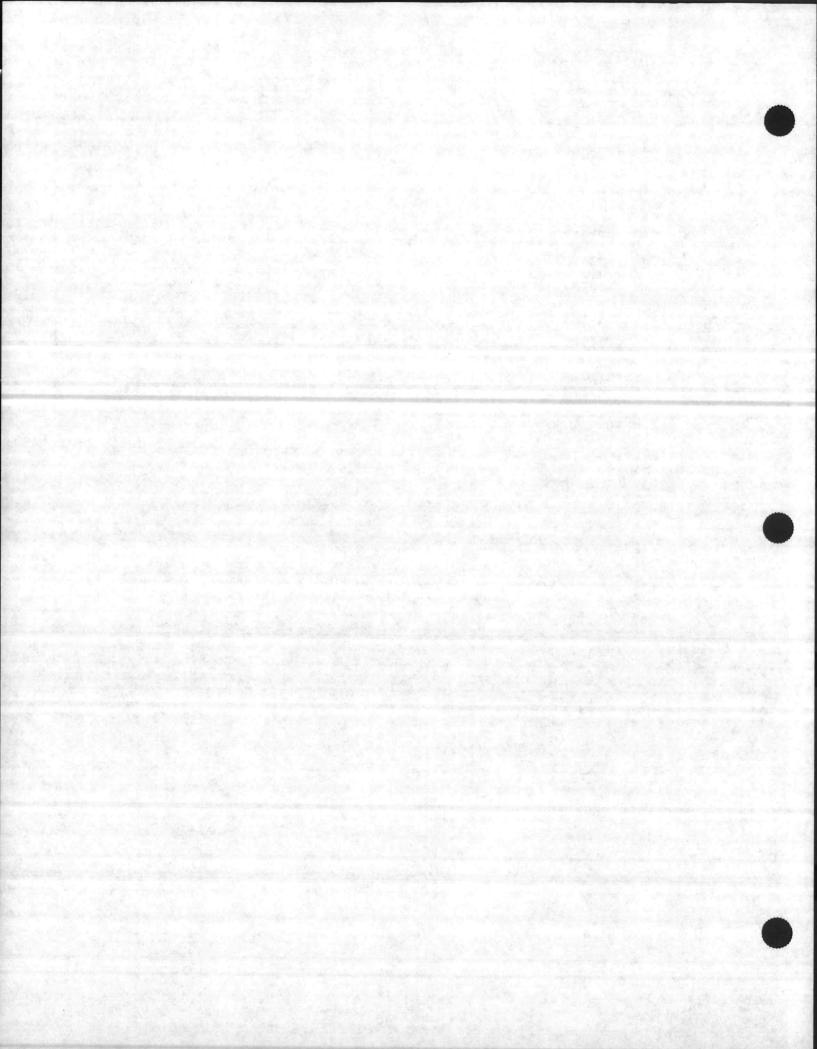
SAMPLE ID: 1-AC NUS SAMPLE NO: P0225107

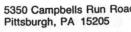
LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

COMMENTS:

In the BTEX analysis. m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.

For sample number P225107, ethylbenzene was not observed in the confirmational analysis. The ethylbenzene result observed in the primary analysis was not reported. A low surrogate recovery was observed for this sample in both the primary and confirmational analyses. The low surrogate recovery was probably due to the matrix.





900 Gemini Avenue Houston, TX 77058



February 23, 1993 Report No.: 00013686 - Section A Page 8

## LABORATORY ANALYSIS REPORT

CLIENT NAME:

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS:

420 ROUSER ROAD

ATTENTION:

CORAOPOLIS, PA 15108-

MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID:

2-0W

P0225108 NUS SAMPLE NO:

P.O. NO.: CTO # 19017

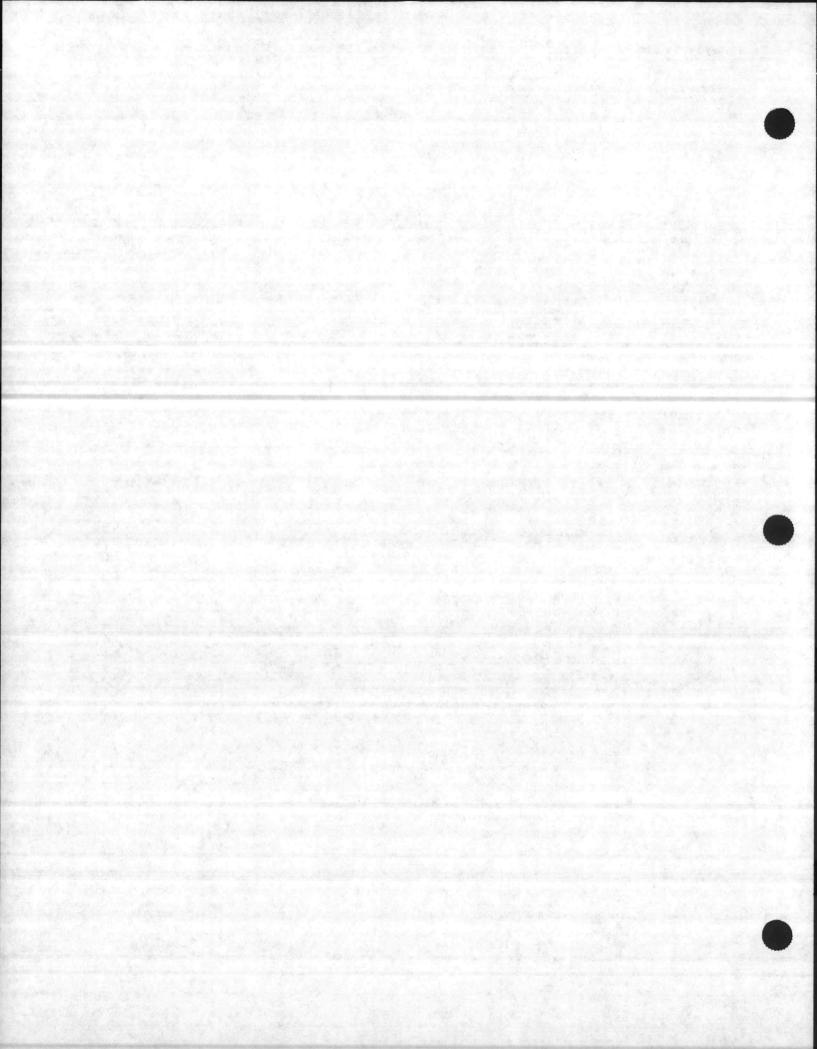
NUS CLIENT NO: 1600 0006 WORK ORDER NO: 55830

**VENDOR NO:** 

02-FEB-93 DATE SAMPLED: 06-FEB-93 DATE RECEIVED:

APPROVED BY:

LN	CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
3	01074	1,2-dimethylbenzene [o-xylene]	< 2	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene {m-/p-xylenes}	< 2	ug/L
		benzene	3	ug/L
		ethylbenzene	< 2	ug/L
		methylbenzene [toluene]	5	ug/L
5	G100W	PURGEABLE HALOCARBONS		
,	OTOON	1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/l
		cis-1,3-dichloropropene	< 2	ug/l
		dibromochloromethane	< 2	ug/l
		dichlorodifluoromethane	< 2	ug/l
		dichloromethane [methylene chloride]	. < 5	ug/l





900 Gemini Avenue Houston, TX 77058

February 23, 1993 Report No.: 00013686 Section A Page 9

## LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: 2-0W NUS SAMPLE NO: P0225108

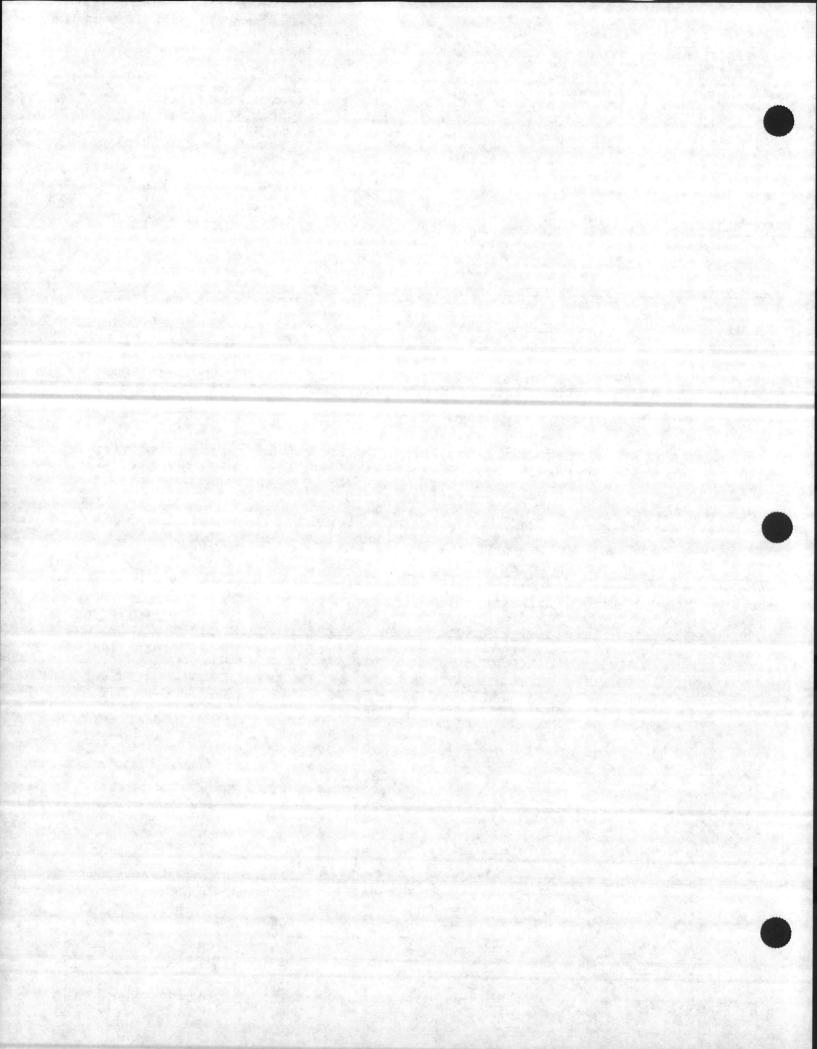
LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 40	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	160 D	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	290 D	ug/L

#### COMMENTS:

In the BTEX analysis, m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.

Sample number P225108 exhibited high surrogate recoveries in both the primary and confirmational analyses. The high surogate recoveries were due to a matrix interference. The matrix interference also interferred with the confirmation of benzene. The benzene result from the primary analysis is reported. Ethylbenzene was not observed in the confirmational analysis. The ethylbenzene result observed in the primary analysis was not reported.

"D" indicates that the result was obtained from an analysis performed at a secondary dilution.





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## LABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

MR. JOHN LOVELY ATTENTION:

Carbon Copy:

NUS SAMPLE NO: P0225109

P.O. NO.: CTO # 19017

NUS CLIENT NO: 1600 0006

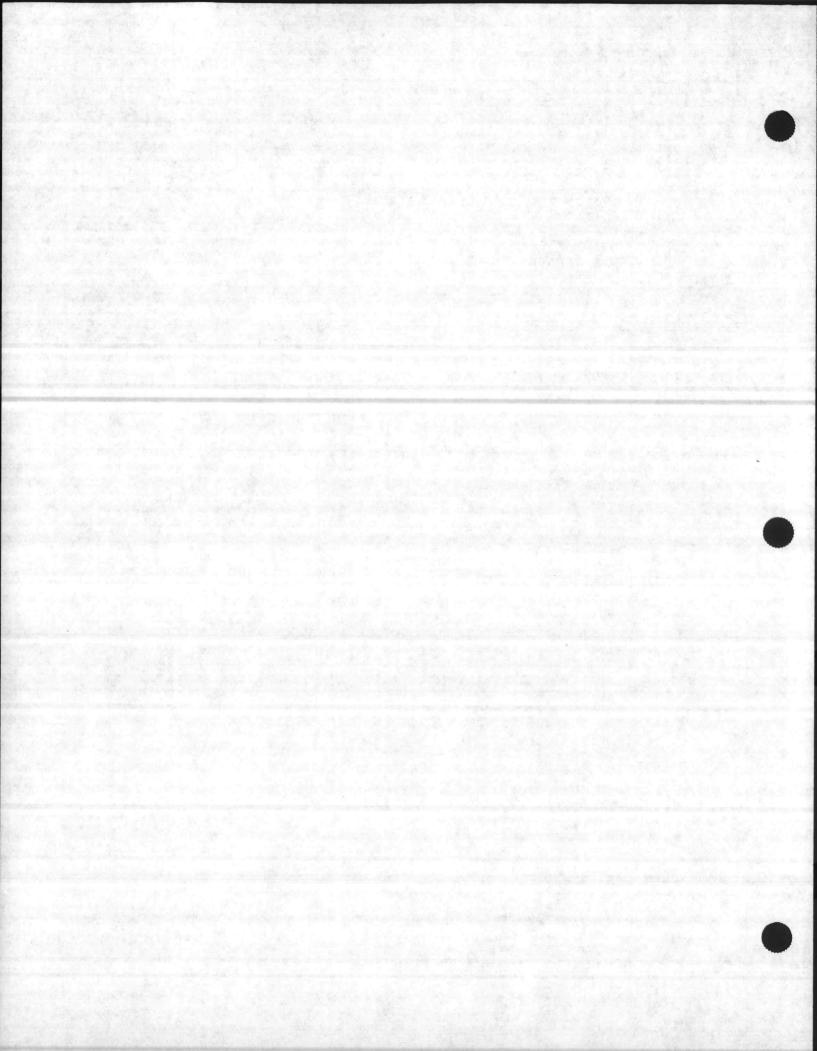
WORK ORDER NO: 55830

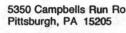
VENDOR NO:

03-FEB-93 DATE SAMPLED: SAMPLE ID: 2-AS DATE RECEIVED: 06-FEB-93

APPROVED BY:

<u>LN</u>	TEST CODE	DETERMINATION	RESULT	UNITS
	A 51 511	TAL METALS & CLP DATA PACKAGE	DONE	
1	ACLPW		DONE	
2	DPACK	CLP Data Package Deliverable		
3	G107W	BTEX PACKAGE  1,2-dimethylbenzene [o-xylene]	8	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	10	ug/L
		benzene	3	ug/L
			14	ug/L
		ethylbenzene methylbenzene [toluene]	10	ug/L
_	G100W	PURGEABLE HALOCARBONS		12.5
5	GIOOM	1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L





900 Gemini Avenue Houston, TX 77058

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## LABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: 2-AS NUS SAMPLE NO: P0225109

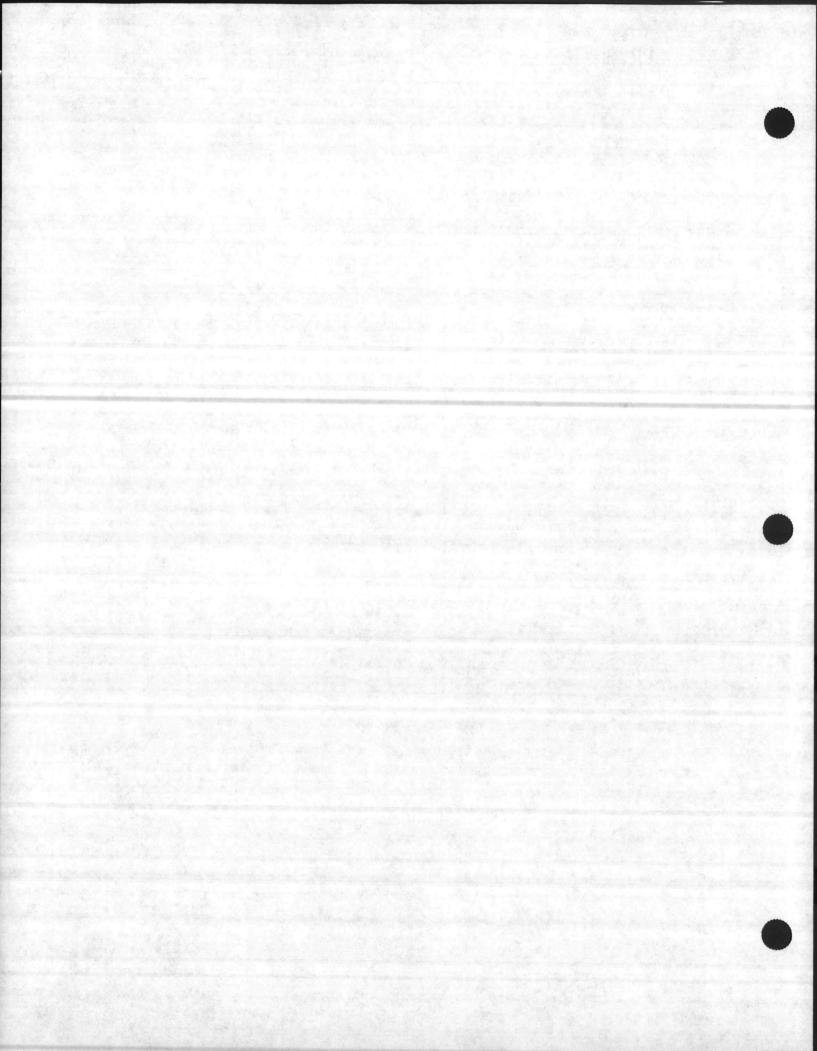
HALLIBURTON NUS
Environmental Corporation

**Environmental Laboratories** 

	TEST			
LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column.

The concentration reported represents the sum of the two isomers.



1600 0006

55830

900 Gemini Avenue Houston, TX 77058



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## LABORATORY ANALYSIS REPORT

/NAVY CLEAN CLIENT NAME: BAKER ENVIRONMENTAL, INC.

420 ROUSER ROAD ADDRESS:

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID:

NUS SAMPLE NO: P0225110

> CTO # 19017 P.O. NO.:

VENDOR NO:

DATE SAMPLED: 03-FEB-93

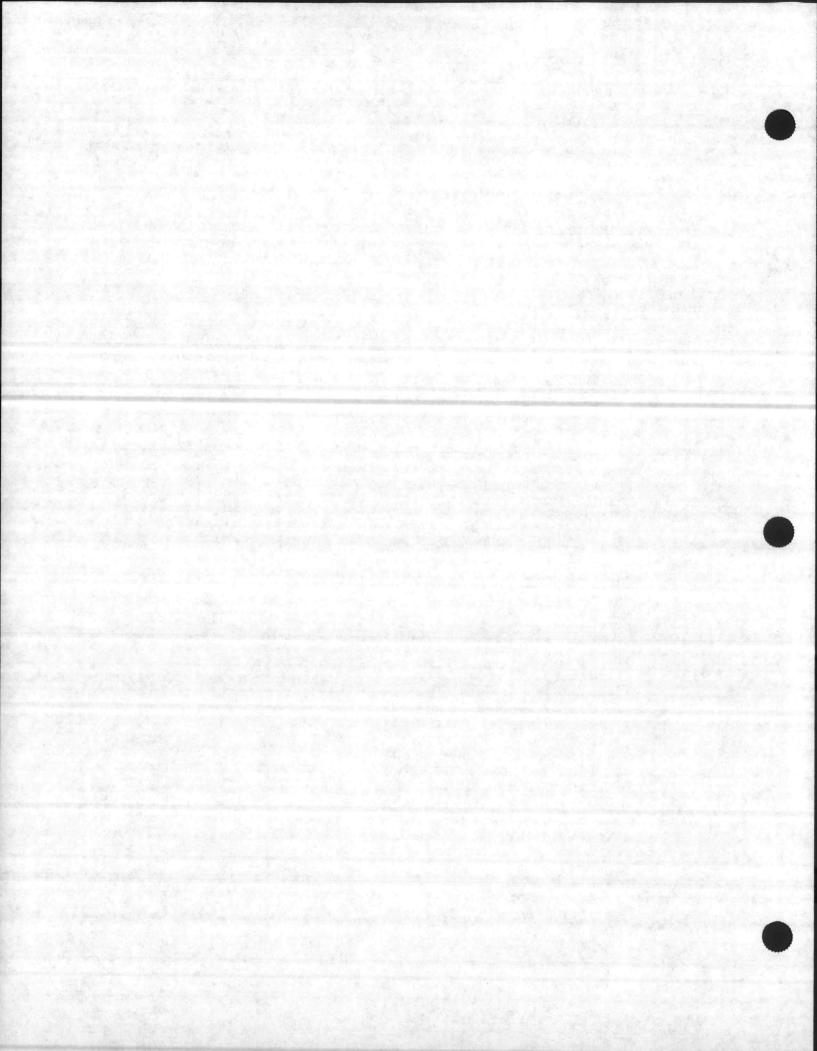
DATE RECEIVED: 06-FEB-93

APPROVED BY:

NUS CLIENT NO:

WORK ORDER NO:

LN	TEST CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
The second second		1,2-dimethylbenzene [o-xylene]	< 2	ug/L
		1.3-dimethylbenzene, 1.4-dimethylbenzene [m-/p-xyelenes]	< 2	ug/L
		benzene	< 2	ug/L
		ethylbenzene	3	ug/L
		methylbenzene [toluene]	2	ug/L
5	G100W	PURGEABLE HALOCARBONS		
		1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1.1-dichloroethene [1.1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1.2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
ALC: N		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L





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## LABORATORY ANALYSIS REPORT

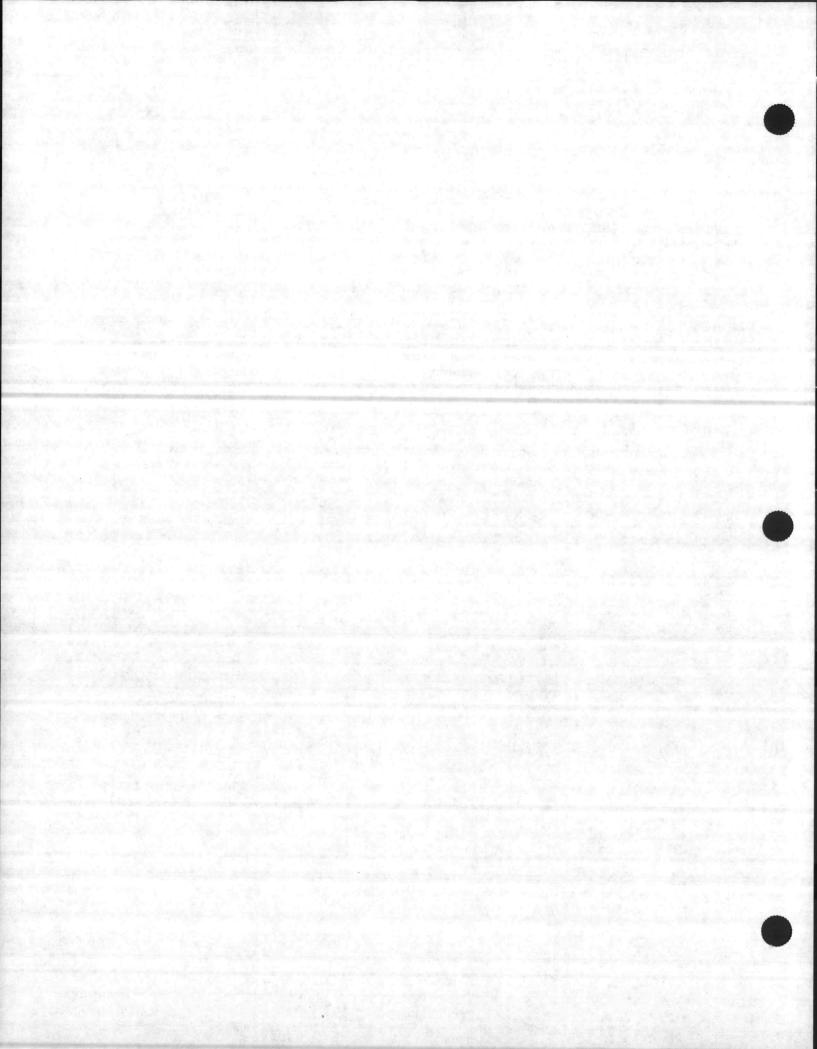
CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: 2-AC NUS SAMPLE NO: P0225110

LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column.

The concentration reported represents the sum of the two isomers.





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#### LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: 3-0W NUS SAMPLE NO: P0225111

P.O. NO.: CTO # 19017

NUS CLIENT NO: 1600 0006 WORK ORDER NO: 55830

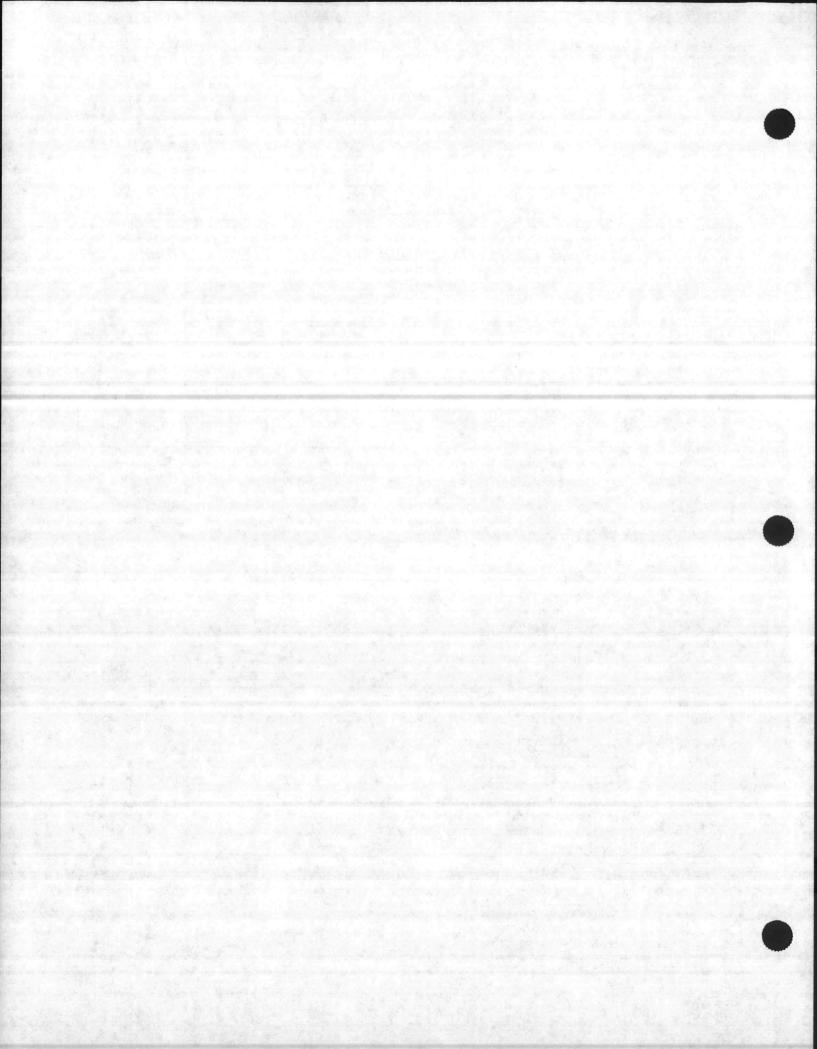
NK OKDEK NO: 5583

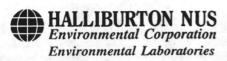
VENDOR NO:

DATE SAMPLED: 03-FEB-93
DATE RECEIVED: 06-FEB-93

APPROVED BY: Joanne Simanic

LN	CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
Tool of		1.2-dimethylbenzene [o-xylene]	11	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	< 2	ug/L
		benzene	3	ug/L
		ethylbenzene	2	ug/L
		methylbenzene [toluene]	5	ug/L
5	G100W	PURGEABLE HALOCARBONS		
		1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	. < 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
10.00		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	"ug/L





900 Gemini Avenue Houston, TX 77058

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#### LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: 3-0W NUS SAMPLE NO: P0225111

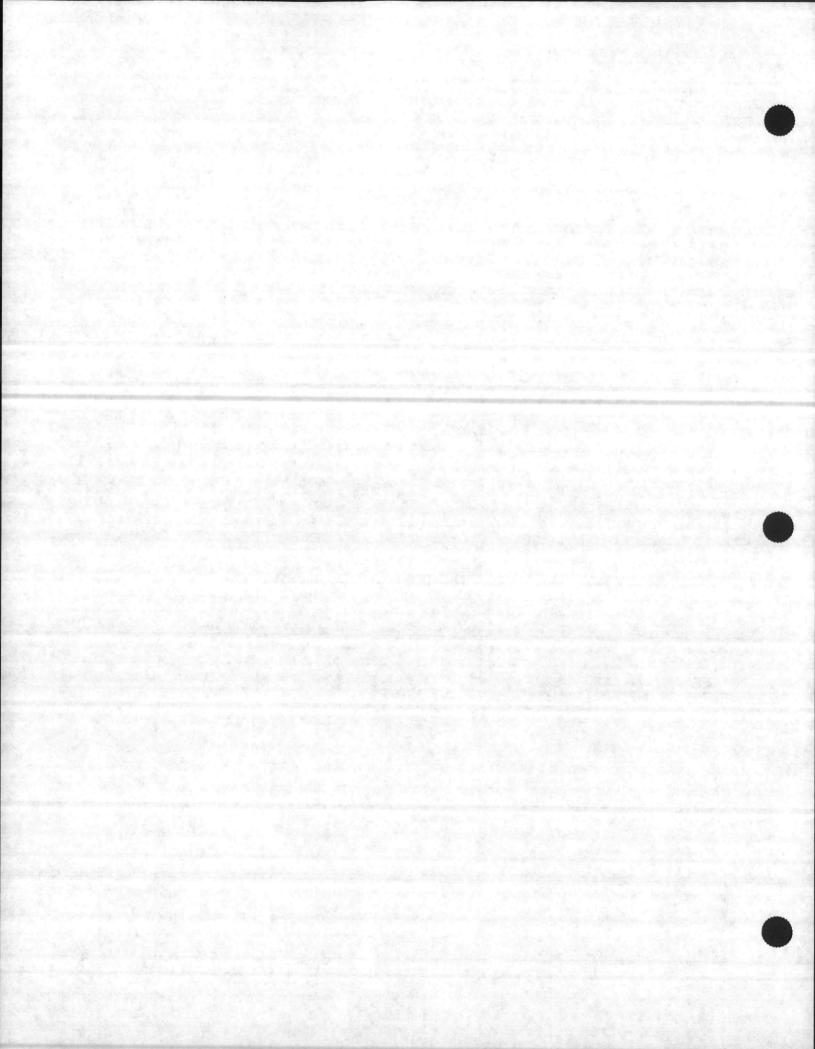
LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 40 D	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	180 D	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	320 D	ug/L

#### COMMENTS:

In the BTEX analysis, m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.

Sample number P225111 exhibited high surrogate recoveries in both the primary and confirmational analyses. The high surrogate recoveries were due to a matrix interference. The matrix interference also interferred with the confirmation of benzene. The benzene result from the primary analysis is reported. Ethylbenzene was not observed in the confirmational analysis. The ethylbenzene result observed in the primary analysis was not reported.

"D" indicates that the result was obtained from an analysis performed at a secondary dilution.



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## LABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

MR. JOHN LOVELY ATTENTION:

Carbon Copy:

SAMPLE ID: 3-AS

NUS SAMPLE NO: P0225112

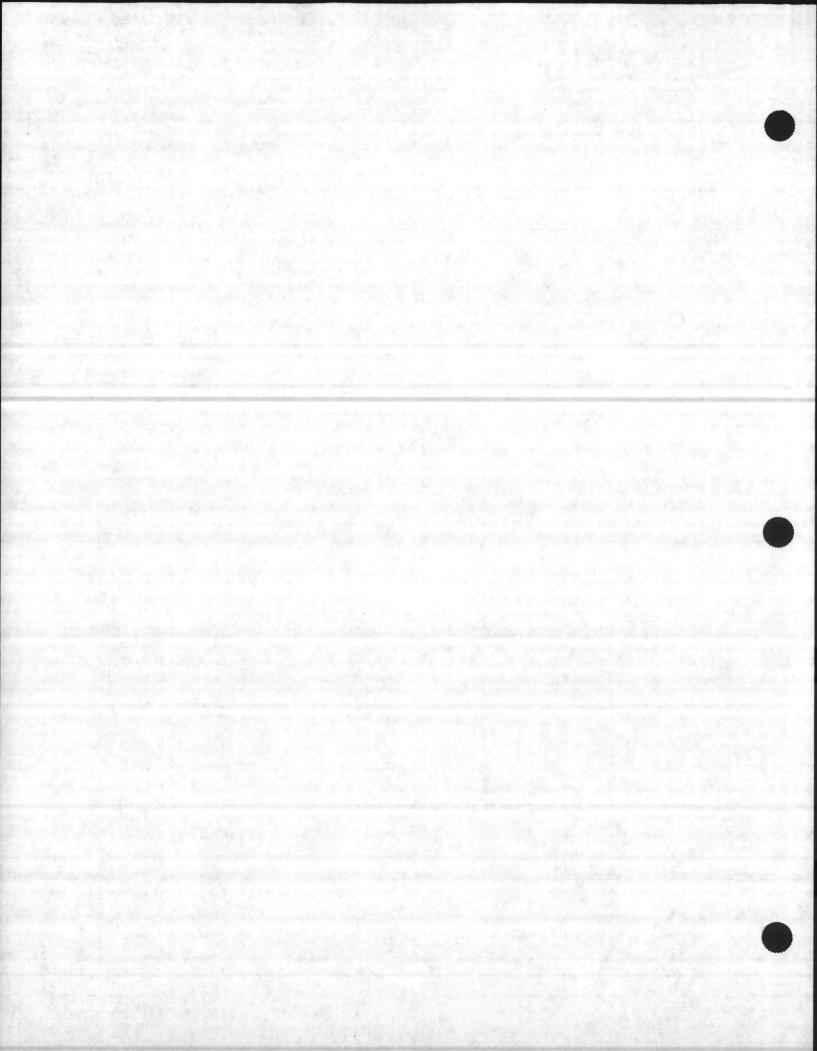
P.O. NO.: CTO # 19017

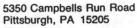
NUS CLIENT NO: 1600 0006 WORK ORDER NO: 55830

VENDOR NO:

03-FEB-93 DATE SAMPLED: 06-FEB-93 DATE RECEIVED: Joanne Simanic APPROVED BY:

LN	CODE	DETERMINATION	RESULT	UNITS
	ACI DII	TAL METALS & CLP DATA PACKAGE	DONE	
1	ACLPW		DONE	
2	DPACK	CLP Data Package Deliverable BTEX PACKAGE		
3	G107W		7	ug/L
		1,2-dimethylbenzene [o-xylene] 1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	9	ug/L
		에도 물리에게 가장 되었다면 그게 가는 것이 되었다. 그는 그는 그는 그는 그를 보는 것이 없는 것이 없는 것이 없었다. 그는 그를 다 먹는 것이 그 사람이 되었다. 그는 그는 그는 그를 다 먹는 것이 없는 것이 없는 것이 없는 것이 없다.	3	ug/L
		benzene	14	ug/L
		ethylbenzene	9	ug/L
100		methylbenzene [toluene]	•	- ug/ -
5	G100W	PURGEABLE HALOCARBONS	< 2	ug/L
		1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 5	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 2	
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane		ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L







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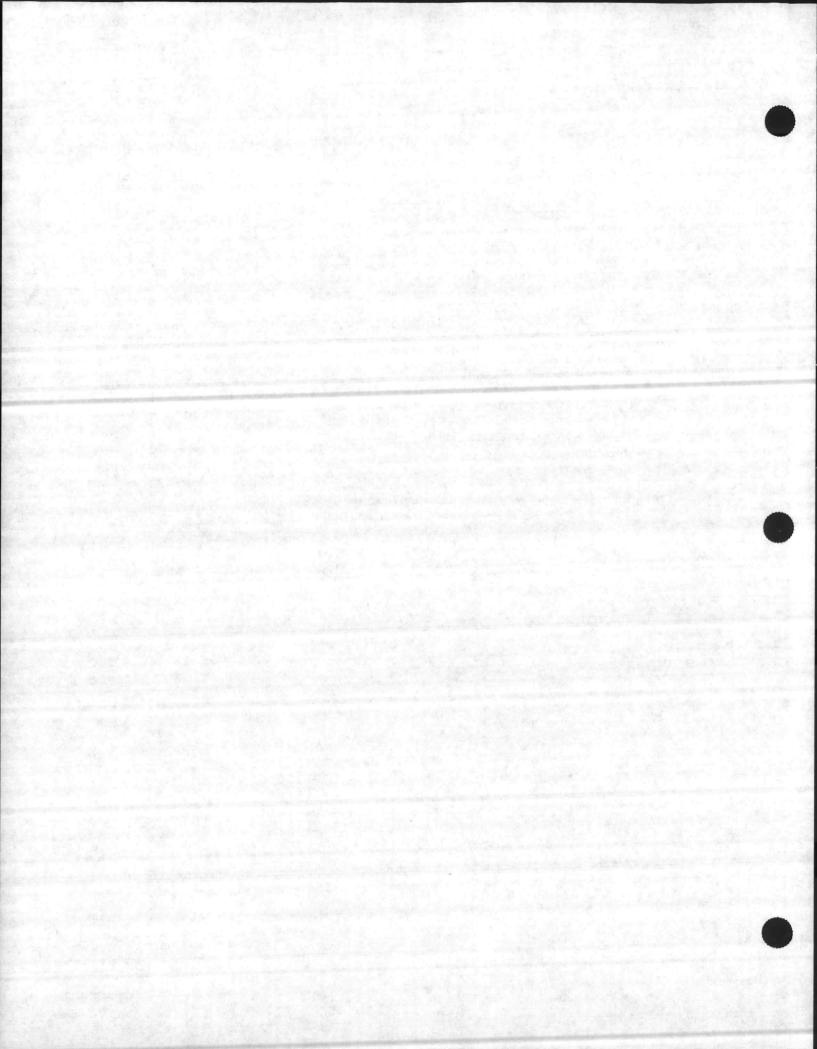
# LABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: 3-AS NUS SAMPLE NO: P0225112

LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.



900 Gemini Avenue Houston, TX 77058



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## ABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

420 ROUSER ROAD ADDRESS:

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: 3-AC

NUS SAMPLE NO: P0225113

P.O. NO.: CTO # 19017

NUS CLIENT NO: 1600 0006 WORK ORDER NO:

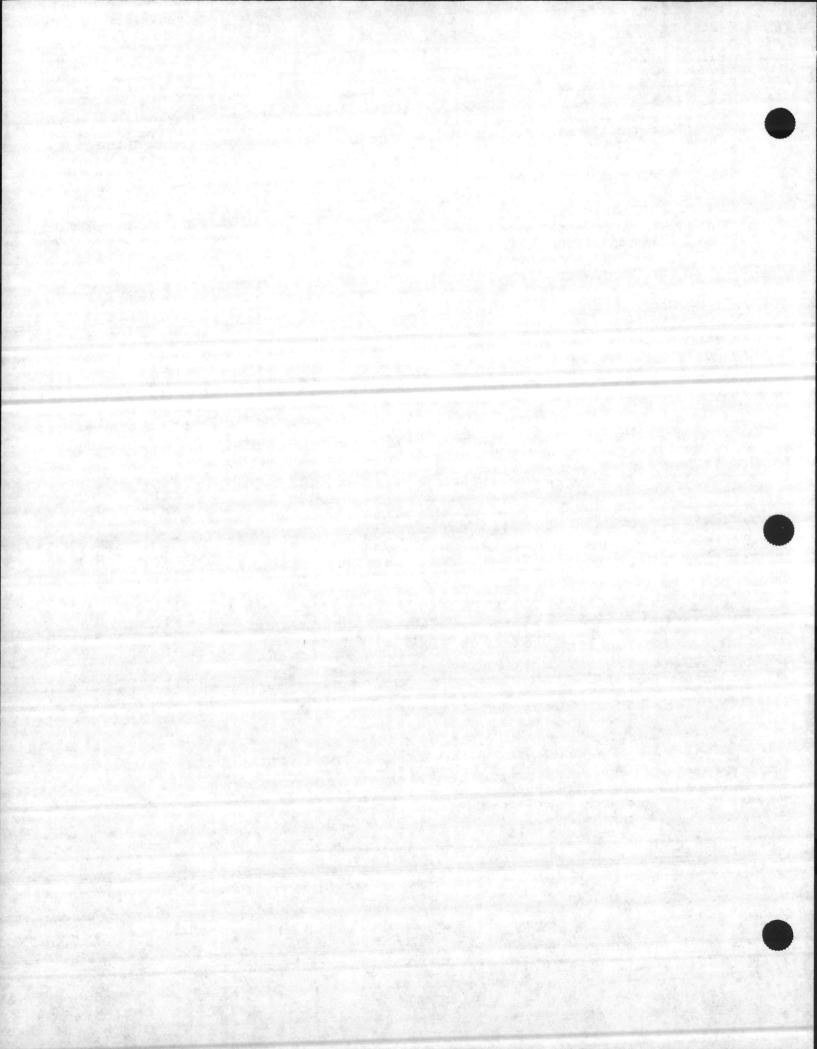
55830

**VENDOR NO:** 

DATE SAMPLED: 03-FEB-93 DATE RECEIVED: 06-FEB-93

APPROVED BY: Joanne Simanic

<u>LN</u>	TEST CODE	DETERMINATION	RESULT	UNITS
	ACI DII	TAL METALC & CLD DATA DACKACE	DONE	
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DOIL	
3	G107W	BTEX PACKAGE	< 2	ug/L
		1,2-dimethylbenzene [o-xylene]	< 2	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene (m-/p-xylenes)	< 2	ug/L
		benzene	< 2	ug/L
		ethylbenzene	< 2	ug/L
28		methylbenzene [toluene]		ug/L
5	G100W	PURGEABLE HALOCARBONS	< 2	ug/L
		1,1,1-trichloroethane	< 2	
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane		ug/L
		1.1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L



900 Gemini Avenue Houston, TX 77058

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## LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

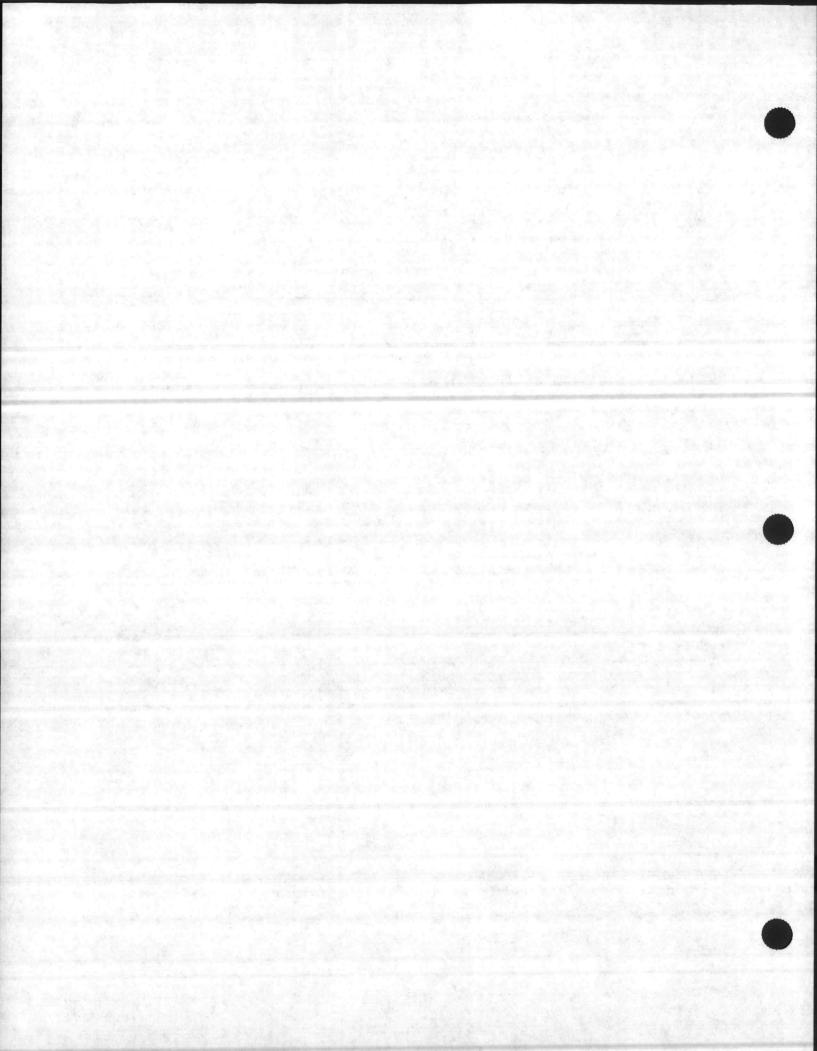
SAMPLE ID: 3-AC NUS SAMPLE NO: P0225113

LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

COMMENTS:

In the BTEX analysis, m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.

For sample number P225113, benzene was not observed in the confirmational analysis. The benzene result observed in the primary analysis was not reported. A low surrogate recovery was observed for this sample in both the primary and confirmational analyses. The low surrogate recoveries were probably due to the matrix.





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## LABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

420 ROUSER ROAD ADDRESS:

CORAOPOLIS, PA 15108-

MR. JOHN LOVELY ATTENTION:

Carbon Copy:

SAMPLE ID: 7-OW

NUS SAMPLE NO: P0225118

P.O. NO .: CTO # 19017

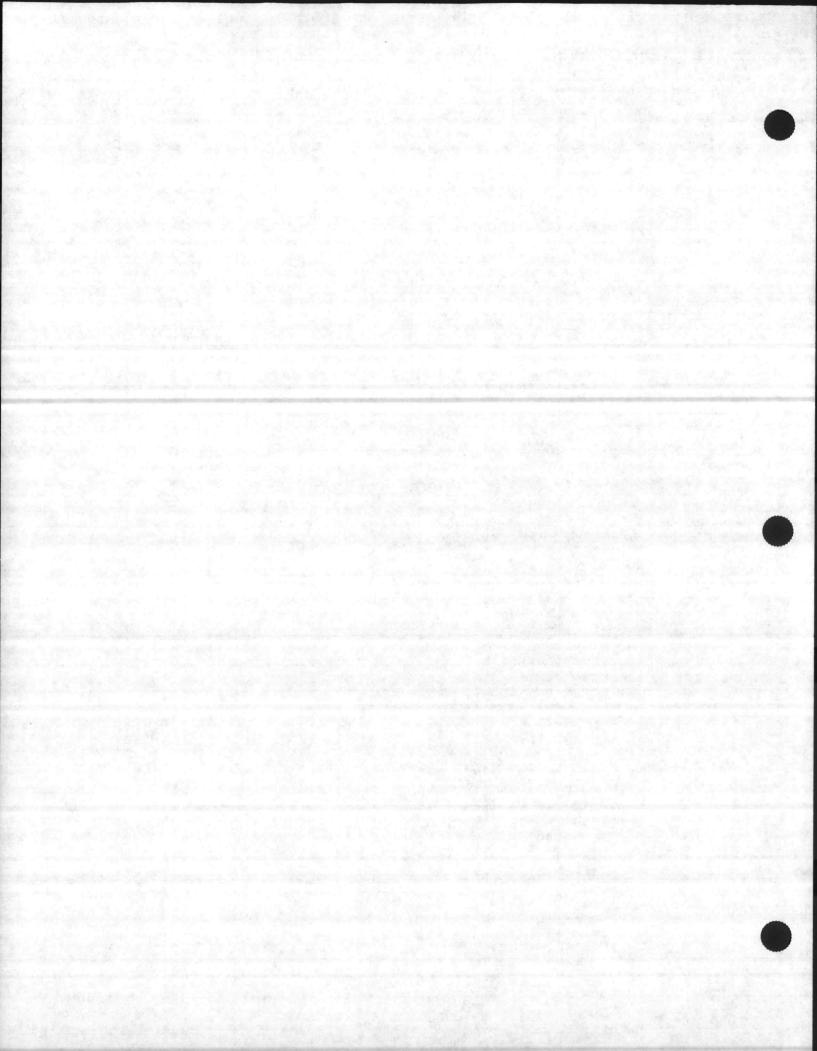
NUS CLIENT NO: 1600 0006 WORK ORDER NO: 55830

VENDOR NO:

05-FEB-93 DATE SAMPLED: 06-FEB-93 DATE RECEIVED:

APPROVED BY: Joanne Simanic

	LN	TEST CODE	DETERMINATION	RESULT	UNITS
			THE METAL C. C. C. D. DATA DACKACE	DONE	
	1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
	2	DPACK	CLP Data Package Deliverable	00.12	
	3	G107W	BTEX PACKAGE	2	ug/L
			1,2-dimethylbenzene [o-xylene]	< 2	ug/L
			1.3-dimethylbenzene. 1.4-dimethylbenzene [m-/p-xylenes]	2	ug/L
			benzene	< 2	ug/L
			ethylbenzene	12	ug/L
			methylbenzene [toluene]		-9
	5	G100W	PURGEABLE HALOCARBONS	< 2	ug/L
			1,1,1-trichloroethane	< 2	ug/L
			1,1,2,2-tetrachloroethane	< 2	ug/L
			1,1,2-trichloroethane	< 2	ug/L
			1,1-dichloroethane	2	ug/L
			1,1-dichloroethene [1,1-dichloroethylene]	< 5	ug/L
			1,2-dichlorobenzene [o-dichlorobenzene]	< 2	ug/L
			1,2-dichloroethane	< 2	ug/L
			1,2-dichloropropane	< 5	ug/L
			1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
			1,4-dichlorobenzene [p-dichlorobenzene]	< 2	ug/L
			2-chloroethylvinyl ether	< 2	ug/L
			bromodichloromethane [dichlorobromomethane]	< 2	ug/L
			bromomethane [methyl bromide]	< 2	ug/L
			carbon tetrachloride	< 2	ug/L
			chlorobenzene	< 2	The second secon
			chloroethane		ug/L
			chloroform	< 2	ug/L
			chloromethane [methyl chloride]	< 2	ug/L
			cis-1,3-dichloropropene	< 2	ug/L
			dibromochloromethane	< 2	ug/L
			dichlorodifluoromethane	< 2	ug/L
			dichloromethane [methylene chloride]	< 5	ug/L



900 Gemini Avenue Houston, TX 77058



February 23, 1993 Report No.: 00013686 Section A Page 29

## LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: 7-OW NUS SAMPLE NO: P0225118

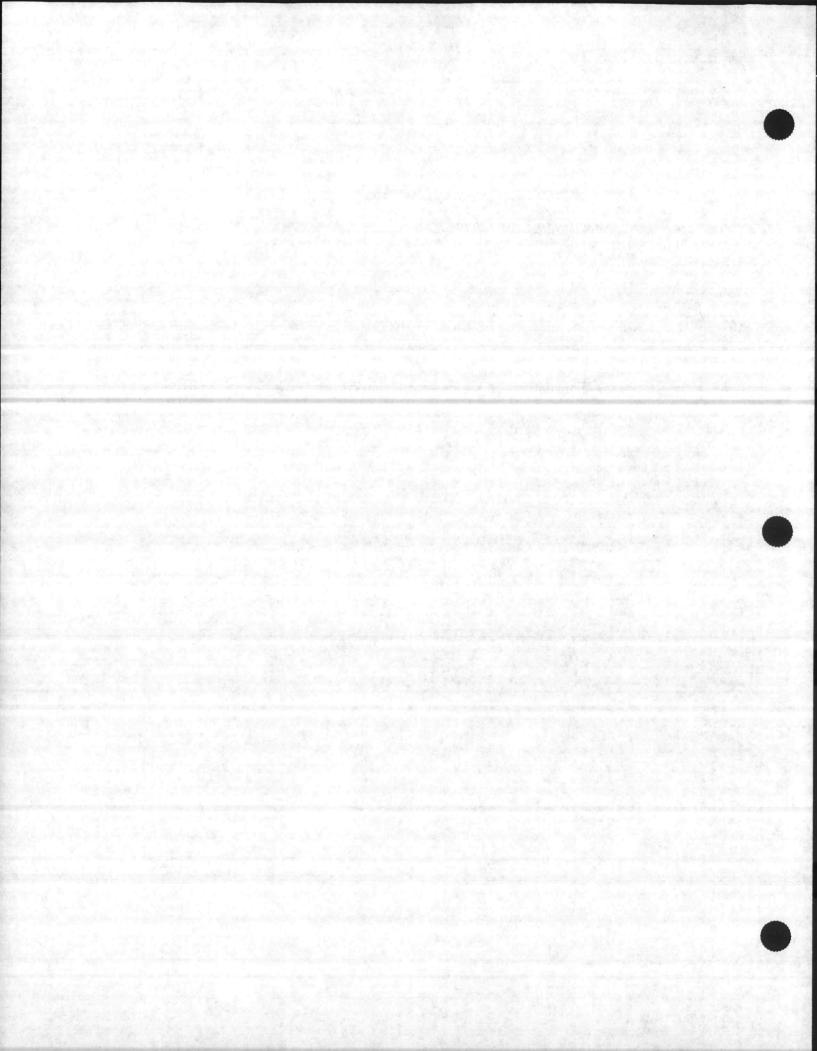
LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 40 D	ug/L
		trans-1.3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	120 D	ug/L
		trichlorofluoromethane	< 2	ug/L

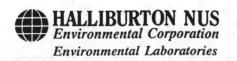
COMMENTS:

In the BTEX analysis, m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.

Sample number P225118 exhibited high surrogate recoveries in both the primary and confirmational analyses. The high surrogate recoveries were due to a matrix interference. The matrix interference also interferred with the confirmation of benzene. The benzene result from the primary analysis is reported.

"D" indicates that the result was obtained from an analysis performed at a secondary dilution.





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# LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: 7-AS

NUS SAMPLE NO: P0225119

> P.O. NO .: CTO # 19017

DATE SAMPLED:

05-FEB-93 DATE RECEIVED: 06-FEB-93

1600 0006

55830

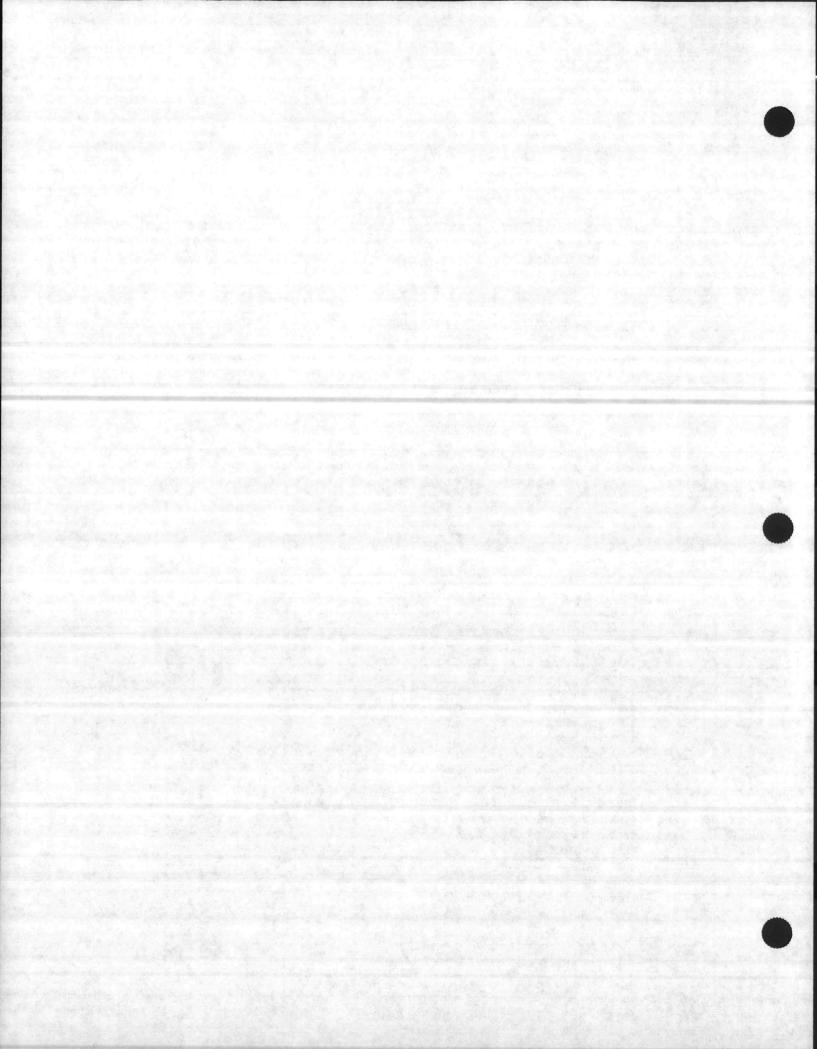
APPROVED BY:

NUS CLIENT NO:

WORK ORDER NO:

VENDOR NO:

LN	CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
		1,2-dimethylbenzene [o-xylene]	2	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	3	ug/L
		benzene	< 2	ug/L
		ethylbenzene	< 2	ug/L
		methylbenzene [toluene]	11	ug/L
5	G100W	PURGEABLE HALOCARBONS		
		1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L





February 23, 1993 Report No.: 00013686 Section A Page 31

## LABORATORY ANALYSIS REPORT

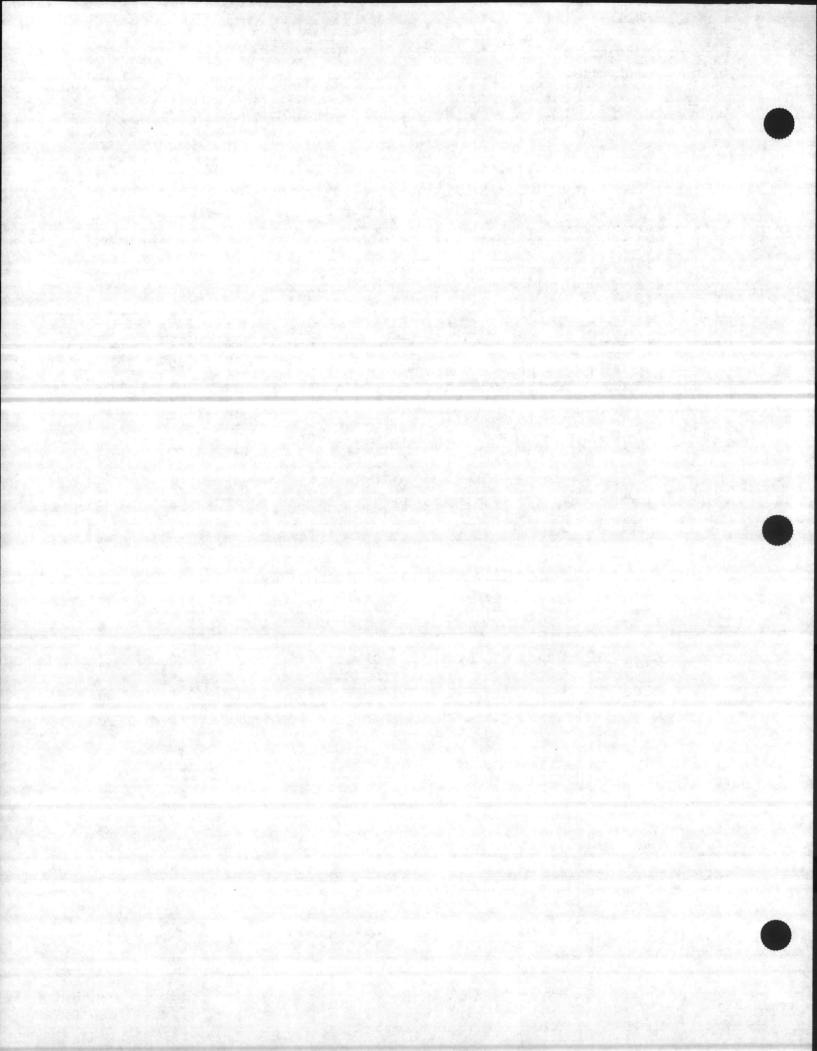
CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

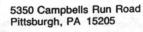
SAMPLE ID: 7-AS NUS SAMPLE NO: P0225119

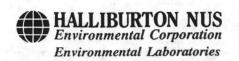
LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column.

The concentration reported represents the sum of the two isomers.







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# LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: 7-AC

NUS SAMPLE NO: P0225120

P.O. NO.: CTO # 19017

DATE SAMPLED:

NUS CLIENT NO:

WORK ORDER NO:

VENDOR NO:

05-FEB-93

1600 0006

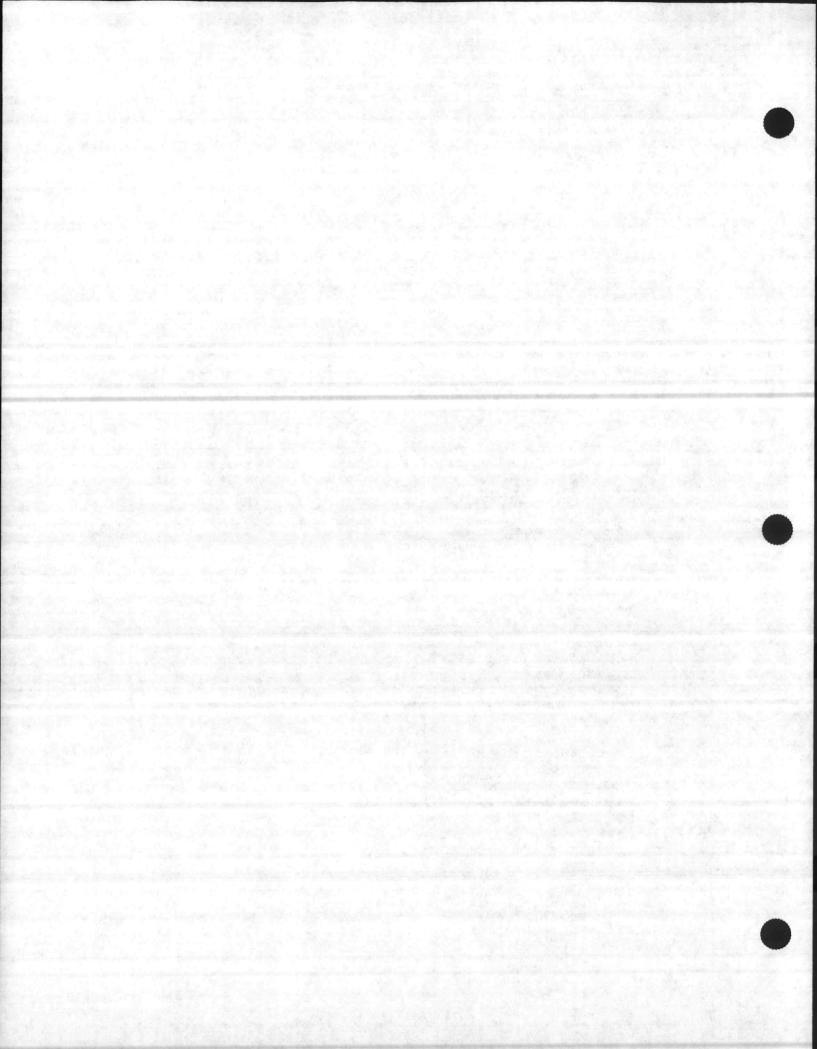
55830

DATE RECEIVED:

06-FEB-93

APPROVED BY:

LN	CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
		1,2-dimethylbenzene [o-xylene]	< 2	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	< 2	ug/L
		benzene	< 2	ug/L
		ethylbenzene	< 2	ug/L
		methylbenzene [toluene]	10	ug/L
5	G100W	PURGEABLE HALOCARBONS		
		1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1.1.2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1.1-dichloroethene [1.1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L



5350 Campbells Run Road

900 Gemini Avenue Houston, TX 77058



February 23, 1993 Report No.: 00013686 - Section A Page 33

## LABORATORY ANALYSIS REPORT

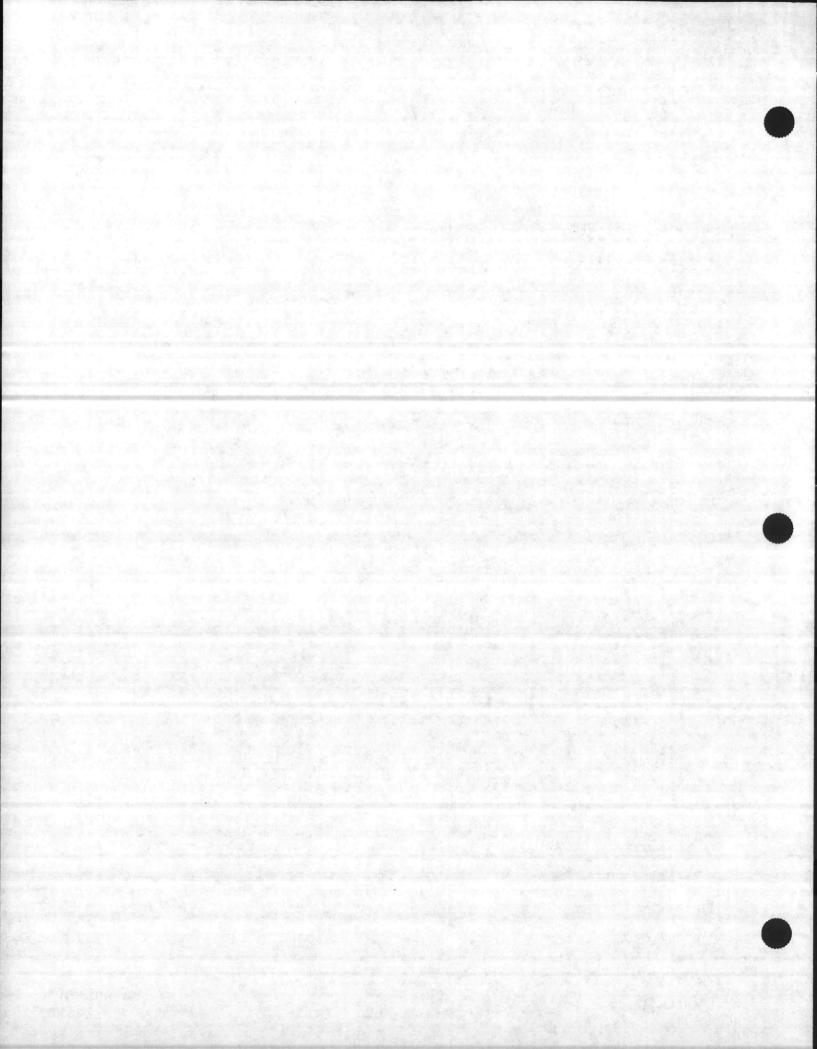
BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

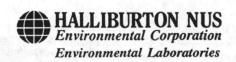
SAMPLE ID: 7-AC NUS SAMPLE NO: P0225120

LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1.2-dichloroethene [trans-1.2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

In the BTEX analysis, m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.

For sample number P225120, toluene was not observed in the confirmational analysis. The toluene result observed in the primary analysis was not reported.





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## LABORATORY ANALYSIS REPORT

CLIENT NAME:

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS:

420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

P.O. NO.: CTO # 19017

NUS CLIENT NO:

1600 0006

WORK ORDER NO:

55830

VENDOR NO:

Carbon Copy:

SAMPLE ID: 7-DL

NUS SAMPLE NO: P0225121

DATE SAMPLED:

05-FEB-93

DATE RECEIVED:

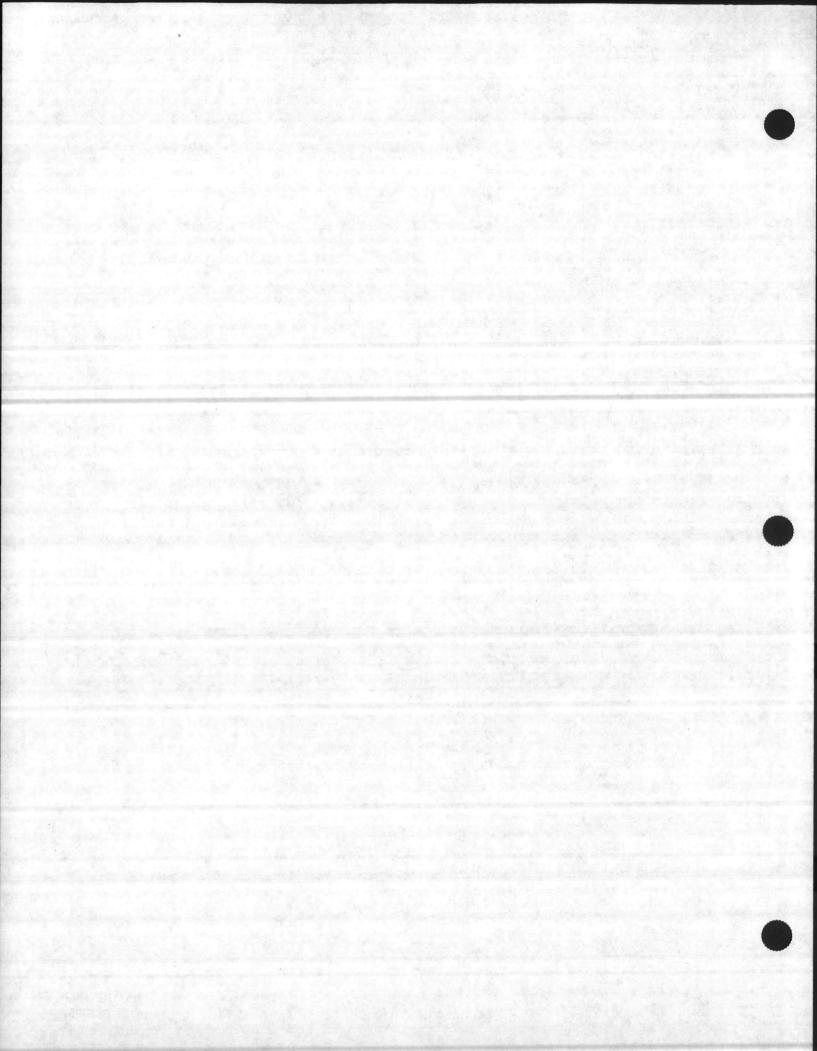
06-FEB-93

APPROVED BY:

Ruth Volk

<u>LN</u>	TEST CODE	DETERMINATION	RESULT	UNITS
2	TEON	Oil and Greace. Gravimetric	< 3	mg/L
4		s = [24] [전투] (1.47)(1.17) [전투] (2.27)	< 0.1	mg/L
5		그 그리고를 하나 무슨 물을 하나 살아가 있는데 그는 것이 되었다면서 살아가 되었다면 하는데 그는 것이 살아 살아 있다면 살아 없다면 살아 싶다면 살아 없다면 살아 살아 살아 살아 살아 살아 싶다면 살아	44	mg/L
		Ammonia (as N), Direct	0.5	mg/L
7	1020	Alkalinity, Pht (as CaCO3)	0	mg/L
8			26	mg/L
9		# - [ ] 그 그 문자를 가득하는 경험에 가게 된 사람들에 가게 되었다면 되었다면 되었다면 보다 되었다. [ ] - [ ] 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그	26	mg/L
10			0	mg/L
		마네네워드 (1985) [1986] [1986] 전 1986 [1986] 전	24	mg/L
		4. MANGARI BANGBANG BANGBANG MATURING MENUNGKAN BANGBANG BANGBANG BANGBANG BANGBANG BANGBANG BANGBANG BANGBANG	< 0.02	mg/L
- M. M. Z.		Solids, Dissolved at 1800	87	mg/L
14	1610	Solids, Suspended at 103C	< 10	mg/L
	3 4 5 6 7 8 9 10 11 12 13	3 I680 4 I391 5 I320 6 I030 7 I020 8 I023 9 I024 10 I026 11 I130 12 I410 13 I590	LN CODE  DETERMINATION  3 I680 Oil and Grease, Gravimetric 4 I391 Nitrate/Nitrite 5 I320 Hardness, Total (as CaCO3) 6 I030 Ammonia (N), Direct Ammonia (as N), Direct 7 I020 Alkalinity, Pht (as CaCO3) 8 I023 Alkalinity, Total (as CaCO3) 9 I024 Alkalinity, Bicarbonate (as CaCO3) 10 I026 Alkalinity, Carbonate (as CaCO3) 11 I130 Chloride (as Cl) 12 I410 Nitrite (as N) 13 I590 Solids, Dissolved at 180C	LN   CODE   DETERMINATION   RESULT

COMMENTS:





February 23, 1993 Report No.: 00013686 Section A Page 35

# LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

ADDRESS:

SAMPLE ID: 6-OW

NUS SAMPLE NO: P0225122

P.O. NO .: CTO # 19017

VENDOR NO:

55830

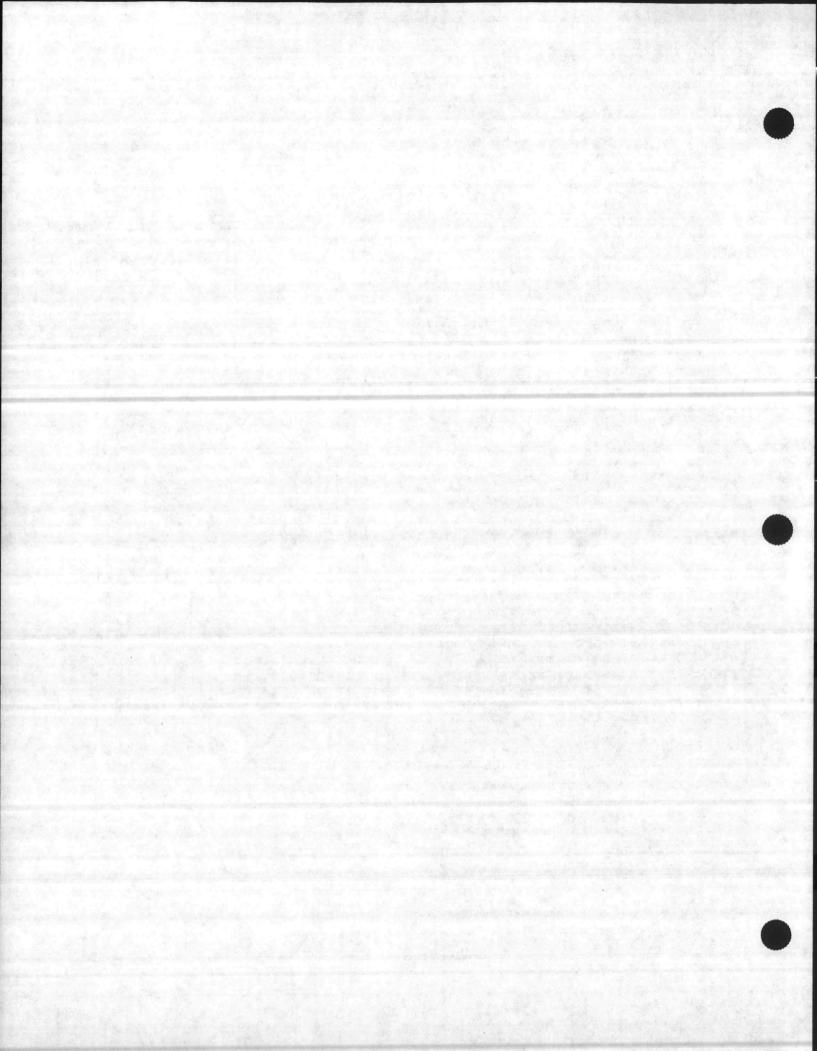
NUS CLIENT NO: 1600 0006

WORK ORDER NO:

DATE SAMPLED: 04-FEB-93
DATE RECEIVED: 06-FEB-93

APPROVED BY: Joanne Simanic

LN	CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
		1,2-dimethylbenzene [o-xylene]	< 2	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene {m-/p-xylenes}	< 2	ug/L
		benzene	3	ug/L
		ethylbenzene	< 2	ug/L
		methylbenzene [toluene]	10	ug/L
5	G100W	PURGEABLE HALOCARBONS		
		1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1.2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1.3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L





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#### LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

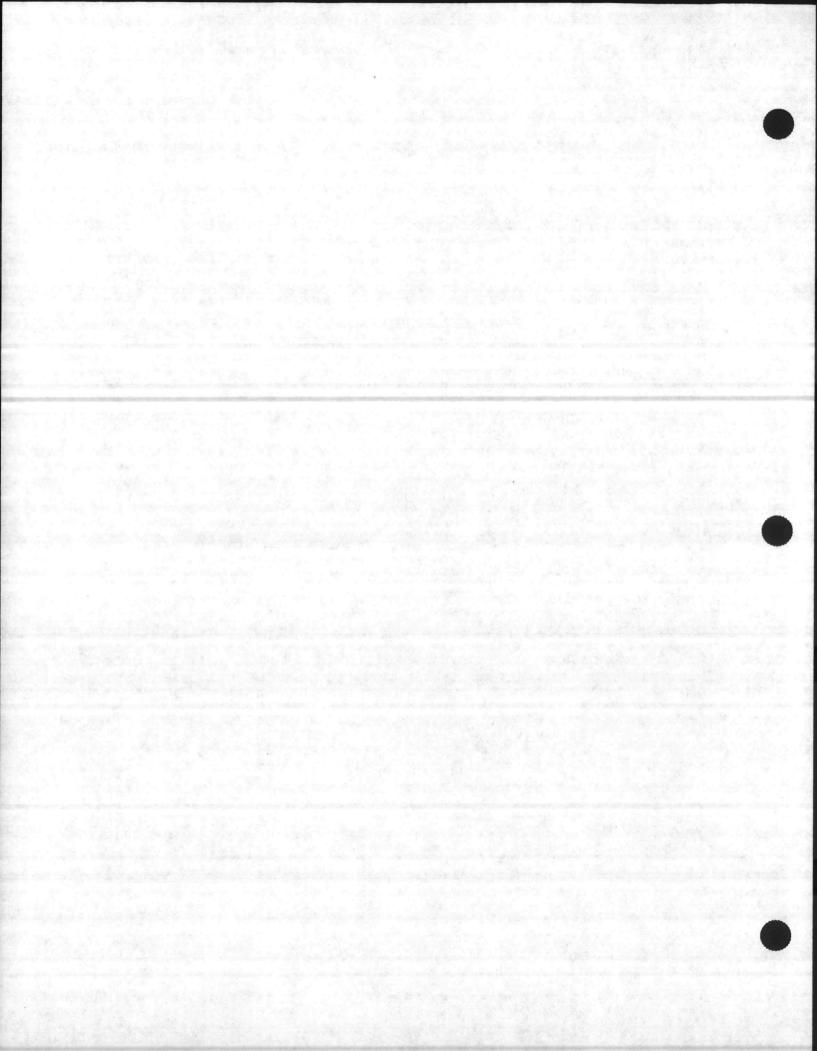
SAMPLE ID: 6-0W NUS SAMPLE NO: P0225122

LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1.2-dichloroethene [trans-1.2-dichloroethylene]	< 40 D	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	180 D	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	360 D	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene coelute on the capillary column. The value reported is the total of both isomers.

> Sample number P225122 exhibited high surrogate recoveries in both the primary and confirmational analyses. The high surrogate recoveries were due to a matrix interference. The matrix interference also interferred with the confirmation of benzene. The benzene result from the primary analysis is reported.

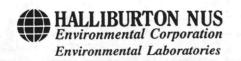
"D" indicates that the result was obtained from an analysis performed at a secondary dilution.



1600 0006

55830

900 Gemini Avenue Houston, TX 77058



February 23, 1993 Report No.: 00013686 Section A Page 37

NUS CLIENT NO:

WORK ORDER NO:

VENDOR NO:

## LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: 6-AS NUS SAMPLE NO: P0225123

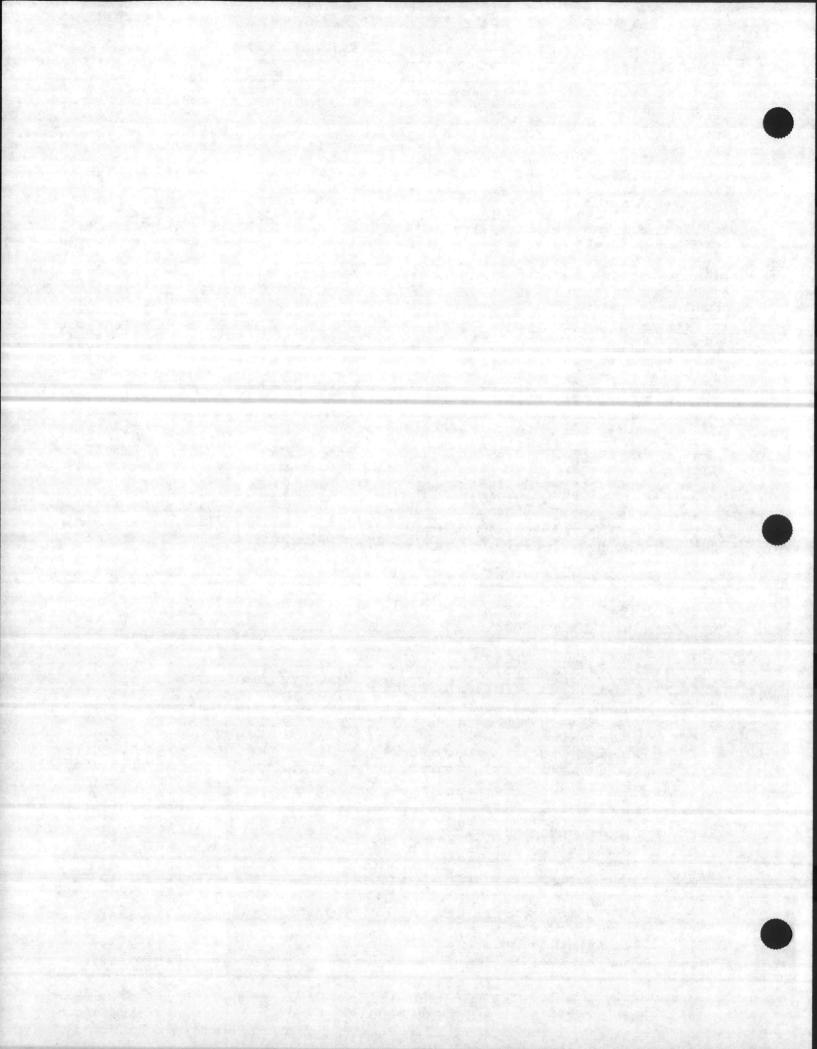
P.O. NO.: CTO # 19017

DATE SAMPLED: 04-FEB-93

DATE RECEIVED: 06-FEB-93

APPROVED BY: Joanne Simanic

LN	CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
		1,2-dimethylbenzene [o-xylene]	2	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	4	ug/L
		benzene	< 2	ug/L
		ethylbenzene	< 2	ug/L
		methylbenzene [toluene]	10	ug/L
5	G100W	PURGEABLE HALOCARBONS		
	0.00	1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1.1.2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/l
		1,2-dichloropropane	< 2	ug/l
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/l
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/l
		2-chloroethylvinyl ether	< 2	ug/l
		bromodichloromethane [dichlorobromomethane]	< 2	ug/l
		bromomethane [methyl bromide]	< 2	ug/l
		carbon tetrachloride	< 2	ug/l
		chlorobenzene	< 2	ug/l
		chloroethane	< 2	ug/l
		chloroform	< 2	ug/
		chloromethane [methyl chloride]	< 2	ug/
		cis-1,3-dichloropropene	< 2	ug/
		dibromochloromethane	< 2	ug/l
		dichlorodifluoromethane	< 2	ug/l
		dichloromethane [methylene chloride]	< 5	ug/l





5350 Campbells Run Road Pittsburgh, PA 15205 900 Gemini Avenue Houston, TX 77058

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### LABORATORY ANALYSIS REPORT

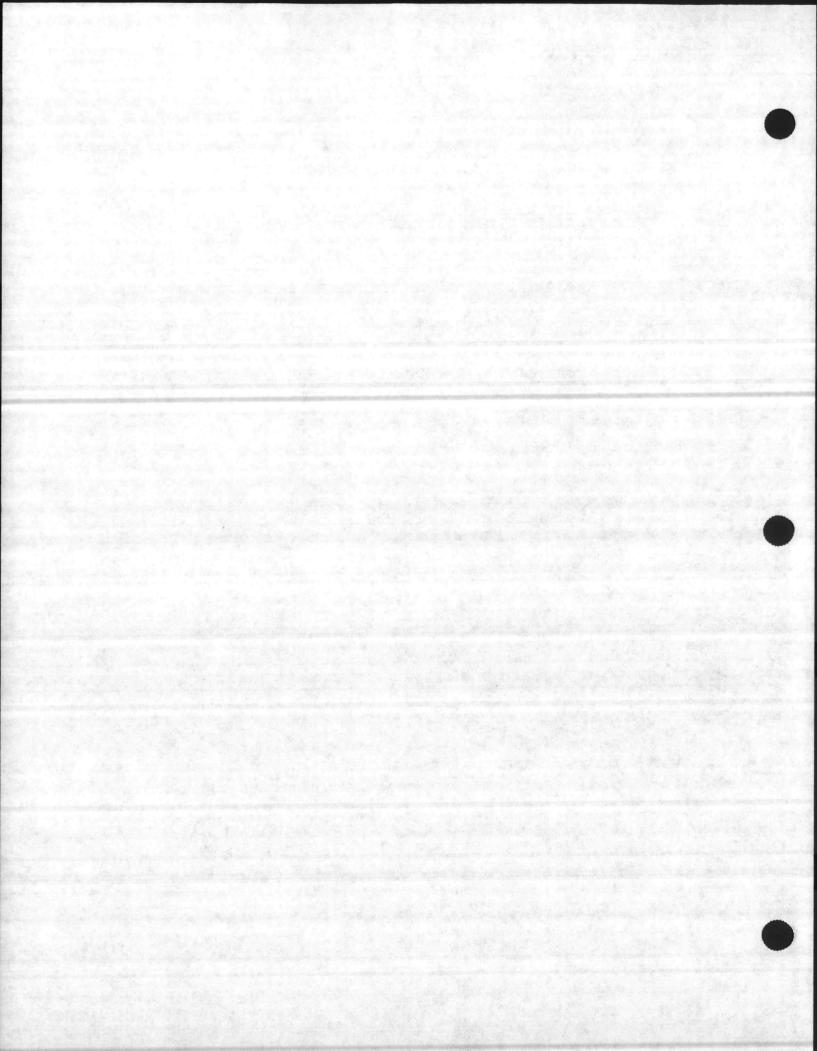
CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: 6-AS NUS SAMPLE NO: P0225123

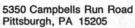
LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1.2-dichloroethene [trans-1.2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column.

The concentration reported represents the sum of the two isomers.



1600 0006



900 Gemini Avenue Houston, TX 77058



February 23, 1993 Report No.: 00013686 Section A Page 39

### LABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

420 ROUSER ROAD ADDRESS:

CORAOPOLIS, PA 15108-

MR. JOHN LOVELY ATTENTION:

Carbon Copy:

SAMPLE ID: 6-AC

NUS SAMPLE NO: P0225124

P.O. NO.: CTO # 19017

WORK ORDER NO: 55830

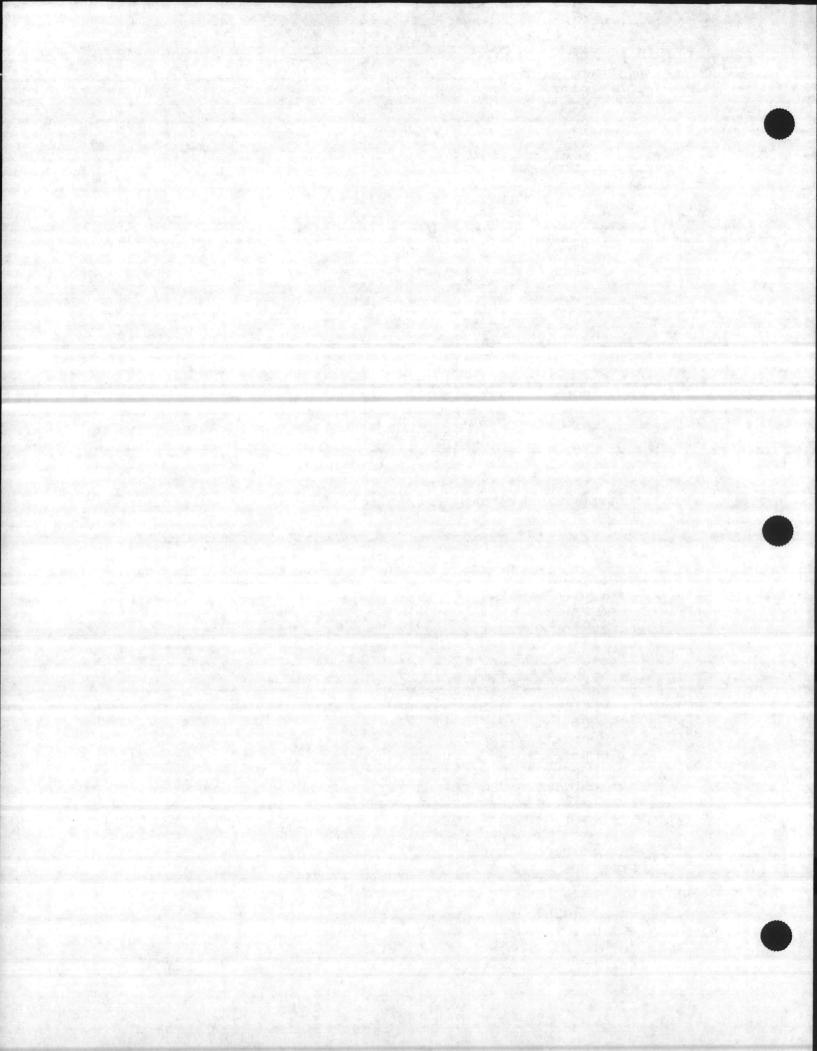
**VENDOR NO:** 

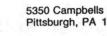
NUS CLIENT NO:

DATE SAMPLED: 04-FEB-93 DATE RECEIVED: 06-FEB-93

Joanne Simanic APPROVED BY:

LN	CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
		1,2-dimethylbenzene [o-xylene]	< 2	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	< 2	ug/L
		benzene	< 2	ug/L
		ethylbenzene	< 2	ug/L
		methylbenzene [toluene]	4	ug/L
5	G100W	PURGEABLE HALOCARBONS		
		1.1.1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1.1-dichloroethene [1.1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
a second		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L





5350 Campbells Run Road Pittsburgh, PA 15205

900 Gemini Avenue Houston, TX 77058



February 23, 1993 Report No.: 00013686 - Section A Page 40

#### LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

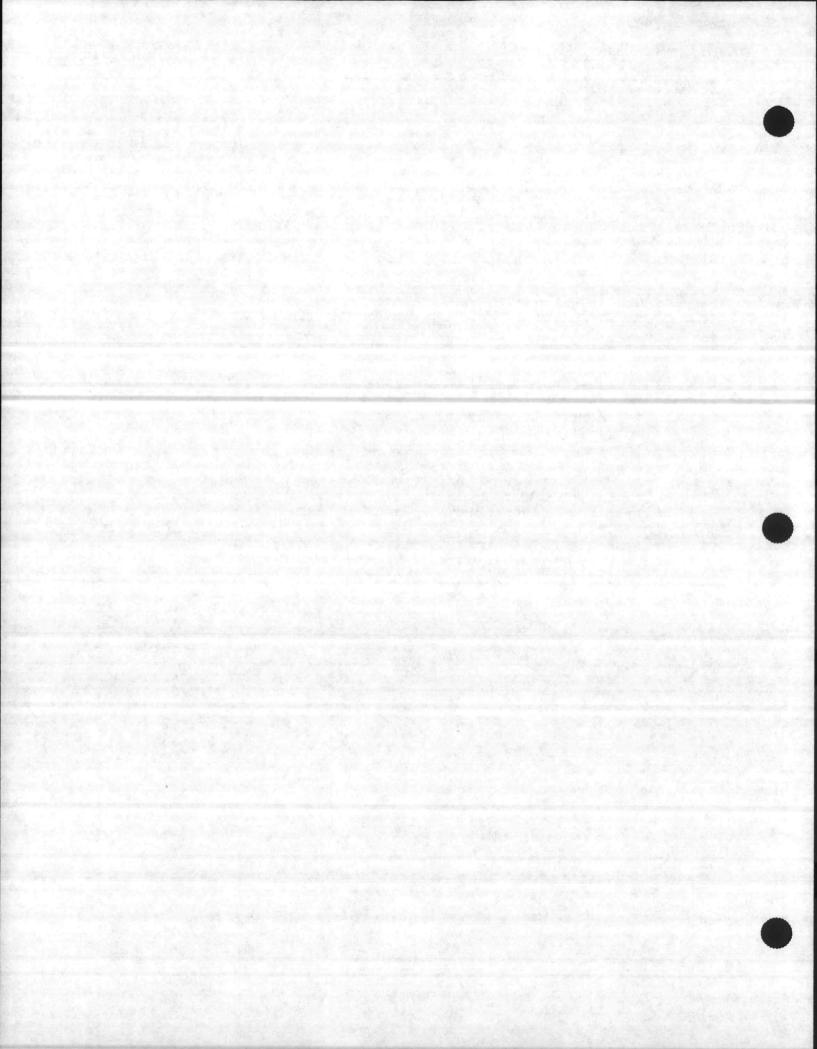
SAMPLE ID: 6-AC NUS SAMPLE NO: P0225124

 LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column.

The concentration reported represents the sum of the two isomers.

For sample number P225124, toluene was not observed in the confirmational analysis. The toluene result observed in the primary analysis was not reported.





February 23, 1993 Report No.: 00013686 Section A Page 41

NUS CLIENT NO: 1600 0006

CLIENT NAME: ADDRESS:

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: 5-OW

NUS SAMPLE NO: P0225125

P.O. NO.: CTO # 19017

04-FEB-93

55830

DATE SAMPLED: DATE RECEIVED:

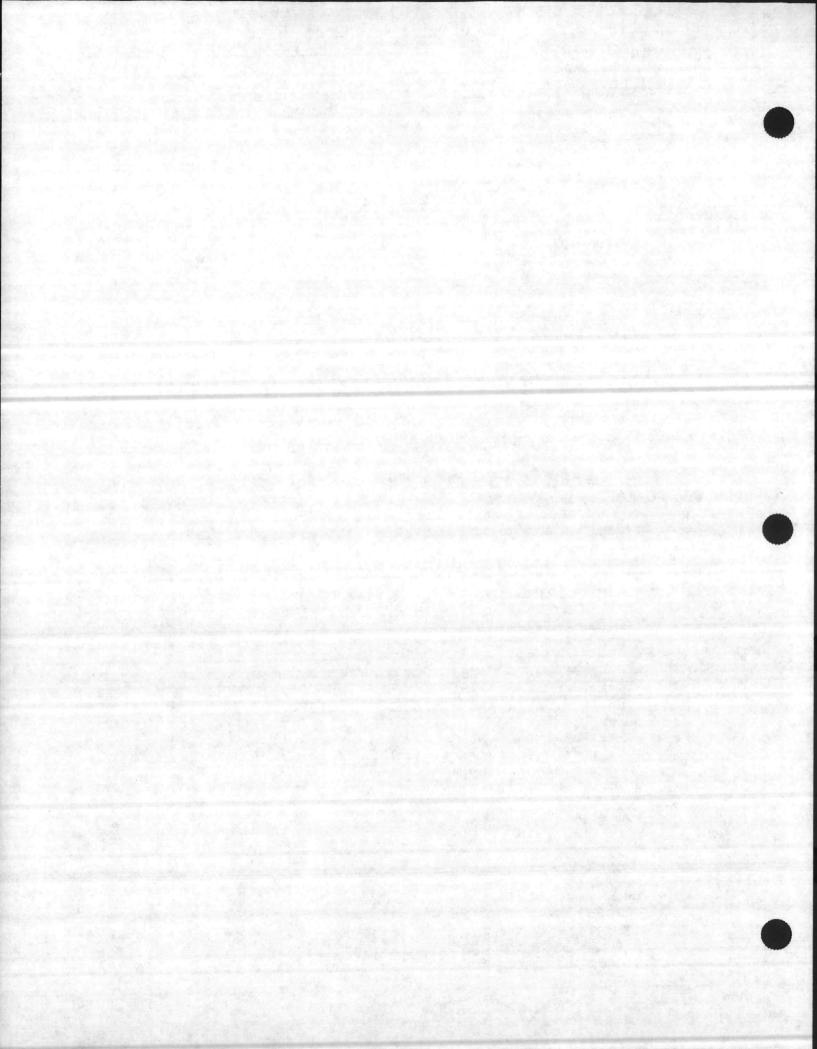
WORK ORDER NO:

**VENDOR NO:** 

06-FEB-93

APPROVED BY:

LN	TEST	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE	DOIL	
		1,2-dimethylbenzene [o-xylene]	< 2	ug/L
		1.3-dimethylbenzene, 1.4-dimethylbenzene [m-/p-xylenes]	< 2	ug/L
		benzene	3	ug/L
		ethylbenzene	< 2	ug/L
		methylbenzene [toluene]	6	ug/L
5	G100W	PURGEABLE HALOCARBONS		ug/ L
		1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	3	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	
		cis-1,3-dichloropropene	62	ug/L
		dibromochloromethane	< 2	-
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L





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### LABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

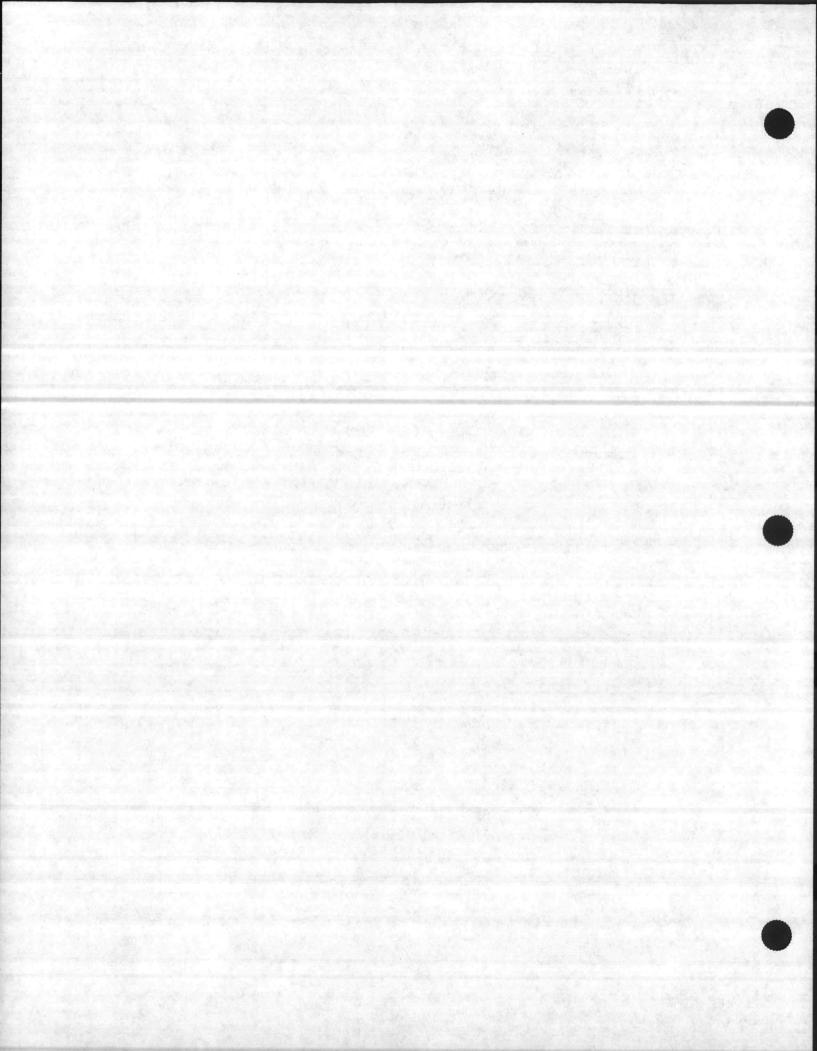
SAMPLE ID: 5-0W NUS SAMPLE NO: P0225125

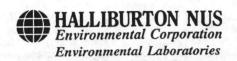
LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 40 D	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	180 D	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	350 D	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.

> Sample number P225125 exhibited high surrogate recoveries in both the primary and confirmational analyses. The high surrogate recoveries were due to a matrix interference. The matrix interference also interferred with the confirmation of benzene. The benzene result from the primary analysis is reported.

"D" indicates that the result was obtained from an analysis performed at a secondary dilution.





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NUS CLIENT NO: 1600 0006

55830

## LABORATORY ANALYSIS REPORT

CLIENT NAME: ADDRESS: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID:

5-AS P0225126

NUS SAMPLE NO: P.O. NO.: CTO # 19017

WORK ORDER NO:

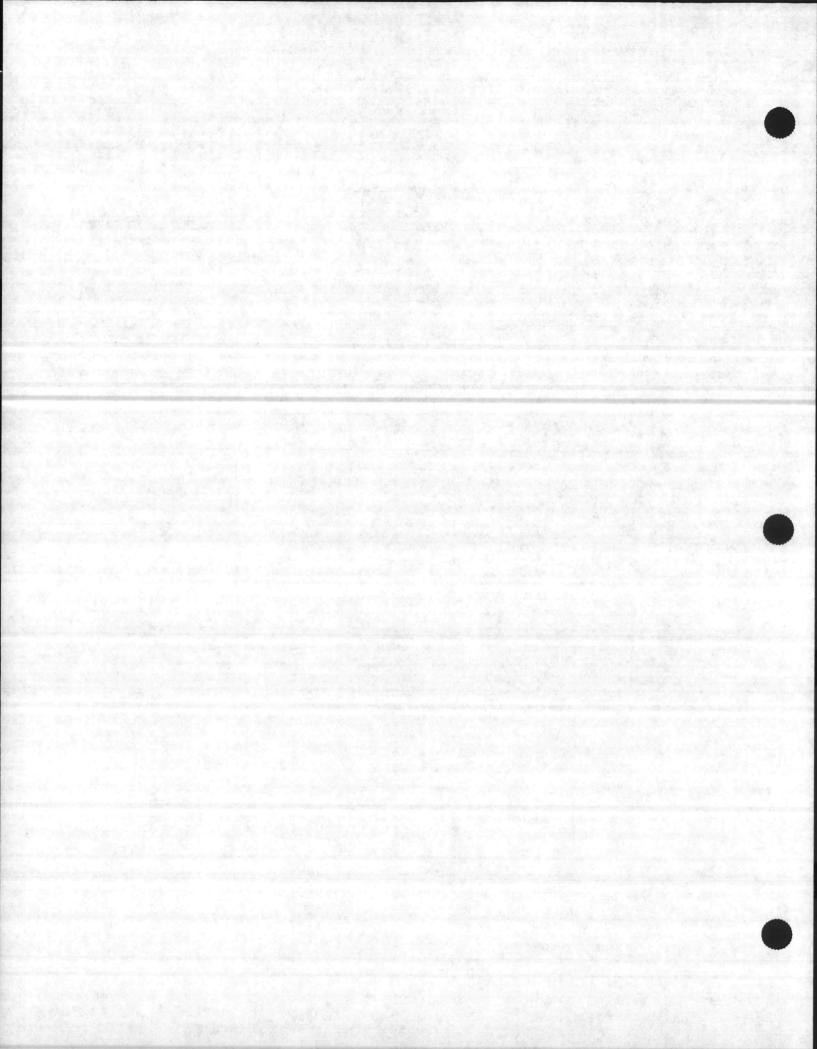
**VENDOR NO:** 

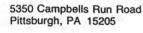
DATE SAMPLED: 04-FEB-93

DATE RECEIVED: 06-FEB-93

APPROVED BY:

	LN	TEST CODE	DETERMINATION	RESULT	UNITS
				DONE	
	1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
	2	DPACK	CLP Data Package Deliverable	DONE	
	3	G107W	BTEX PACKAGE		1100 /1
			1,2-dimethylbenzene [o-xylene]	< 2	ug/L
1			1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	5	ug/L
			benzene	< 2	ug/L
			ethylbenzene	2	ug/L
			methylbenzene [toluene]	10	ug/L
	5	G100W	PURGEABLE HALOCARBONS		
			1,1,1-trichloroethane	< 2	ug/L
			1,1,2,2-tetrachloroethane	< 2	ug/L
			1,1,2-trichloroethane	< 2	ug/L
			1,1-dichloroethane	< 2	ug/L
			1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
			1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
			1,2-dichloroethane	< 2	ug/L
			1,2-dichloropropane	< 2	ug/L
			1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
			1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
			2-chloroethylvinyl ether	< 2	ug/L
			bromodichloromethane [dichlorobromomethane]	< 2	ug/L
			bromomethane [methyl bromide]	< 2	ug/L
			carbon tetrachloride	< 2	ug/L
			chlorobenzene	< 2	ug/L
			chloroethane	< 2	ug/L
			chloroform	< 2	ug/L
			######################################	< 2	ug/L
			chloromethane [methyl chloride]	< 2	ug/L
			cis-1,3-dichloropropene	< 2	ug/L
100			dibromochloromethane	< 2	ug/L
A section			dichlorodifluoromethane dichloromethane [methylene chloride]	< 5	ug/l







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## LABORATORY ANALYSIS REPORT

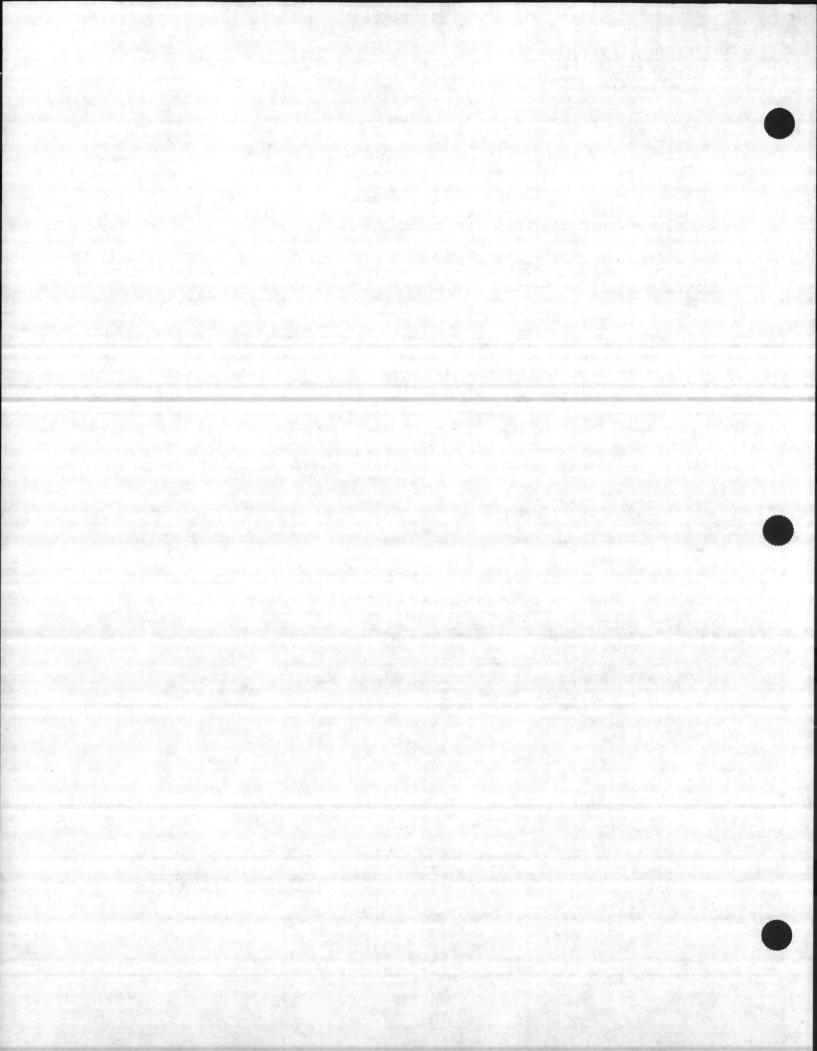
CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: 5-AS NUS SAMPLE NO: P0225126

LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

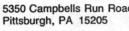
COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column.

The concentration reported represents the sum of the two isomers.



1600 0006

55830



5350 Campbells Run Road

900 Gemini Avenue Houston, TX 77058



February 23, 1993 Report No .: 00013686 Section A Page 45

NUS CLIENT NO:

WORK ORDER NO:

VENDOR NO:

# LABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

MR. JOHN LOVELY ATTENTION:

Carbon Copy:

SAMPLE ID: 5-AC

NUS SAMPLE NO: P0225127

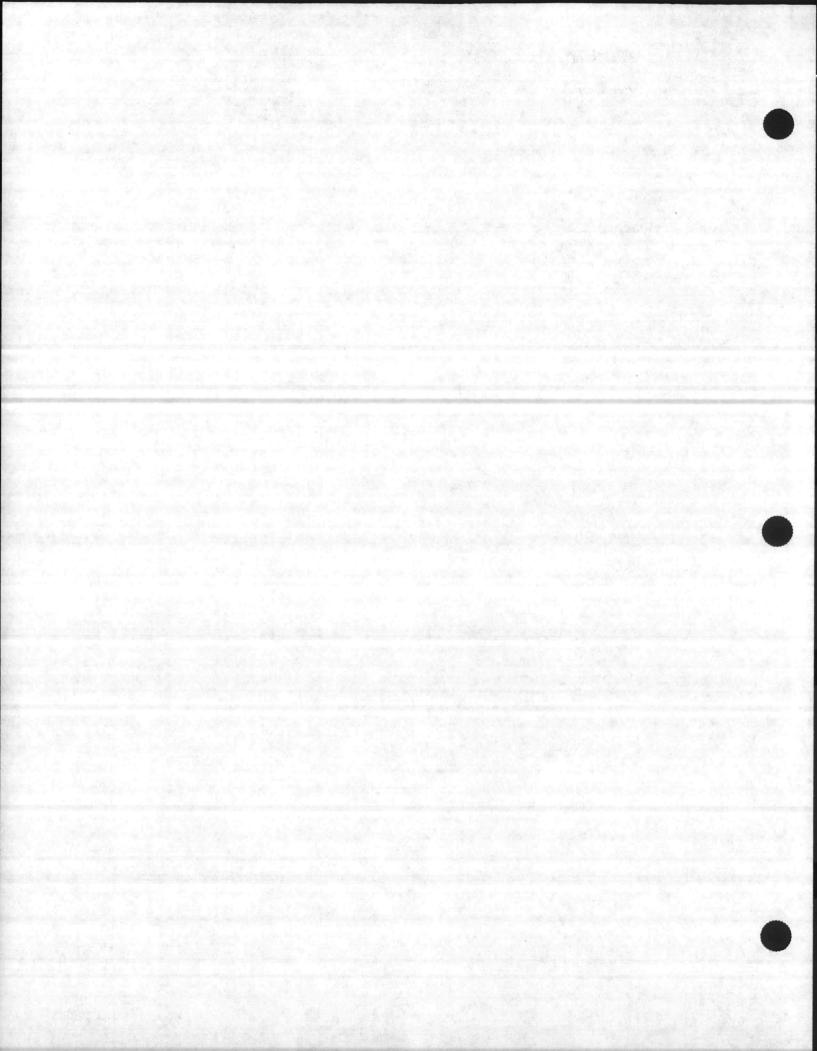
P.O. NO .: CTO # 19017

DATE SAMPLED: 04-FEB-93

06-FEB-93 DATE RECEIVED:

Joanne Simanic APPROVED BY:

LN	CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
3	010/11	1,2-dimethylbenzene [o-xylene]	< 2	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	< 2	ug/L
		benzene	< 2	ug/L
		ethylbenzene	< 2	ug/L
		methylbenzene [toluene]	3	ug/L
5	G100W	PURGEABLE HALOCARBONS		
7	Oloon	1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/l
		carbon tetrachloride	< 2	ug/l
		chlorobenzene	< 2	ug/l
		chloroethane	< 2	ug/l
		chloroform	< 2	ug/l
		chloromethane [methyl chloride]	< 2	ug/l
		cis-1,3-dichloropropene	< 2	ug/l
		dibromochloromethane	< 2	ug/l
		dichlorodifluoromethane	< 2	ug/l
		dichloromethane [methylene chloride]	< 5	ug/l





5350 Campbells Run Road Pittsburgh, PA 15205

900 Gemini Avenue Houston, TX 77058

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# LABORATORY ANALYSIS REPORT

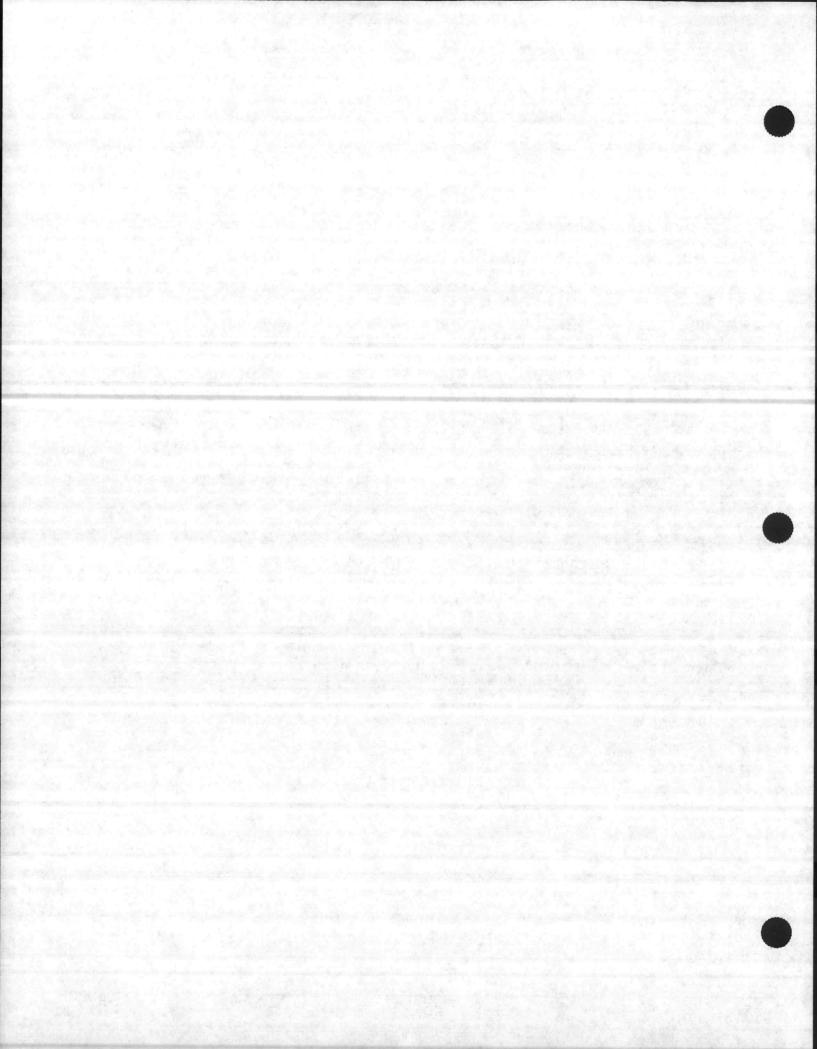
BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: 5-AC NUS SAMPLE NO: P0225127

LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1.2-dichloroethene [trans-1.2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.

> For sample number P225127, toluene was not observed in the confirmational analysis. The toluene result observed in the primary analysis was not reported.





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# ABORATORY ANALYSIS REPORT

CLIENT NAME:

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS:

420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

NUS CLIENT NO: 1600 0006

WORK ORDER NO:

55830

VENDOR NO:

Carbon Copy:

SAMPLE ID:

4-0W

P0225128

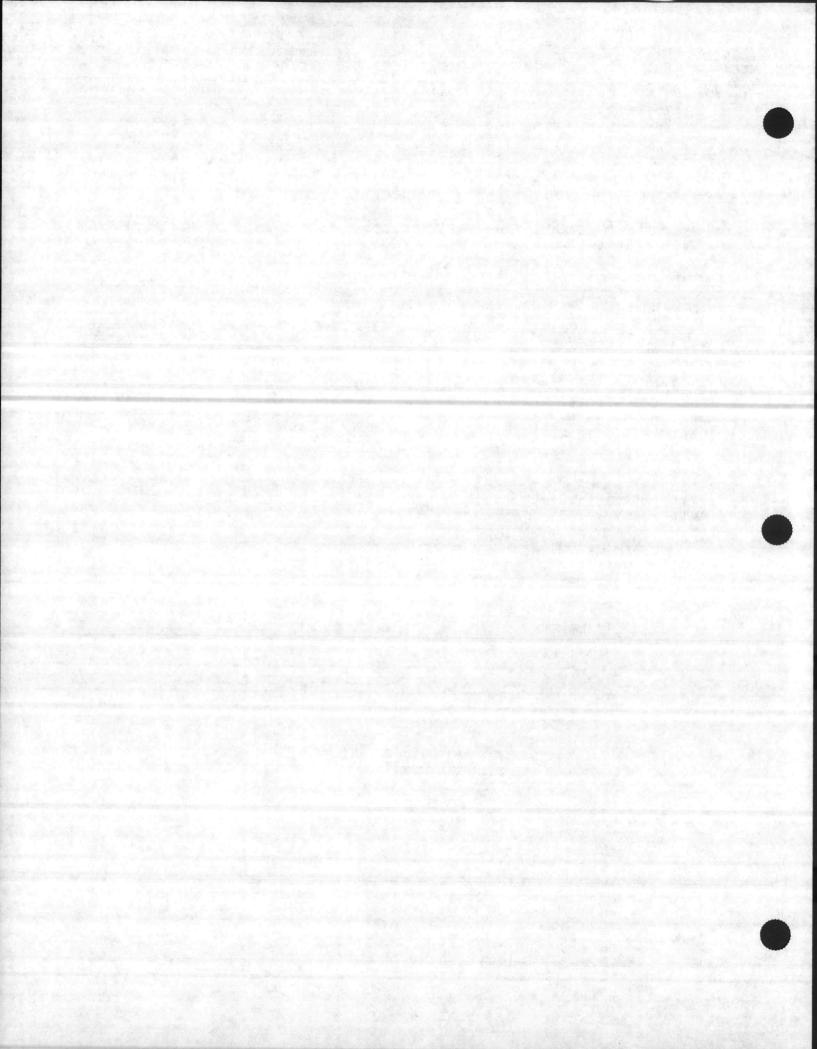
NUS SAMPLE NO: CTO # 19017 P.O. NO .:

DATE SAMPLED: 03-FEB-93

DATE RECEIVED: 06-FEB-93

APPROVED BY:

LN	CODE	DETERMINATION	RESULT	UNITS
	ACI DII	TAL METALS & CLP DATA PACKAGE	DONE	
1	ACLPW DPACK	CLP Data Package Deliverable	DONE	
2	G107W	BTEX PACKAGE		
3	GIU/W	1,2-dimethylbenzene [o-xylene]	2	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	< 2	ug/L
		benzene	3	ug/L
		ethylbenzene	< 2	ug/L
		methylbenzene [toluene]	5	ug/L
	G100W	PURGEABLE HALOCARBONS		
5	GIOOM	1.1.1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1.1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1.2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L



5350 Campbells Run Road

900 Gemini Avenue Houston, TX 77058



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# LABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: 4-OW NUS SAMPLE NO: P0225128

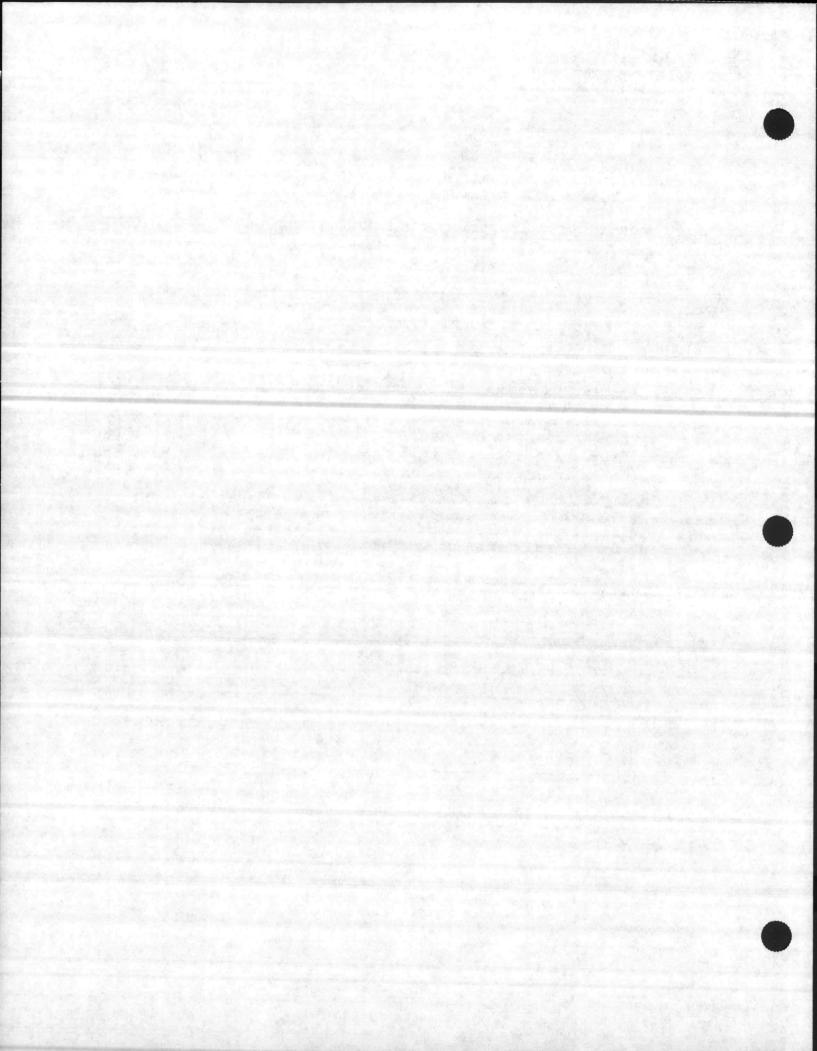
LN CODE	DETERMINATION	RESULT	UNITS
	tetrachloroethene [tetrachloroethylene]	< 2	ug/L
	trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 40 D	ug/L
	trans-1,3-dichloropropene	< 2	ug/L
	tribromomethane [bromoform]	< 5	ug/L
	trichloroethene [trichloroethylene]	190 D	ug/L
	trichlorofluoromethane	< 2	ug/L
	vinyl chloride	330 D	ug/L

COMMENTS:

In the BTEX analysis, m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.

Sample number P225128 exhibited high surrogate recoveries in both the primary and confirmational analyses. The high surrogate recoveries were due to a matrix interference. The matrix interference also interferred with the confirmation of benzene. The benzene result from the primary analysis is reported.

"D" indicates that the result was obtained from an analysis performed at a secondary dilution.



5350 Campbells Run Road

900 Gemini Avenue Houston, TX 77058



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# LABORATORY ANALYSIS REPORT

NUS CLIENT NO: 1600 0006 BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

WORK ORDER NO: 55830 ADDRESS: 420 ROUSER ROAD

**VENDOR NO:** CORAOPOLIS, PA 15108-

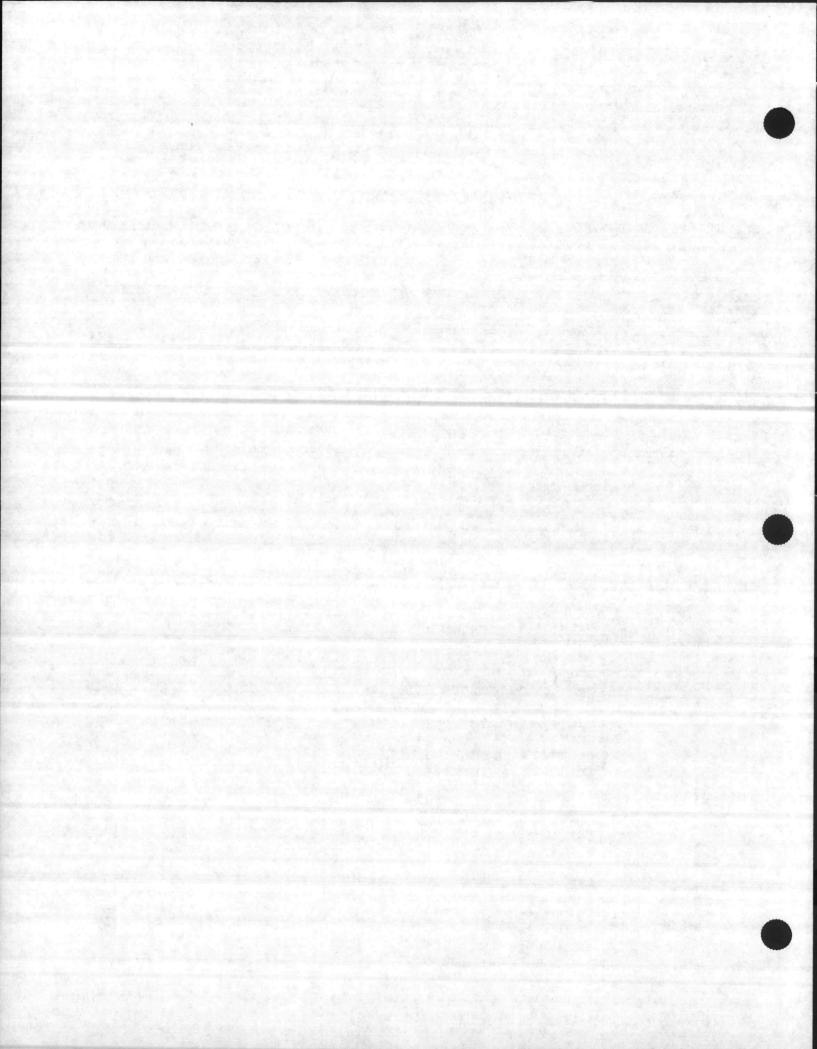
MR. JOHN LOVELY ATTENTION:

Carbon Copy:

03-FEB-93 DATE SAMPLED: SAMPLE ID: 4-AS DATE RECEIVED: 06-FEB-93 NUS SAMPLE NO: P0225129

Joanne Simanic APPROVED BY: P.O. NO .: CTO # 19017

LN	CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
	A BESTELLA	1,2-dimethylbenzene [o-xylene]	2	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	4	ug/L
		benzene	< 2	ug/L
		ethylbenzene	< 2	ug/L
		methylbenzene [toluene]	8	ug/L
5	G100W	PURGEABLE HALOCARBONS		
		1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L





5350 Campbells Run Road Pittsburgh, PA 15205 900 Gemini Avenue Houston, TX 77058

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# LABORATORY ANALYSIS REPORT

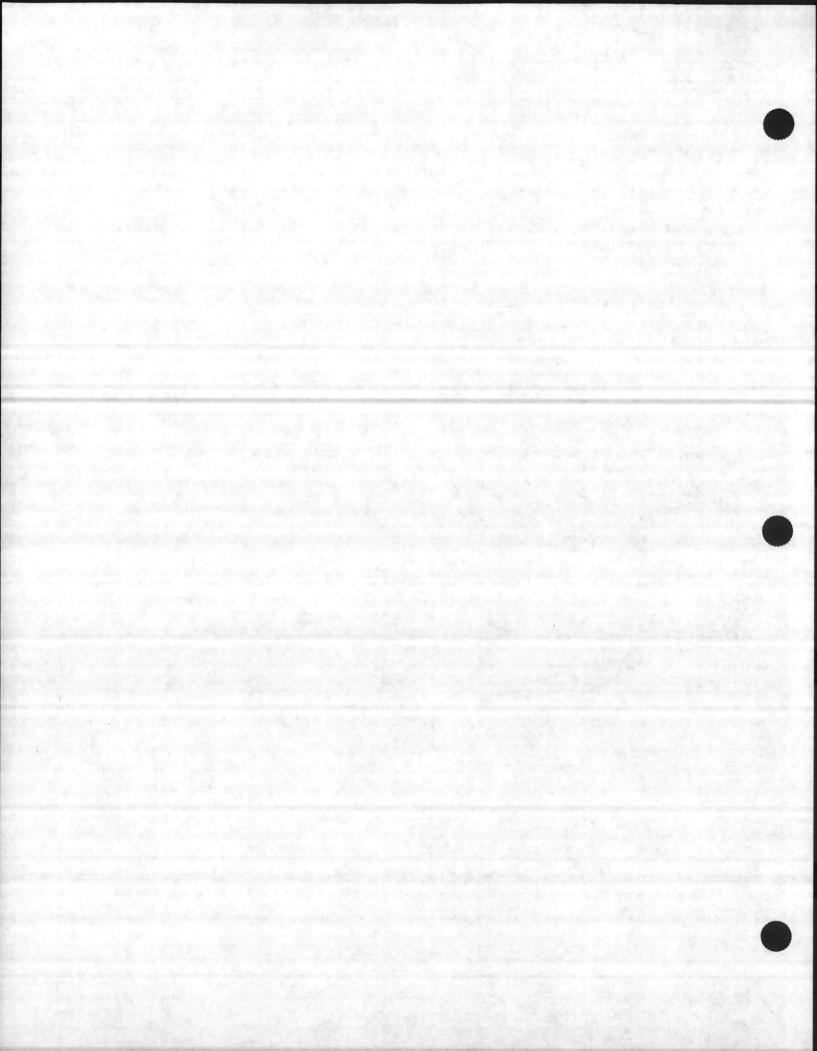
CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: 4-AS NUS SAMPLE NO: P0225129

LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column.

The concentration reported represents the sum of the two isomers.



900 Gemini Avenue Houston, TX 77058



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# LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: 4-AC

NUS SAMPLE NO: P0225130

P.O. NO.: CTO # 19017

NUS CLIENT NO: 1600 0006

WORK ORDER NO: 55830

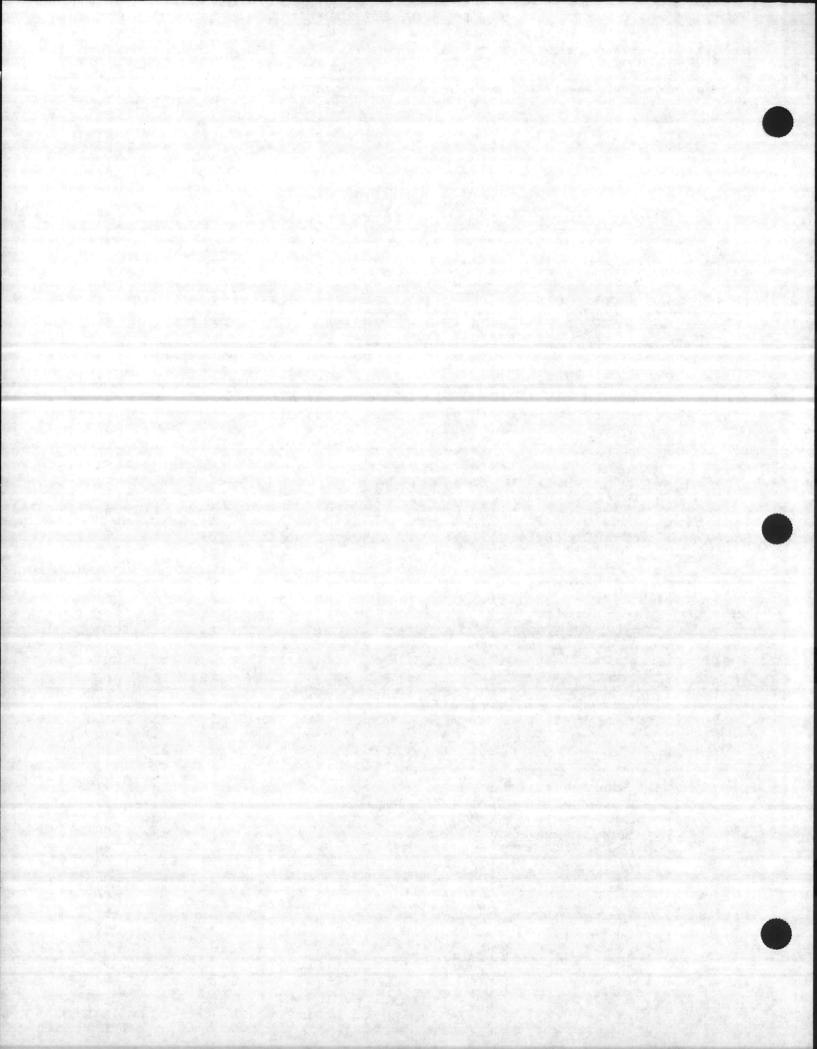
VENDOR NO:

DATE SAMPLED: 03-FEB-93
DATE RECEIVED: 06-FEB-93

APPROVED BY:

Joanne Simanic

LN	CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
		1,2-dimethylbenzene [o-xylene]	< 2	ug/L
4 5		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	< 2	ug/L
		benzene	< 2	ug/L
		ethylbenzene	< 2	ug/L
		methylbenzene [toluene]	< 2	ug/L
5	G100W	PURGEABLE HALOCARBONS		
		1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1.1-dichloroethene [1.1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L



900 Gemini Avenue Houston, TX 77058



February 23, 1993 Report No.: 00013686 Section A Page 52

# LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

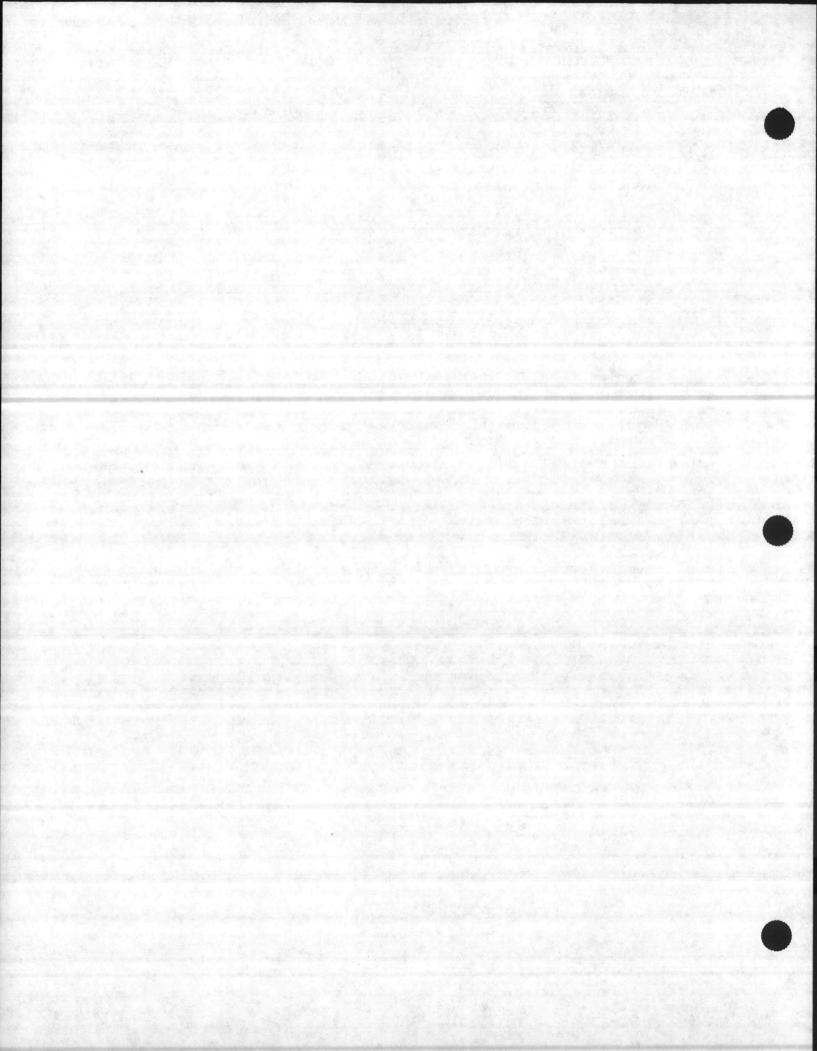
SAMPLE ID: 4-AC NUS SAMPLE NO: P0225130

LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

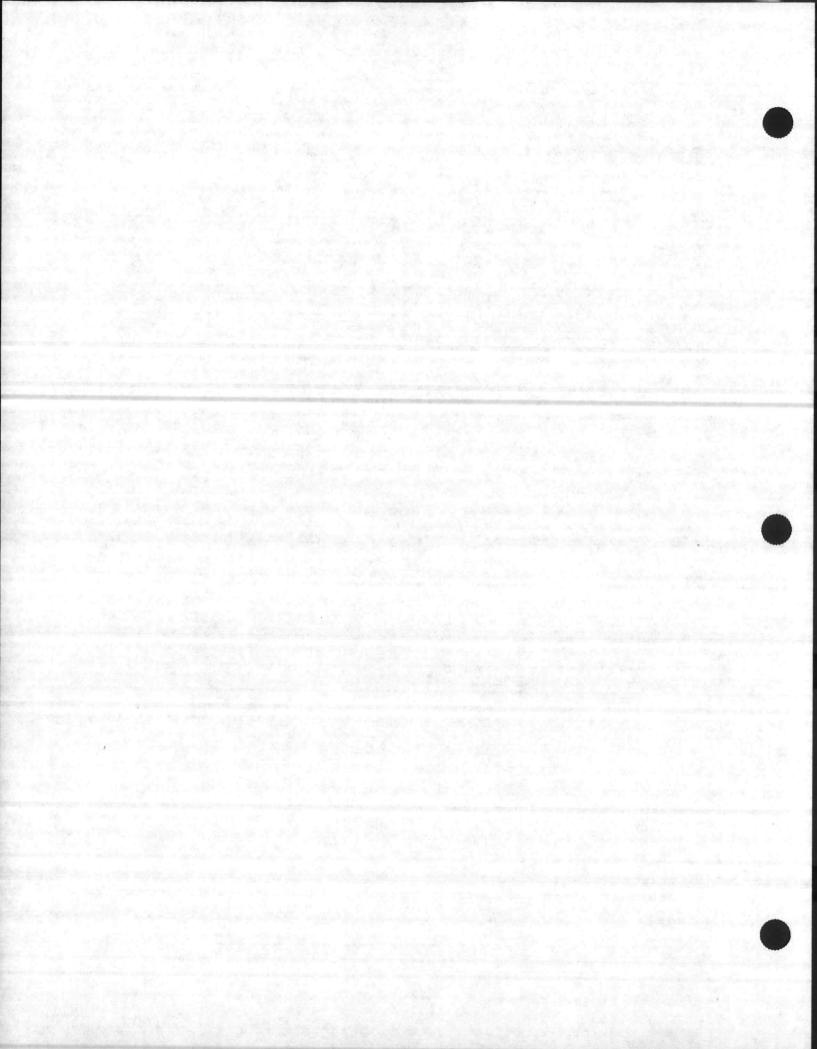
COMMENTS:

In the BTEX analysis, m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.

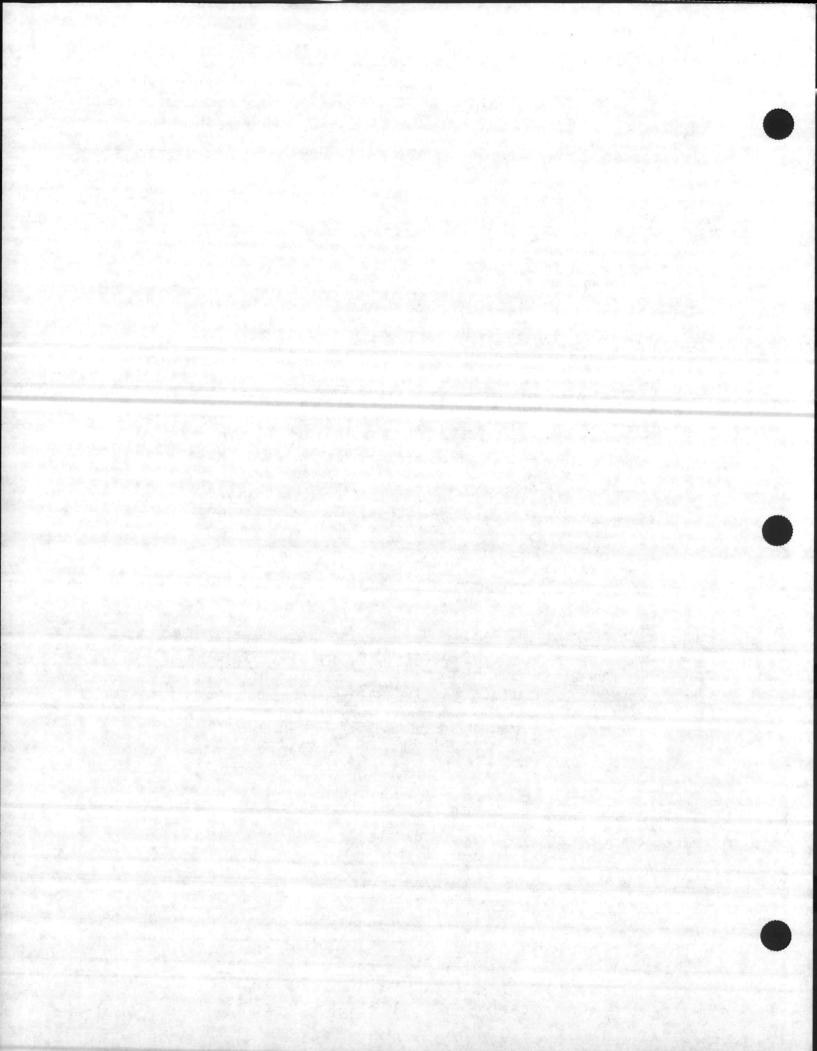
For sample number P225130, toluene was not observed in the confirmational analysis. The toluene result observed in the primary analysis was not reported.



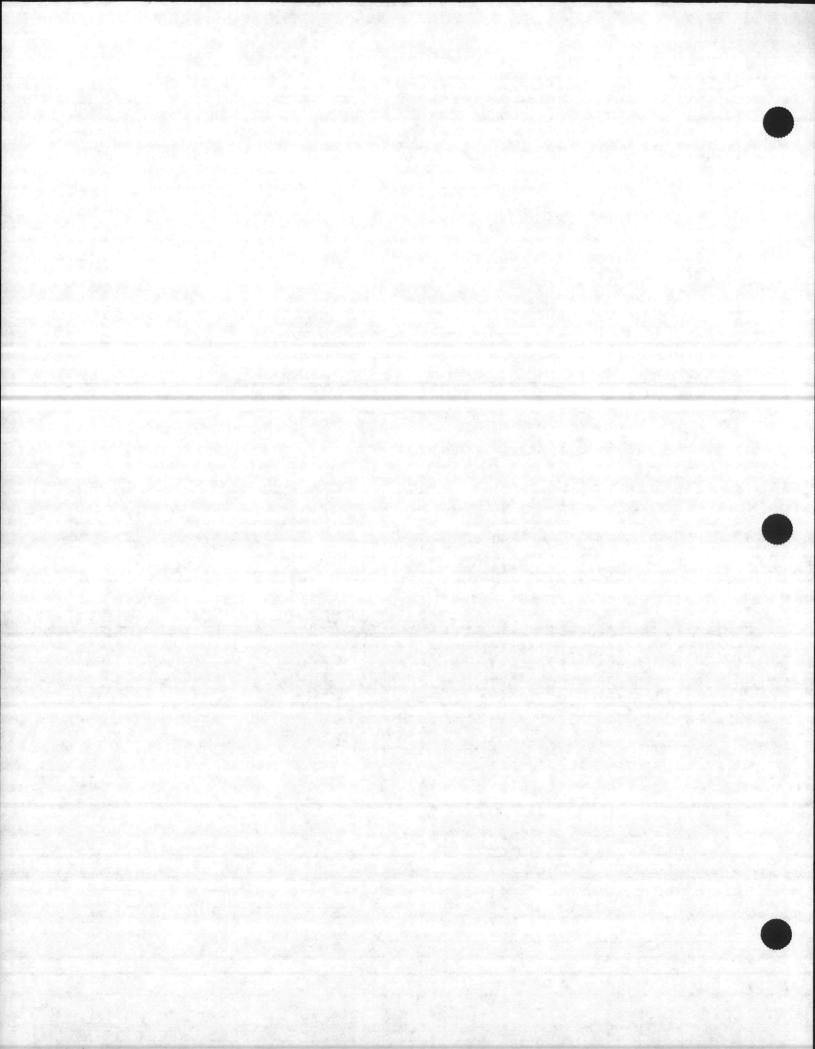
		IALYSES DATA S		
				1-AC
IBURTON_NUS		Contract:		
Ca	se No.: BKHI	SAS No.:		_ SDG No.: PKG2_
ater): WATE	₹		Lab Sa	mple ID: P225107_
): LOW_			Date R	deceived: 02/02/93
0.	0			
ncentration	Units (ug/l	. or mg/kg dry	weigh	it): UG/L_
1	1	PROPERTY AND AND ASSESSMENT OF THE PROPERTY OF	and show on	
ICAS No.	! Analyte !	Concentration!	CI Q	IM I
17420-00-5	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	7620!		-iPi
17447-70-3	!Antimony	24.51	B:	IF I
17440-30-0	!Areanic !	13.7!		IF I
17440-30-2	! Banium !	110!	B!	IP I
17440-31-3	!Barvllium!	1.0!	B!	IP I
17440-43-9	!Cadmium !	5.01	U!	IP I
17440-70-7	!Calcium !	159001		IP I
17440-47-3	!Chromium !	-19.01		IP I
17440-48-4	!Cohalt !	8.01	UI	IP I
17440-50-8	Copper	1201	1	IP_I
17439-89-6	Iron I	172001		IP_I
17439-92-1	Lead	13.4		[F_1
17439-95-4	Magnesium	5080		!P_!
17439-96-5	! Manganese!	1911		(P_(
17439-97-6	!Mercury !	0.208	:U!	(CV!
17440-02-0	Nickel	28.01	_ _	IP_I
17440-09-7	!Potassium!	4550	B!	!P_!
17782-49-2	Selenium_!	1.2	BI_W	1F_1
17440-22-4	Silver	3.0	:U:	!P_!
17440-23-5	Sodium_	234001	1_1	IP_I
17440-28-0	{Thallium !	1.0	:U!	!F_!
17440-62-2	!Vanadium_!	17.0	B!	(P_1
17440-66-6	IZinc!	136	1_1	P_
BLACK	Clarit	y Before: OPAC	QUE	Texture:
COLORLESS	Clarit	y After: CLE	AR_	Artifacts:
	Casater): WATER  ater): WATER  : LOW			Date F



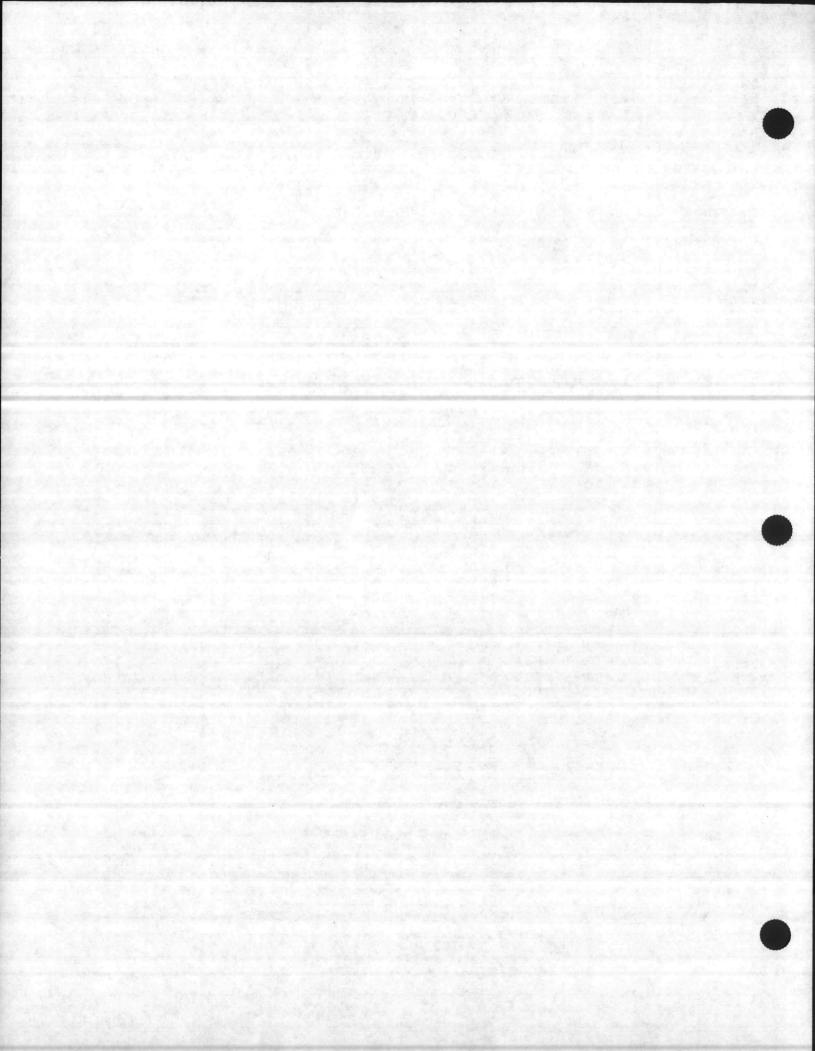
ab Name: HALLIBURTON_NUS Contract:	ab Name: HALLIBURTON_NUS				1 NALYSES DATA SHEET	
Code: HNUS_	Description   Case No.: BKHD   SAS No.: Sp6 No.: PKG   Sample ID: P225106   Sample ID: P225106   Sample ID: P225106   Solids:					1-AS
Low	Lab Sample ID: P225106  // (low/med): LOW	Name: HALL	IBURTON_NUS		Contract:	_ !
Date Received: 02/02/93   Concentration Units (ug/L or mg/kg dry weight): UG/L_	Date Received: 02/02/9   Concentration Units (ug/L or mg/kg dry weight): UG/L_   CAS No.   Analyte   Concentration   C   Q   M     7429-90-5   Aluminum   886!   P-     7440-36-0   Antimony   10.0!U   F-     7440-38-2   Arsenic   15.4!   F-     7440-41-7   Beryllium   71.0!B    P-     7440-41-7   Beryllium   5.0!U   P-     7440-43-9   Cadmium   5.0!U   P-     7440-47-3   Chromium   10.0!U   P-     7440-48-4   Cobalt   8.0!U   P-     7440-48-6   Copalt   8.0!U   P-     7439-89-6   Iron   39000   P-     7439-95-1   Lead   80.5    F-     7439-95-5   Manganese   199   P-     7439-97-6   Mercury   0.20!U   CV     7440-02-0   Nickel   23.0    P-     7440-22-4   Selenium   1440 B   P-     7740-22-5   Sodium   1440 B   P-     7740-22-6   Thallium   1.0!U   P-     7440-22-1   Vanadium   4.0!U   P-     7440-66-6   Zinc   289   P-     7440-66-6   Zinc   289   P-     17440-66-6   Zinc   289   P-     17440-66-6   Zinc   289   P-     17440-66-6   Zinc   289   P-     17440-66-6   Zinc   289   P-     100   Before: CLEAR   Texture:	Code: HNUS	Ca	se No.: BKH	ID SAS No.:	SDG No.: PKG2_
Concentration Units (ug/L or mg/kg dry weight): UG/L    CAS No.	Concentration Units (ug/L or mg/kg dry weight): UG/L_    CAS No.   Analyte   Concentration   C  Q   M	trix (soil/w	ater): WATE	R	Lab San	nple ID: P225106
CAS No.   Analyte   Concentration   C   Q   M	Concentration Units (ug/L or mg/kg dry weight): UG/L_    CAS No.   Analyte   Concentration   C    Q   M     7429-90-5   Aluminum	vel (low/med	): LOW_		Date Re	eceived: 02/02/93
CAS No.   Analyte   Concentration   C    Q   M	CAS No.   Analyte   Concentration   C   Q   M	Solids:	_0.	0		
CAS No.   Analyte   Concentration   C   Q   M	CAS No.   Analyte   Concentration   C    Q   M	Co	ncentration	Units (ug/	'L or mg/kg dry weigh	t): UG/L_
7429-90-5   Aluminum	7429-90-5   Aluminum		1 5 5 6	1	24.3 K 2 m 1 1 1	<u> </u>
7449-90-5   Aluminum	7440-36-0   Antimony		ICAS No.	! Analyte !	Concentration C  Q	
17440-36-0   Antimony	17440-36-0   Antimony   10.0 U   F   17440-38-2   Arsenic   15.4      F   17440-39-3   Barium   71.0 B    F   17440-41-7   Beryllium   1.0 U   F   17440-43-9   Cadmium   5.0 U   F   17440-47-3   Chromium   10.0 U   F   17440-47-3   Chromium   10.0 U   F   17440-48-4   Cobalt   8.0 U   F   17439-89-6   Iron   39000    F   17439-89-6   Iron   39000    F   17439-95-4   Magnesium   4520 B   F   17439-95-4   Magnesium   4520 B   F   17439-97-6   Mercury   0.20 U   CV   17440-02-0   Nickel   23.0    F   17440-02-0   Nickel   23.0    F   17440-02-4   Silver   3.0 U   F   17440-23-5   Sodium   1440 B   F   17440-23-5   Sodium   14400    F   17440-28-0   Thallium   1.0 U   F   17440-66-6   Zinc   289    Zinc   Zi		17479-90-5	: Aluminum	00011	
17440-38-2   Arsenic			17440-36-0	:Antimony	10.0101	iFi
7440-41-7   Beryllium	17440-41-7   Beryllium		17440-38-2	!Arsenic	15.41	IF_I
7440-41-7   Beryllium	1.0		17440-30-2	!Barium	71.0 B	!P!
	17440-43-9   Cadmium		17440-37-3	! Banvillium!	1.0101	IP I
7440-70-2   Calcium	7440-70-2   Calcium		17440-41-7	Cadaina	5.0111	IP I
	7440-47-3   Chromium		17440-43-9	Cadmium_	13800!!	IP I
7440-48-4   Cobalt	7440-48-4   Cobalt		17440-70-2	:Calcium_	10.0111	TIP I
17440-50-8   Copper	17440-50-8   Copper		17440-47-3	[Chromium_	10.0101	
7437-87-6   Troll	7439-92-1   Lead		17440-48-4	(Cobalt	8.0101	
7437-87-6   Troll	7439-92-1   Lead		17440-50-8	Copper	45.01_1	—; <u>[-</u> ;
7439-95-4	7439-95-4   Magnesium		1/437-07-0	TLOU		
	7439-96-5   Manganese   1991   1901		17439-92-1	Lead	80.51	
			17439-95-4	! Magnesium	4520 B:	!!
7440-02-0   Nickel	7440-02-0   Nickel		17439-96-5	: Manganese	:199;_i	
			17439-97-6	!Mercury	0.20101	
			17440-02-0	!Nickel	23.01	iFi
			17440-09-7	Potassium	!1440 B	!P_!
			17782-49-2	Selenium	1.0:0:	
			17/1/0-22-/	ICITYON	. 3.0(U)	ir i
			17440-23-5	Sodium	144001_1	iP_i
			17440-28-0	!Thallium	1.0:0:	iFi
7440-66-6   Zinc   289   _     P _	7440-66-6   Zinc     289   _     P_		17440-62-2	!Vanadium_	14.0!U!	IP_I
olor Before: COLORLESS Clarity Before: CLEAR_ Texture:	olor Before: COLORLESS Clarity Before: CLEAR_ Texture: _		17440-66-6	:Zinc	12891_1	IP_I
l			A SECTION AND ASSESSMENT			
			1	1		
olor After: COLORLESS Clarity After: CLEAR_ Artifacts:	olor After: COLORLESS Clarity After: CLEAR_ Artifacts: _	olor Before:	COLORLESS	Clari	ty Before: CLEAR_	Texture:
		olor After:	COLORLESS	Clari	ty After: CLEAR_	Artifacts:
omments:	omments:	omments:				



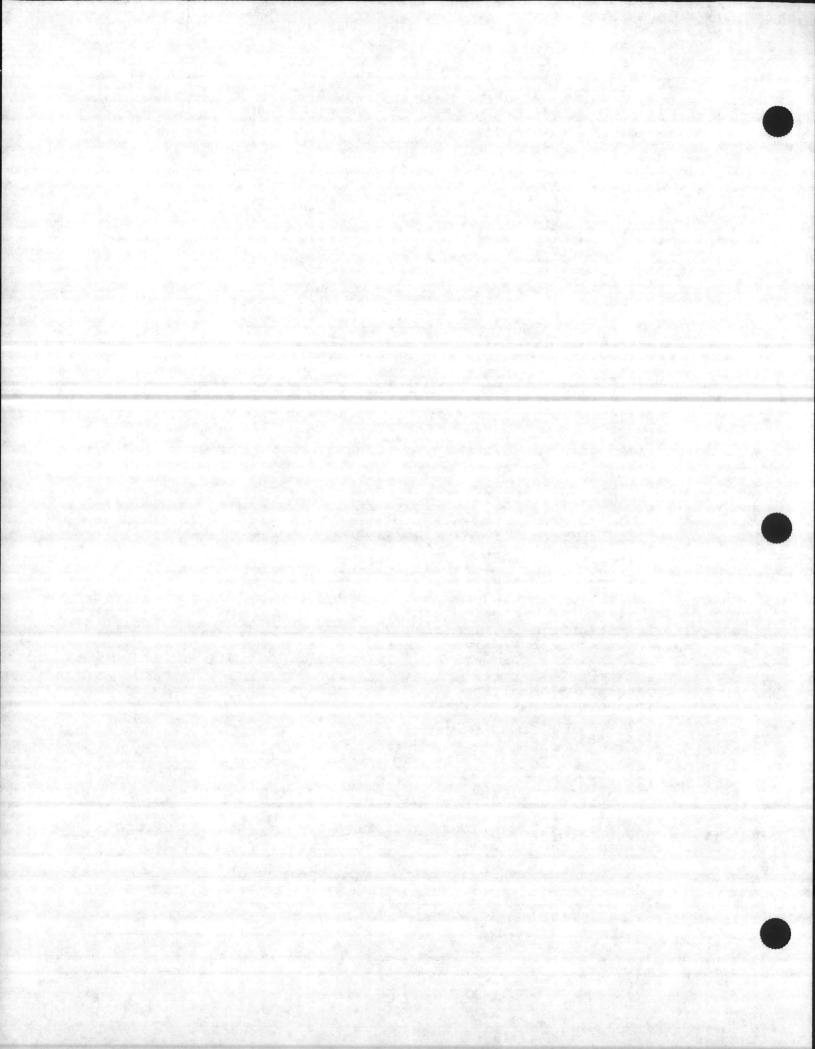
			INORGANIC A	ANALYSES DATA SHEET	1
	1101.1	IDUDION NUC		Contract:	1-0W
o Co	de: HNUS	Ca	se No.: BKH	HD SAS No.:	SDG No.: PKG2
trix	(soil/w	ater): WATE	R	Lab Sam	ple ID: P225105_
vel	(low/med	): LOW_		Date Re	eceived: 02/02/93
Soli	ds:	_0.	0		
	Co	ncentration	Units (ug/	/L or mg/kg dry weight	:): UG/L_
					<del></del>
		ICAS No.	! Analyte	Concentration C  Q	IM I
· 4 E		17429-90-5	Aluminum	3441_1	IP_I
		17440-36-0	Antimony	10.0 U	_IF_I
		17440-38-2	Arsenic	2.0101	_IF_I
		17440-39-3	Barium	77.01B1	IP_1
		17440-41-7	Bervllium	1.0 B	(P_1
		17440-43-9	Cadmium	5.0101	IP_1
		17440-70-2	:Calcium	112001_1	IP_I
		17440-47-3	!Chromium	10.0 U	iP_i
1		17440-48-4	Cobalt	8.0101	IP_I
		17440-50-8	Copper	9.01B1	_IP_I
19,		17439-89-6	Iron	86101_1	IP_I
		17439-92-1	!Lead	52.01_1	IF_I
		17439-95-4	Magnesium	2810   B	IP_I
		17439-96-5	! Manganese	56.01_1	!F_!
		17439-97-6	Mercury	0.20101	ICVI
		17440-02-0	Nickel	20,0 U	IP_I
		17440-09-7	!Potassium	1290(B)	IP_I
		17782-49-2	Selenium	1.0101	IF_I
		17440-22-4	Silver	13.0IUI	IP_I
		17440-23-5	:Sodium	13500   1	IP_I
		17440-28-0	:Thallium	1.0:0:	
		17440-62-2	!Vanadium	4.0101	!P_!
				185 _	{P_{
				1	11
		1	!	tt_1_t	_'_'
olor	Before:	COLORLESS	Clari	ty Before: CLEAR_	Texture:
olor	After:	COLORLESS	Clari	ty After: CLEAR_	Artifacts:
ommen	ts:				
Color Commen ——		COLORLESS	Clari	ty After: CLEAR_	Hrtifacts.



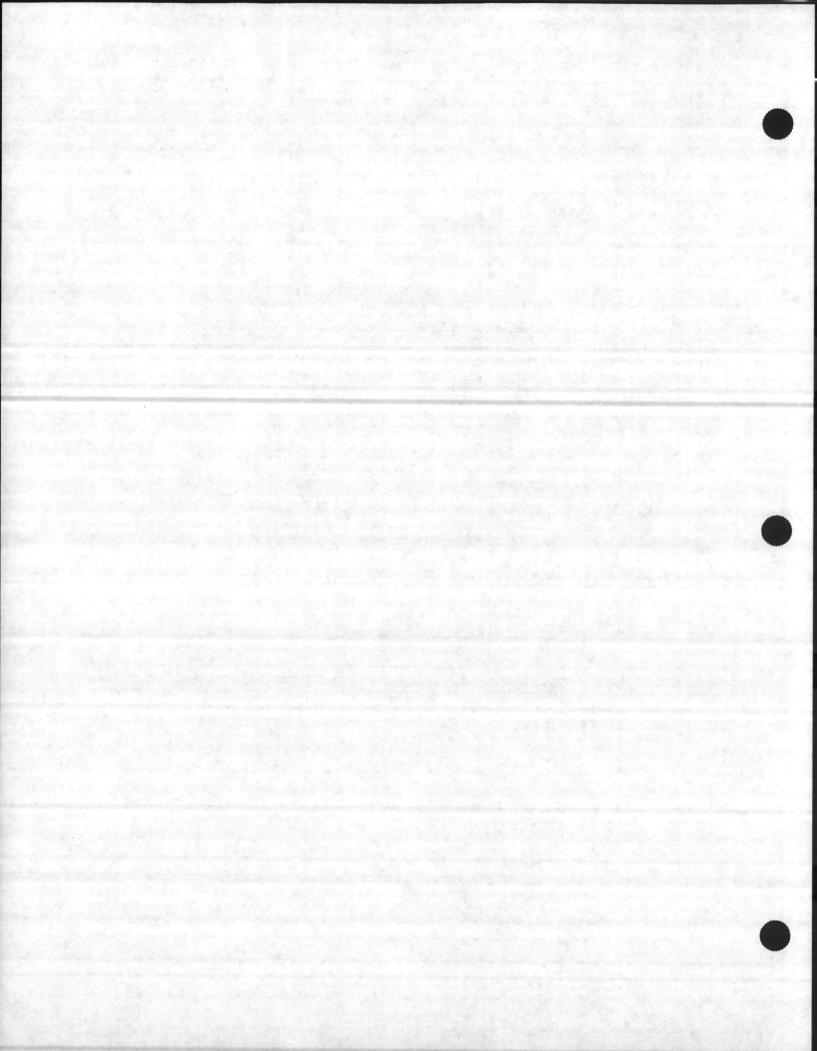
			INDECONIC A	1 NALYSES DATA SHEET	EPA SAMPLE NO.
			INOKOHIVIC A	MACTOCO BITTI GITCO	
b Na	me: HALL	IBURTON_NUS		Contract:	2-AC
				D SAS No.:	
					mple ID: P225110_
itrix	(S011/W	ater): WATE			
evel	(low/med	): LOW_		Date R	eceived: 02/03/93
Soli	.ds:	0.	9	en de la companya de Na la companya de la	
	Co	ncentration	Units (ug/	L or mg/kg dry weigh	t): UG/L_
			1		
		ICAS No.	: Analyte :	Concentration C: Q	IM
			1		
		17429-90-5	:Aluminum_:	2280!_!	'
		17440-36-0	Antimony_	10.0!U!_W_	-:[-:
		17440-38-2	Arsenic	11.1!!	
		17440-39-3	Barium	85.0!B!	!5-:
		17440-41-7	Beryllium	1.0101	:[-:
		17440-43-9	Cadmium	5.01U!	—;e-;
		17440-70-2	Calcium	12600 _	— iP-i
		17440-47-3	Chromium_	18.01_1	— <u>:</u> [-:
100		17440-48-4	Cobalt	9.01B1	!5-!
		17440-50-8	Copper	1021_1	!5-!
		17439-89-6	Iron	13200;_i	i F i
		:7439-92-1	Lead	14.11_1	
		17439-95-4	Magnesium	32301B1	!P_!
		17439-96-5	:Manganese	1491_1	!F_!
		17439-97-6	!Mercury	0.20 U	
		17440-02-0	!Nickel	1861_1	!P_!
		:7440-09-7	Potassium	2270 B	; P_;
		17782-49-2	Selenium_	1.0101	!!
		17440-22-4	!Silver	3.0 U	
		17440-23-5	Sodium	15500:_!	! <u>F</u> _!
				1.0 U	
		17440-62-2			!P_!
		17440-66-6	!Zinc	190   -	!P_!
		1	1		
		1	!		
olor	Before:	BLACK	Clari	ty Before: OPAQUE	Texture:
olor	After:	COLORLESS	Clari	ty After: CLEAR_	Artifacts:
commer	nts:				
-mme	The state of the same				
	THE RESERVE OF THE PARTY OF THE				



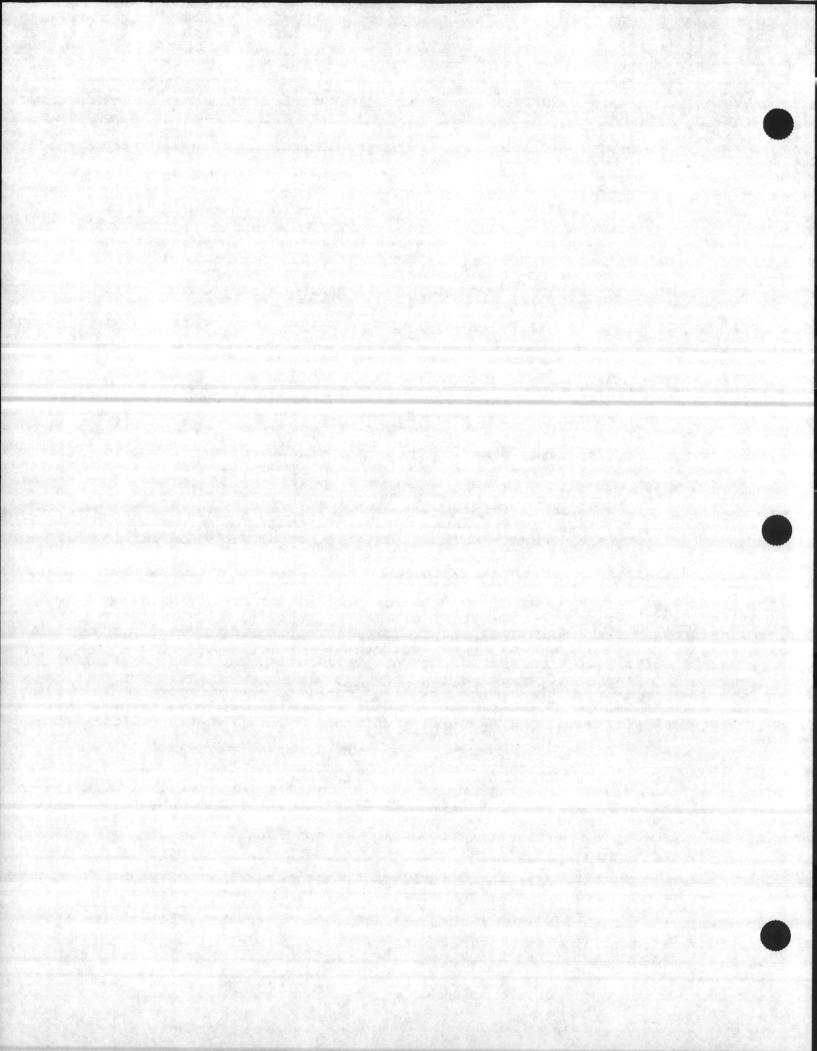
			INDICOMINE P	ANALYSES DATA SHEET	2-AS
Nam	e: HALL	IBURTON_NUS		Contract:	
Cod	le: HNUS	Ca	se No.: BKH	HD SAS No.:	SDG No.: PKG2_
		ater): WATE			Gample ID: P225109
		): LOW_		Date	Received: 02/03/93
vei (	10W/med	,. Low_			
Solid	ls:	_o.	0		
					best uc/
	Со	ncentration	Units (ug.	/L or mg/kg dry weig	int): DB/L_
		!	1		T
		ICAS No.	Analyte	Concentration C	IM!
		1			II
		17429-90-5	Aluminum_	451	IP_I
		17440-36-0	!Antimony_	10.0:0:	IF BIS CARE TO SERVE
		17440-38-2	Arsenic	!2.0!U!	1F_1
		17440-39-3	Barium	!71.0 B	1P_1
		17440-41-7	{Beryllium	11.0 B	IP_I
		17440-43-9	:Cadmium	:5.0:U:	!P_!
		17440-70-2	:Calcium	11100 _ _	IP_I
		17440-47-3	Chromium_	110.0 U	IP_I
		17440-48-4	:Cobalt	8.0101	!P_!
		17440-50-8	Copper	120.0;B;	iFi
		17439-89-6	!Iron	183401_1	iPi
		17439-92-1	[Lead	189.51_1	!F_!
		7439-95-4	: Magnesium	!2720 B	!P_!
		17439-96-5	Manganese	165.01_1_	IF_I
		17439-97-6	!Mercury	0.20 U	1CV1
		17440-02-0	!Nickel	120.0 U	IP_I
		17440-09-7	:Potassium	[1300 B	IP_I
		17782-49-2	Selenium_	11.0 U	!F_!
		17440-22-4	!Silver	13.01U1	!P_!
		17440-23-5	-		! <u>P</u> _!
		17440-28-0	THE RESIDENCE OF STREET STREET, STREET		!F_!
		17440-62-2			!P_!
		17440-66-6	Zinc	192	[F_]
			1	!	
		1	1	'	
olor I	Before:	COLORLESS	Clari	ty Before: CLEAR_	Texture:
olor 6	After:	COLORLESS	Clari	ty After: CLEAR_	Artifacts:
ommen	ts:				
-					



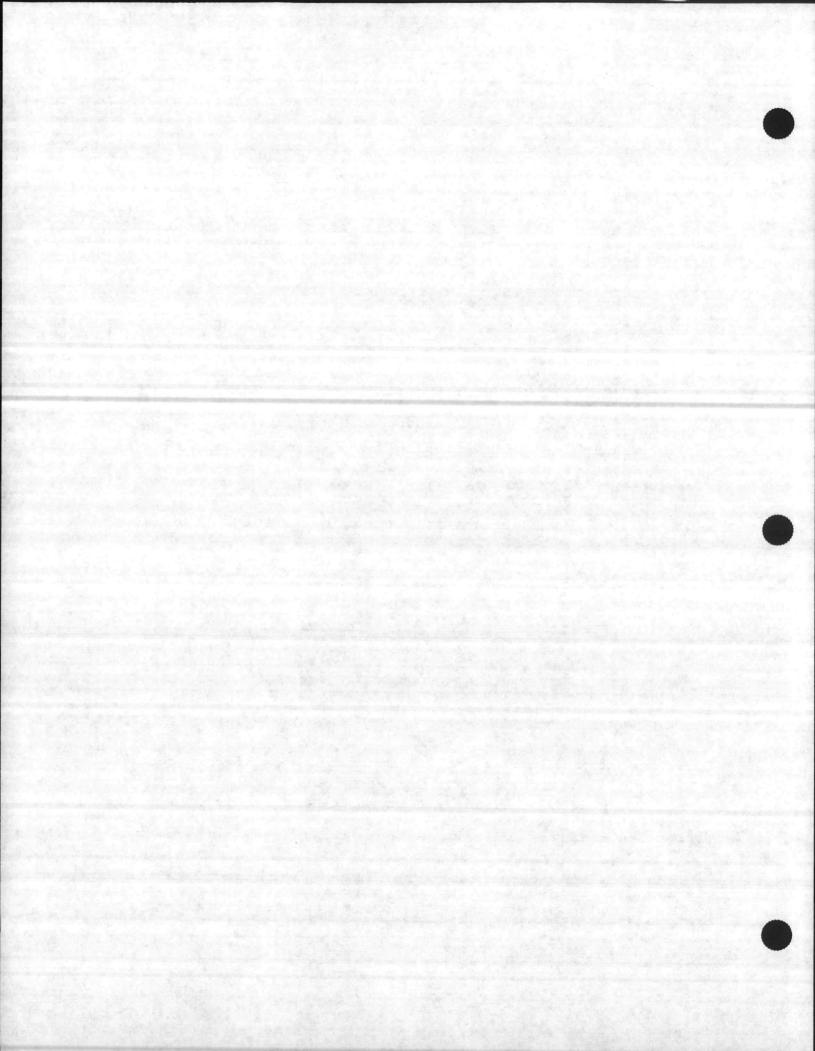
			INDEGANIC A	1 NALYSES DATA SHEE		-A SAMPLE NO.
						2-0W
ь Na	me: HALL	IBURTON_NUS		Contract:		
ь Са	de: HNUS	Ca	se No.: BKH	D_ SAS No.:	Si	OG No.: PKG2_
trix	(soil/w	ater): WATE	₹	Lab	Sample	ID: P225108_
evel	(low/med	): LOW_		Dat	e Receiv	ed: 02/02/93
Soli	ds:	o.	0			
				L or mg/kg dry we	ioht): U	G/L
	Lo	ncentration		WANTED TO THE TOTAL PROPERTY.		
		1		1 1		
		CAS No.	! Analyte !	Concentration   C	Q iM	
		1		1001-1	:-	
		17429-90-5	Aluminum_	6081_1	:[-	
		17440-36-0	Antimony_	10.0101	:-	
		17440-38-2	Arsenic	2.0101	- ip-	
		17440-39-3	Barium	74.01B1	:b-	
		17440-41-7	Beryllium	1.0 U		
		17440-43-9	Cadmium	6.01_1		
100		17440-70-2	Calcium_	107001_1		
		17440-47-3	Chromium_	10.0101		
		17440-48-4	Cobalt	10.0 B		
		17440-50-8	Copper	14.0 B		·
je ba		17439-89-6	!Iron	7740!_!	iP_	
		17439-92-1	!Lead	34.61_1.	;F	
		17439-95-4	! Magnesium !	2560   B		
		17439-96-5	! Manganese !	51.01_1	; P	
		17439-97-6	Mercury	0.20101		
		17440-02-0	Nickel	20.01U1	(F_	
		17440-09-7	Potassium	1330(B)	F_	
		17782-49-2	Selenium_	1.0 U	:F_	
		17440-22-4	!Silver	3.0:0:	:F'_	
		17440-23-5	Sodium	133001_1	!F_	
		17440-28-0	!Thallium_	1.0(U)	!F_	
			Vanadium_		IP_	
			!Zinc	121	[P_	
		1	1			
		1	.1			
olor	Before:	COLORLESS	Clarit	by Before: CLEAR_	T€	exture:
olor	After:	COLORLESS	Clari	ty After: CLEAR_	Ar	tifacts:
ommei	nts:					
		TANK THE PARTY OF	AND A			
_						



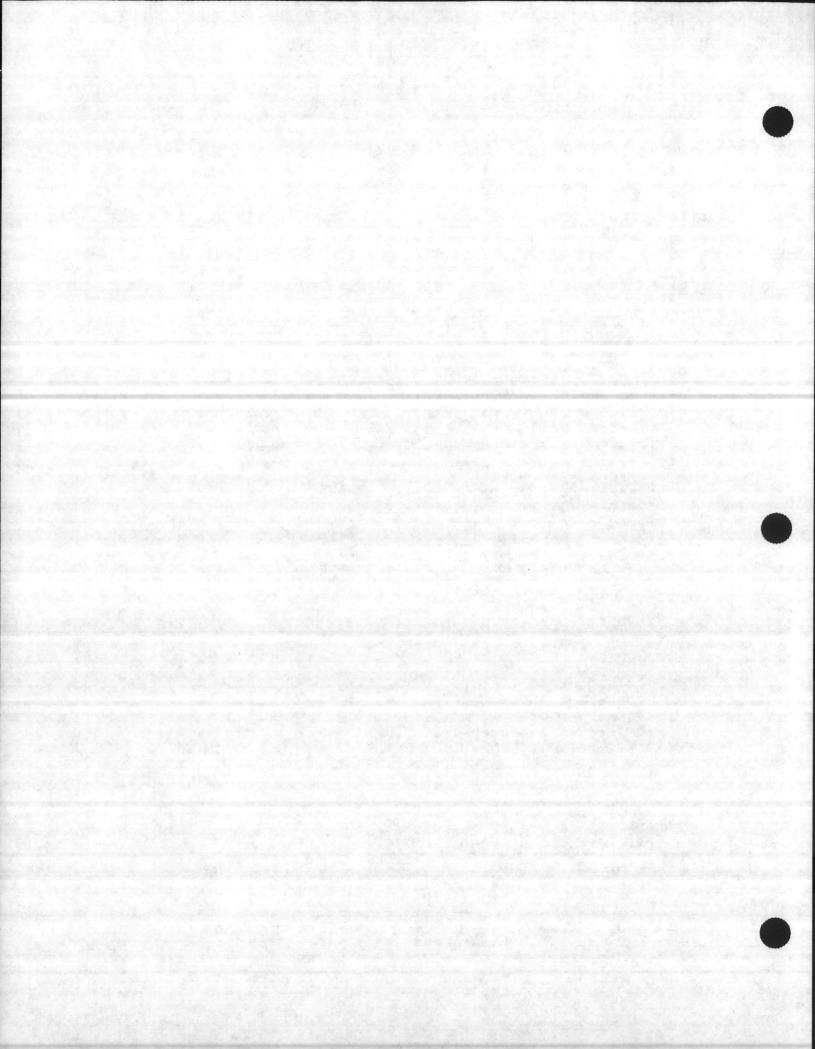
			INORGANIC A	1 NALYSES DATA SH	EET	EPA SAMPLE NO.
						3-AC
b Na	me: HALL	IBURTON_NUS		Contract:		_ 1
ь Со	de: HNUS	Ca	se No.: BKH	D_ SAS No.:		SDG No.: PKG2_
trix	(soil/w	ater): WATE	R	L	ab Sam	ole ID: P225113
vel	(low/med	): LOW_		D	ate Re	ceived: 02/03/93
Soli	ds:	_0.	0			
	Co	ncentration	Units (ug/	L or mg/kg dry	weight	): UG/L_
		1	1	l l	1	TI
		ICAS No.	: Analyte	Concentration (C	: Q	IM I
		17429-90-5	Aluminum	65101		IP_I
		17440-36-0	Antimony	10.01	1: W_	_IF_I
		17440-38-2	Arsenic	9.1   E	31	_IF_I
		17440-39-3	Barium	101 I E	31	_IP_I
		17440-41-7	!Bervllium!	1.0!E	31	[P]
		17440-43-9	Cadmium	5.011	11	IP_I
		17440-70-2	Calcium	123001	1	[P]
		17440-47-3	Chromium	23.01		_IP_I
		ITAAA AA A	10-4-14	0 0 11	A COLUMN TO A COLUMN	
		17440-50-8	(Copper	1031	1	_IP_I
1		17439-89-6	IIron	192001	1	IP_I
		17439-92-1	Lead	23.61	1	_!F_!
		17439-95-4	Magnesium	1031 192001 23.61 256018	31	_(P_1
		17439-96-5	! Manganese	1931	1	_IP_I
		17439-97-6	Mercury	0.2011 33.01	J (	_ICVI
		17440-02-0	Nickel	33.01	1	_!P_!
		17782-49-2	!Selenium	1.010	J!	_!F_!
		17440-22-4	Silver	3.011	١١	_IP_I
		17440-23-5	Sodium	3.010 150001	1	_IP_I
			!Thallium_	1.011	J!	{ F_
			!Vanadium_	18.011	31	_IP_I
			Zinc	1531	_11	_!P_!
			1			
olor	Before:	BLACK	Clari	ty Before: OFAQ	JE	Texture:
olor	After:	COLORLESS	Clari	ty After: CLEA	R_	Artifacts:
ommer	ıts:	British Artist Land				
2			4.40			
-						



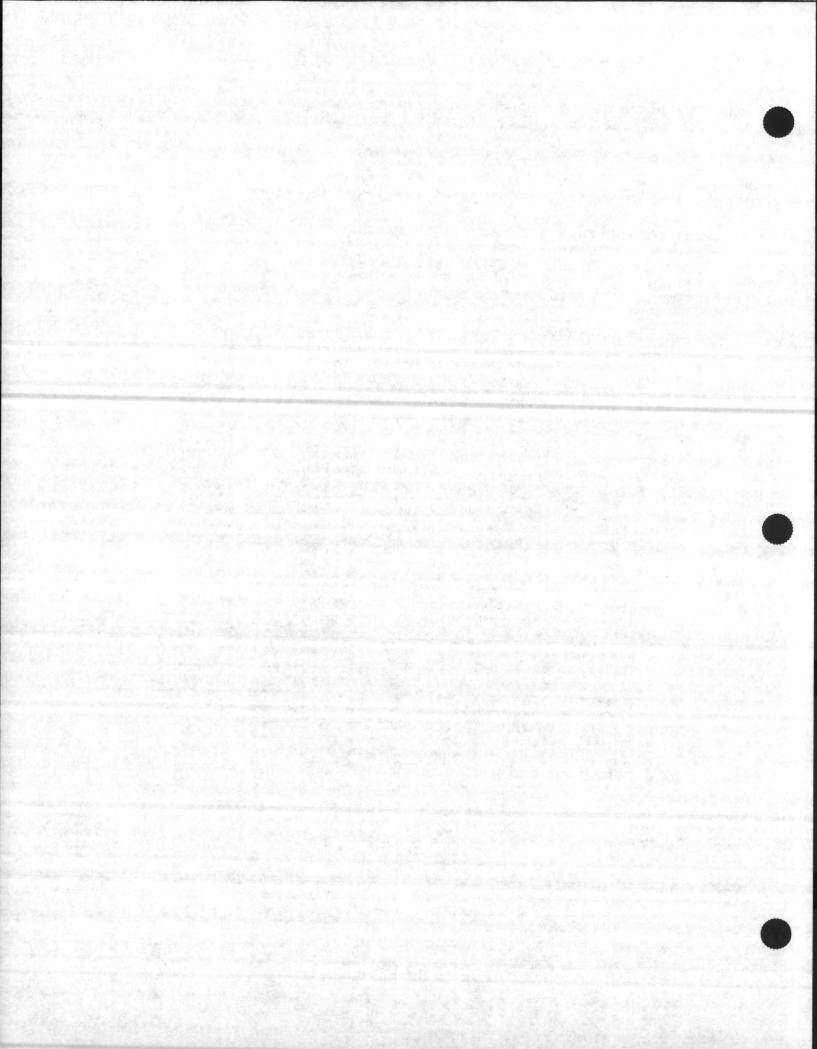
			INDIVIDANTE	ANALYSES DATA S			
b Nam	ne: HALL	.IBURTON_NUS		Contract:		1 3-A	5
ь Сос	de: HNUS	Ca	se No.: BKH	HD SAS No.:		SDG No.:	PK62_
trix	(soil/w	ater): WATE	R		Lab S	ample ID: P22	5112_
vel	(low/med	): LOW_			Date	Received: 02/	03/93
Solid	ds:	0.	0				
			Unite (un	/L or mg/kg dry	wein	ht): UG/L	
	Lo	ncentration	Onres (ag.				
					Samuel and Samuel		
		ICAS No.	Analyte	Concentration	ili u	im i	
			21	717	-		
		17429-90-5	Aluminum_	317	\_;\		
		17440-36-0	Antimony_	10.0		- F	
		17440-38-2	Arsenic		101		
		17440-39-3	Barium		1 D 1		
		17440-41-7	Beryllium	1.0		- ip-i	
		17440-43-9	:Cadmium	5.0		- ip-i	
		17440-70-2	Carcium_	11200	17:-	IP.	
		17440-47-3	ichromium_	10.0		TIP-	
14.56		17440-48-4	Cobalt	8.0	. D.		
		:7440-50-8	Copper	24.0	1 1	ib-i	
		17439-89-6	ilron	6910	:-:	- iF	
		17439-92-1	iLead	45.0	'-'	- ie	
		17439-95-4	Magnesium	2670	101-		
		17439-96-5	Manganese	57.0	111		
		17439-97-6	Mercury	0.20		- IE	
		17440-02-0	:Nickel	20.0	.D.	Tip-	
		17440-09-7	Potassium	1380	1111	— ;- ;	
		17/82-49-2	iSelenium_	3.0	!!!!		
		17440-22-4	Silver	14200	-	IP.	
		17440-23-3	Thalling	11.0	1111	IF!	
		17440-28-0		4.0	1111	ip_i	
		17440-62-2	'7ioc	144	1 1	The state of the s	
				100			
olor	Before:	COLORLESS	Clari	ty Before: CLE	AR_	Texture:	
olor	After:	COLORLESS	Clari	ty After: CLE	AR_	Artifact	s:
ommen	ts:						
	The state of the state of						



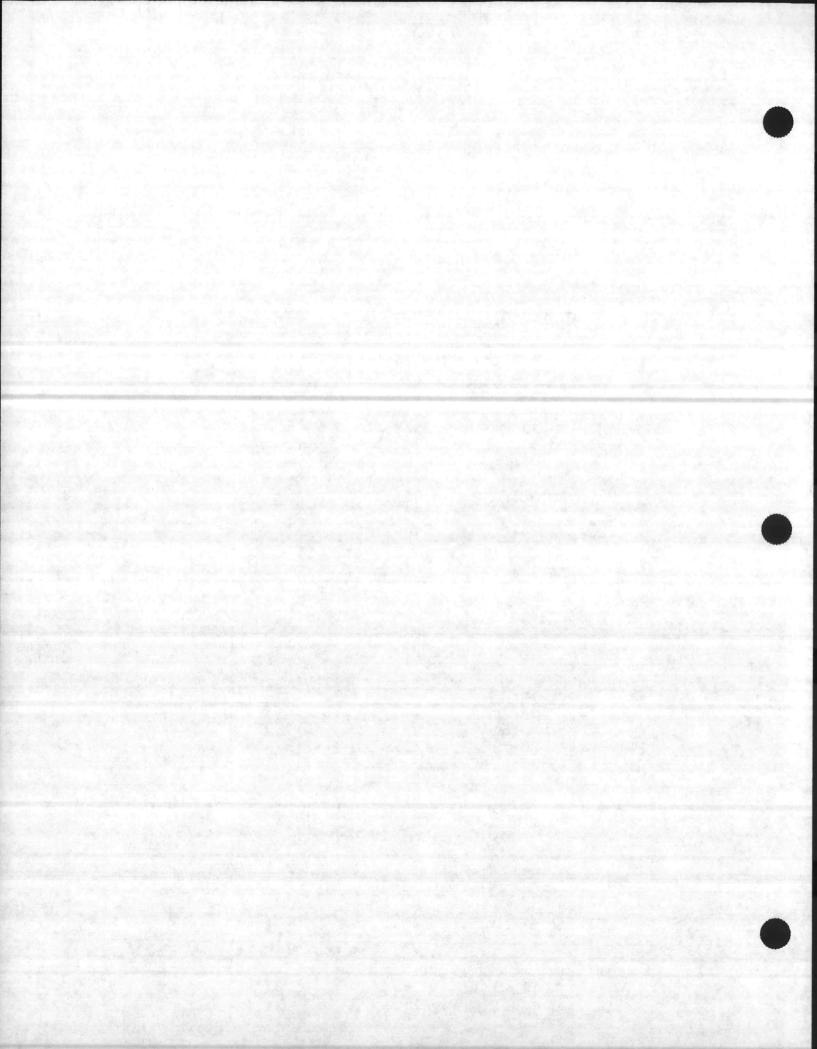
		INORGANIC A	1 NALYSES DATA SHEET	EFA SAMPLE NO.
				3-0W
b Name: HALL	IBURTON_NUS		Contract:	1
b Code: HNUS	6 Ca	se No.: BKH	HD SAS No.:	SDG No.: PKG2_
atrix (soil/w	water): WATE	R	Lab S	Gample ID: P225111_
evel (low/med	i): LOW_		Date	Received: 02/03/93
Solids:	_0.	0		
Co	oncentration	Units (ug/	'L or mg/kg dry weig	ht): UG/L_
			Para sandara de Salanga (san [ ] c	
	ICAS No.	! Analyte !	Concentration C	II
	17429-90-5	Aluminum	166   B	IP_I
	1/440-30-0	IMILOTINOTTY	20.01	
	17440-38-2	Arsenic	2.0101	!F_!
	17440-39-3	Barium	80.0181	IF_I
	17440-41-7	Bervllium	1.0101	IP_I
	17440-43-9	Cadmium	5.0:0:	IP_I
	17440-70-2	!Calcium	106001_1	[P_I
	17440-47-3	Chromium	10.0 U	IP_I
	17440-48-4	!Cobalt	10.0 U    8.0 U    14.0 B	[P_I
	17440-50-B	!Copper	14.0 B	IP I
	17439-89-6	!Iron	72701_1_	IP I
	17437-07-0	!lead	25.21_1	IF I
	17439-95-4	! Magnesium	2550 B	IP I
	17437-73 4	! Manganese	46.01_1_	IP I
	17437-70-5	Manguny	0.2010	ICVI
	17437-77-0	'Niekal	22.01_1	IP I
	17440-02-0	IDatassium	1330 B	IP.
	17700 49 7	150lassium	1.0 U	iF i
				IP I
		Silver		IP I
		CONTRACTOR OF THE PARTY OF THE		
		Thallium_		TIP I
		Vanadium_  Zinc		
		<u> </u>		
olor Before:	COLORLESS	Clari	ty Before: CLEAR_	Texture:
color After:	COLORLESS	Clari	ty After: CLEAR_	Artifacts:
comments:				



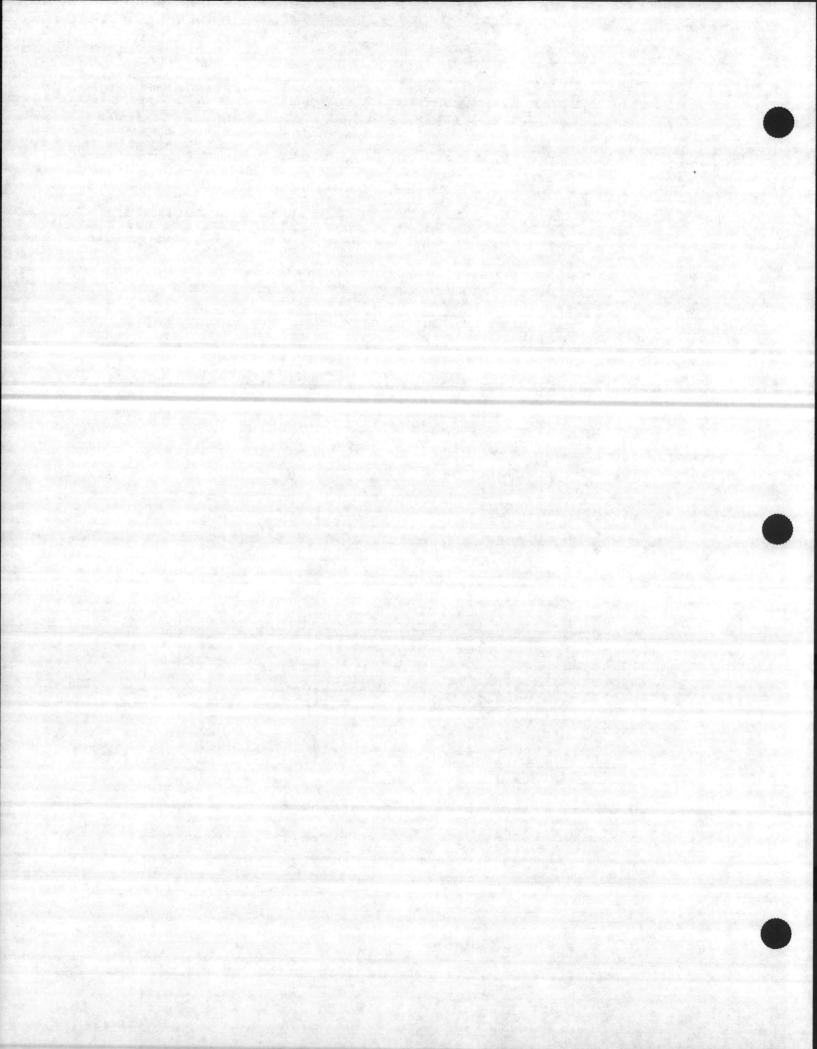
		INORGANIC AN	1 NALYSES DATA SHEET	
				4-AC
b Name: HAL	LIBURTON_NUS		Contract:	
b Code: HNU	S Ca	se No.: BKHI	SAS No.:	SDG No.: PKG2
trix (soil/	water): WATE	R	Lab 9	Sample ID: P225130_
evel (low/me	d): LOW_		Date	Received: 02/03/93
Solids:	_0.	0		
C	oncentration	Units (ug/L	or mg/kg dry weig	ght): UG/L_
	_	<del></del>	Annual research of Late	
	CAS No.		Concentration  C	I MI G
		1	1_1_1_	11
	17429-90-5	Aluminum	1560	IP_I
	17440-36-0	Antimony	10.0:0:	WIF_1
	17440-38-2	!Arsenic !	7.91B1	IF_I
	17440-39-3	Barium :	13.0;B;	iP_i
	17440-41-7	!Bervllium!	1.0(U)	
	17440-43-9	Cadmium	5.0101	IP_I
	17440-70-2	Calcium	11300 _	IP_I
	17440-47-3	Chromium	10.0 U	IP_1
	17440-48-4	(Cobalt	8.0101	!P_!
	17440-50-8	Copper	11.0 B	IP I
The state of	17439-89-6	!Iron !	27301_1_	[P]
	17437-07-0	!! ead !	10.31_1	IF I
	17437 72 1	!Maggesium!	2520 B	IP I
	17437-73-4	!Mannangen!	19.01_1	IP I
	17437-70-3	! Manguny !	0.20101_	ICVI
	17437-77-6	INIckal	20.0101	IP I
	17440-02-0	INICKEL	1590 B	IP I
	17440-07-7	(Colosius !	1.0(U)	IF I
	17/82-49-2	iselenium_i	3 0 111	IP I
	17440-22-4	Silveri	3.0 U  14700 _ _	- P
	17440-23-5	15001UM	1.0 U	F
	17440-28-0		B.01B1_	IP I
	17440-62-2	ivanadium_i	43.01_1_	IP I
	1/440-66-6		43.0	
	i	_ii		
lor Before:	COLORLESS	Clarit	y Before: CLEAR_	Texture:
olor After:	COLORLESS	Clarit	y After: CLEAR_	Artifacts:
omments:				



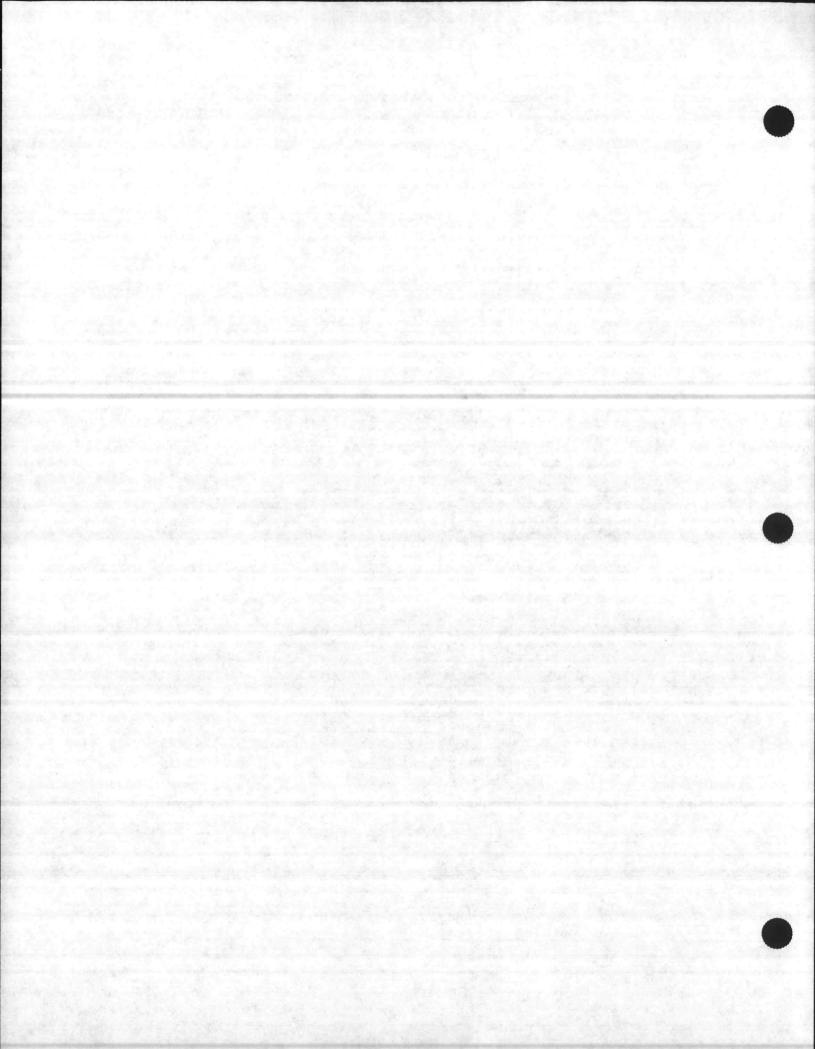
		INDEGANIC AN	1 IALYSES DATA SHEET	EPA SAMPLE NO.
				4-AS
b Name:	HALLIBURTON_NUS	3	Contract:	_ 1
b Code:	: HNUS Ca	ase No.: BKHD	SAS No.:	_ SDG No.: PKG2
trix (s	soil/water): WAT	ER	Lab Sa	mple ID: P225129_
evel (lo	ow/med): LOW	_	Date R	eceived: 02/03/93
Solids	0	.0		
	Concentration	n Units (ug/L	or mg/kg dry weigh	t): UG/L_
		1	y and the second by the I	<del></del>
	ICAS No.	: Analyte :	Concentration   C  Q	IM I
			117(B)	-ip-i
	17429-90-5	'Aluminum_i	10.0101	IF I
	17440-36-0	IANTIMONY_I	2.0111	IF I
	17440-38-2	Arsenici	2.0(U)	IP I
	17440-39-3	Bariumi	83.01B1 1.01U1	IP I
	17440-41-7	(Cadaina	5 0111	IP I
	17440-43-9	Calcium_1	5.0(0)	IP I
	: /440-/0-/	: 1 2 1 5 1 1 1 1 1 1	10/001	
	17440-47-3	ichromium_i	10.0(U) 	IP I
	: 7440-48-4	(Constr	18 O!B!	IP I
	, / 44010-0	I COUDE!		
	1/4.37-07-0	111.011	00.01	
	1/4.37-72-1	ILEau (		
	17439-93-4	imagnesium:	2720   B	IF I
	17439-96-3	Manganeser	51.01_1 0.20!U1 20.0!U!	ICVI
	17439-97-6	INECUTY	20.01111	IP I
	: /440-02-0	INILKEL	20.0.0.	
	17440-09-7	(Colosius )	1410 B  1.0 U	IF I
				IP I
		Silver		IP I
	17440-23-3	Sodium!	1.0101	IF I
	17440-28-0	:  Vanadium_	4.0101	IP I
		Zinc		
olor Be	fore: COLORLESS	Clarit	y Before: CLEAR_	Texture:
olor Af	ter: COLORLESS	Clarit	y After: CLEAR_	Artifacts:
omments				



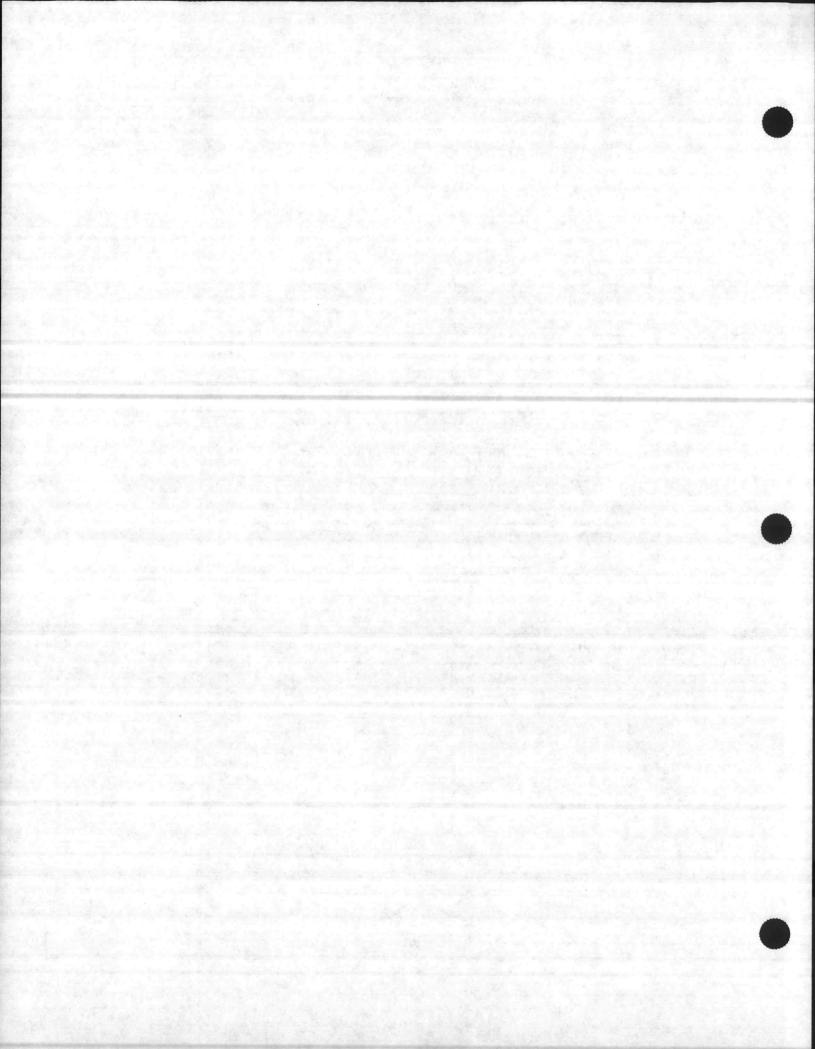
		INORGANIC A	1 NALYSES DATA S		EFA SAMPLE NO.
					4-0W
b Name: HAL	LIBURTON_NUS		Contract:		
ab Code: HNL	JS Ca	se No.: BKHI	SAS No.:		SDG No.: PKG2
atrix (soil/	water): WATE	R		Lab Samp	le ID: P225128_
evel (low/me	ed): LOW_			Date Rec	eived: 02/03/93
Solids:	_0.	0			
C	Concentration	Units (ug/	L or mg/kg dry	weight)	: UG/L_
	ICAS No.	! Analyte !!	Concentration:	CI Q	IM I
Marie Control	7429-90-5	(Aluminum )	70.01	BI	IP_I
	17440-36-0	Antimony_	10.01	U :	_iFi
4	17440-38-2	Arsenic	2.01	UI	IF_I
	17440-39-3	Barium i	86.01	Bi	iP_i
	17440-41-7	Bervllium	1.01	UI	IP_I
	17440-43-9	(Cadmium	5.01	UI	IP_I
	17440-70-2	(Calcium	102001	1	IP I
	17440-47-3	(Chromium )	10.0	U:	IP I
	17440-48-4	(Cobalt	8.01	UI	IP_I
	17440-50-8	(Copper	8.01 5.01 73901	Bl	IP_I
	17439-89-6	IIron I	73901 13.21	1	IP_I
	17439-92-1	Lead	13.21	1	IF_I
	17439-95-4	!Magnesium!	26501	B!	IP_I
	17439-96-5	Manganese	45.01	_1	_IP_I
	17439-97-6	:Mercury :	0.201	Ui	_: [ [ ] [
	: / 4.4: (1(1) /(1)	INICKEL	20.01	111	IF I
	17440-09-7	Potassium	1360	B:	IP_I
	17782-49-2	Selenium	1.01	U!	_IF_I
	17440-22-4	Silver	3.01	U!	_IP_I
	17440-23-5	!Sodium !	142001	_	_!P_!
	17440-28-0	Thallium_	1.01	U!	_IF_I
		[Vanadium_		U1	_IP_I
		Zinc		_!	_IP_I
		11		_!	_11
	1	!!		_'	_11
olor Before:	COLORLESS	Clarit	y Before: CLEA	R_	Texture:
olor After:	COLORLESS	Clarit	y After: CLEA	R_	Artifacts:
omments:					



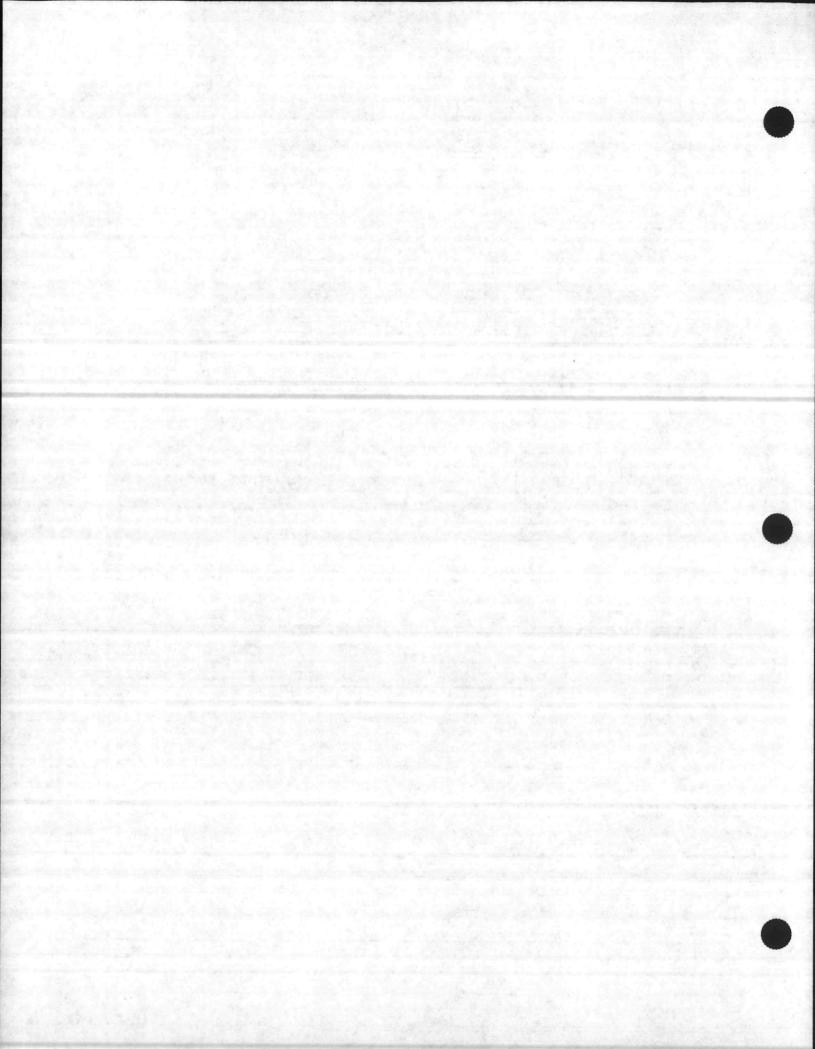
ab Na			TIMOLIOUMITE W	NALYSES DATA SHE		
ab Na						5-AC
	me: HALL	IBURTON_NUS	***	Contract:		1
ab Co	de: HNUS	Ca	se No.: BKH	D SAS No.: _		SDG No.: PKG2
atrix	(soil/w	ater): WATE	R	La	b Samp	le ID: P225127_
evel	(low/med	): LOW_		Da	te Rec	eived: 02/04/93
Soli	.ds:	o.	0			
	Co	ncentration	Units (ug/	L or mg/kg dry w	veight)	: UG/L_
		!	<u> </u>		A 11	
		CAS No.	! Analyte !	Concentration (C)	Q	IM I
		17429-90-5	Aluminum	1850	a Value	IP_I
		17440-36-0	!Antimony !	10.0:0:		1F_1
		17440-38-2	Arsenic	2.0101		IF_I
		17440-39-3	Barium	9.01B		IP_I
		17440-41-7	!Beryllium!	1.0:0:		IP_1
		17440-43-9	Cadmium_	5.0:0:		IP_I
		17440-70-2	Calcium_	113001_		IP_I
		17440-47-3	(Chromium )	10.0:U	L. Hartin	IP_I
		17440-48-4	(Cobalt !	8.0:0		!P_!
		17440-50-8	!Copper!	5.0:B		.1F_1
		17439-89-6	!Iron!	1140;		[P_1
		17439-92-1	!Lead!	3.71_	1	.lF_L
		17439-95-4	: Magnesium:	1400¦B	!	(IP_I
		17439-96-5	! Manganese !	8.0:B	1	1P_1
		17439-97-6	Mercury_	0.20:U	1	[ICVI
		17440-02-0	[Nickel	20.0:U	1	_IP_1
		17440-09-7	(Potassium)	1720 (B	1	_IP_I
		17782-49-2	Selenium_	1.0:0	1	_1F_1
		17440-22-4	Silver	3.0:U	1	_IP_I
		17440-23-5	!Sodium	14700!_	1	_IP_1
		17440-28-0	!Thallium_	1.0:0		_IF_I
		17440-62-2	[Vanadium_	4.0:0	1	_IP_1
		17440-66-6	Zinc	31.01_	i	_IP_I
		1	1 200			
		I was a second			1	
olor	Before:	COLORLESS	Clarit	y Before: CLEAR		Texture:
olor	After:	COLORLESS	Clarit	y After: CLEAR	1	Artifacts:
ommer	nts:					



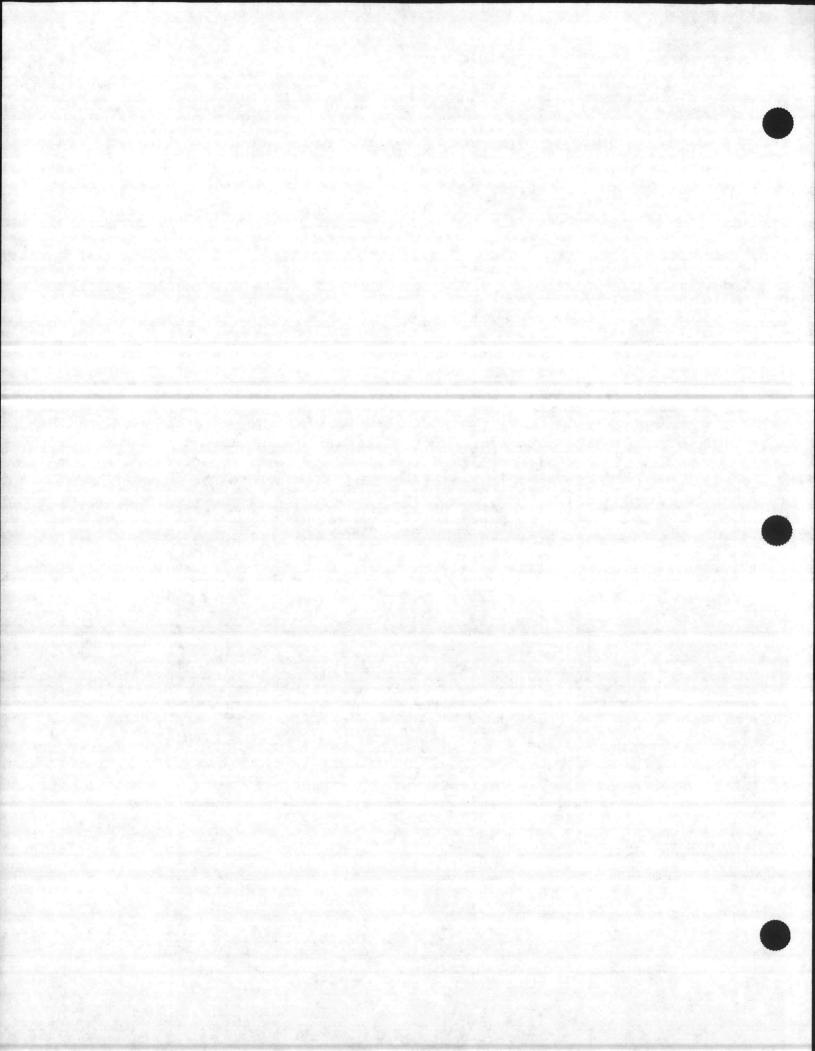
			1 IALYSES <b>DA</b> TA SHEET	EFA SAMPLE NO.
				5-AS
b Name: HAL	LIBURTON_NUS		Contract:	_ 1
Code: HNL	JS Ca	se No.: BKHD	SAS No.:	_ SDG No.: PKG2_
trix (soil	/water): WATE	R	Lab Sad	mple ID: P225126
vel (low/me	ed): LOW_		. Date R	eceived: 02/04/93
Solids:	_0.	0		
(	Concentration	Units (ug/L	or mg/kg dry weigh	t): UG/L_
	1	1		TI
	ICAS No.	! Analyte !C	Concentration   C  Q	IM I
	7429-90-5	Aluminum		IP_I
	17440-36-0	:Antimony :	10.0:U:_W_	!F_!
	17440-38-2	Arsenic	2.0:0:	[F_]
	17440-39-3	Barium	88.01B1	IP_I
	17440-41-7	!Bervllium!	1.0:0:	iPi
	17440-43-9	!Cadmium !	5.0101	iPi
	17440-70-2	Calcium	109001_1	IP_I
	17440-47-3	Chromium	10.0 U	(P_1
	17440-48-4	(Cobalt	8.0101	!P_!
	17440-50-8	Copper	20.01B1	IP_I
	17439-89-6	IIron I	7150   _	IP_I
	:7439-92-1	!Lead !	11.6	IF_1
	17439-95-4	Magnesium	2820 8	IP_I
	17439-96-5	Manoanese	51.01_1	IP_I
	17439-97-6	Mercury	0.20101	ICVI
	17440-02-0	!Nickel !	20.0101	IP_1
	17440-09-7	!Potassium!	1390 B	IP_I
	17782-49-2	Selenium	1.0:0:	ifi
	17440-22-4	Silver	3.0(U)	IP_I
	17440-23-5	Sodium	140001_1	IP_I
	:7440-28-0	Thallium	1.0(U)	IF_I
	17440-62-2	Vanadium	4.0101	IP_I
	17440-66-6	Zinc	1491_1	IP_I
		1		
	- i <u> </u>	1 2 2 1		_1_1
olor Before	: COLORLESS	Clarit	y Before: CLEAR_	Texture:
olor After:	COLORLESS	Clarit	y After: CLEAR_	Artifacts:
omments:				



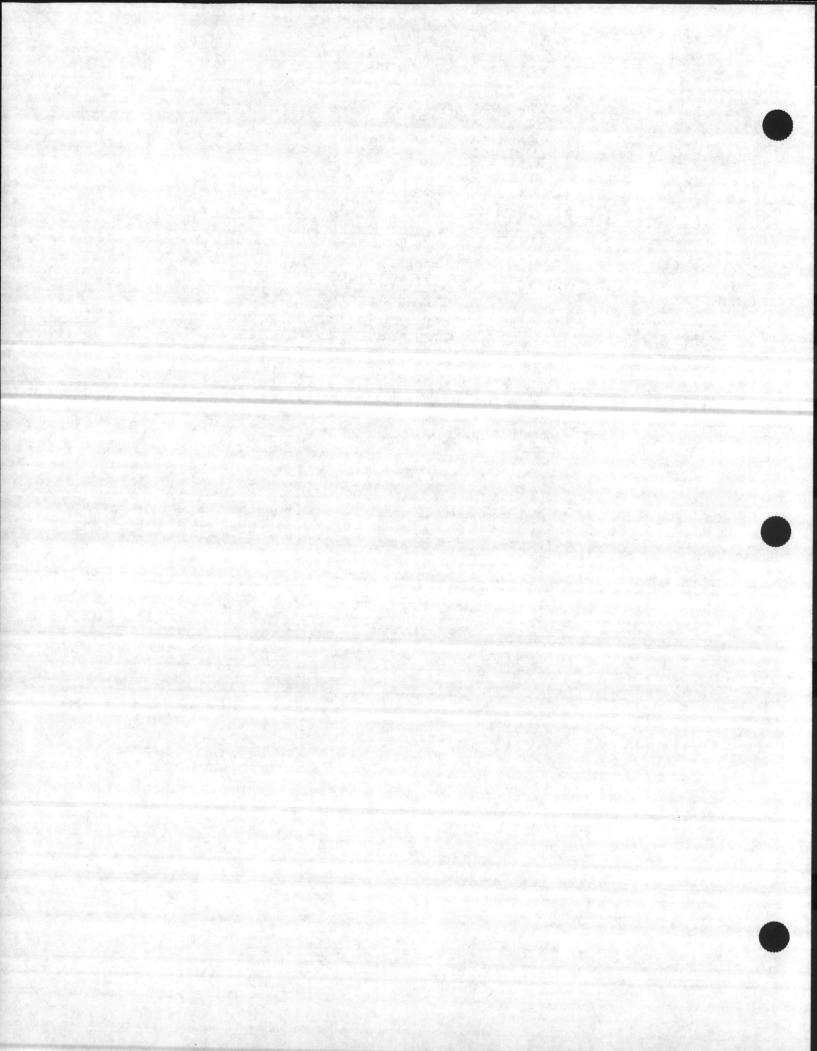
		INORGANIC A	1 ANALYSES DATA SHEE	т	EPA SAMPLE NO.
					5-OW
b Name: HALL	.IBURTON_NUS		Contract:		I
b Code: HNUS	Ca	se No.: BKH	ID SAS No.: _		SDG No.: PKG2_
atrix (soil/w	ater): WATE	R	Lat	Sample	D: P225125
evel (low/med	D: LOW_		Dat	te Rece	ived: 02/04/93
Solids:	_0.	0			
Cc	ncentration	Units (ug/	/L or mg/kg dry we	eight):	UG/L_
	1	1	Compression of American	1	<del>-</del> :
	ICAS No.	! Analyte	Concentration  C	Q !	MI
	7429-90-5	Aluminum	52.0IBI		P_1
	17440-36-0	Antimony	52.0 B  	W !	F_1
	17440-38-2	Arsenic	2.0101	1	F_1
	17440-39-3	Barium	2.0IUI 91.0IBI	1	P_1
	17/1/0-/1-7	Barryllium	i i Gilli		
	17440-43-9	!Cadmium	5.01 1		P_I
	17440-70-2	Calcium	5.01_I 10400I_I		P_1
	17//// // フーマ	Chammitim	10.0:11:		
	17440-48-4	!Cohalt	8.0101	24 C 10 C 10	P I
	17440-50-8	!Copper	8.0 U  51.0 _  7700 _	1	P I
	17439-89-6	!Iron	77001		P-I
	17437-07-0	!lead	17.61_1	!	F
	17437-72-1	! Mannesium	2670 IBI		PI
	17437-75 4	! Mannanese	46.01_1		P I
	17437-70-3	'Manguny	0.20101		cv:
	17437-77-0	'Nickol	20.0101		P!
	17440-02-0	!Dotassium	1340   B		P !
	17440-09-7	(Colassium	1 01111	;	_
	17/82-49-2	.Selenium_	1.0101		P
	17440-22-4	Silver	3.0 U   13500 _		P.I
	17440-23-5	17b = 11	1.0 U		E
					P
	17440-62-2		11061_1		
	1/440-66-6		1081_	and the same of the	_
	-				Tentunes
olor Before:	COLORLESS		ty Before: CLEAR_		Texture:
olor After:	COLORLESS	Clari	ty After: CLEAR_		Artifacts:
omments:					



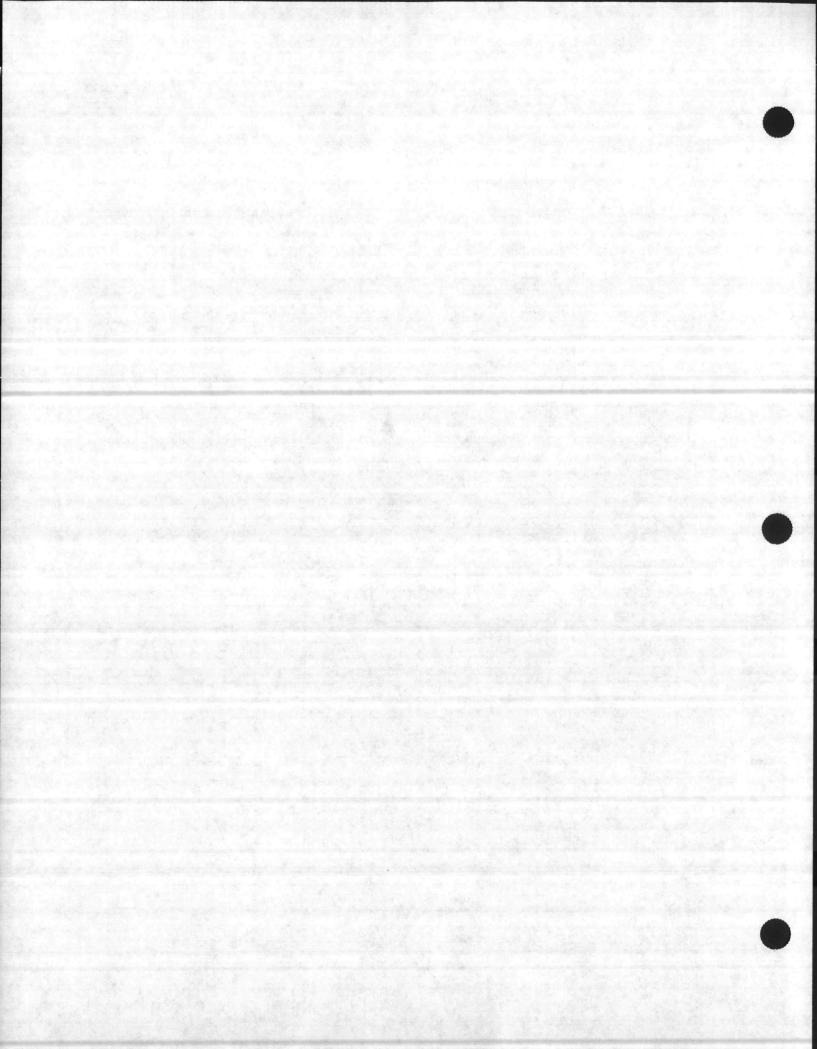
		INORGANIC AN	IALYSES DATA SHEE	T	
					6-AC
b Name: HALL	IBURTON_NUS		Contract:		I
b Code: HNUS	Ca	se No.: BKHI	SAS No.:		SDG No.: PKG2
trix (soil/w	ater): WATE	R	Lat	Sampl	e ID: P225124_
evel (low/med	): LOW_	_	Dat	te Rece	ived: 02/04/93
Solids:	_0.	0			
Co	ncentration	Units (ug/l	or mg/kg dry we	eight):	UG/L_
	CAS No.	! Analyte !!	Concentration(C)	Q !	M   
	7429-90-5	(Aluminum )	1470		P_1
	17440-36-0	!Antimony !	10.0:0:	i	
	17440-38-2	Arsenic	5.9[B]		F_1
	17440-39-3	Barium	21.0 B		P_1
	17440-41-7	!Bervllium!	1.0 U		P_1
	17440-43-9	!Cadmium !	6.01_1		PI
	17440-70-2	!Calcium !	127001_1		PI
	17440-70-2	Chromium !	10.0101		PI
	17440-47-3	'Cobalt	8.0101		PI
	17440-48-4	Conart	17.01B!		PI
	17440-50-8	Copper	47601_1		P !
	17439-89-6	ilron	9 7!!		F !
	: 7439-92-1	iLeadi	9.71_1		P !
	17439-95-4	: magnesium:	3090 IB1		P.
	17439-96-5	Manganese	28.01_1		CU
	17439-97-6	mercury	0.20101		D !
	17440-02-0	Nickel	20.0101		P !
	17440-09-7	(Potassium)	1 450   B		F
	17782-49-2	(Selenium_)	1.0 U		P
	17440-22-4	iSilveri	3.0(0)		P_
	17440-23-5	(Sodium )	13/001_1		
	17440-28-0	iThallium_	1.0(U)		P
	17440-62-2	:Vanadium_!	4.01BI		P
	17440-66-6	Zinc	68.0!_!		
olor Before:	COLORLESS	Clarit	y Before: CLEAR_		Texture:
olor After:	COLORLESS	Clarit	y After: CLEAR_		Artifacts:
omments:					



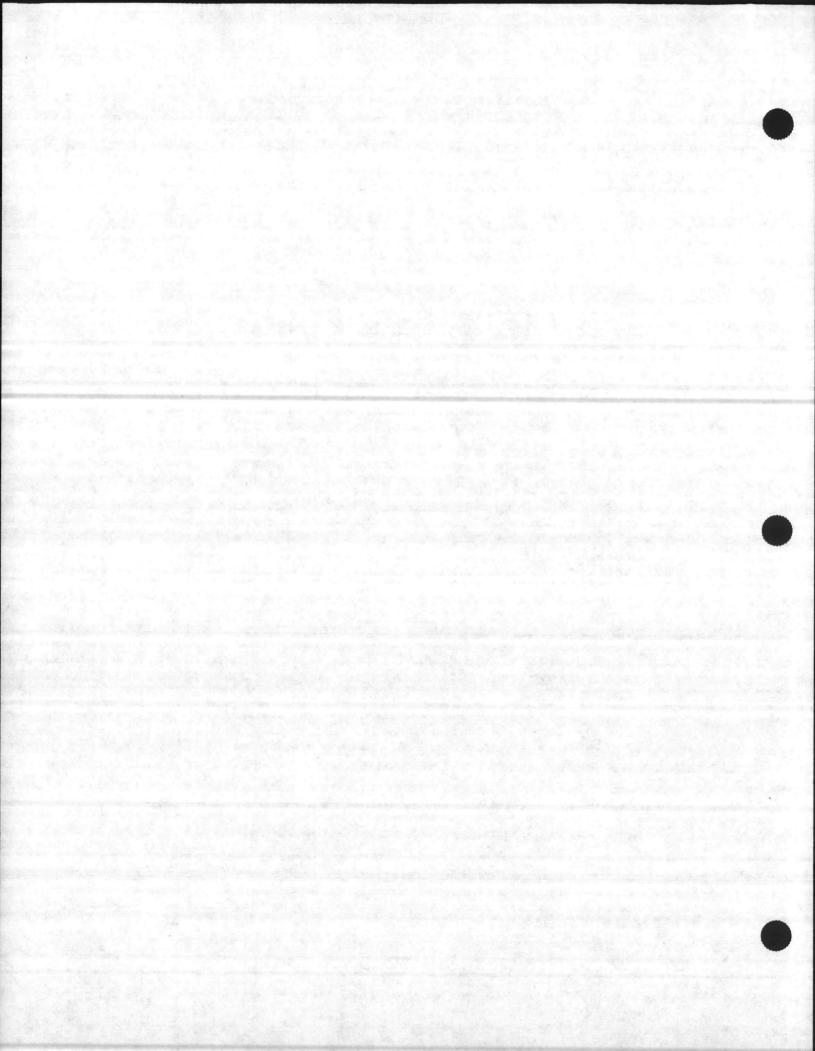
		INDROHNIC F	ANALYSES DATA SHEET	
1 1011	TOUGTON NUC		Contract:	6-AS
ab Name: HALL	TBOKTON_NOS		Contract.	
ab Code: HNUS	Ca	se No.: BKH	HD SAS No.:	SDG No.: PKG2
atrix (soil/w	ater): WATE	R	Lab 9	Sample ID: P225123_
evel (low/med	): LOW_		Date	Received: 02/04/93
Solids:	0.	0		
			Company of the Company	
Co	ncentration	Units (ug/	/L or mg/kg dry weig	ght): UG/L_
	1	I was an work	and the past of the second	
	ICAS No.	: Analyte	Concentration C	I MI
			  84.0 B	
	17429-90-5	:Aluminum_	84.01B1	P
	17440-36-0	'Antimony_	110.0 U	!F_!
	17440-38-2	Arsenic	!2.0!U!	IFI
	17440-39-3	Barium	90.01B1	IP_I
	17440-41-7	Beryllium	i.o U	IP_I
	17440-43-9	!Cadmium	:5.0!U!	IP_I
	17440-70-2	!Calcium	110800!_!	!P_!
	17440-47-3	!Chromium_	110.0 U	IP_I
	17440-48-4	:Cobalt	1 8.0101	IP I
	17440-50-8	Copper	32.01_1	!P_!
	17439-89-6	Iron	167901_1	IP_I
	17439-92-1	Lead	110.81_1	!F_!
	17439-95-4	: Maonesium	[2730 B	[P_I
	17439-96-5	!Manoanese	54.01_1_	1P_1
	17439-97-6	Mercury	0.20101_	ICVI
	17440-02-0	!Nickel	20.0101	IP_I
	17440-09-7	!Potassium	1360(B)	IP_I
			1.0 U	
	17440-22-4	Silver	3.0IUI	IP_I
	17440-23-5	ISodium	137001_1_	IP_I
	17440-28-0	!Thallium	1.0 U	IF I
	17440-62-2	!Vanadium	4.0IUI	IP I
	17440-66-6	17inc	1541_1_	IP I
	1	1 28		
		under State Control of the Sta		
Color Before:	COLORLESS	Clari	ty Before: CLEAR_	Texture:
color After:	COLORLESS	Clari	ty After: CLEAR_	Artifacts:
Comments:				



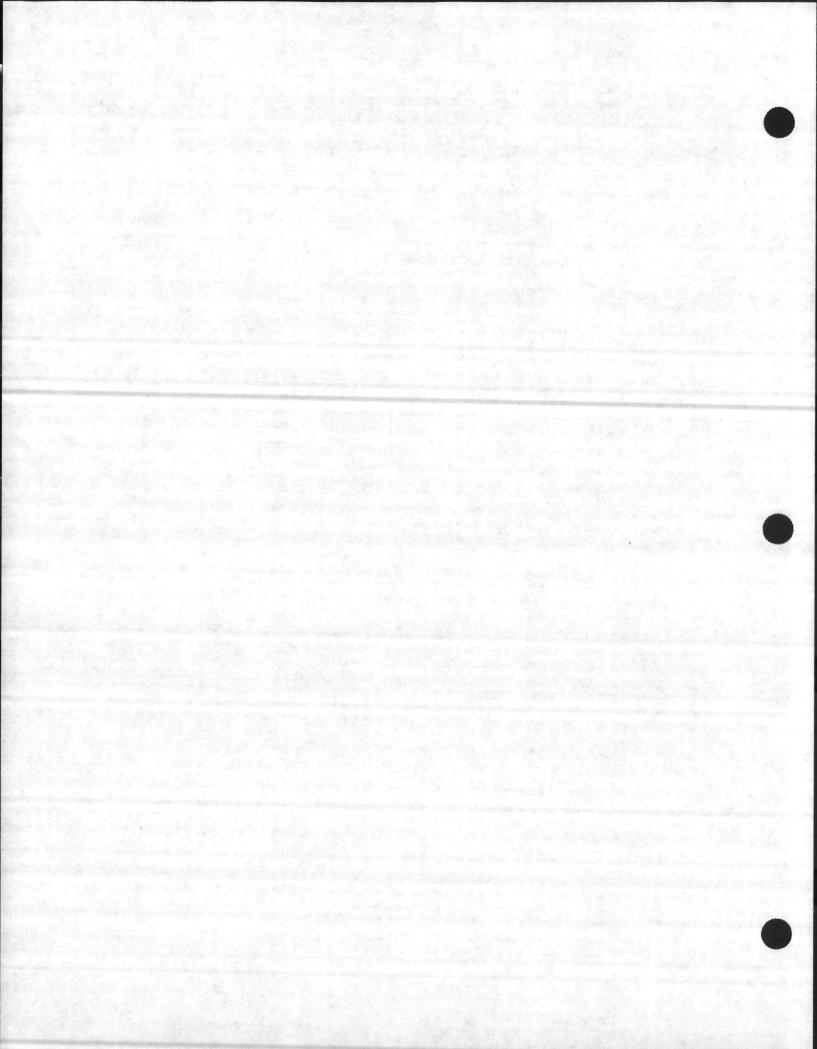
		INORGANIC A	1 NALYSES DATA S		EPA SAMPLE NO.
b Name: HALL	_IBURTON_NUS		Contract:		6-0W
					_ SDG No.: PKG2
b code. Tillo		se non bar			
trix (soil/	water): WATE	R		Lab Sai	mple ID: P225122_
vel (low/med	d): LOW_	_		Date R	eceived: 02/04/93
Solids:	_0.	0			
		Units (ug/	L or mg/kg dry	weigh	t): UG/L_
	-,			1	
	ICAS No.	Analyte	Concentration!	CI Q	IM I
	7429-90-5	Aluminum	104	B!	_IP_I
	17440-36-0	!Antimony_!	10.0	U!	!F_!
	17440-38-2	Arsenic	2.0	U!	IF_I
	17440-39-3	Barium	90.0	B!	!P_!
	17440-41-7	Beryllium	1.0	UI	IP_I
	17440-43-9	Cadmium	5.0	_1	IP_I
	17440-70-2	(Calcium	10400	_I	IP_I
	17440-47-3	Chromium	10.0	U!	!P_!
	17440-48-4	(Cobalt	8.01	UI	IP_I
	17440-50-8	Copper	26.0	_1	IP_I
	17439-89-6	Iron	7570		(P_1
	17439-92-1	Lead	12.7		!F_!
	17439-95-4	! Magnesium!	12.73 2630	B!	!P_!
	17439-96-5	! Manganese !	48.0		!P_!
	17439-97-6	Mercury	0.20	101	1001
	17440-02-0	Nickel	20.0	U:	!P_!
	17440-09-7	[Potassium]	1330	B:	IP_I
	17782-49-2	Selenium_	1330 1.0	U!	!F_!
	17440-22-4	Silver	3.0	101	!P_!
	17440-23-5	!Sodium!	13400	_ _	!P_!
	17440-28-0	Thallium_	1.0	IUI	!F_!
	17440-62-2	[Vanadium_	4.0	:U:	!P_!
	17440-66-6	IZinc	101	1_1	!P_!
	1	1		_	
	1	1		'_'	
lor Before:	COLORLESS	Clarit	y Before: CLE	AR_	Texture:
lor After:	COLORLESS	Clarit	y After: CLE	AR_	Artifacts:
mments:					



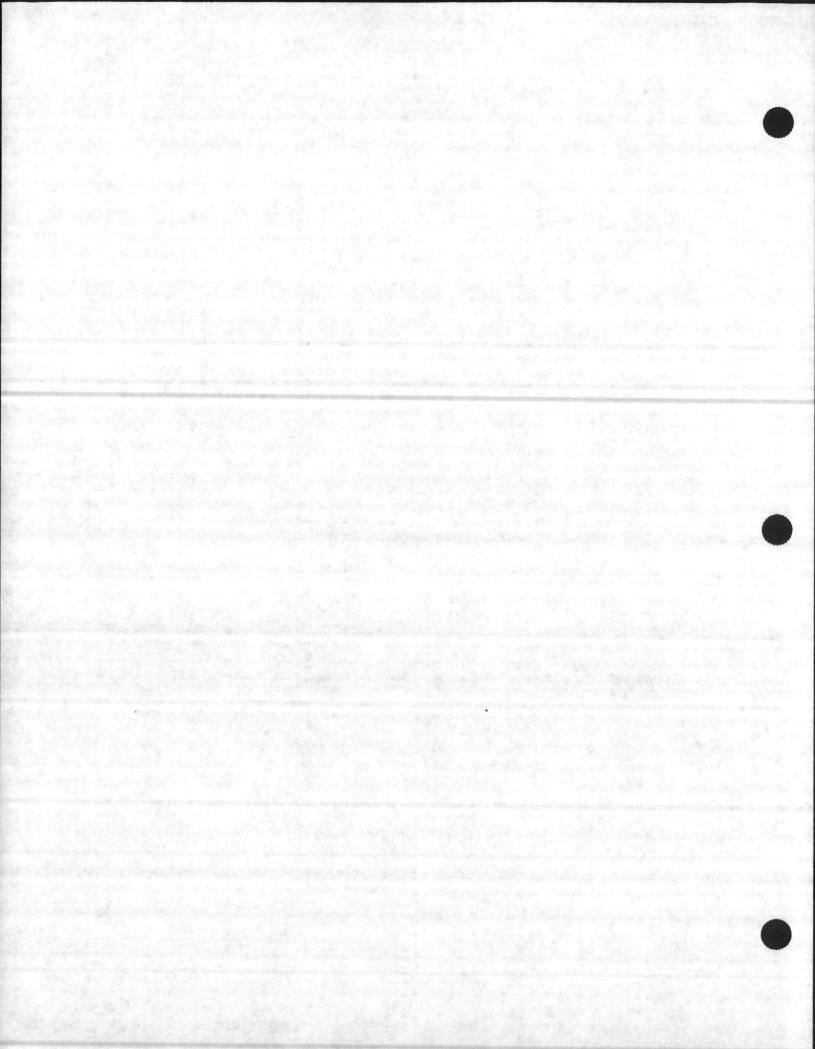
				7-AC
Name: HALL	_IBURTON_NUS		Contract:	
Code: HNUS	6 Ca	se No.: BKHI	SAS No.:	SDG No.: FKG2
trix (soil/w	water): WATE	R	Lab Sam	nple ID: P225120_
vel (low/med	4): LOW_		Date Re	eceived: 02/05/93
Solids:	_0.	0		
r.	ncentration	Units (un/	or mg/kg dry weight	:): UG/L
	I we got the second	1	and grade to Id.	I I
	CAS No.	! Analyte !!	Concentration(C) Q	im i
	7429-90-5	'Aluminum !	8931_1 10.01U1	_ip_i
	17440-36-0	!Antimony !	10.0101	!F_!
	17440-38-2	Arsenic	2.0 B	[F]
	17440-39-3	Barium	2.0 B  10.0 B	TIP_I
	17440-41-7	!Bervllium!	1.0 U  5.0 U  12600 _	IP I
	17440-43-0	!Cadmium !	5.0101	TIP I
	17440-43-7	'Calcium !	12600!	IP I
	17440-47-3	'Cobalt !	8.0!!!	IP I
2 (10 m) 1 (10 m) 1 (10 m)	17440-40-4	'Copper	8.0 U  7.0 B  1580 _  5.0 _  2690 B	IF.
	17440-30-6	Lopper	1580!!	- IP
	17437-67-6	ilron	5.01	- F
	17439-92-1	iLeaoi	3480'B'	Tip-i
	17439-95-4	: Magnesium:	7 O.B.	-(;-)
	1/4.59-96-5	: Mannanese i	/. U.D.	1.1
	17439-97-6	Mercury_	0.20(U)	:CV;
	17440-02-0	Nickel	20.0 U  1500 B	![-:
	17440-09-7	Potassium	1500181	
	17782-49-2	Selenium_	1.0(U)	
	17440-22-4	Silver	3.0 U  14300 _	
	17440-23-5	Sodium	143001_1	!P_!
	17440-28-0	Thallium_	1.0 U	!F!
			4.0101	F
	17440-66-6	Zinc		HONE SECTION (1) 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1
	1	11		
	- F	_!!	1_1	
olor Before:	COLORLESS	Clarit	y Before: CLEAR_	Texture:
olor After:	COLORLESS	Clarit	y After: CLEAR_	Artifacts:
omments:				
-				



ab Name: HALLIBURTON_NUS			INORGANIC AN	1 NALYSES DATA SHEET	EFA SAMPLE NO.
ab Code: HNUS Case No.: BKHD SAS No.: SDG No.: PK atrix (soil/water): WATER					7-AS
Sample ID: P22511   Pate Received: 02/05/	b Name: HA	ALLIBURTON_NUS		Contract:	_ '
Cancentration Units (ug/L or mg/kg dry weight): UG/L_   CAS No.   Analyte   Concentration   C   Q   M	b Code: HN	IUS Ca	se No.: BKHI	SAS No.:	_ SDG No.: PKG2_
Cas No.   Analyte   Concentration   C   Q   M	atrix (soil	/water): WATE	R	Lab Sa	ample ID: P225119_
Cas No.   Analyte   Concentration C  Q   M	evel (low/m	ned): LOW_		Date F	Received: 02/05/93
CAS No.   Analyte   Concentration   C   Q   M     7429-90-5   Aluminum	Solids:	_0.	0		
CAS No.   Analyte   Concentration   C   Q   M		Concentration	Units (ug/l	or mg/kg dry weigh	nt): UG/L_
CAS No.   Analyte   Concentration   C   Q   M		1	1		
		CAS No.	Analyte	Concentration   C  Q	IM I
		17429-90-5	(Aluminum	143 B	IP_I
7440-38-2   Arsenic		17440-36-0	!Antimony !	10.0:0:	iF_i
17440-41-7   Beryllium		17440-38-2	Arsenic	2.0101	IF_I
		17440-39-3	Barium	91.0 B	IP_I
7440-70-2   Calcium		17440-41-7	Bervllium!	1.0:0:	!P_!
7440-70-2   Calcium		17440-43-9	Cadmium	5.0101	IP_I
17440-47-3   Chromium		17440-70-2	Calcium	107001	[P_1
17440-48-4   Cobalt		17440-47-3	!Chromium !	10.0!!!	!P_!
7439-87-6   Iron	No. 4 Tree	17440-48-4	(Cobalt	8.0(U)	IP_I
7439-87-6   Iron	April 10 P. 10 J. 150 A	17440-50-8	!Copper !	37.01 1	!P_!
7440-02-0   Nickel		17439-89-6	Iron !	68701	[P]I
7440-02-0   Nickel		17439-92-1	!Lead !	18.2!	[F_!
7440-02-0   Nickel		17439-95-4	:Magnesium:	2680   B	IP_I
7440-02-0   Nickel		17439-96-5	Manganese	51.0:	IP_I
		17439-97-6	Mercury	0.20(U)	ICV!
		17440-02-0	Nickel	20.0(U)	!P_!
1.0 U		17440-09-7	Potassium	1350   B	IP_I
		17782-49-2	Selenium	1.0:0:	iFi
		17440-22-4	Silver	3.0101	IP_I
		17440-23-5	Sodium	13400   _	IP_I
		17440-28-0	!Thallium !	1.0:0:	!F!
7440-66-6   Zinc				4.0101	IP_I
olor Before: COLORLESS Clarity Before: CLEAR_ Texture:				146 _	
			<u> </u>		
olor After: COLORLESS Clarity After: CLEAR_ Artifacts: _	olor Before	e: COLORLESS	Clarit	y Before: CLEAR_	Texture:
	olor After	COLORLESS	Clarit	y After: CLEAR_	Artifacts:
omments:	omments:				



			IALYSES DATA SHEET	7-0W
Name: HALL	IBURTON_NUS		Contract:	
Code: HNUS	Ca	se No.: BKHD	) SAS No.:	_ SDG No.: PKG2_
trix (soil/w	ater): WATE	R	Lab Sa	ample ID: P225118
vel (low/med	): LOW_		Date F	Received: 02/05/93
Solids:	_0.	0		
Co	ncentration	Units (ug/L	or mg/kg dry weigh	it): UG/L_
	1	<u> </u>	1.1	<del></del>
	ICAS No.	! Analyte !C	Concentration C  Q	IM I
	17429-90-5	!Aluminum !	115 B	IP I
	17440-36-0	!Antimony !	10.0 U	IF_I
	17440-38-2	Arsenic	2.0101	IF_I
	17440-39-3	Barium	91.0 B	IP I
	17440-41-7	!Bervllium!	1.0 B	IP I
	17440-43-9	!Cadmium !	7.01_1	IP I
	17440-70-7	!Calcium !	10500	IP I
	17440-47-3	(Chromium !	10.0101	TIP I
	17440-48-4	!Cohalt !	8.0101	IP I
	17440-50-8	!Copper !	26.01_1	IP I
	17439-89-6	!Iron	75801_1	IP I
	17439-92-1	!Lead !	9.41_1	IF I
	17439-95-4	!Maonesium!	2630 B	IP I
	17439-96-5	!Mannanese!	46.01_1	IF I
	17439-97-6	!Mercury !	0.20101	:CV:
	17440-02-0	!Nickel !	20.0101	IP I
	17440-09-7	!Potassium!	1350 B	IP I
	17782-49-2	Selenium	1.0 U	IF_I
	17440-22-4	Silver	3.0101	IP_I
	17440-23-5	Sodium	132001_1	[P]
	17440-28-0	!Thallium !	1,0 0	IF I
	17440-62-2	[Vanadium ]	4.0101	IP_I
	17440-66-6	(Zinc	1101_1	IP_I
		1		
	1			
lor Before:	COLORLESS	Clarit	y Before: CLEAR_	Texture:
lor After:	COLORLESS	Clarit	y After: CLEAR_	Artifacts:
omments:				





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#### ANALYTICAL REPORT

CUSTOMER:

Baker Environmental

WORK ORDER #: 93-02-097-01

RESULT

FACILITY:

Coraopolis, PA

REPORT TO:

Steve Kretschman

02/04/93 COLLECTED: 02/05/93 RECEIVED:

SAMPLE:

PARAMETER

MCB Camp Lejeune NC 4-AC Grab 2/4/93

METHOD

REPORTED:

ANALYZED

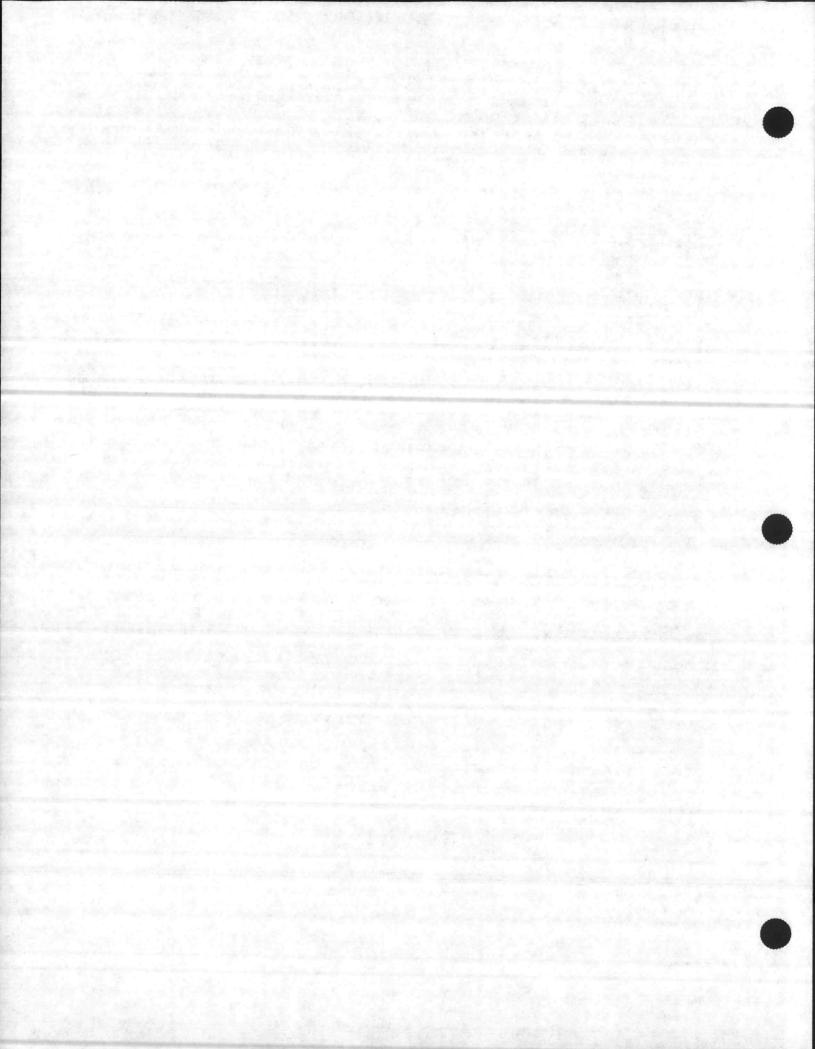
02/15/93

LC50, Fathead 48-Hour

02/08/93 EPA600485013 02/05/93

STARTED

> 100 %





#### ACUTE TOXICITY DATA SHEET Page 2 of 3

9302097-01 Baker Environmental SAMPLE:

4-AC Grab (After Carbon) 2/4

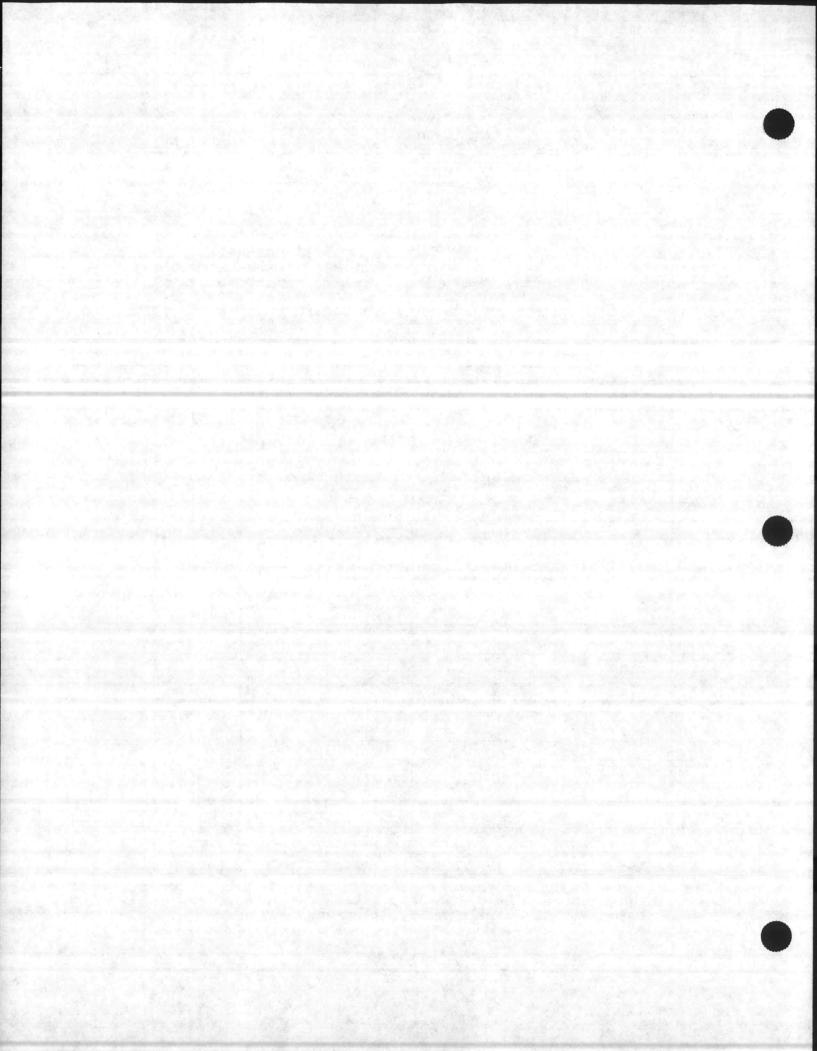
TEST ORGANISM: Pimephales promelas

DATE BEGUN: 2/5/93 TIME BEGUN: 1600 By: arm

1500 DATE ENDED: 2/7/93 TIME ENDED: By: mac

Chamber #	Toxicant %	Total Volume mls	Deaths at 48hrs	D.O. at 48hrs	pH at 48hrs	Other Temp	Other
1	0	200	0	7.5	7.68	25.1	
2	0	200	0				
3	12.5	200	0	7.5	7.74	25.3	
4	12.5	200	0				
5	25	200	0				
6	25	200	0				
7	50	200	1				
8	50	200	1				
9	100	200	0				
10	100	200	2	7.5	7.98	25.9	

Notes: High conc. @ 0 hr.: DO = 8.1 ppm pH = 9.36 Temp. = 25.0 degrees C



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## ACUTE TOXICITY DATA SHEET Page 3 of 3

#### TEST INFORMATION

TEST #: 9302097-01 CLIENT: Baker Environmental

SAMPLE: Baker Environmental

4-AC Grab (After Carbon) 2/4

NPDES #: n/a

TEST ORGANISM: Pimephales promelas

AGE OF TEST ORGANISM: 8 to 11 days of age

TEMPERATURE RANGE: 25 degrees C +/- 1 degree C

TEST TYPE: 48 hour Pimephales promelas acute static

DATE BEGUN: 2/5/93 TIME BEGUN: 1600

DATE ENDED: 2/7/93 TIME ENDED: 1500

END POINT OF TEST: Death or immobility after 48 hours.

### EFFLUENT PARAMETERS

pH: 9.41 CHLORINE: n/a

DISSOLVED OXYGEN: 8.45 ppm

SPECIFIC CONDUCTANCE: 169 micromhos at 25 C

TEMPERATURE: 1.6 degrees C COLOR: colorless

OTHER:

### DILUTION WATER PARAMETERS

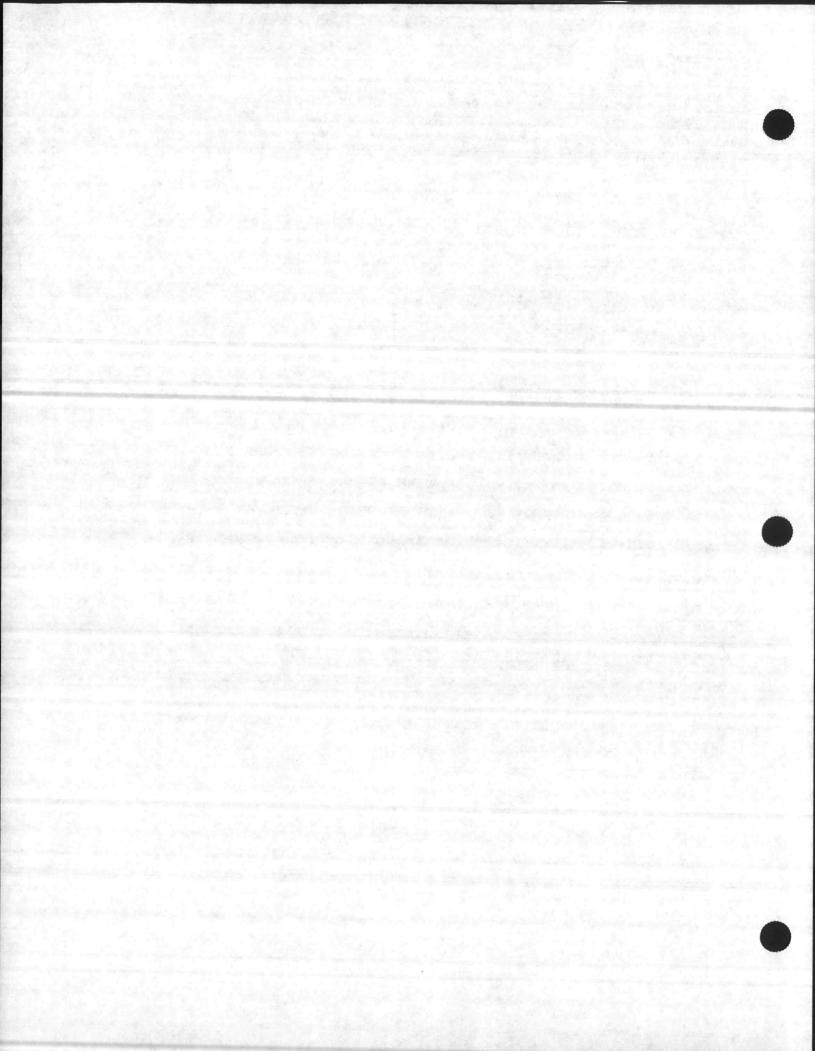
DILUTION WATER: IR-Lake mixture LOT #: 1-25L;2-2I

pH: 7.99 DISSOLVED OXYGEN: 8.65 ppm

SPECIFIC CONDUCTANCE: 159 micromhos at 25 C

HARDNESS: 46 ppm as calcium carbonate

LAST COMPREHENSIVE DILUTION WATER CHEMISTRY: 1/93



# BURLINGTON RESEARCH, INC. TRIMMED SPEARMAN-KARBER METHOD FOR CALCULATION OF EC50 AND LC50 VALUES IN BIOASSAYS

DATE: 2/5/93 THROUGH 2/7/93

WORK ORDER #: 9302097-01

CHEMICAL: Baker Environmental (After carbon)

SPECIES: Pimephales promelas

DURATION: 48 HOURS

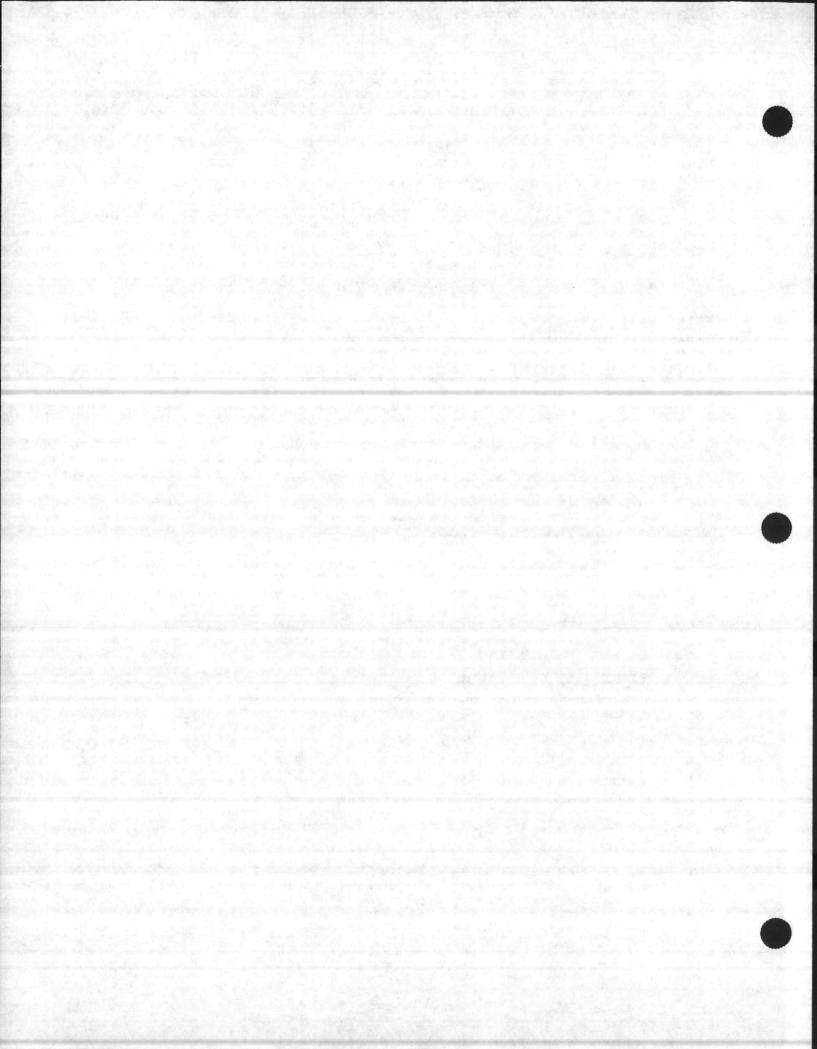
RAW DATA

CONCENTRATION(%) 12.5 25 50 100 1n CONCENTRATION 2.53 3.22 3.91 4.61 NUMBER EXPOSED 20 20 21 20 MORTALITIES 0 0 2 2

The minimum required trim 90.0 is too large. The LC50 IS > 100 %, so SK is not calculable.

#### REFERENCE:

M.A. HAMILTON, R.C. RUSSO, AND R.V. THURSTON. 1977. TRIMMED SPEARMAN-KARBER METHOD FOR ESTIMATING MEDIAN LETHAL CONCENTRATIONS IN TOXICITY BIOASSAYS. ENVIRON. SCI. TECHNOL. 11:714-719; CORRECTION 12:417 (1978).





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#### ANALYTICAL REPORT

CUSTOMER:

Baker Environmental

WORK ORDER #: 93-02-097-02

FACILITY:

REPORT TO:

Coraopolis, PA Steve Kretschman

02/04/93 COLLECTED: RECEIVED:

SAMPLE:

PARAMETER

MCB Camp Lejeune NC 4-AS Grab 2/4/93

METHOD

REPORTED:

ANALYZED

02/05/93 02/15/93

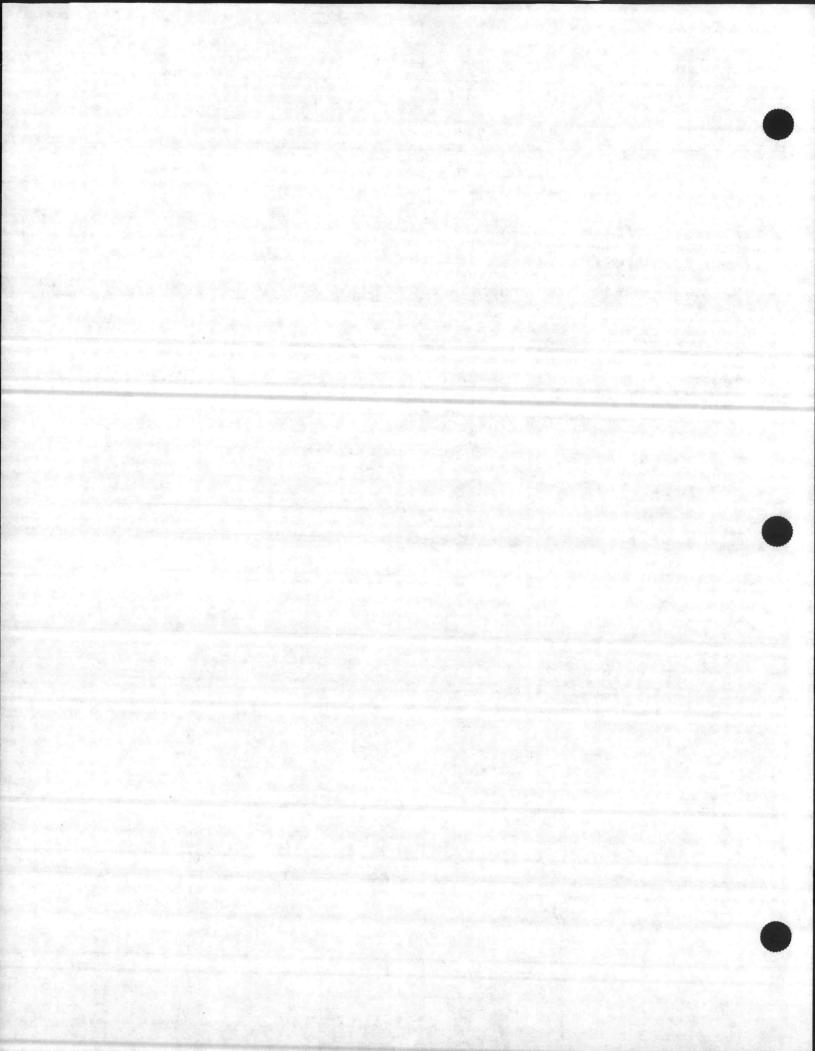
•			
	LC50,	Fathead	48-Hour

02/05/93 02/08/93 EPA600485013

STARTED

> 100 %

RESULT





## ACUTE TOXICITY DATA SHEET Page 1 of 3

TEST #: 9302097-01 SAMPLE: Baker Environmental

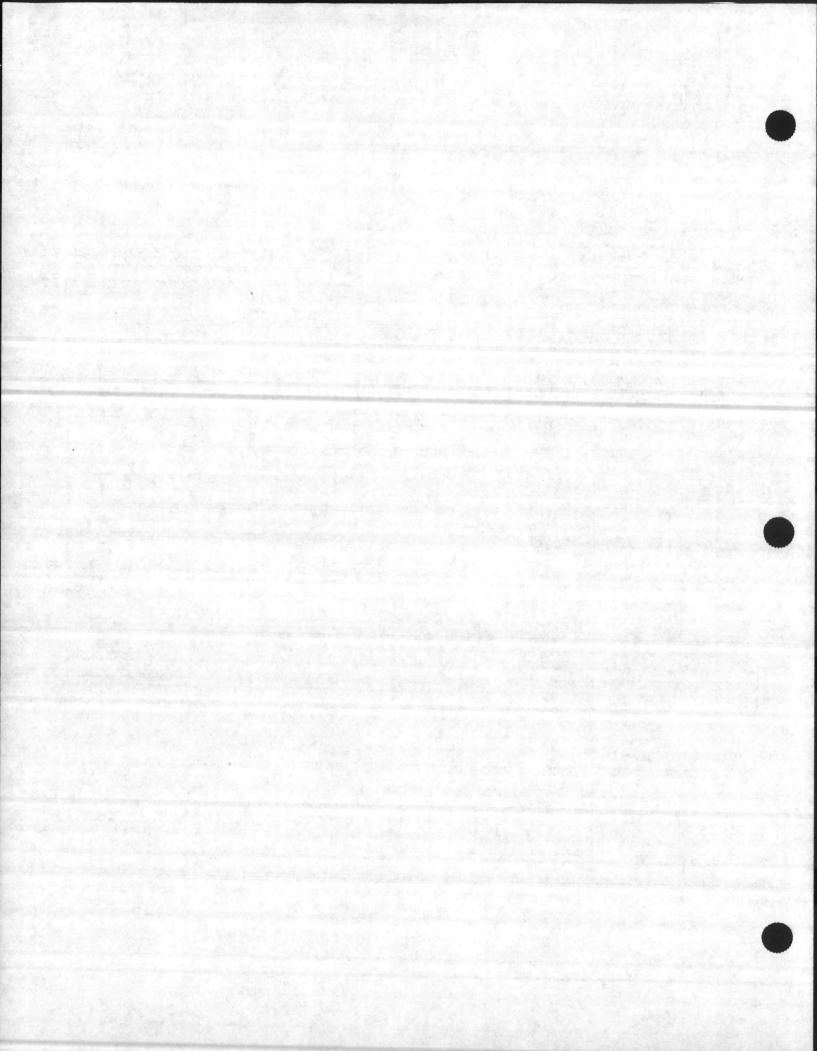
Baker Environmental
4-AC Grab (After Carbon) 2/4

TEST ORGANISM: Pimephales promelas

DATE BEGUN: 2/5/93 TIME BEGUN: 1600 By: arm

DATE ENDED: 2/7/93 TIME ENDED: 1500 By: mac

Chamber #	Toxicant %	Total Volume mls	Volume Dilution mls	Volume Toxicant mls	Volume Transfer mls	# of Organisms	Deaths at 48hrs
1	0	200	200	0	0	10	0
2	0	200	200	0	0	10	0
3	12.5	200	175	25	0	10	0
4	12.5	200	175	25	0	10	0
5	25	200	150	50	0	10	0
6	25	200	150	50	0	10	0
7	50	200	100	100	0	11	1
8	50	200	100	100	0	10	1
9	100	200	0	200	0	10	0
10	100	200	0	200	0	10	2
	Section 200						





#### ACUTE TOXICITY DATA SHEET Page 1 of 3

TEST #: 9302097-02 SAMPLE: Baker Environmental

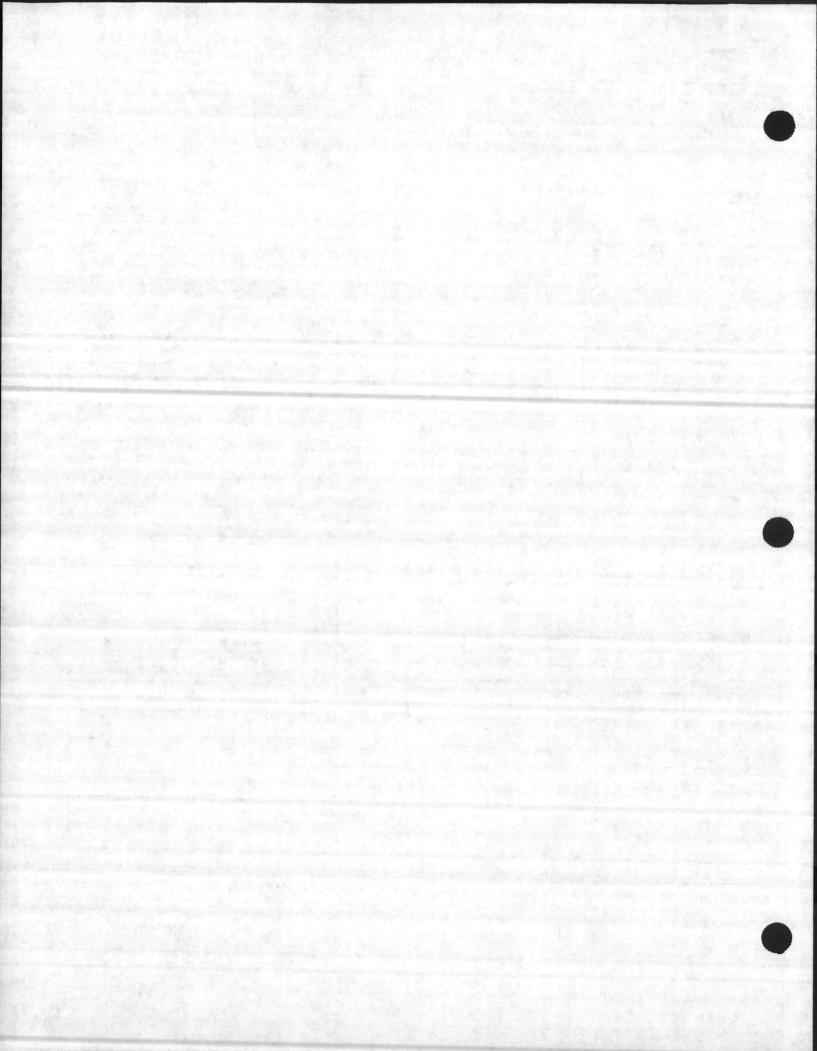
Baker Environmental
4-AS (Air Stripper) Grab 2/4

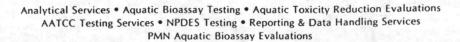
TEST ORGANISM: Pimephales promelas

DATE BEGUN: 2/5/93 TIME BEGUN: 1610 By: dlj

DATE ENDED: 2/7/93 TIME ENDED: 1510 By: mac

Chamber #	Toxicant %	Total Volume mls	Volume Dilution mls	Volume Toxicant mls	Volume Transfer mls	# of Organisms	Deaths at 48hrs
1	0	200	200	0	0	10	0
2	0	200	200	0	0	10	0
3	10	200	180	20	0	10	0
4	10	200	180	20	0	11	1
5	25	200	150	50	0	10	0
6	25	200	150	50	0	10	0
7	50	200	100	100	0	10	0
8	50	200	100	100	0	10	1
9	75	200	50	150	0	10	0
10	75	200	50	150	0	10	0
11	100	200	0	200	0	10	0
12	100	200	0	200	0	10	0
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1							







#### ACUTE TOXICITY DATA SHEET Page 2 of 3

TEST #: 9302097-02 SAMPLE: Baker Environmental

Baker Environmental
4-AS (Air Stripper) Grab 2/4

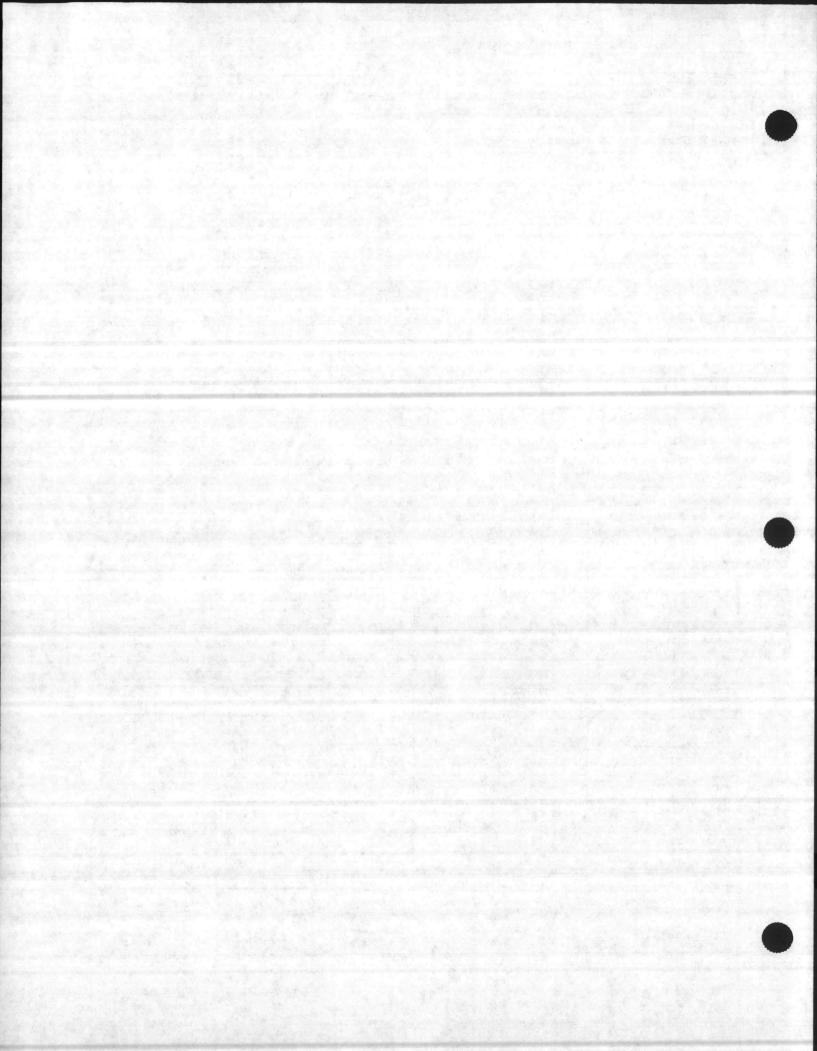
TEST ORGANISM: Pimephales promelas

DATE BEGUN: 2/5/93 TIME BEGUN: 1610 By: dlj

DATE ENDED: 2/7/93 TIME ENDED: 1510 By: mac

Chamber #	Toxicant %	Total Volume mls	Deaths at 48hrs	D.O. at 48hrs	pH at 48hrs	Other Temp	Other
1	0	200	0	7.4	7.85	25.5	
2	0	200	0				
3	10	200	0				
4	10	200	1	7.45	7.78	25.9	
5	25	200	0				
6	25	200	0				4 × 2 × 2 × 2 × 2 × 2 × 2 × 2 × 2 × 2 ×
7	50	200	0				
8	50	200	1				
9	75	200	0				
10	75	200	0		A		
11	100	200	0				4 4
12	100	200	0	7.5	7.64	25.3	
							Transfer
				A Service of Association			

Notes: High conc. @ 0 hr.: DO = 8.1 ppm pH = 7.52 Temp. = 25.0 degrees C



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### ACUTE TOXICITY DATA SHEET Page 3 of 3

#### TEST INFORMATION

TEST #: 9302097-02 CLIENT: Baker Environmental

SAMPLE: Baker Environmental

4-AS (Air Stripper) Grab 2/4

NPDES #: n/a

TEST ORGANISM: Pimephales promelas

AGE OF TEST ORGANISM: 8 to 11 days of age

TEMPERATURE RANGE: 25 degrees C +/- 1 degree C

TEST TYPE: 48 hour Pimephales promelas acute static

DATE BEGUN: 2/5/93 TIME BEGUN: 1610

DATE ENDED: 2/7/93 TIME ENDED: 1510

END POINT OF TEST: Death or immobility after 48 hours.

#### EFFLUENT PARAMETERS

pH: 7.21 CHLORINE: n/a

DISSOLVED OXYGEN: 8.6 ppm

SPECIFIC CONDUCTANCE: 175 micromhos at 25 C

TEMPERATURE: 2.8 degrees C COLOR: yellow-beige

OTHER:

#### DILUTION WATER PARAMETERS

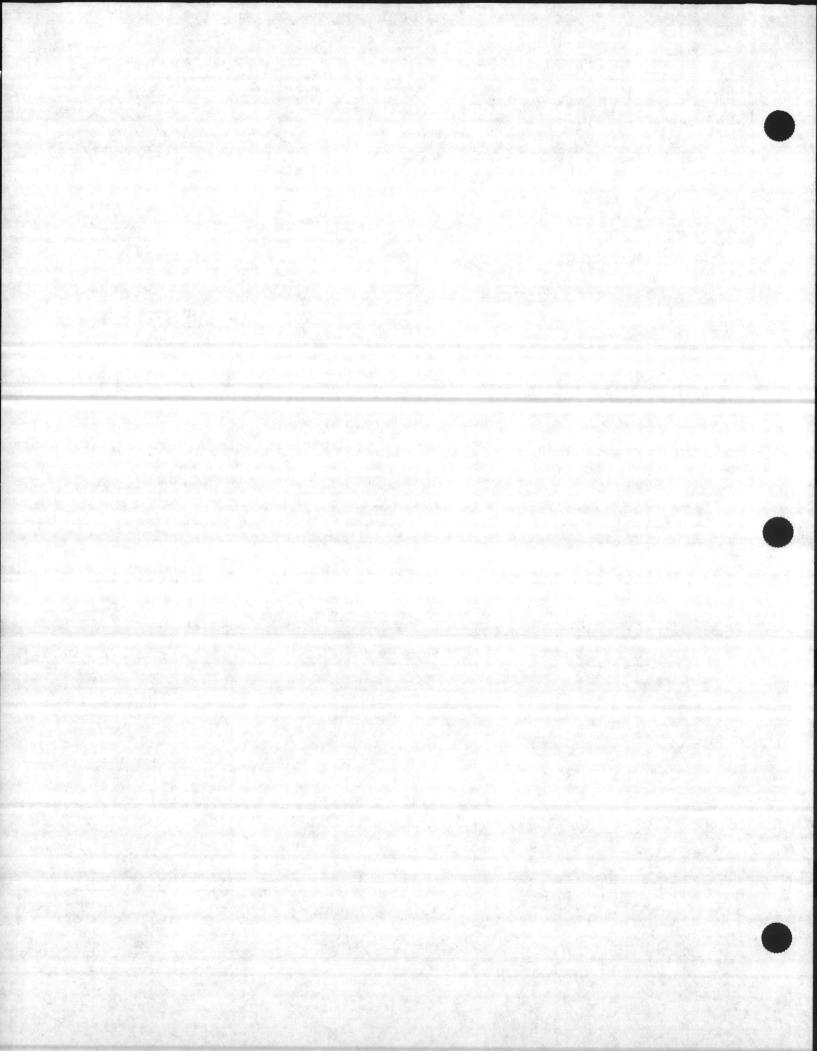
DILUTION WATER: IR-Lake mixture LOT #: 1-25L;2-2I

pH: 7.99 DISSOLVED OXYGEN: 8.4 ppm

SPECIFIC CONDUCTANCE: 159 micromhos at 25 C

HARDNESS: 46 ppm as calcium carbonate

LAST COMPREHENSIVE DILUTION WATER CHEMISTRY: 1/93



# BURLINGTON RESEARCH, INC. TRIMMED SPEARMAN-KARBER METHOD FOR CALCULATION OF EC50 AND LC50 VALUES IN BIOASSAYS

DATE: 2/5/93 THROUGH 2/7/93

WORK ORDER #: 9302097-02

CHEMICAL: Baker Environmental (Air Stripper)

SPECIES: Pimephales promelas

DURATION: 48 HOURS

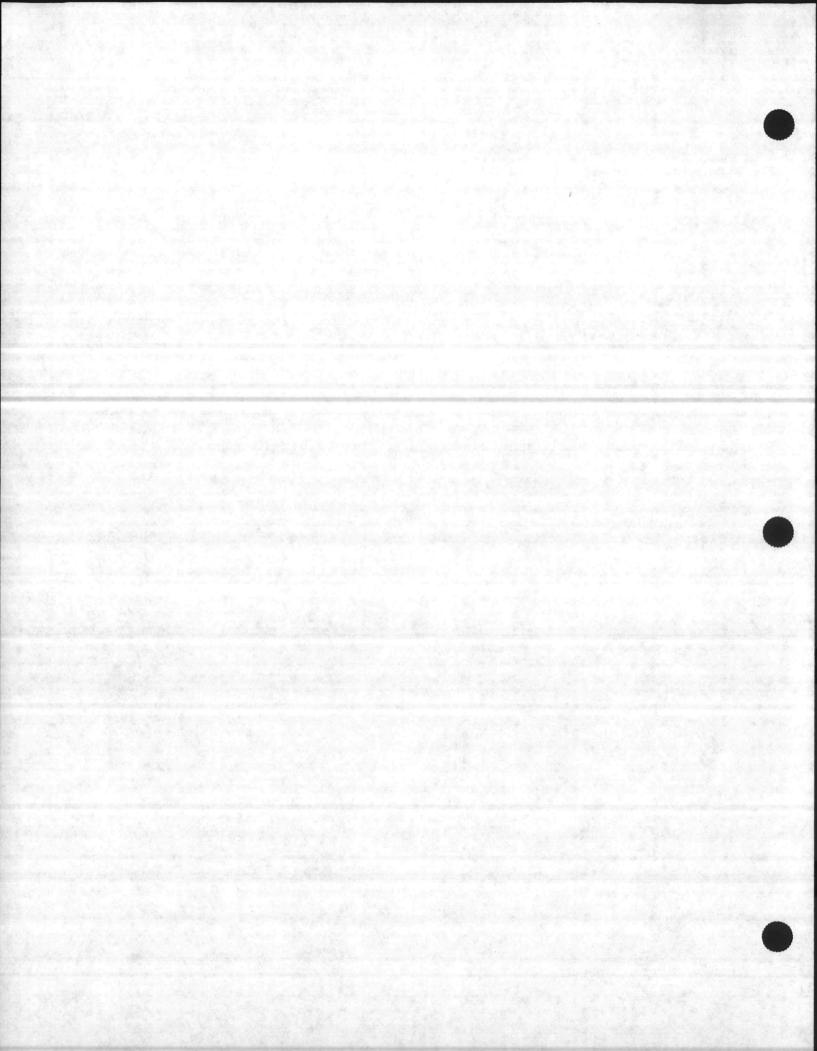
#### RAW DATA

CONCENTRATION( %) 10 25 50 75 100 ln CONCENTRATION 2.30 3.22 3.91 4.32 4.61 NUMBER EXPOSED 21 20 20 20 MORTALITIES 1 0 1 0

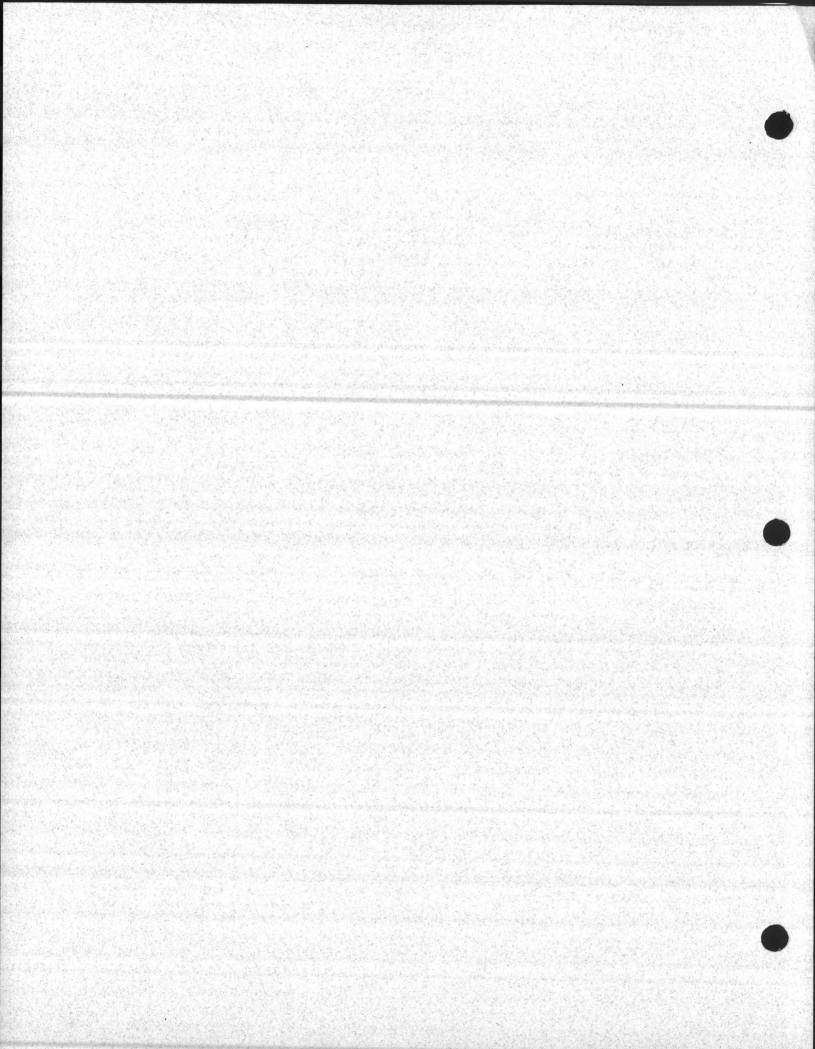
The minimum required trim 98.0 is too large. The LC50 IS > 100 %, so SK is not calculable.

#### REFERENCE:

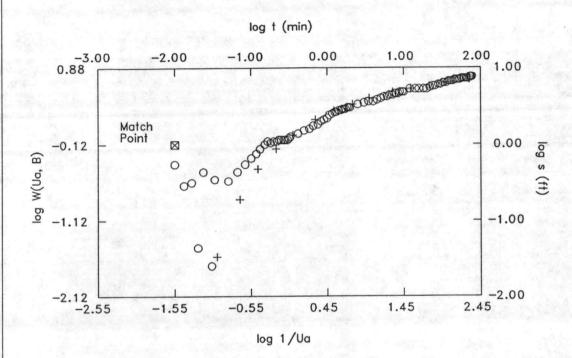
M.A. HAMILTON, R.C. RUSSO, AND R.V. THURSTON. 1977. TRIMMED SPEARMAN-KARBER METHOD FOR ESTIMATING MEDIAN LETHAL CONCENTRATIONS IN TOXICITY BIOASSAYS. ENVIRON. SCI. TECHNOL. 11:714-719; CORRECTION 12:417 (1978).



APPENDIX J AQUIFER TEST RESULTS

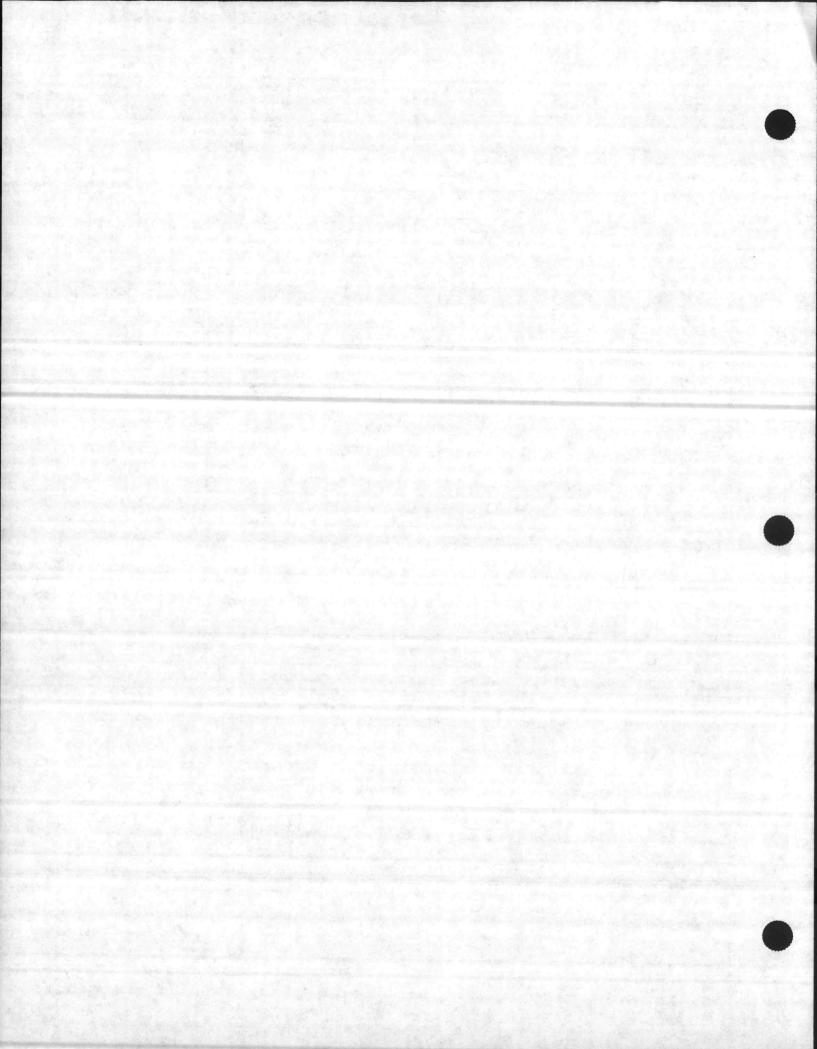




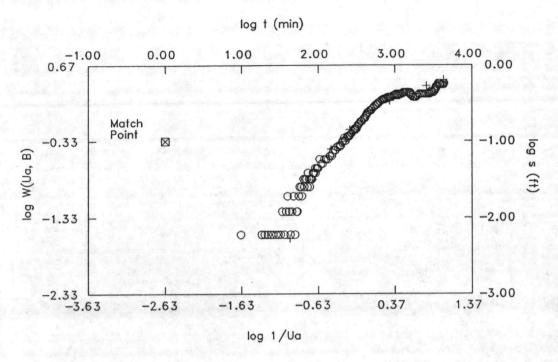


○ - Data
 + - Type Curve
 Unconf. Elastic: beta = 0.001

MA	MATCH POINT		SOL	UTION
t s 1/Ua W(Ua, B)	=	1.000E-0002 1.000E+0000 2.818E-0002 7.586E-0001	Transmissivity (T) Hydraulic Conductivity (K) Storativity (S)	= 1.304E+0002 gpd/ft = 5.215E+0000 gpd/sq ft = 6.872E-0002
			WELL INFORMATION	
WELL IDENTIFICATION  DATE OF AQUIFER TEST  AQUIFER THICKNESS (b)  DISCHARGE RATE (Q)  PUMPING WELL RADIUS (r)  DISTANCE OF OBSERVATION WELL FROM PUMPING WEI			FROM PUMPING WELL (d)	: RW-1 : 1/93 : 2.500E+0001 ft : 1.500E+0000 gpm : 2.500E-0001 ft : 2.500E-0001 ft

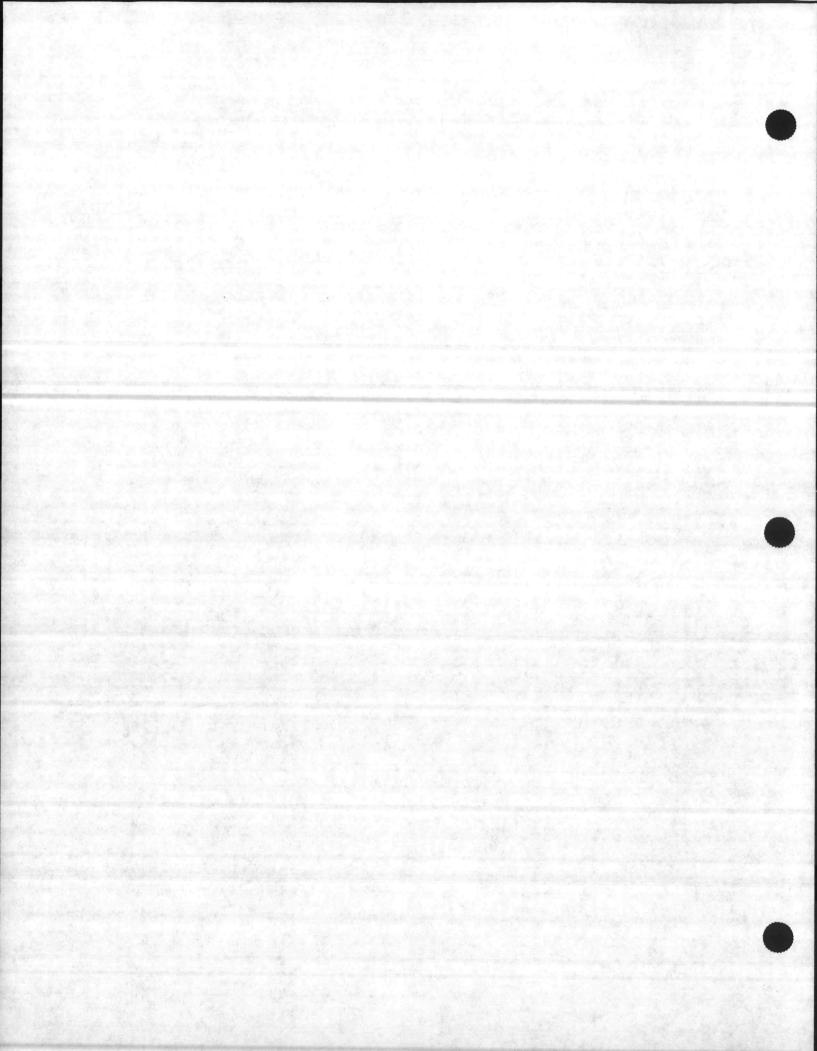




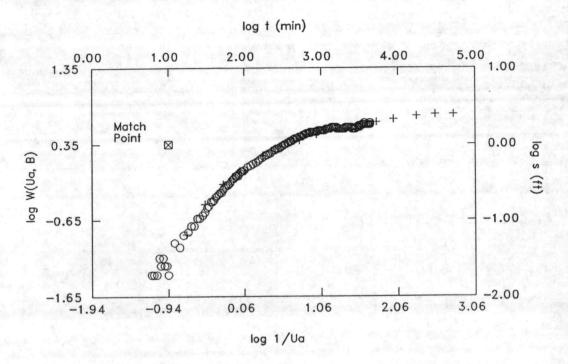


O — Data + — Type Curve Unconf. Elastic: beta = 0.001

MA	TCH I	POINT	SOL	UTION
t s	=	1.000E+0000 1.000E-0001	Transmissivity (T) Hydraulic Conductivity (K)	= 8.038E+0002  gpd/ft = $3.215E+0001 \text{ gpd/sq ft}$
1/Ua W(Ua, B)	=	2.344E-0003 4.677E-0001	Storativity (S)	= 4.061E-0002
11(00, 0)		1.0772 0001	WELL INFORMATION	
WELL IDEN				: P-1
DATE OF AQUIFER TEST AQUIFER THICKNESS (b)				: 1/93 : 2.500E+0001 ft
DISCHARGE RATE (Q)				: 1.500E+0000 gpm
PUMPING WELL RADIUS (r) DISTANCE OF OBSERVATION WELL FROM PUMPING WELL (d)			FROM PUMPING WELL (d)	: 2.500E-0001 ft : 2.800E+0001 ft







MA	TCH	POINT	SOL	UTIC	N
t s 1/Ua W(Ua, B)	=	1.000E+0001 1.000E+0000 1.148E-0001 2.239E+0000	Transmissivity (T) Hydraulic Conductivity (K) Storativity (S)	=	3.847E+0002 gpd/ft 1.539E+0001 gpd/sq ft 8.671E-0004
			WELL INFORMATION		
WELL IDENTIFICATION DATE OF AQUIFER TEST				:	P-2 1/93

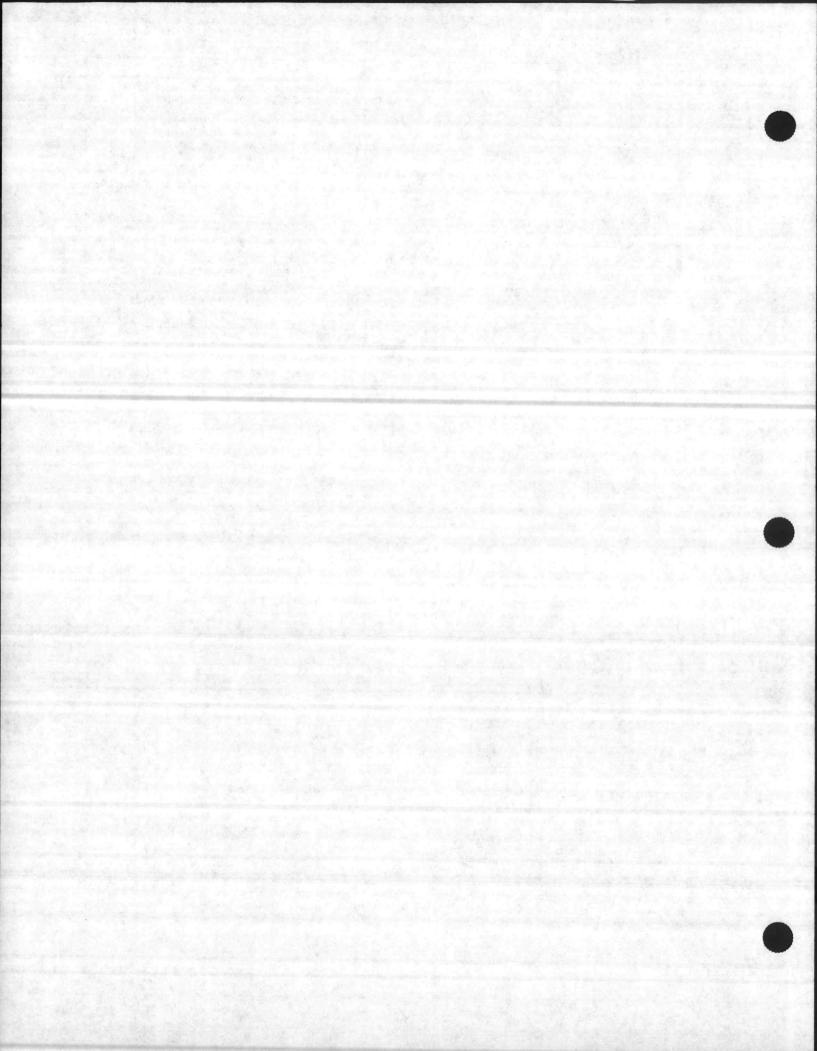
DATE OF AQUIFER TEST : 1/93

AQUIFER THICKNESS (b) : 2.500E+0001 ft

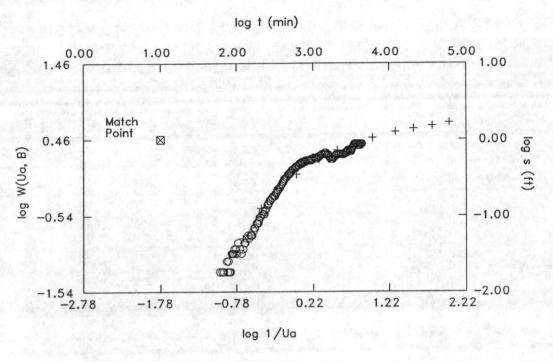
DISCHARGE RATE (Q) : 1.500E+0000 gpm

PUMPING WELL RADIUS (r) : 2.500E-0001 ft

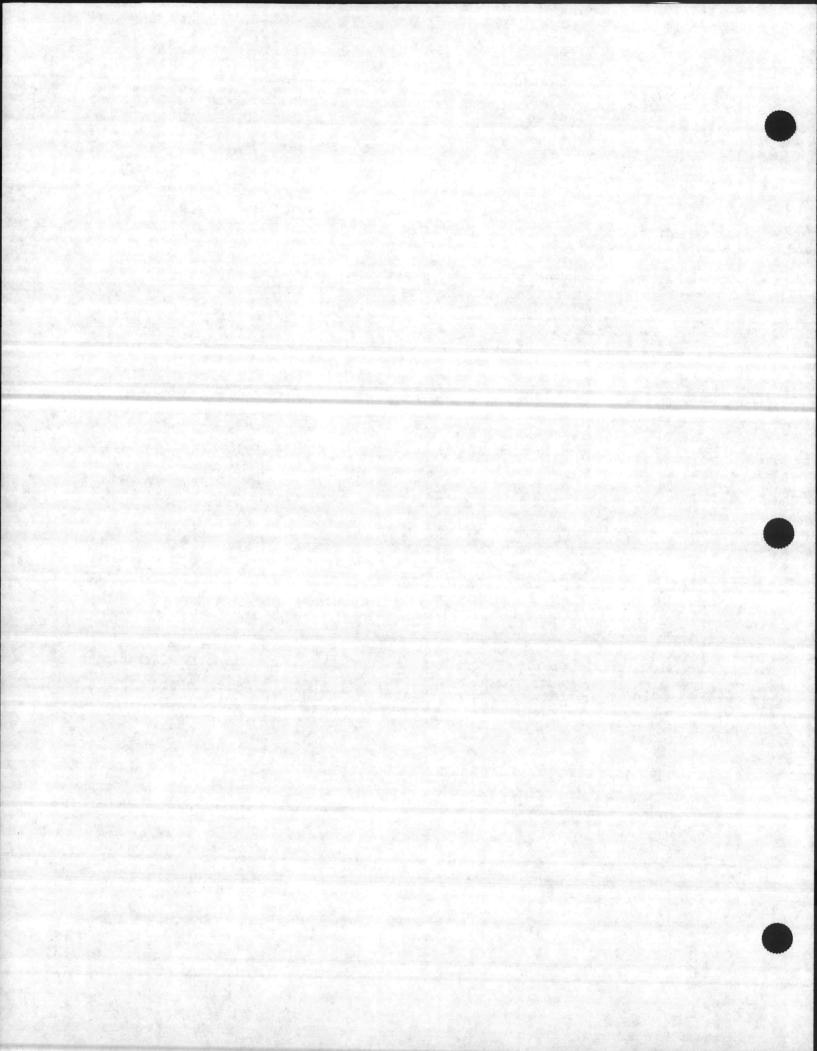
DISTANCE OF OBSERVATION WELL FROM PUMPING WELL (d) : 5.990E+0001 ft



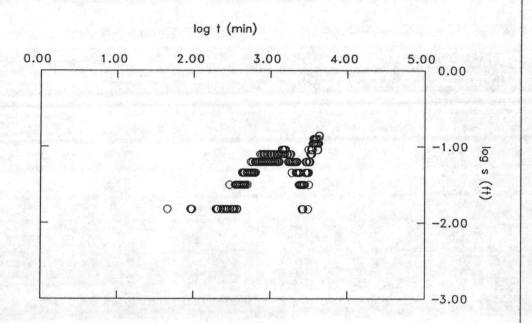




MATCH POINT			SOL	UTION
t s 1 /Ua W(Ua, B)	=	1.000E+0001 1.000E+0000 1.660E-0002 2.884E+0000	Transmissivity (T) Hydraulic Conductivity (K) Storativity (S)	= 4.956E+0002 gpd/ft = 1.983E+0001 gpd/sq ft = 4.891E-0003
148			WELL INFORMATION	
WELL IDENTIFICATION DATE OF AQUIFER TEST AQUIFER THICKNESS (b) DISCHARGE RATE (Q) PUMPING WELL RADIUS (r) DISTANCE OF OBSERVATION WELL FROM PUMPING WELL (d)				: 24-1 : 1/93 : 2.500E+0001 ft : 1.500E+0000 gpm : 2.500E-0001 ft : 7.530E+0001 ft







O - Data

## WELL INFORMATION

WELL IDENTIFICATION : 24-2

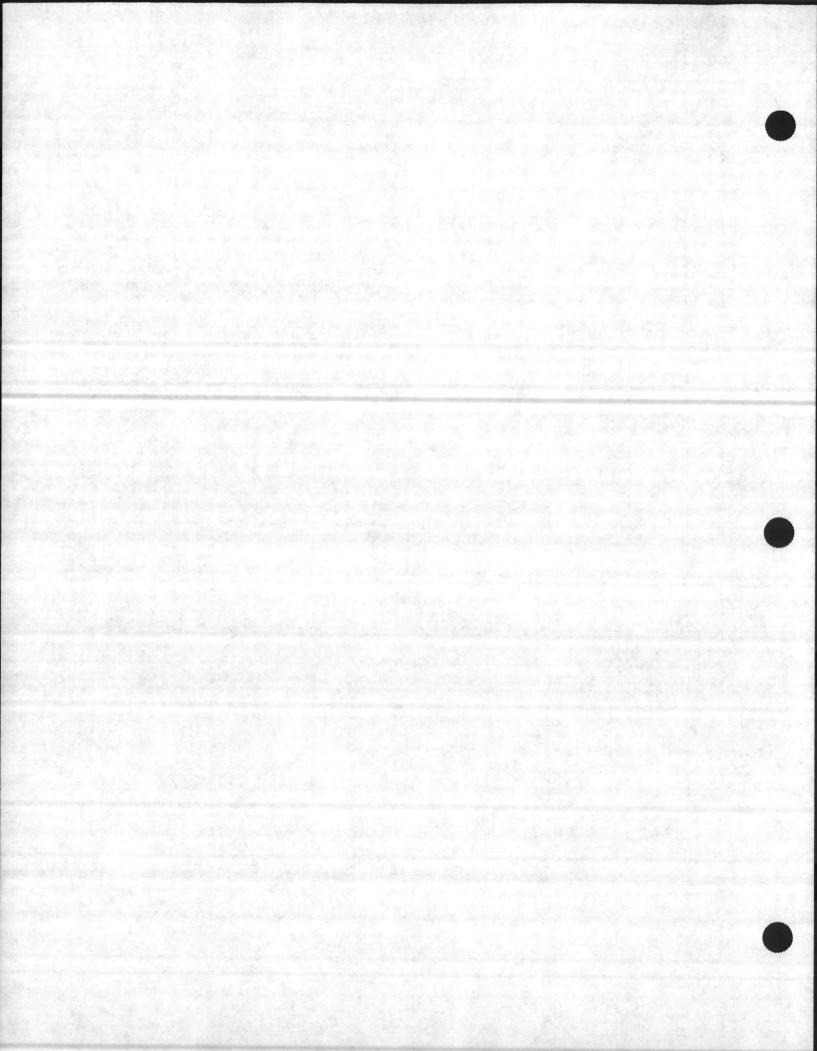
DATE OF AQUIFER TEST : 1/93

AQUIFER THICKNESS (b) : 2.500E+0001 ft

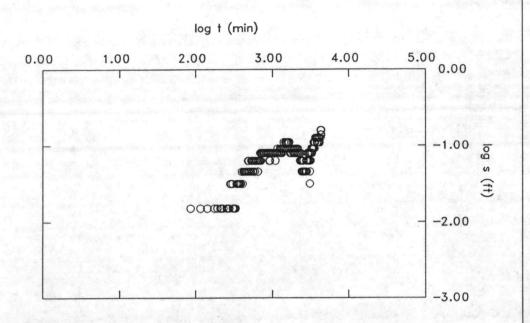
DISCHARGE RATE (Q) : 1.500E+0000 gpm

PUMPING WELL RADIUS (r) : 2.500E-0001 ft

DISTANCE OF OBSERVATION WELL FROM PUMPING WELL (d) : 9.670E+0001 ft

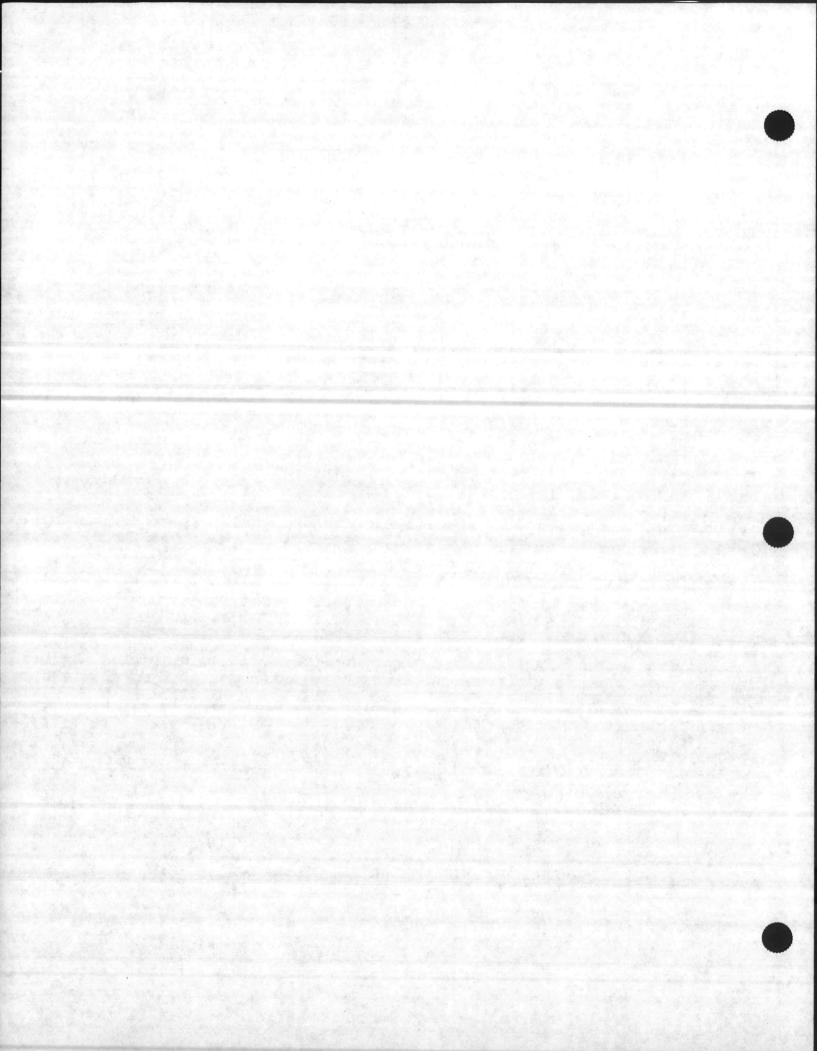




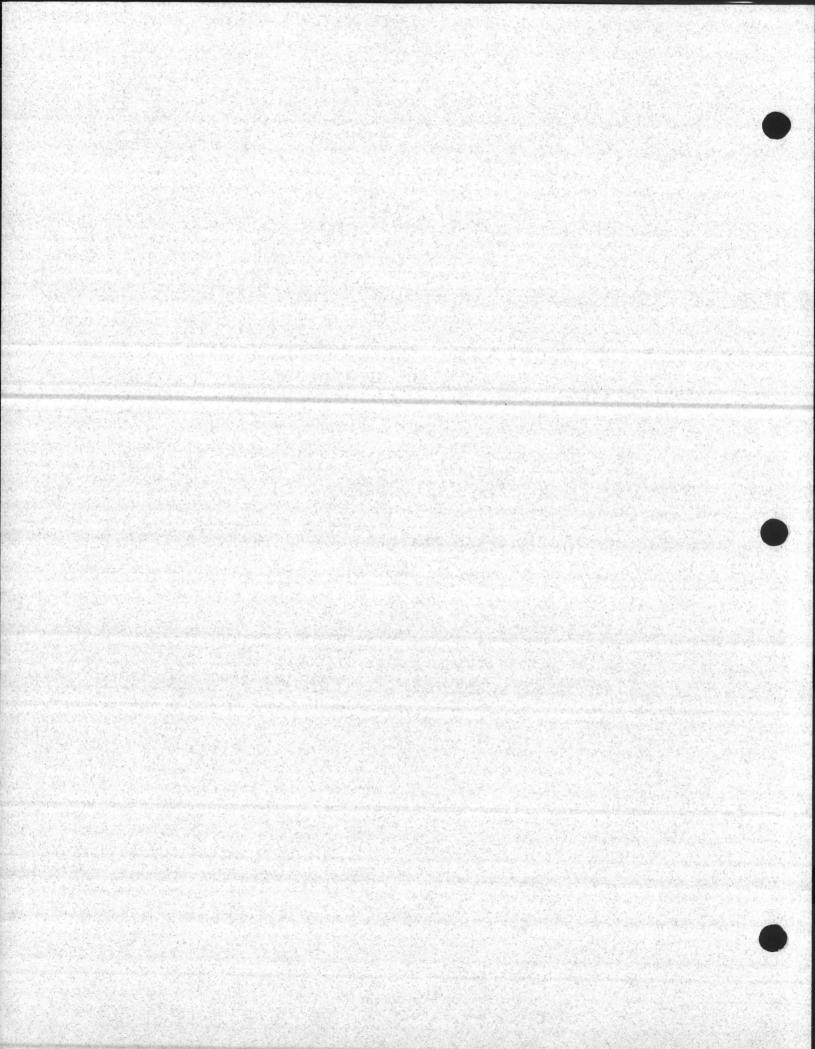


# O - Data

WELL INFORMATION					
WELL IDENTIFICATION	: 24-3				
DATE OF AQUIFER TEST	: 1/93				
AQUIFER THICKNESS (b)	: 2.500E+0001 ft				
DISCHARGE RATE (Q)	: 1.500E+0000 gpm				
PUMPING WELL RADIUS (r)	: 2.500E-0001 ft				
DISTANCE OF OBSERVATION WELL FROM PUMPING WELL (d)	: 1.187E+0002 ft				



APPENDIX K
PILOT-SCALE TREATABILITY STUDY ANALYTICAL
RESULTS - QA/QC





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#### LABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

420 ROUSER ROAD ADDRESS:

CORAOPOLIS, PA 15108-

MR. JOHN LOVELY ATTENTION:

Carbon Copy:

SAMPLE ID: 8-0M

NUS SAMPLE NO: P0225115

P.O. NO.: CTO # 19017

NUS CLIENT NO: 1600 0006 WORK ORDER NO: 55830

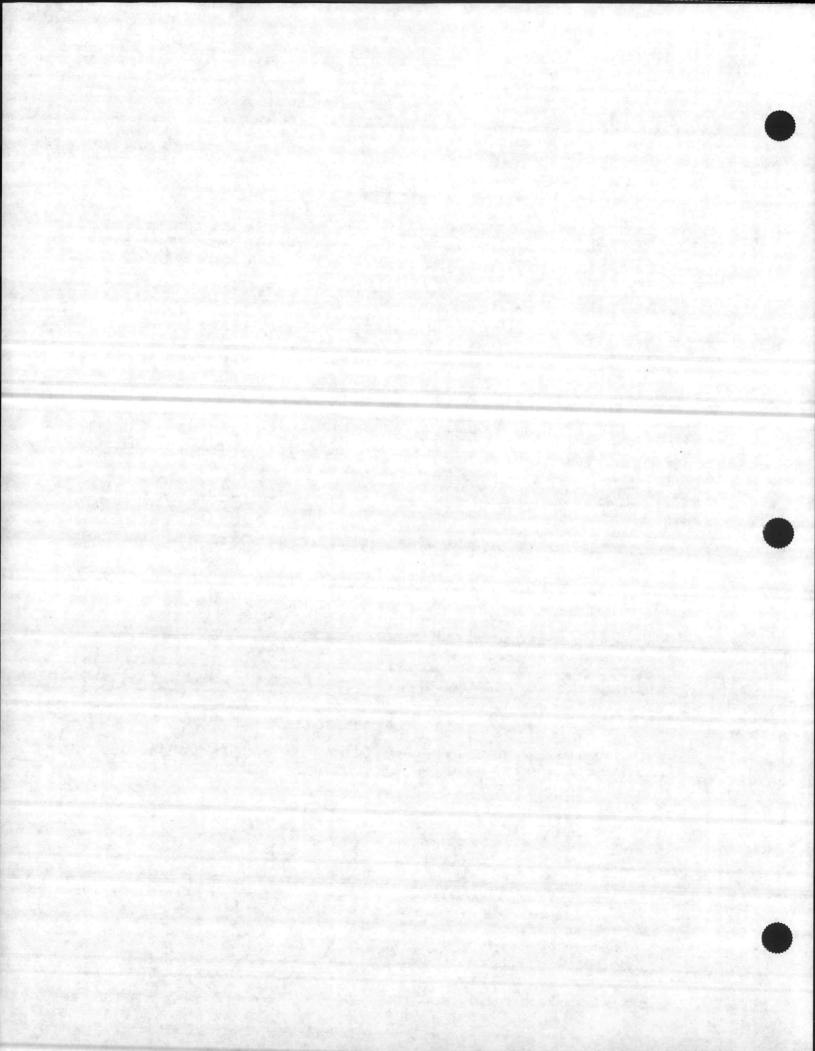
VENDOR NO:

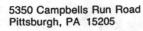
DATE SAMPLED: 05-FEB-93 DATE RECEIVED: 06-FEB-93

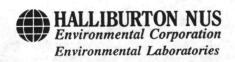
APPROVED BY:

Joanne Simanic

LN	TEST CODE	DETERMINATION	RESULT	UNITS
			DOME	
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
		1,2-dimethylbenzene [o-xylene]	4	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	< 2	ug/L
		benzene	3	ug/L
		ethylbenzene	2	ug/L
		methylbenzene [toluene]	9	ug/L
5	G100W	PURGEABLE HALOCARBONS		
		1,1,1-trichloroethane	< 2	ug/L
		1.1.2.2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1.1-dichloroethene [1.1-dichloroethylene]	3	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/l
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L







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# LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: 8-0W NUS SAMPLE NO: P0225115

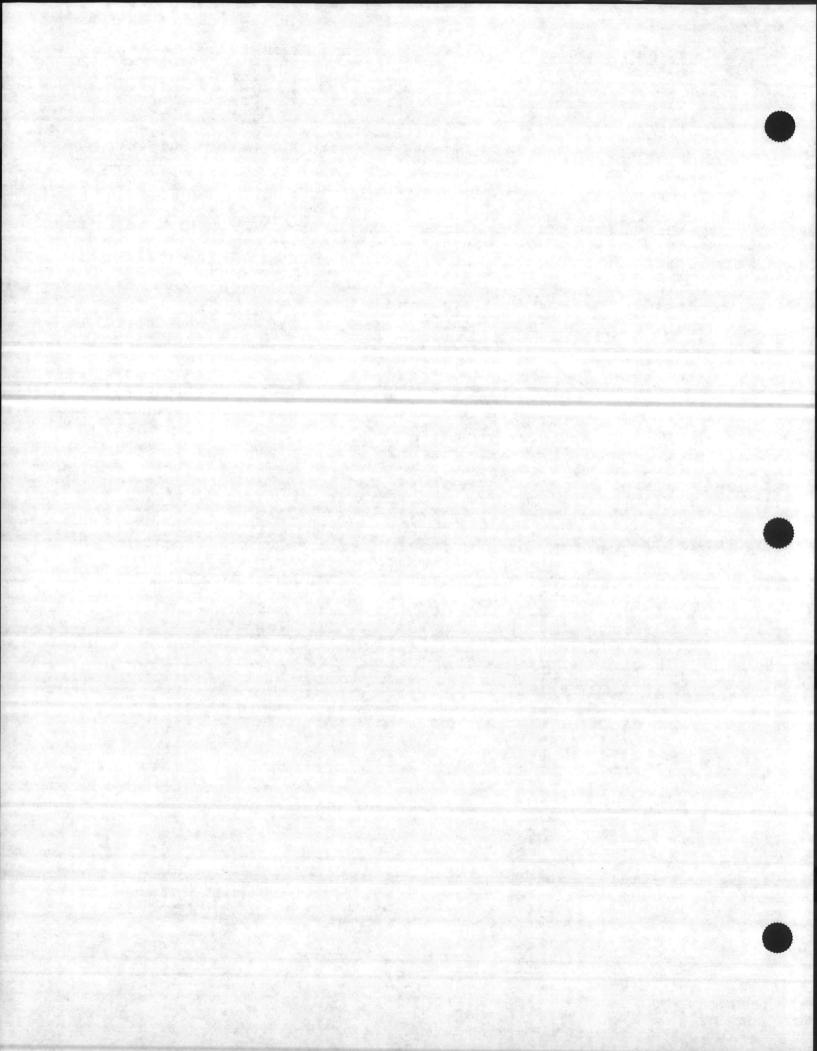
LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 40 D	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	180 D	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	340 D :	ug/L

#### COMMENTS:

In the BTEX analysis, m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.

Sample number P225115 exhibited high surrogate recoveries in both the primary and confirmational analyses. The high surrogate recoveries were due to a matrix interference. The matrix interference also interferred with the confirmation of benzene. The benzene result from the primary analysis is reported. M/P-xylene was not observed in the confirmational analysis. The m/p-xylene result observed in the primary analysis was not reported.

"D" indicates that the result was obtained from an analysis performed at a secondary dilution.





MR. JOHN LOVELY

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#### LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN NUS CLIENT NO: 1600 0006

ADDRESS: 420 ROUSER ROAD WORK ORDER NO: 55830

CORAOPOLIS, PA 15108- VENDOR NO:

Carbon Copy:

ATTENTION:

SAMPLE ID: 8-AS

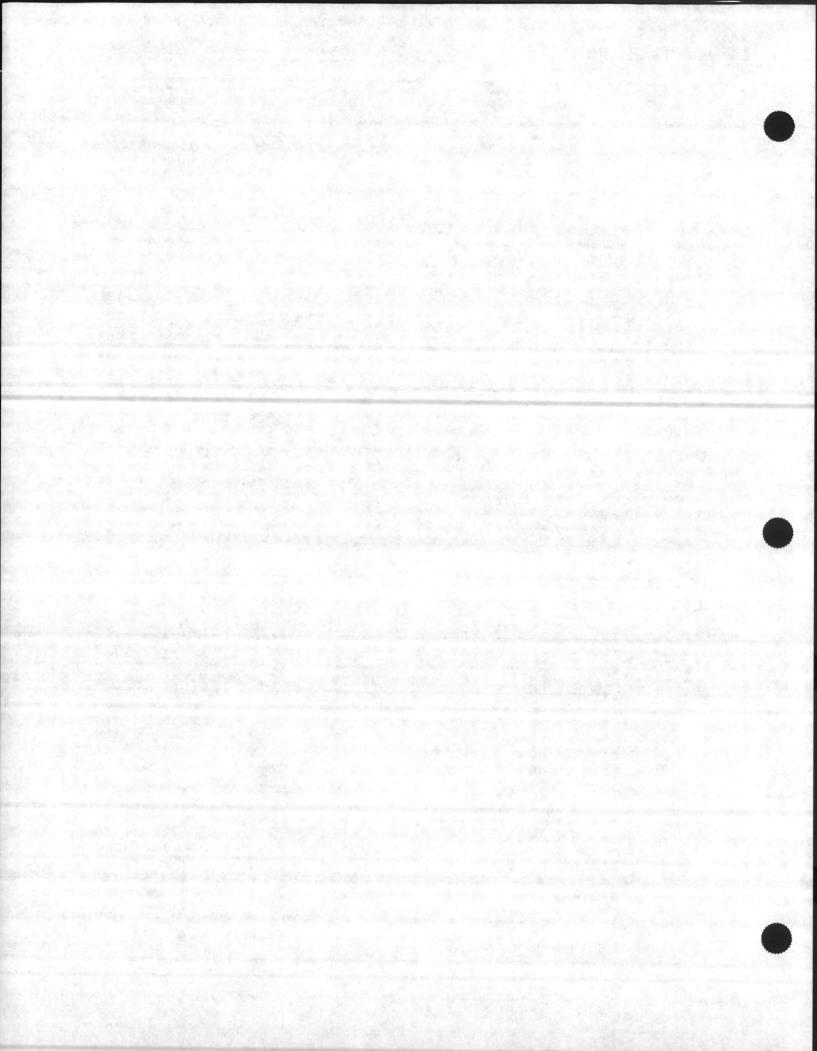
DATE SAMPLED: 05-FEB-93

NUS SAMPLE NO: P0225116

DATE RECEIVED: 06-FEB-93

P.O. NO.: CTO # 19017 APPROVED BY: Joanne Simanic

LN	CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
	0.0711	1,2-dimethylbenzene [o-xylene]	5	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	10	ug/L
		benzene	2	ug/L
		ethylbenzene	13	ug/L
		methylbenzene [toluene]	13	ug/L
5	G100W	PURGEABLE HALOCARBONS		
		1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/l
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/l
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/l
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L





5350 Campbells Run Road Pittsburgh, PA 15205 900 Gemini Avenue Houston, TX 77058

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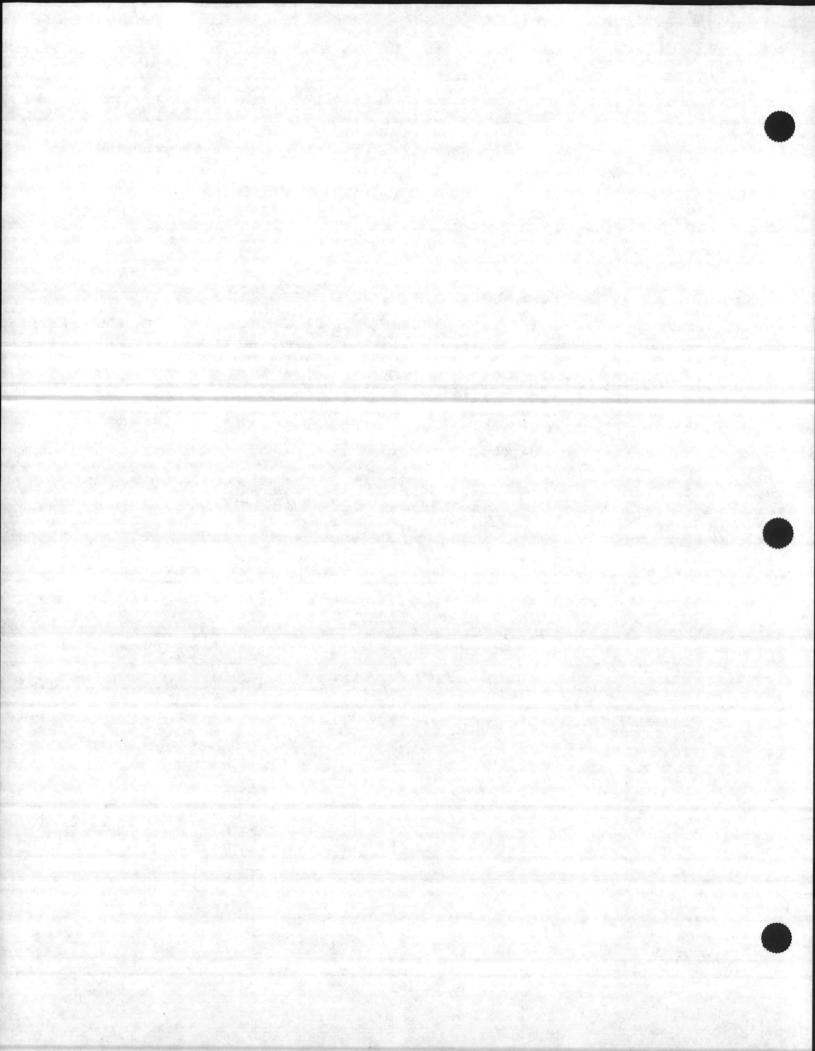
## LABORATORY ANALYSIS REPORT

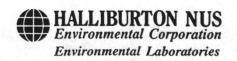
CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: 8-AS NUS SAMPLE NO: P0225116

LN	CODE	DETERMINATION	RESULT	UNITS
		tetrachloroethene [tetrachloroethylene]	< 2	uq/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.





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#### LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN NUS CLIENT NO: 1600 0006

ADDRESS: 420 ROUSER ROAD WORK ORDER NO: 55830

CORAOPOLIS, PA 15108- VENDOR NO:

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: 8-AC

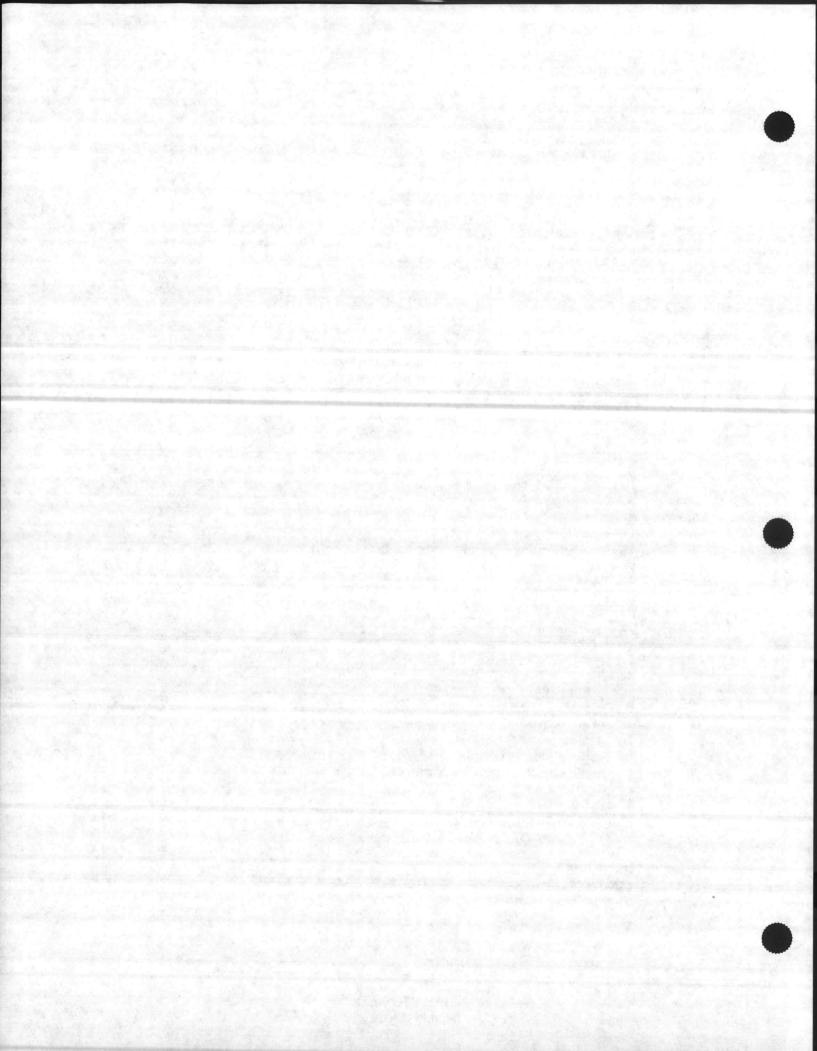
NUS SAMPLE NO: P0225117

DATE SAMPLED: 05-FEB-93

DATE RECEIVED: 06-FEB-93

P.O. NO.: CTO \* 19017 APPROVED BY: Joanne Simanic

LN	CODE	DETERMINATION	RESULT	UNITS
1	ACLPW	TAL METALS & CLP DATA PACKAGE	DONE	
2	DPACK	CLP Data Package Deliverable	DONE	
3	G107W	BTEX PACKAGE		
		1,2-dimethylbenzene [o-xylene]	< 2	ug/L
		1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	< 2	ug/L
		benzene	< 2	ug/L
		ethylbenzene	3	ug/L
		methylbenzene [toluene]	4	ug/L
5	G100W	PURGEABLE HALOCARBONS		
1. 190.0		1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L



5350 Campbells Run Road

900 Gemini Avenue Houston, TX 77058



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#### LABORATORY ANALYSIS REPORT

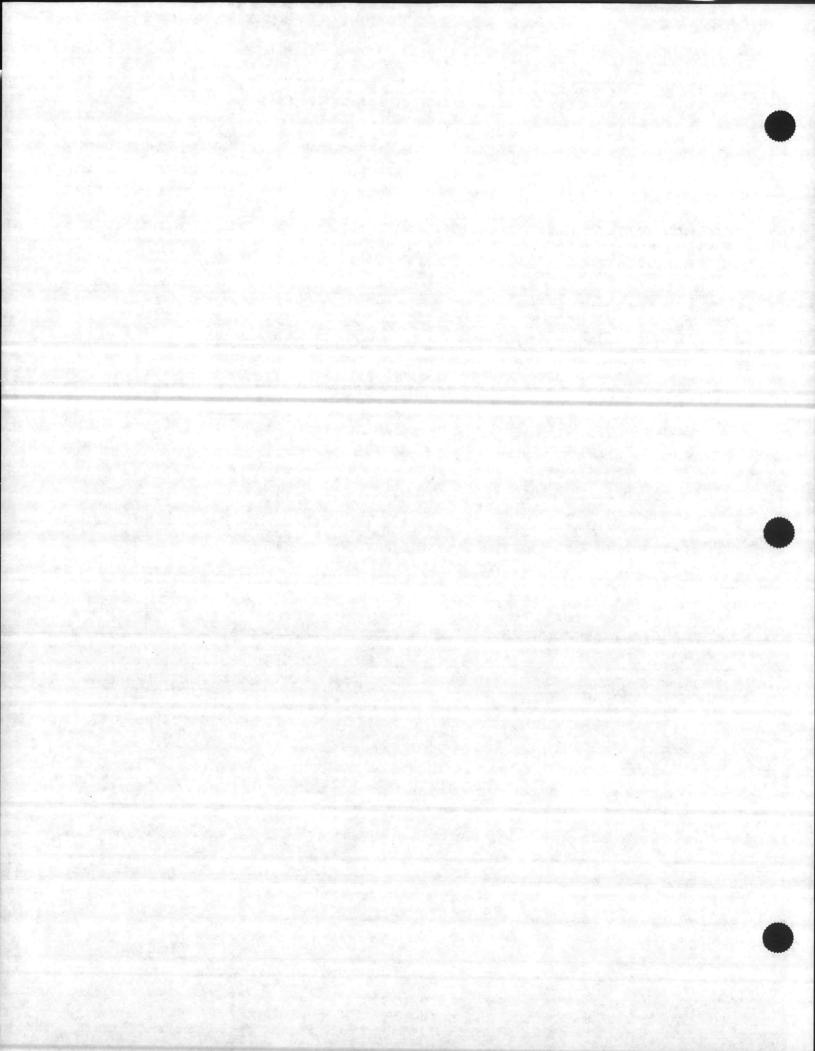
BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: 8-AC NUS SAMPLE NO: P0225117

	TEST			
LN	CODE	DETERMINATION	RESULT	UNITS
de region				
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column.

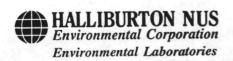
For sample number P225117, benzene and toluene were not observed in the confirmational analysis. The benzene and toluene results observed in the primary analysis were not reported. A low surrogate recovery was observed for this sample in both the primary and confirmational analyses. The low surrogate recoveries were proabably due to the matrix.



05-FEB-93

06-FEB-93

Joanne Simanic



February 23, 1993 Report No.: 00013686 Section A Page 20

## LABORATORY ANALYSIS REPORT

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN CLIENT NAME:

420 ROUSER ROAD ADDRESS:

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

TB SAMPLE ID:

P0225114 NUS SAMPLE NO:

NUS CLIENT NO: 1600 0006

WORK ORDER NO: 55830

VENDOR NO:

DATE SAMPLED:

DATE RECEIVED:

APPROVED BY:

	Р.	0. NO.:	СТО # 19017		
	LN	TEST CODE	DETERMINATION	RESULT	UNITS
			CLD Data Daskara Daliusaahla	DONE	
	2	DPACK	CLP Data Package Deliverable		
	3	G107W	BTEX PACKAGE	13	ug/L
			1,2-dimethylbenzene [o-xylene]	2	ug/L
			1,3-dimethylbenzene, 1,4-dimethylbenzene [m-/p-xylenes]	< 2	ug/L
-			benzene	< 2	ug/L
			ethylbenzene methylbenzene [toluene]	6	ug/L
	5	G100W	PURGEABLE HALOCARBONS		
			1,1,1-trichloroethane	< 2	ug/L
			1,1,2,2-tetrachloroethane	< 2	ug/L
			1,1,2-trichloroethane	< 2	ug/L
			1,1-dichloroethane	< 2	ug/L
			1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
			1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
			1,2-dichloroethane	< 2	ug/L
			1,2-dichloropropane	< 2	ug/L
			1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
			1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
			2-chloroethylvinyl ether	< 2	ug/L
			bromodichloromethane [dichlorobromomethane]	< 2	ug/L
			bromomethane [methyl bromide]	< 2	ug/L
			carbon tetrachloride	< 2	ug/L
			chlorobenzene	< 2	ug/L
				< 2	ug/L
			chloroethane	< 2	ug/L
			chloroform	< 2	ug/L
			chloromethane [methyl chloride]	< 2	ug/L
			cis-1,3-dichloropropene	< 2	ug/L
			dibromochloromethane	()	na/l

dichlorodifluoromethane

dichloromethane [methylene chloride]

tetrachloroethene [tetrachloroethylene]

ug/L

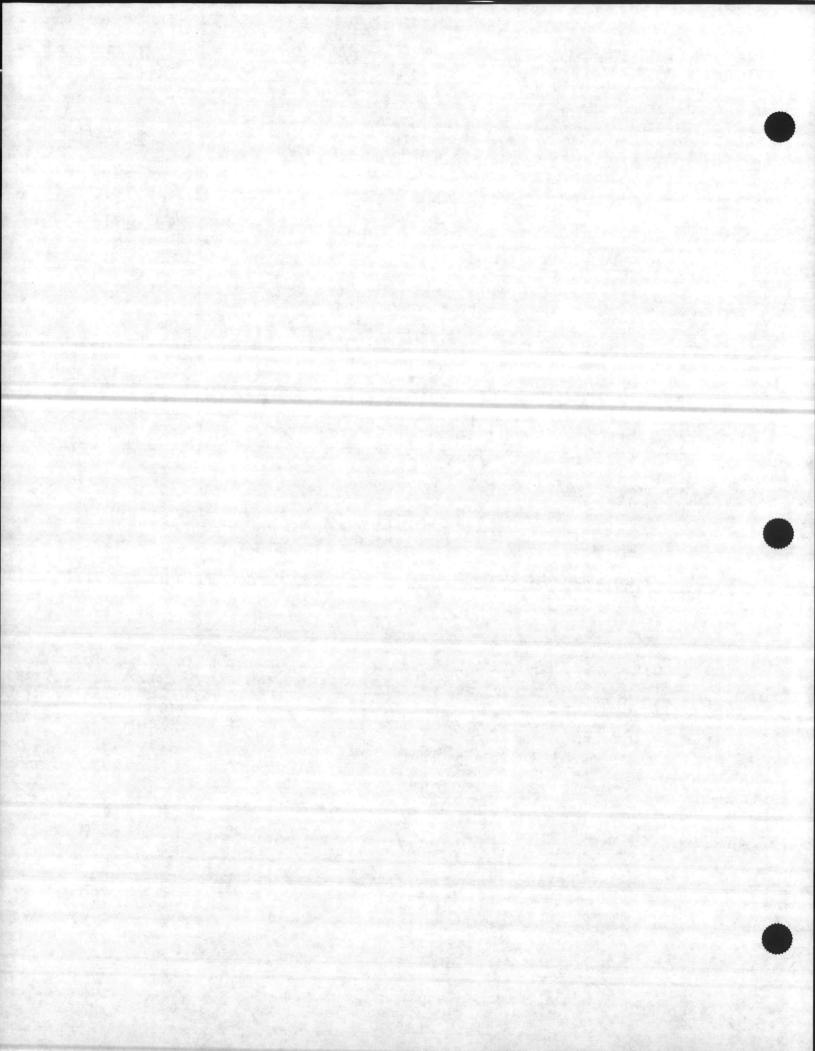
ug/L

ug/L

< 2

< 5

< 2





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## LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

SAMPLE ID: TB
NUS SAMPLE NO: P0225114

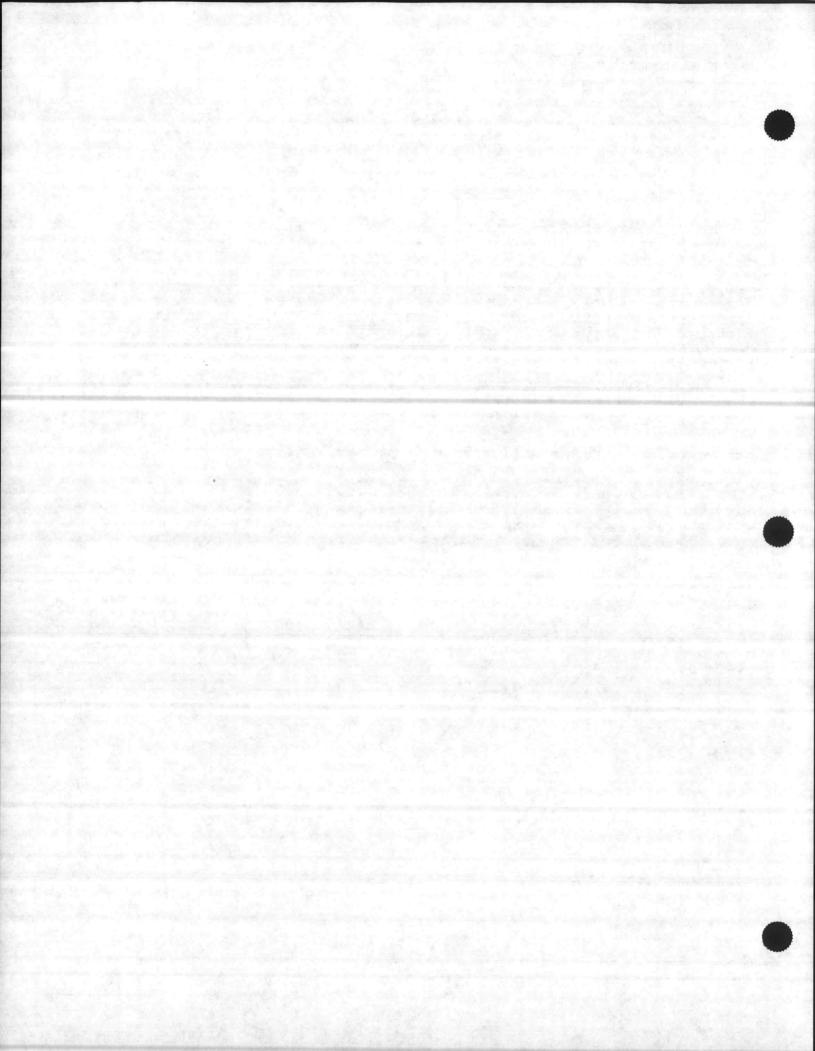
LN	CODE	DETERMINATION	RESULT	UNITS
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column.

The concentration reported represents the sum of the two isomers.

For sample P225114, o-xylene and m/p-xylenes were not observed in the confirmational analysis. The results for these compounds observed in the

primary analysis were not reported.



1600 0006

55830



February 23, 1993 Report No.: 00013686 Section A Page 53

NUS CLIENT NO:

WORK ORDER NO:

VENDOR NO:

# LABORATORY ANALYSIS REPORT

CLIENT NAME: BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS: 420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION: MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID: TRIP 1

NUS SAMPLE NO: P0225131

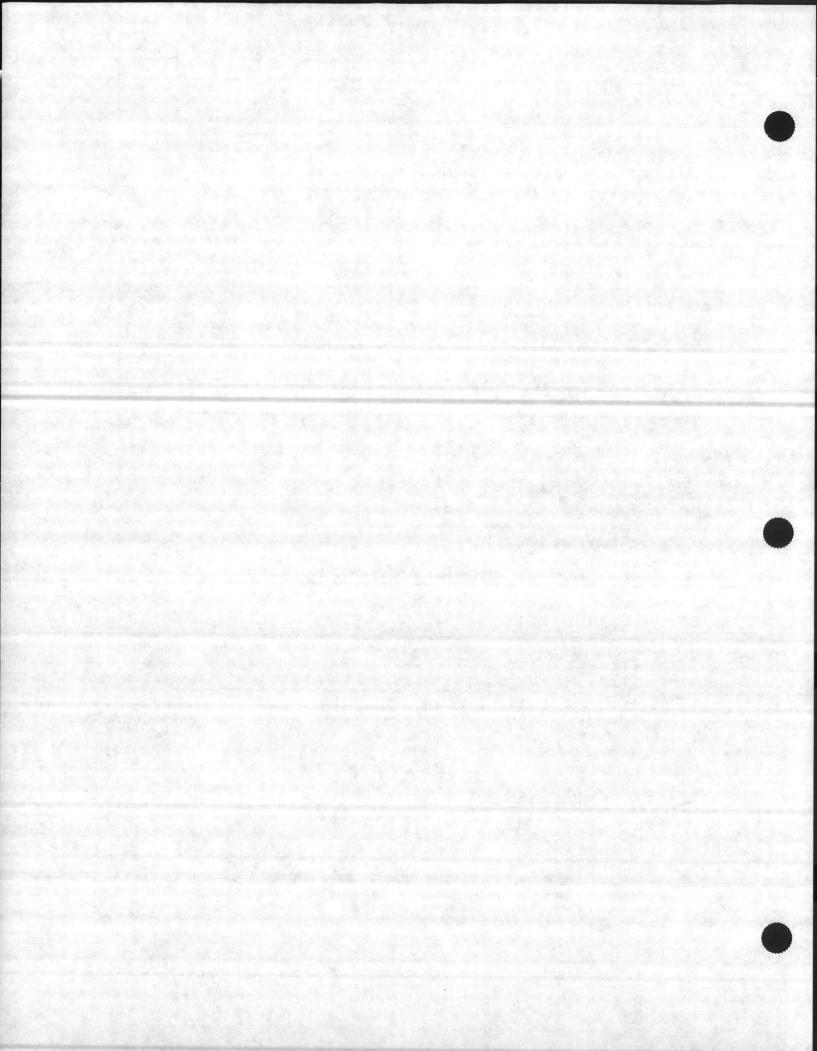
P.O. NO.: CTO # 19017

DATE SAMPLED: UnAvail

DATE RECEIVED: 06-FEB-93

APPROVED BY: Joanne Simanic

<u>LN</u>	CODE	DETERMINATION	RESULT	UNITS
2	DPACK	CLP Data Package Deliverable	DONE	
5	G100W	PURGEABLE HALOCARBONS		
		1,1,1-trichloroethane	< 2	ug/L
		1,1,2,2-tetrachloroethane	< 2	ug/L
		1,1,2-trichloroethane	< 2	ug/L
		1,1-dichloroethane	< 2	ug/L
		1,1-dichloroethene [1,1-dichloroethylene]	< 2	ug/L
		1,2-dichlorobenzene [o-dichlorobenzene]	< 5	ug/L
		1,2-dichloroethane	< 2	ug/L
		1,2-dichloropropane	< 2	ug/L
		1,3-dichlorobenzene [m-dichlorobenzene]	< 5	ug/L
		1,4-dichlorobenzene [p-dichlorobenzene]	< 5	ug/L
		2-chloroethylvinyl ether	< 2	ug/L
		bromodichloromethane [dichlorobromomethane]	< 2	ug/L
		bromomethane [methyl bromide]	< 2	ug/L
		carbon tetrachloride	< 2	ug/L
		chlorobenzene	< 2	ug/L
		chloroethane	< 2	ug/L
		chloroform	< 2	ug/L
		chloromethane [methyl chloride]	< 2	ug/L
		cis-1,3-dichloropropene	< 2	ug/L
		dibromochloromethane	< 2	ug/L
		dichlorodifluoromethane	< 2	ug/L
		dichloromethane [methylene chloride]	< 5	ug/L
		tetrachloroethene [tetrachloroethylene]	< 2	ug/L
		trans-1,2-dichloroethene [trans-1,2-dichloroethylene]	< 2	ug/L
		trans-1,3-dichloropropene	< 2	ug/L
		tribromomethane [bromoform]	< 5	ug/L
		trichloroethene [trichloroethylene]	< 2	ug/L
		trichlorofluoromethane	< 2	ug/L
		vinyl chloride	< 5	ug/L





February 23, 1993 Report No.: 00013686 Section A Page 55

NUS CLIENT NO: 1600 0006

#### LABORATORY ANALYSIS REPORT

CLIENT NAME:

BAKER ENVIRONMENTAL, INC. /NAVY CLEAN

ADDRESS:

420 ROUSER ROAD

CORAOPOLIS, PA 15108-

ATTENTION:

MR. JOHN LOVELY

Carbon Copy:

SAMPLE ID:

TRIP 2

NUS SAMPLE NO: P0225132

P.O. NO.: CTO # 19017

DATE SAMPLED:

UnAvail

55830

DATE RECEIVED: APPROVED BY:

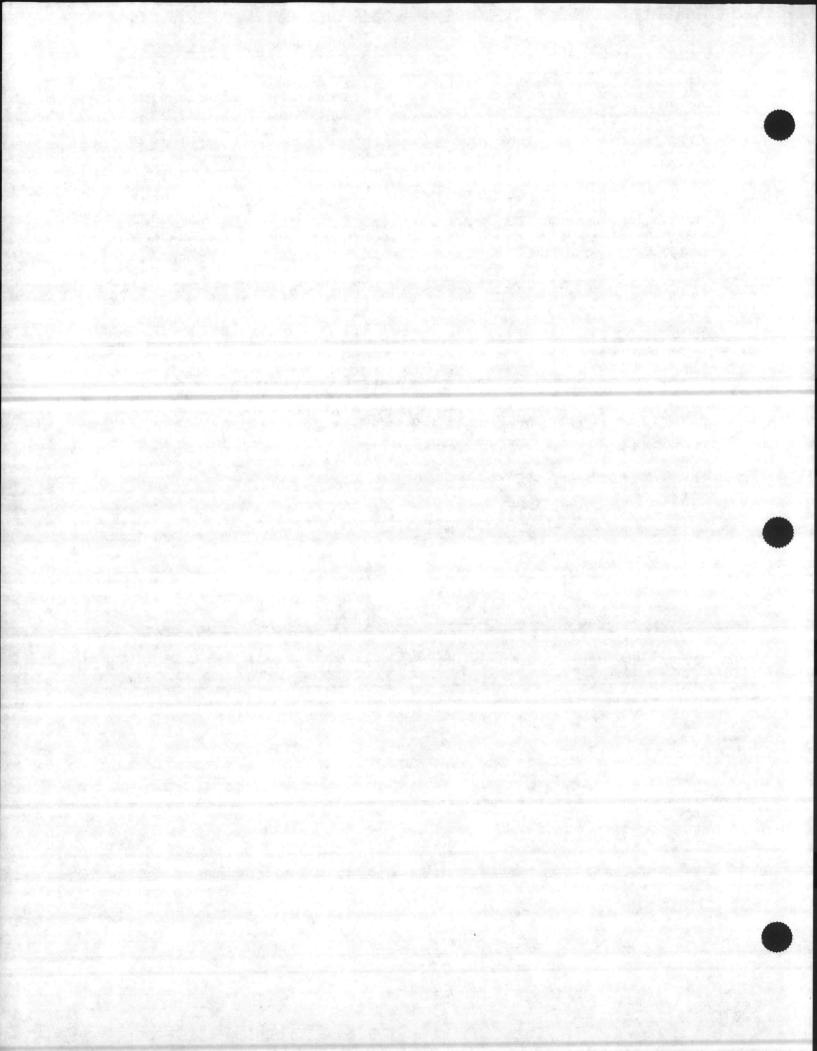
WORK ORDER NO:

**VENDOR NO:** 

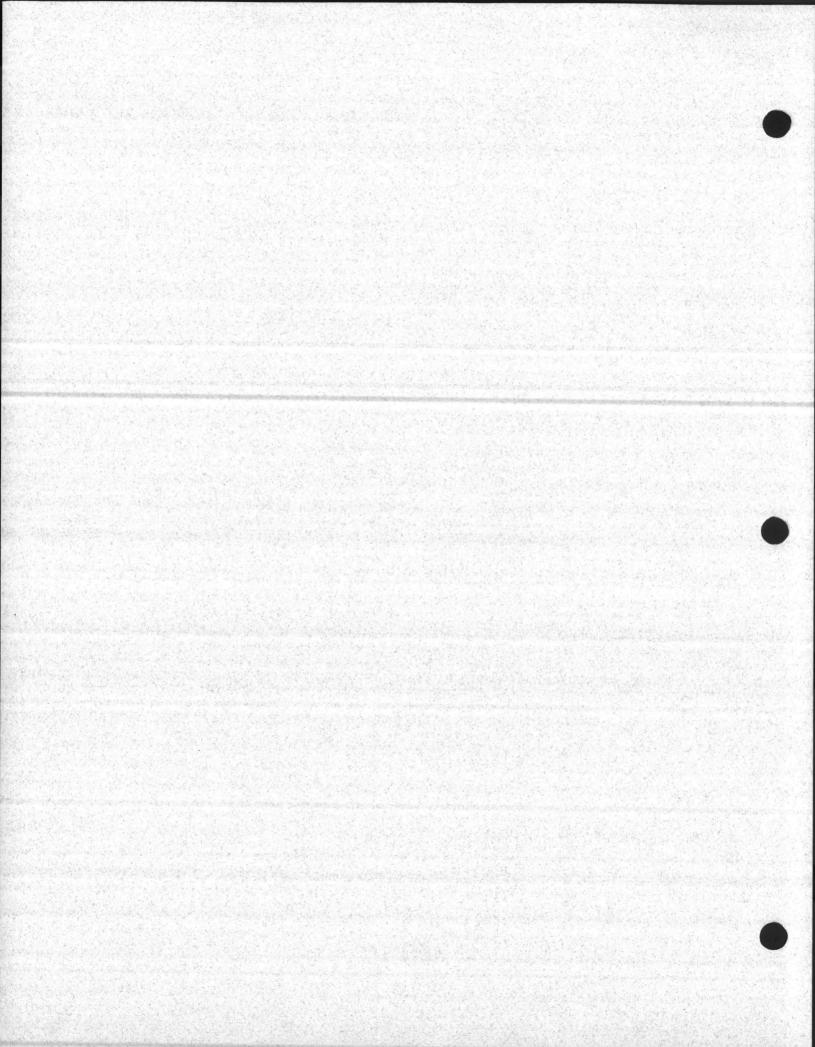
06-FEB-93 Joanne Simanic

	LN	CODE	DETERMINATION	RESULT	UNITS
	2	DPACK	CLP Data Package Deliverable	DONE	
	3	G107W	BTEX PACKAGE		
			1,2-dimethylbenzene [o-xylene]	< 2	ug/L
			1,3-dimethylbenzene,1,4-dimethylbenzene [m-/p-xylenes]	< 2	ug/L
			benzene	< 2	ug/L
-			ethylbenzene	< 2	ug/L
			methylbenzene [toluene]	< 2	ug/L

COMMENTS: In the BTEX analysis, m- and p-xylene co-elute on the capillary column. The concentration reported represents the sum of the two isomers.



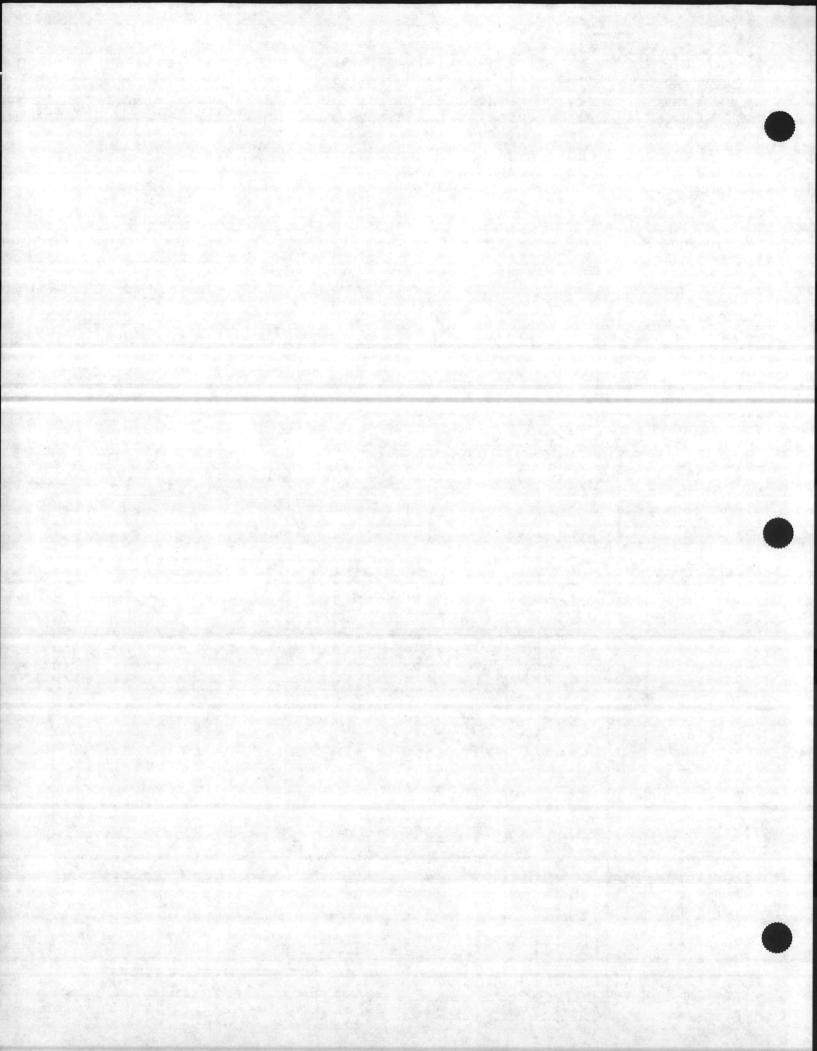
APPENDIX L
WELL CONSTRUCTION AND BORING DATA





#### **FIELD TEST BORING RECORD**

Bake	r Envi	ironm	ental, Inc.		S.C	ORD	.: 19	017 - 50 : EAST: _ URFACE: _			NOR	ING NO.: _Rw RTH: OF PVC CASING:		49 2	
RIG:	B	2-8	5							in de la			TOP OF CASING WATER		
			SPLIT SPOON	ı cz	SING	AL	JGERS	CORE BARREL	DATE	PROG (F		WEATHER	DEPTH (FT)	TII	ME
SIZE (D	AM.)		ain			8	.25"T.	p.	1-29-93	25	FT	WARM, SUNN	4		
LENGT	4		2 FT				5FT								
TYPE			STD			H.	S.A.				7				
НАММ	ER W	т.	140#												
FALL			30 in												
STICK (															
EMARI M	ast	COL	JUD N	LOT E	pare BE P	ed f	FOM ED AN	AUGER 40 There	Cottings FORE SO VISUA	217 5	poon	overhead w Samples w ON	tilities ere no	, th	مال
D E	1 1 1 1 Page 1 115 1 1					Classification (Grain Size, Principal Constituents, Etc.)			Color	Consist. or Density	Organic Con	ntent, and	S O I L	ELEV	
P T H	R O C K	Type No. (N = No Samp	(Ft. & %)	RQD (Ft & %)	Pen. Rate	PID (ppm)	1	Classificati ne, Grain Size Constituents	, Principal	Color	Hardne:	Weathering, Fracturing, as Observa	nd Other	ROCK	ATION
1 -							SILT Tra	, utle ce San	Clay,	BROW	n Met Dens		2.	.0.	
3 —							SAL		L, Little	BROW	MEN				
4 — 5 —															
6 —							6.5			_			6	.5	1
7 8							SAN	L SILT	graine	Grey	MEN	SE encount G.W. at	To We ered 7-91		
	100	1										and the second of the second			1
9 —		Pol Se		TO PO	1 4		1.00								1



### Baker

#### FIELD TEST BORING RECORD

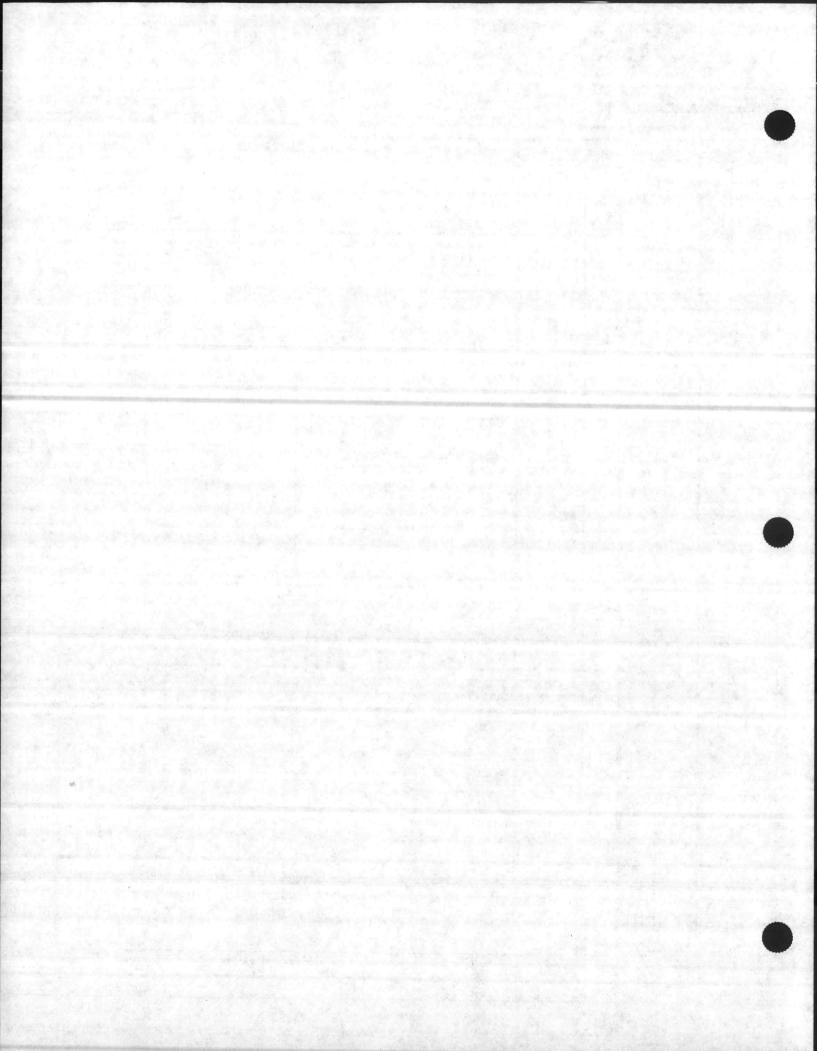
Baker Environmental, Inc.

PROJECT:			A COLUMN STATE	
SO NO:	19017-50-SRN	BORING NO.:	RW-1	1

4	DF	RILL RE	COR	D		4	VISUA	L DESC	RIPTIO	N		
D E	S O I L	Sample ID	Rec.	SPT Blows Per 0.5'	Lab. Class		Classification (Grain Size, Principal Constituents, Etc.)	Color	Consist. or Density	Moisture Content, Organic Content, Plasticity, and Other Observations	S O I L	ELEV
P T H	R O C K	Type - No. (N = No Samp.)	(Ft. & %)	RQD (Ft. & %)	Pen. Rate	PID (ppm)	Classification (Name, Grain Size, Principal Constituents, Etc.)	Color	Hardness	Weathering, Bedding, Fracturing, and Other Observations	ROCK	TION
1-							SAND, Finegrain LITTLE SILT	ed, Crey	MED. Dense	wer		
2-											-	
3-											_	
4- 5-		_	_		_		15.0	-				1
6-										LOST RECOVER DUE	70	1
7-					25					CLAY & SILT ADHERING TO		
8-										CLAY & SILT ADHERING TO AUGERS AND OF BOREHOLE.	SID	-
9-										OF BOREHOLE.		1
0											, i	1
1-											y 7	1
2 -												7
3 —										V		-
4-	- 100		F12.64				25.0			2.	5.0	1
5							END OF BORING	AT	25.0	FEET		1
7-												1
8-												1
9-												+
1	in a											1

DRILLING CO.: HARDIN-HUBER INC. BAKER REP.: () COLP

DRILLER: POYCE KEENAN BORING NO.: RWH SHEET 2 OF 2





#### FIELD TEST BORING RECORD

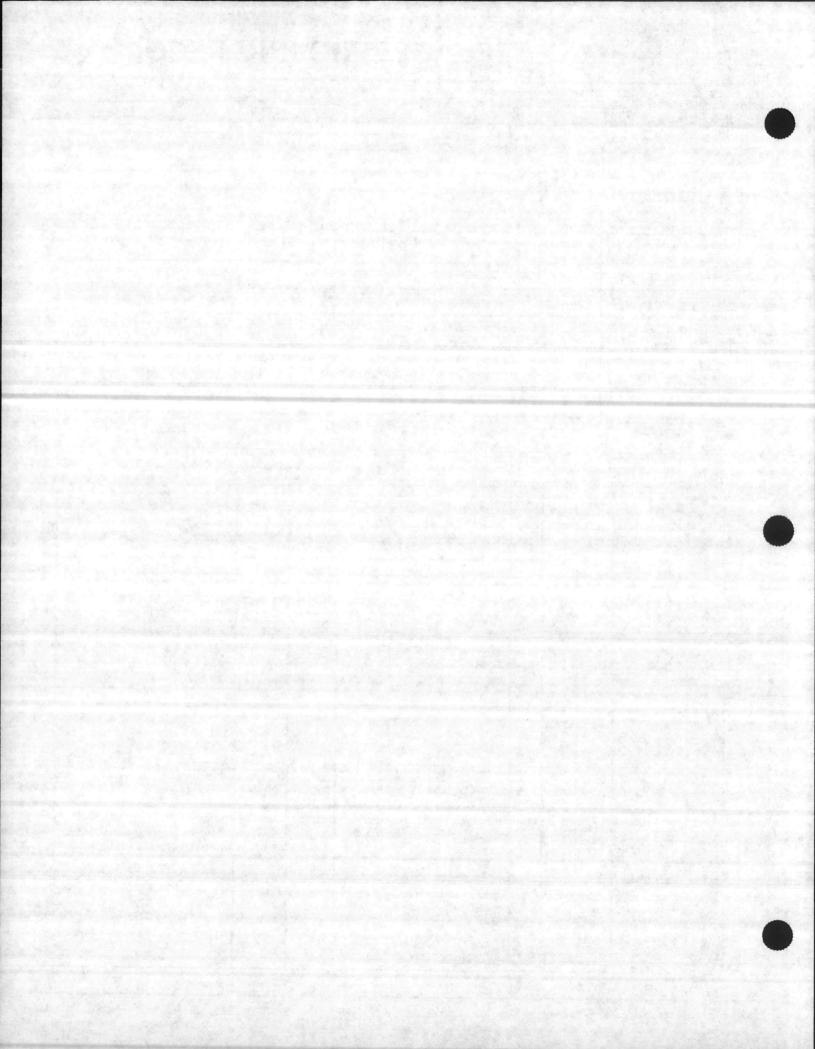
PROJECT:	
S.O. NO .: 19017-50-SRN	BORING NO.: P-/
COORDINATES: EAST:	NORTH:
ELEVATION: SURFACE:	TOP OF PVC CASING:

RIG: 13-8	30				DATE		WEATHER	TOP OF CASING WATER DEPTH (FT)	and the last
	SPLIT SPOON	CASING	AUGERS	CORE BARREL		PROGRESS (FT)			TIME
SIZE (DIAM.)	2 m.		4.25" H.S.	9.	1-29-73	26.0 FT	WARM, SUNNY		
LENGTH	2 FT.		5 FT.						
TYPE	STD		H.S.A.						
HAMMER WT.	140#								
FALL	30 m.								
STICK UP									

REMARKS: BORING WAS ADVANCED TO A DEPTH OF 26.0 FT BUT W PIEZOMETER WAS

		NSTA RILL RI					VISUA	L DES	CRIPTIO	N	
DE	S O I L		Samp. Rec.	SPT Blows Per 0.5'	Lab. Class.		Classification (Grain Size, Principal Constituents, Etc.)	Color	Consist. or Density	Moisture Content, Organic Content, Plasticity, and Other Observations	S O I L
P T H	R O C K	Type - No. (N = No' Samp.	(Ft. & %)	RQD (Ft & %)	Pen. Rate	PID (ppm)	. Classification (Name, Grain Size, Principal Constituents, Etc.)	Color	Hardness	Weathering, Bedding, Fracturing, and Other Observations	ROCK
		۸.				N.R.	Some Sand	LIGHT BROWN	MEDIUM DENSE	Damp	
		A.N.					3.5	<u></u>	_		3. <u>5</u>
			1.0	1 3		110	grained, Some SILT B 6.0 SAND, Fine grained, U	LIGHT	n Dense	6.0	6.0
7 -			50%	375		7.1.		Grey	DENSE	Moist, encounte Groundwater at FEST.	7.0_
3 -		A.N.									
						. 6					

DRILLING CO .: Hardin-HUBER Inc	BAKERREP .: J. COLP	A Commence of the Commence of
DRILLER: Royce Keenan	BORING NO.: P-1	SHEET _ L OF _2



# Baker

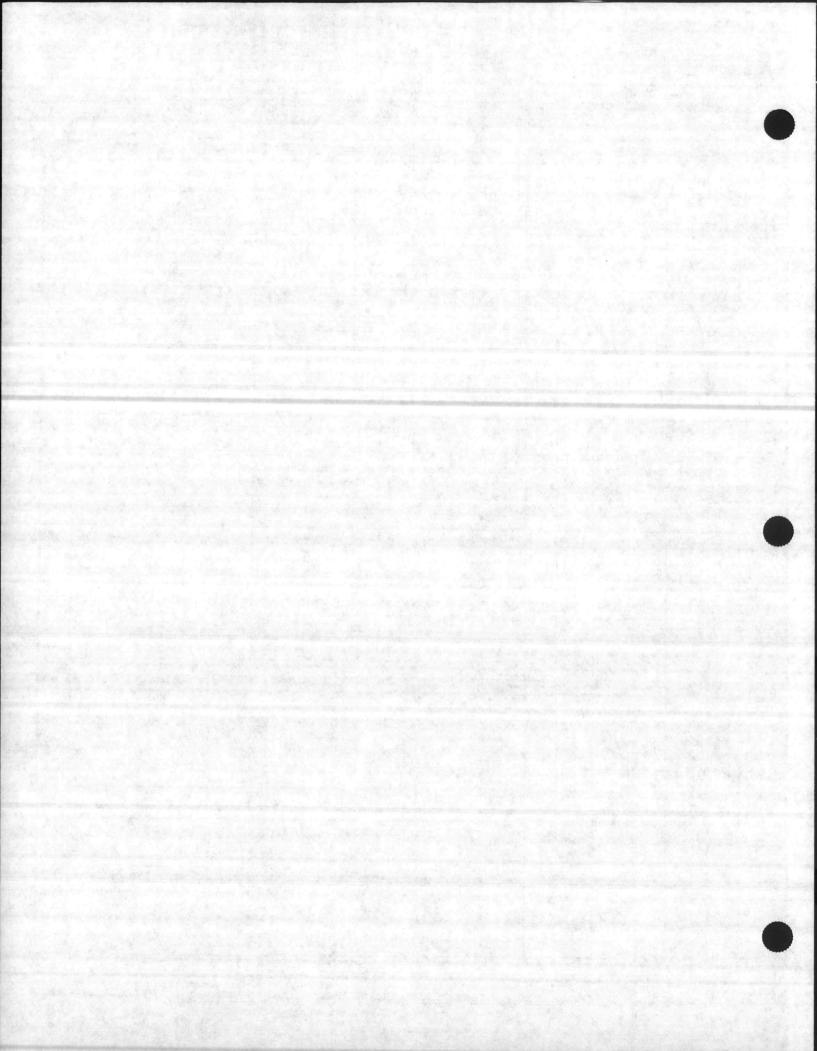
#### FIELD TEST BORING RECORD

Baker Environmental, Inc.

PROJECT:		Control of the State of the Sta	· 连 · 4.42	
S.O. NO.:	19017-50-SRN	BORING NO.:	P-1	

	DF	RILL RI	COR	D			VISUA	L DESC	RIPTIO	V		
0	S O I L	Sample ID	Rec.	SPT Blows Per 0.5'	Lab. Class		Classification (Grain Size, Principal Constituents, Etc.)	Color	Consist. or Density	Moisture Content, Organic Content, Plasticity, and Other Observations	S O I L	
P T	R O C K	Type - No. (N = No Samp.)	(Ft. & %)	RQD (Ft. & %)	Pen. Rate	PID (ppm)	Classification (Name, Grain Size, Principal Constituents, Etc.)	Color	Hardness	Weathering, Bedding, Fracturing, and Other Observations	R O C K	
1-			1.6 2.0 80%	4 3 44		N.R	SAND, Fine grained, Little SILT	Grey	M Loose	WET		
3-		A.N.									_	
5- 6- 7-			2.0	0 0 0 1		N.R.	Clayey Silt, Little Sand	LIGHT	Very Soft	WET	15.8_ - -	
8- 9-		A.N.									-	1
0 -			2.0	33		N.R	21.0				21.0	1
2			100%	2		N.K	SILTY PEAT, Trace Sand	BROW	LOOSE	DAMP TO DRY	<u> </u>	1
3 -			2.0	30 20		N.R.	SILTY PEAT, Trace Sand	Brown	LOOSE	DAMP TO DRY, at 24.0 FEET	wer -	1
5 –			2.0	3435		N.R.	SAND, MEDIUM TO PINE	LIGHT	LOOSE	LIET	25.0	-
6			100%		4.5		GRAINED, LITTLE SILT TERMINATIO	Crey DE	PTH =		26.6	1
7-8-									en e			1
9-												1
0-								19 6 6			-	1

AKER REP.: J. Wif
DRING NO.: P-I SHEET 2 OF 2

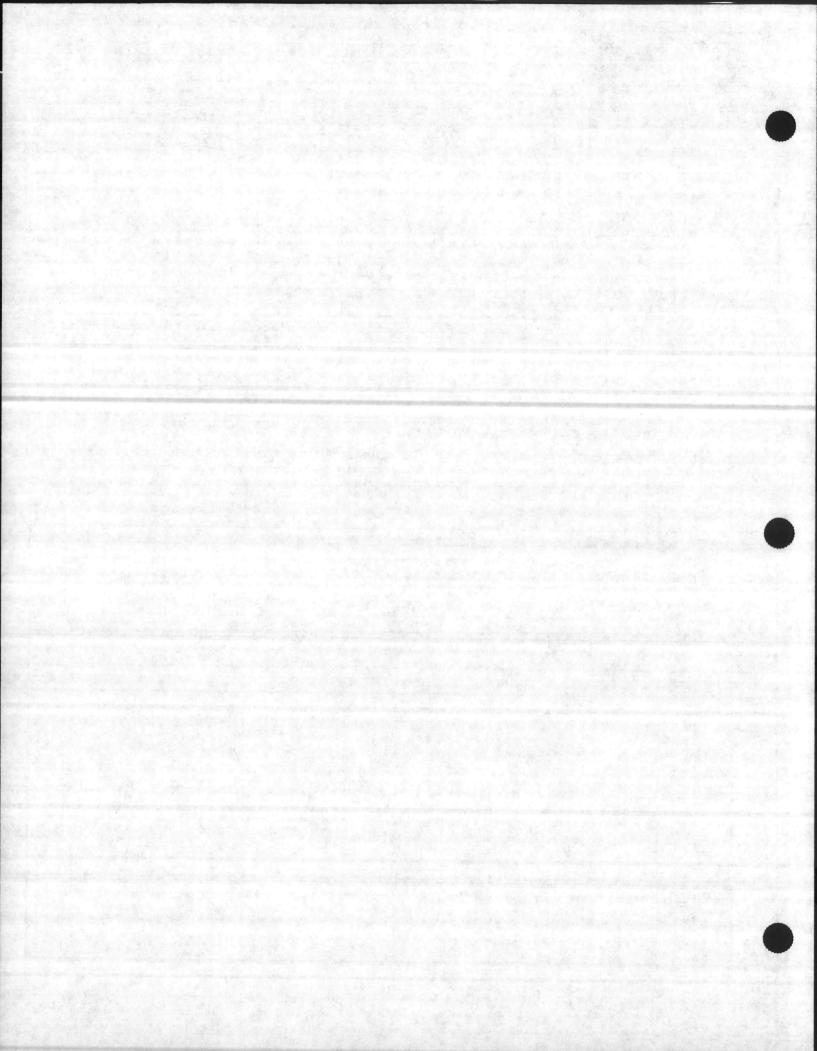




Bak	er Env	ironn	nental, In	с.	CO	ORDIN	IATES:	<b>9017 - 50</b> : EAST: _ JRFACE: _	-SRN			RING NO.: <u>P-2</u> RTH: OF PVC CASING	PERSONAL PROPERTY OF THE PERSON OF THE PERSO		
RIG:		B-8	0				Y						TOP OF CASING WATER		
			SPLIT		ASING	AUG	ERS	CORE BARREL	DATE		GRESS FT)	WEATHER	DEPTH (FT)	TII	ME
SIZE (D	IAM.)		2 m.	lije s		4.25	5"I.b		1-29-93	24.	OFT	WARM, SUNN	,		
LENGT	Н	5.5	2FT.		11.50	5	FT					and the second state of the second state of the second second second second second second second second second			
TYPE			STD			H.S	s.A.								
HAMN	1ER W	т.	140H												
FALL			30 in												
STICK	UP						-								
EMAR	1	1A5	WAS F COVI RECOF	LD NO	ARE T BE	PAI	SED	AND TI	HEREFORE	. Spu	T SPOC	erhead Util On Samples (	LITIES, TH	E T BE	Col
D E	S O I L	Sam ID	ple Samp. Rec.	SPT Blows Per 0.5'	Lab. Class.		745	Classification rain Size, Pri Constituents,	ncipal	Color	Consist. or Density	Organic Con	ntent, and	S O 1 L	ELEV
P T H	R	No.	(Ft.	RQD	Pen.	PID		Classificati	on			Weathering,		R	AT

	DH	ILL KI	ECOR	U			VISUA	ור חבאי	CKIPITO	N		
DE	S O I L		Samp. Rec.	SPT Blows Per 0.5'	Lab. Class.		Classification (Grain Size, Principal Constituents, Etc.)	Color	Consist. or Density	Moisture Content, Organic Content, Plasticity, and Other Observations	S O 1 L	ELEV
P T H	R O C K	Type - No. (N = No ' Samp.	(Ft. & %)	RQD (Ft. & %)	Pen. Rate	PID (ppm)	. Classification (Name, Grain Size, Principal Constituents, Etc.)	Color	Hardness	Weathering, Bedding, Fracturing, and Other Observations	ROCK	ATION
1 –							SLET, LITTLE CLAY, SOME SAND	CIGHT		" DRY	-	3
2 —							2.5					
3 —							SAND, MEDIUM TO Fine grained, Little SILT	Brown	DENSE	M DAMP TO MOIST		
5 —							50			5.0	-	
6 —							SAND, Fine grained, Trace SILT	Grey	LOOSE	Moist to wet, encountered of. between 7-9 Ft.	-	
7 –			all the state							DET WEET 1-9 FT.	100	
8 –												
9 _												
10 -												

DRILLING CO .: Hardin-Huben Inc.	BAKER REP .: J. COUP	er en apare Alain, en egen en Marie en den La companya de la co
DRILLER: Royce Keenan	BORING NO.: P-2	SHEET ( OF 2



# Baker

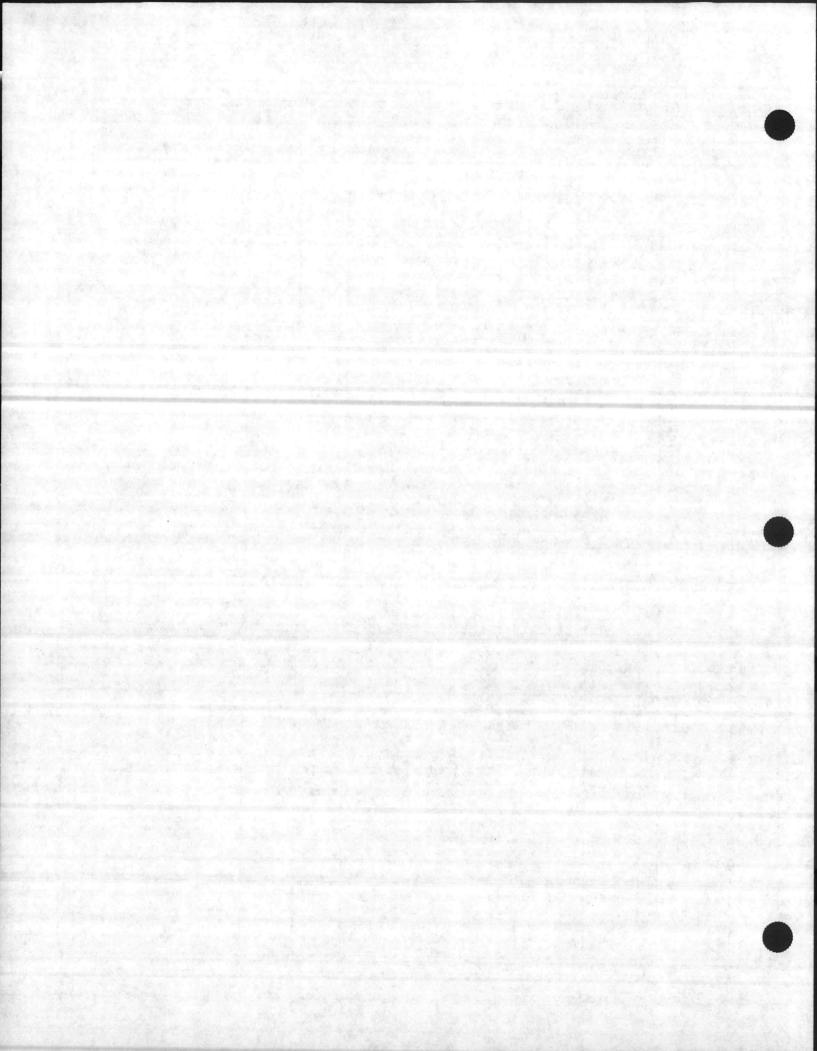
### FIELD TEST BORING RECORD

Baker Environmental, Inc. PRO

PROJECT:		A PROBLEM STATE	No. 1 . September 25	14.000
	19017-50-SEN	BORING NO.:	P-2	

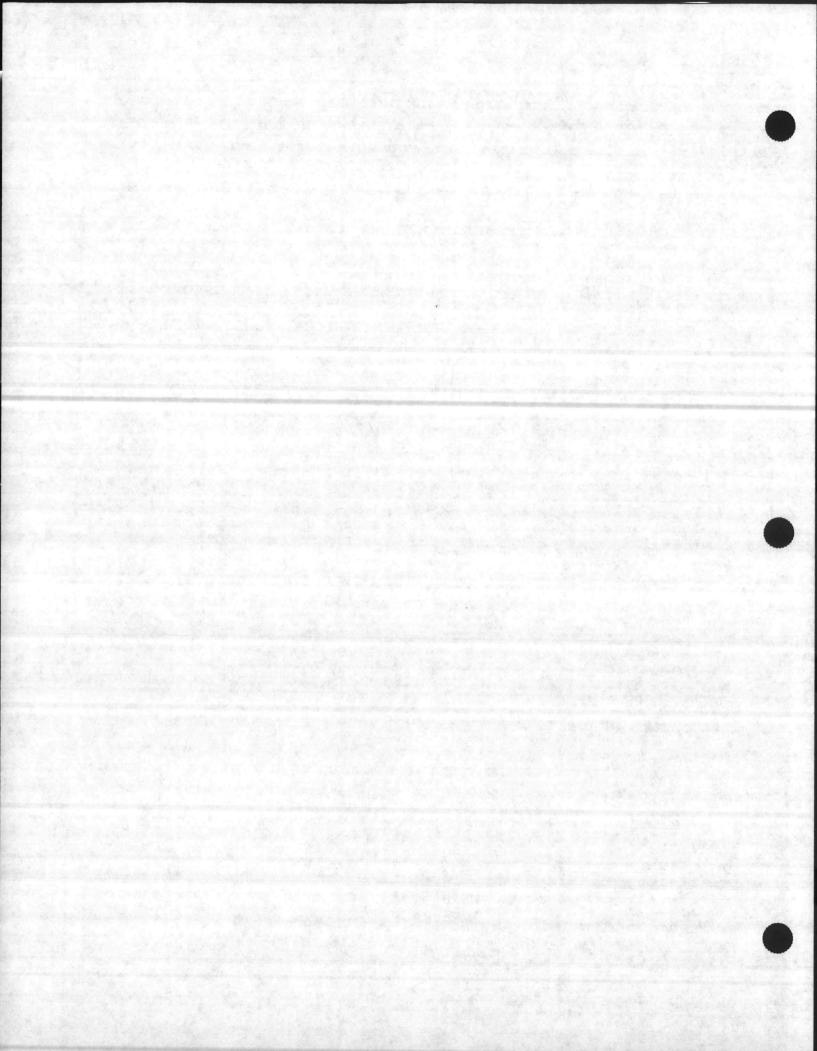
DRILL RECORD			VISUA	L DESC	RIPTIO	V						
D E	S 0 1 L	Sample ID	Rec.	SPT Blows Per 0.5'	Lab. Class		Classification (Grain Size, Principal Constituents, Etc.)	Color	Consist. or Density	Moisture Content, Organic Content, Plasticity, and Other Observations	S O I L	ELEV
P T H	R O C K	Type - No. (N = No Samp.)	(Ft. & %)	RQD (Ft. & %)	Pen. Rate	PID (ppm)	Classification (Name, Grain Size, Principal Constituents, Etc.)	Color	Hardness	Weathering, Bedding, Fracturing, and Other Observations	ROCK	A T I O N
1-							SAND, Fine grained Trace SILT	Grey	Loose	WET		
2-												
3-											-	
4-											-	
5-											-	1
6-										_		1
7-	1	-	-	I VE	+	-	17.0	-	_		.0	1
8- 9-								1000		OF SOILS DUE TO Clay ADHERING TO LUGERS AND		1
0-										SIDES OF BOREH		1
1-											-	1
2 –												1
3 –								1.00		A		1
4-							24.0				4.0	1
5 -				10.00			END OF BORIN	5 AT	24.0	FT.		1
6-												1
7-												1
8-												1
9-				100						197		-
9-					7							-

DRILLING CO .: HARDIN - HUBER THE.	BAKER REP .: J.COLP	
DRILLER: ROYCE KEENAN	BORING NO.: P-2	SHEET & OF 2



OJECT No.: 19017-50-SEN	DATE STARTED: /-29-93
JECT NAME:	DATE COMPLETED: 1-29-93
L No.: RW-1	DATE DEVELOPED:
LLING CO .: Hardin - Huber	DEVELOPMENT METHOD.
	CONCRETE PAD
PROTECTIVE STEEL	
SLEEVE WITH	3 PROTECTIVE STEEL BOLLARDS (TYP.)
LOCKING CAP	
	HEIGHT OF RISER
ROUND SURFACE	2.5 ft.
	332 1
DIAMETER OF	
WELL CASING	
	LENGTH OF
TYPE OF WELL MATERIAL	RISER
STAINLESS STEEL	/ <u>//</u> ft.
	TOTAL TOTAL LENGTH DEPT
DEPTH TO	OF PYE STAINLESS OF BORIL
BENTONITE 3.5 ft.	27.5 ft. STEEL 25 ft.
DEPTH TO 5.5 ft.	
DIAMETER OF BOREHOLE	
	LENGTH OF
DRILLING METHOD	SCREEN
<u> </u>	14.85ft.
SCREEN SIZE: 0.01 in.	
SCKEEN SIZE:	

BAKER ENVIRONMENTAL REPRESENTATIVE:



Bering No. HPGW 24 0.01 Slot Hole Size 2" PUL Screen Size Mat'1 PUC Z Mac'l asing Size David Brentlinger ologist Date Start 11/13/86 Finish ESE Contractor Davis Driller

Filter Materials Silica Sand

Grout Type Bintonile Pellets

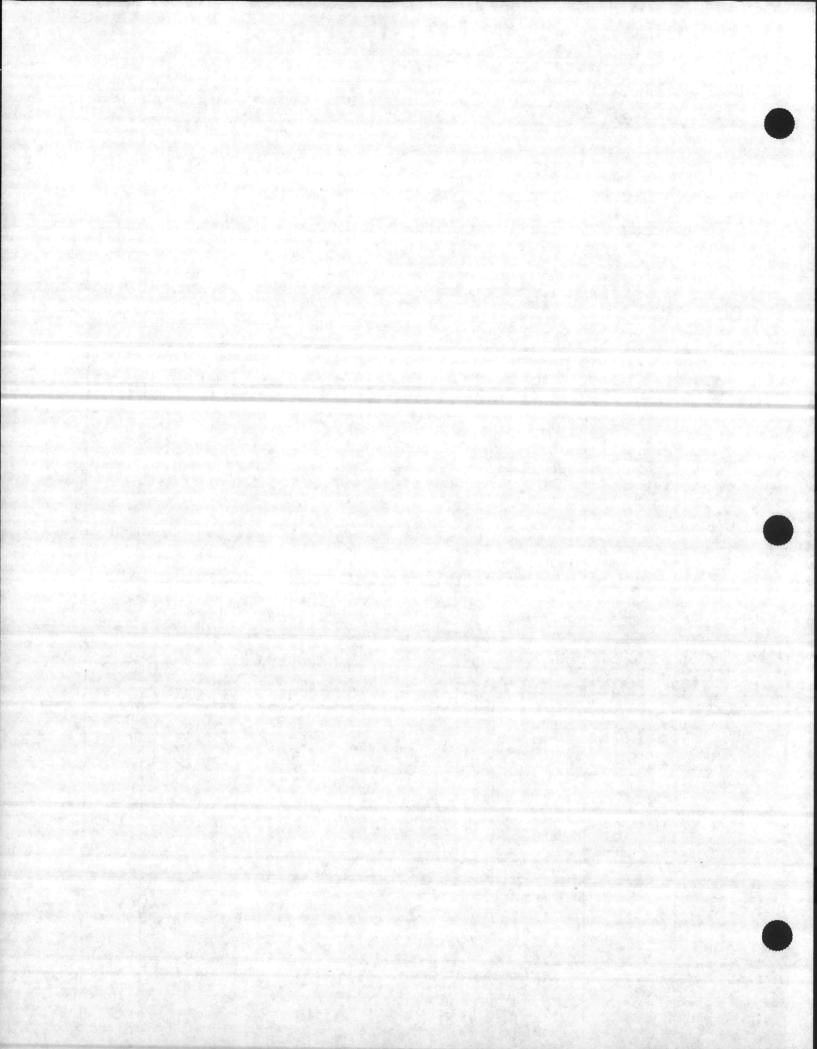
Development

Static Water Level 6.83'

Top of Well Elevation 9.33'

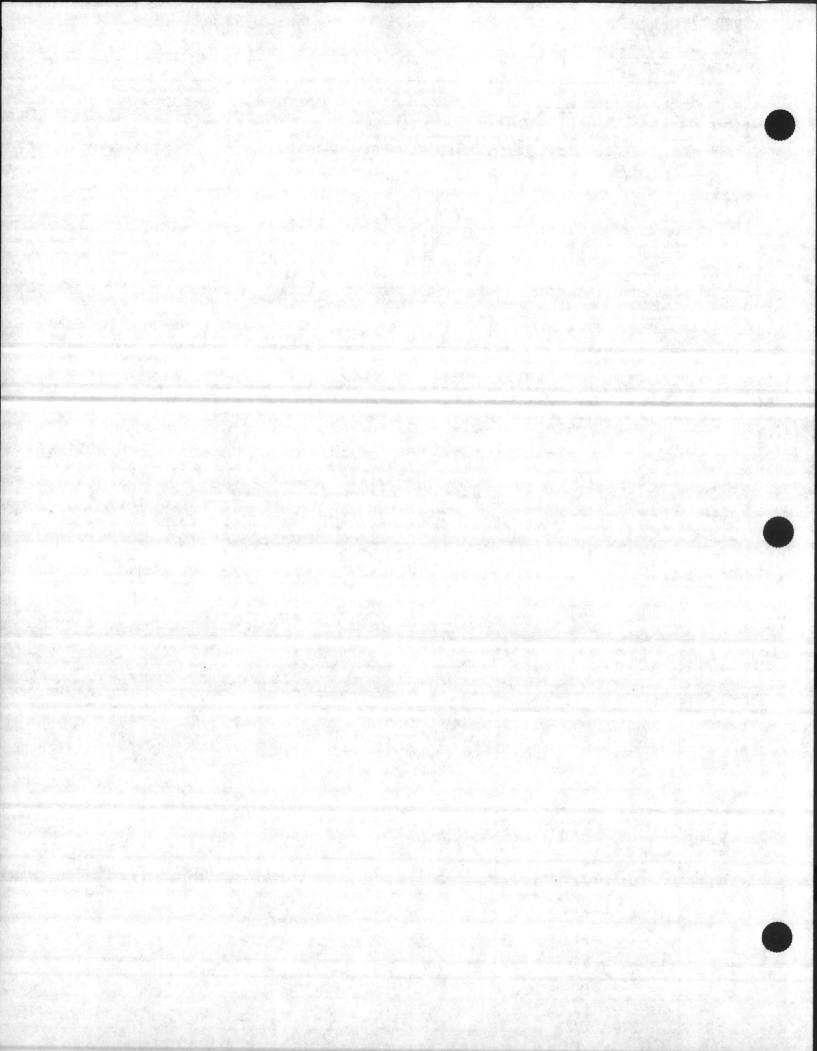
Drill Type Hollow Stem Auger

Depth (feet)	Sample	Sketch	Lithology, Color	USCS	SPT (BL/FT
2.0-1.5		0.0-0.75	10 YR 2.5/1 Black Silks  (-inc Sand 50% organic  matter, saturated 1+20  104R 6.5/3 Pale - Very Aak Brown  Silky Fine Sand Lsilt 25%),  1605e, wet, Slighty dense	sm	4 3 4
1.5- 3.0			Same as (0.75 - 1.5) less wet	5m	4 8 6
3,0-4.5			10 4R 513, light Brown with Black-gry silty clay mothles throughout, Silty fine Sond (silt 30%), moist non-plastic, Slightly dense	sm	5 9 7
4.5-6.0			1042 4.5/z, Gry-dark arry Silty Clayey Sand, (silf+Cky 45%), slightly dense - Midi dense, Moist, Slightly plustic	SC/58	2 3 4
6.0-7.5			1042 4.5/4 Ye llow Brown - dark yellow Brown; S. Hz Clayer Sand, (S. it + Clay 45%), Slightly Plustic - Plustic, Moist, Slightly Slightly dense	SC Sm	3 4 7

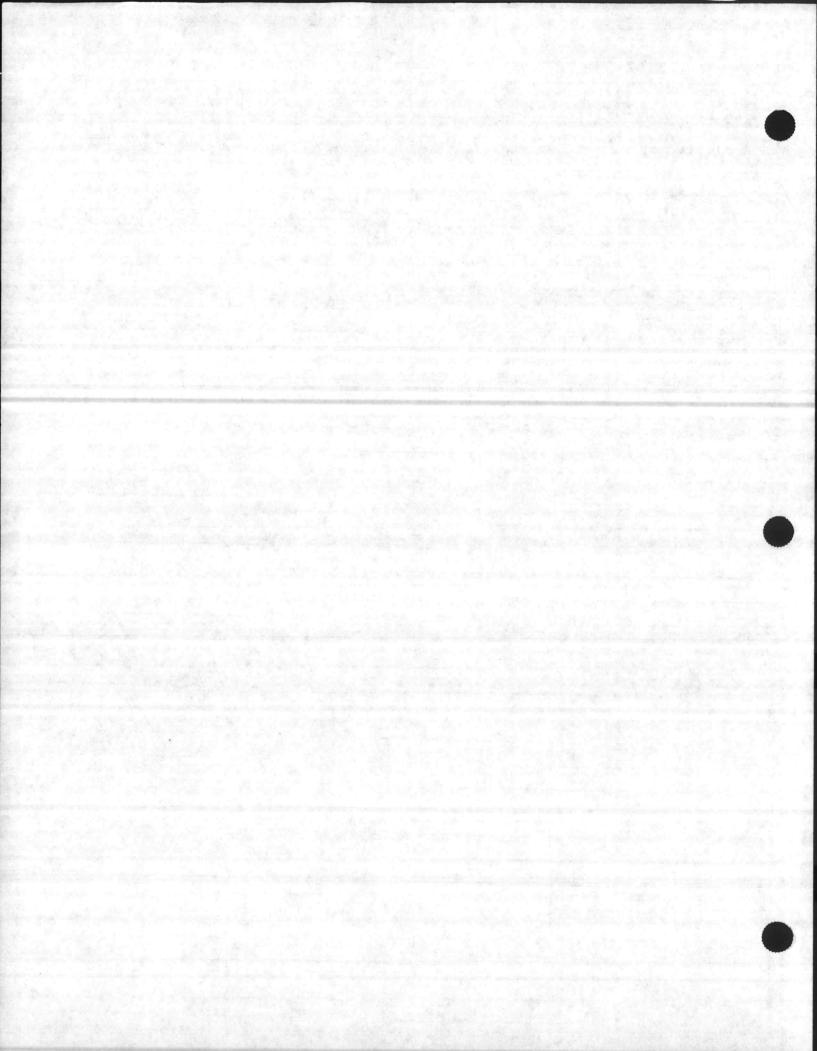


Boring No. HP Gu	24	Location Coordinates N
Hole Size .	Slot	<u>E</u>
Screen Size	Mat 1	Filter Materials
asing Size	Mac'l	Grout Type
ologist		Development
Date Start 11/17	Finish 11/12	Static Water Level
Contractor		Top of Well Elevation_
Driller		Drill Type

Sample	Sketch	Lithology, Color	USCS	SPT (BL/FT
		10 42 4/1 , dark Grey Silty-Clayey Sand, (Silt+ Clay 45%), Moist, Slightle Plasta, Mrd. dense-dense	SC Sm	5 10 26
		1042 6,5/1, Grey- Light Grey,	) SW	9 12 15
		2.54 4.5/6 Gray-dark Gray, Silly Fire Sandy Clay (silt+ Sand 30%) Sticky, Slights dense, Slightly plaste, wet	SC	2 1
		74R-2/0 Black, Silty ORGanic Clay (organic matter 45%), Firm, dense, moist, Slightly plastic	ML Pt	235
		1048 2.5/1 Black, Silty Sandy Peat (silt + Sand 30%, dry, Mod. densi	Pt	5610
	Sample	Sample Sketch	10 40 4/1 Clayey Sand, (Silf+ Clay H5%), Moist, Slightle Plastic, Mid. dense-dense  10 42 6.5/1, Grey-light Grey, Silty Fine Sand (Silt 10-15%) 1005e, Slightly, dense, moist-weft Top 5" Black Silty Sand  2.5 4.5/6 Grey-dark Grey, Silty Fine Sandy Clay (Silt+ Sand 30%) Sticky, Slightly dense, Slightly plastic, wet  742-2/0, Black, Silty ORganic Clay (organic matter H5%), Firm, dense, moist, Slightly plastic  1042 2.5/1 Black Silty Sandy Peat (Silt+ Sand 30%), dry, Mod.	10 40 4/1 , dark Grey  S. 1 14 - Clayey Sand, (SI/++ SC  Clay 45%), Moist, Slight Sm  10 42 6.5 1 , Grey - light Grey,  Silty Fine Sand (SIL+10-15%)  1005e, Slightly dency, moist-wef Top 5" Black Silty Sand  2.5 4 4.5 /6 Grey - dark Grey,  Silty Fine Sandy Clay (S. 14+ Sand 30%) Sticky, Slightly SC  dence, Slightly plaste, wet  742 - Z/o , Black, Silty  ORGanic Clay (organic matter ML  45%), Firm, densy, moist, Pt  Slightly plaste  1042 2.5 / Black  Silty Sandy Peat (Silt + Sand 30%), dry, Rod.



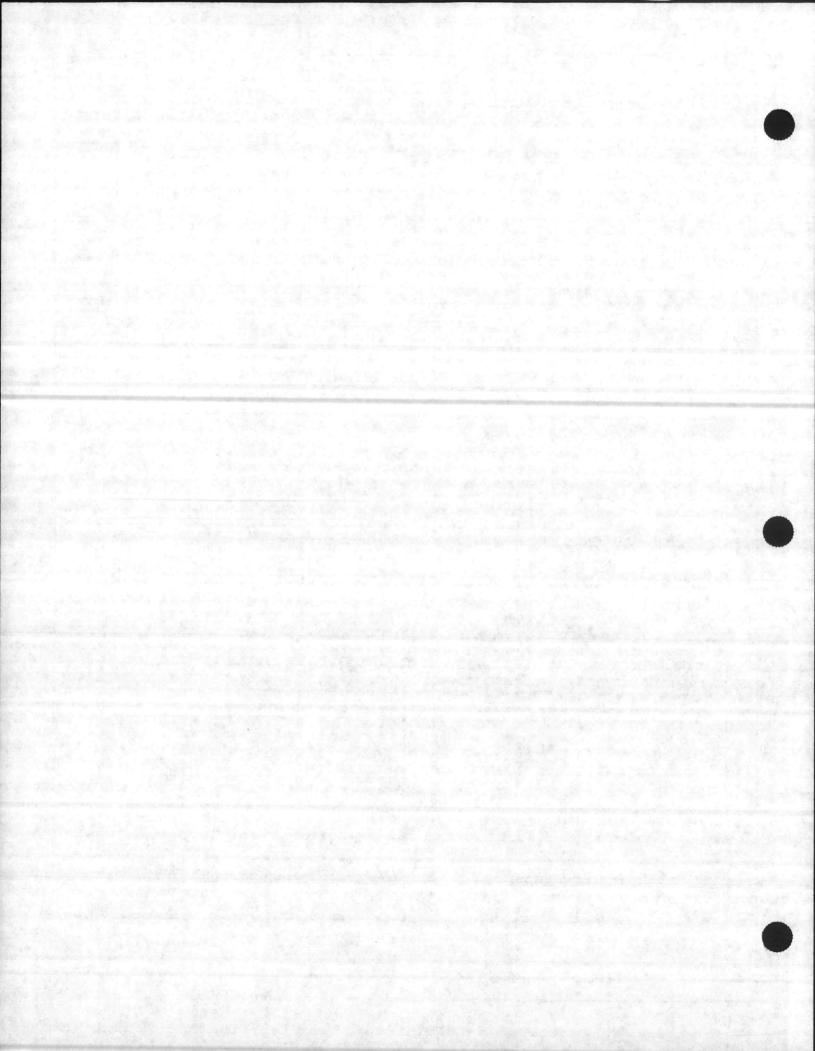
oring No. HPGW24	SHEETOF_
	11/12/86
On Site 1215 PM	1 100
1220	
1st Spon 1220	
1 ast Spoon 120	
Well Complife 150	
Standard Well Specs	
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	Carlo K
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	1460 10 150 150 150 150 150 150 150 150 150
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	-//
DAT	TE SIGNED



## OVERBURDEN WONITORING WELL SHEET

WELL NO. HP. Gw 24-1

PROJECT NO. 4	Camp Lejeuri - HPIA 9-02036 BORING I DATE 111 David DTRHinger	NO. HP-GW24	DRILLER DRILLING DRILLING METHOD ALLOW HER DELVELOPMENT METHOD	y.co. x Ayer
GROUND ELEVATION		ELEVATION OF TOP  ELEVATION OF TOP  STICK—UP TOP OF  STICK—UP RISER  TYPE OF SURFACE  TYPE OF SURFACE  TYPE OF SURFACE  TYPE OF RISER P  BOREHOLE DIAME  TYPE OF BACKFIL  ELEVATION/DEPTH  TYPE OF SCREEN:  SLOT SIZE X LENG  TYPE OF SAND P  ELEVATION/DEPTH  TYPE OF SAND P  ELEVATION/DEPTH  TYPE OF SAND P	E SURFACE CASING:  PIPE:  E SEAL: CONCRETE  CASING: ST.  E CASING: Carbon steel  IPE: Simble 40 pic  ITER: (c"  L: Crincrete  AND PACK:  TOP OF SCREEN:  Schedule 40 pic  ITH: Color & 200  ACK: Cimpi Silve Sund  H BOTTOM OF SCREEN:  H BOTTOM OF SAND PACK:  L BELOW OBSERVATION	32.31' 2.70' 1.55' 3 5'
	NOT TO SCALE			



NORTH CAROLINA DEPARTMENT OF NATURAL RESOURCES AND COMMUNITY DEVELOPMENT FOR OFFICE USE ONLY DIVISION OF ENVIRONMENTAL MANAGEMENT - GROUNDWATER SECTION Serial No. P.O. BOX 27687 - RALEIGH, N.C. 27611, PHONE (919) 733-6083 Quad. No. Minor Basin . Basin Code \_ Header Ent. STATE WELL CONSTBUCTION PERMIT NUMBER: 46 - 0135 - WM - 014/ DRILLER REGISTRATION NUMBER 1. WELL LOCATION: (Show sketch of the location below) Nearest Town: Jacksonville NC County: DRILLING LOG Depth (Road, Community, or Subdivision and Lot No.) 2. OWNER ADDRESS Zip Çode 86 USE OF WELL MONITO! 4. TOTAL DEPTH 25.5 CUTTINGS COLLECTED Tes ON 5. DOES WELL REPLACE EXISTING WELL? Yes Who 6. STATIC WATER LEVEL: 6.83 FT. Dabove TOP OF CASING. TOP OF CASING IS 2 150 FT. ABOVE LAND SURFACE. 7. YIELD (gpm): \_\_ \_\_\_\_ METHOD OF TEST \_ ATER ZONES (depth): \_\_\_ 9. CHLORINATION: \_\_\_\_ Amount 10. CASING: If additional space is needed use back of form. LOCATION SKETCH (Show direction and distance from at least two State Roads, or other map reference points) 11. GROUT: See Fig. (2-5) Method From 0.0 To 2.0 Ft 12. SCREEN: Slot Size Material Diameter

	From	то	Ft	in	in
. G	RAVEL PACK:				
		Depth		Size	Material
	From _3.	0 TO 6	5 Ft. C	oarse	SANO
	From	To	Ft.		

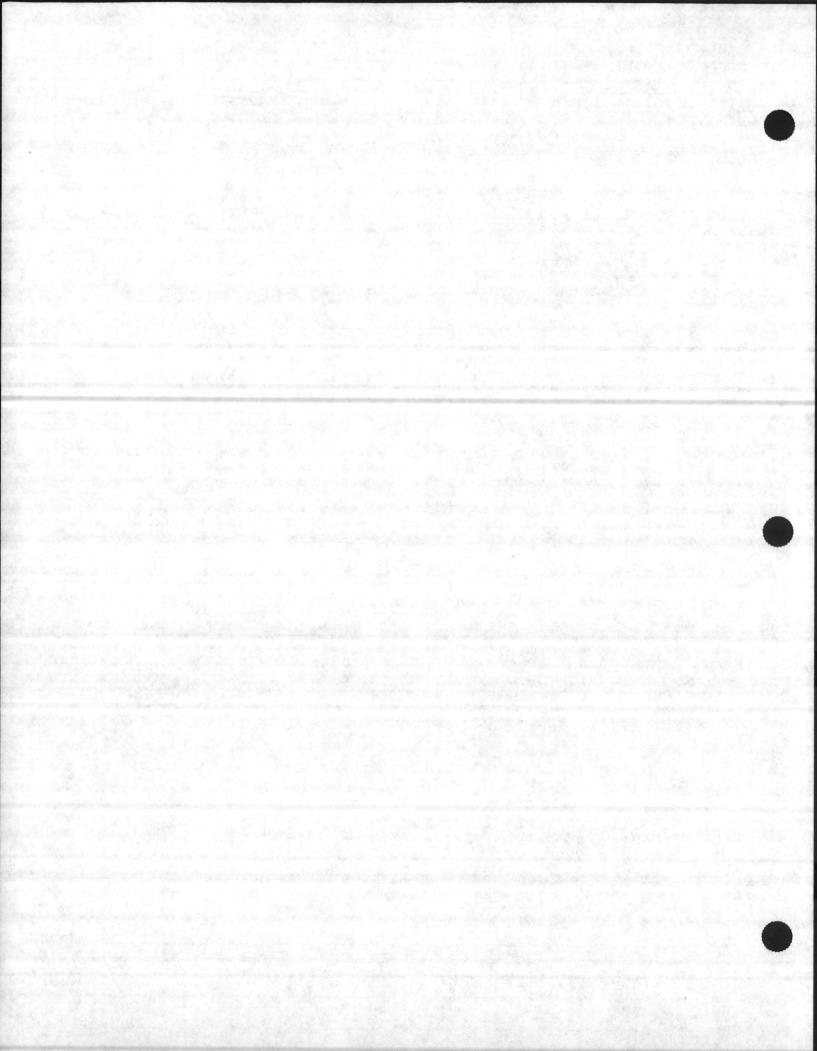
From 5.0 To 25 Ft. 2 11 in 0.01 in. PUC

I DO HEREBY CERTIFY THAT THIS WELL WAS CONSTRUCTED IN ACCORDANCE WITH WINCAC 2C. WELL CONSTRUCTION STANDARDS, AND THAT A COPY OF THIS RECORD HAS BEEN PROVIDED TO THE WELL OWNER.

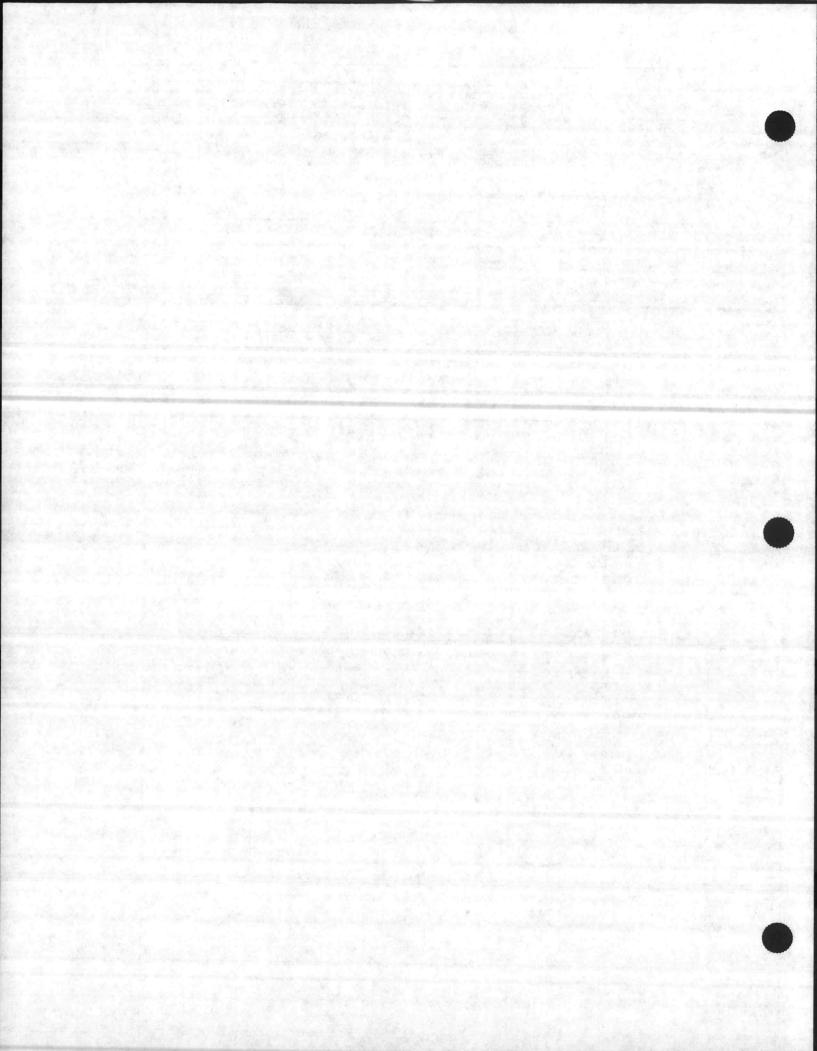
SIGNATURE OF CONTRACTOR OR AGENT

DATE

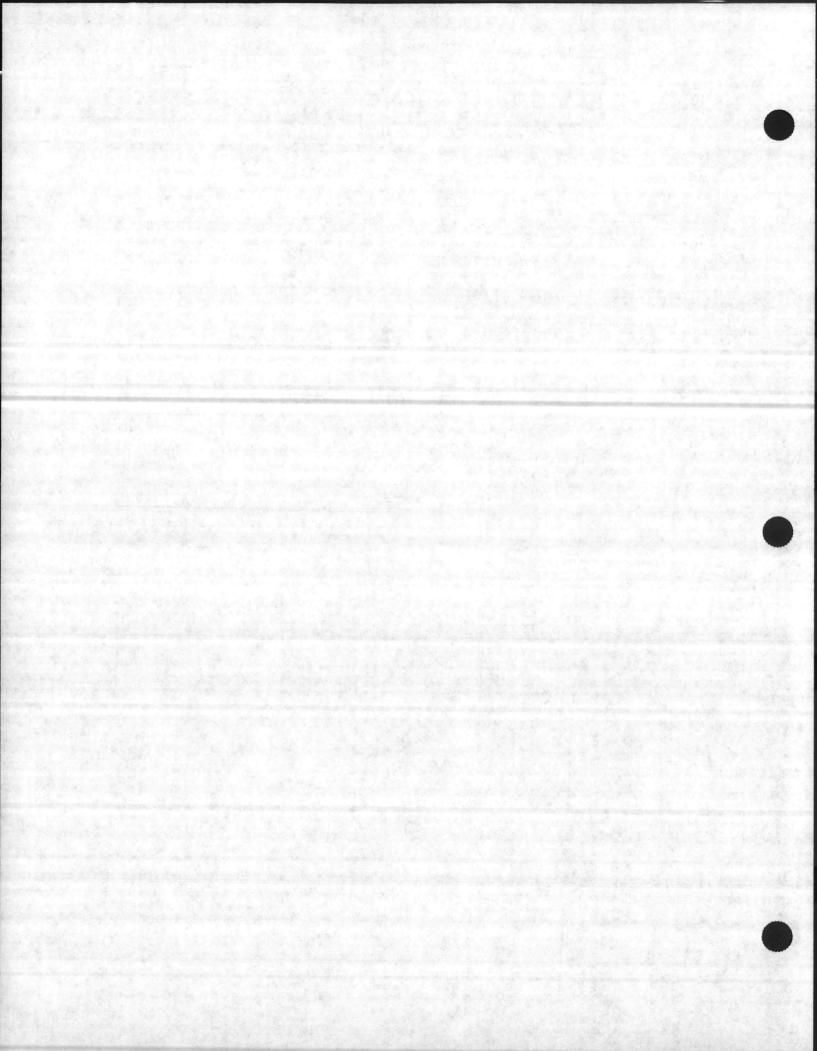
EMARKS:



ologist_ ate Start contractor	6/8/87 ESE ATEC	ntlinge/	Top of Well Elevation 3.37	4 13.	11.º
Depth (feet)	Sample	Sketch	Lithology, Color	uscs	(BI
0-5			Silty Fine Sand		•
5-10			Silly fine sand		
10-15			Silty fine Sand		
15-20			Silly very fine sound		
Q - 25			very fixe sand		
25-30			white fines, coarse muterial well rounded		
30-35			W/y fine sund Some as about		
35 - 40			very time silly-clayer fine sand		
<b>3</b> -50			Same as about  35-40  with more clay		

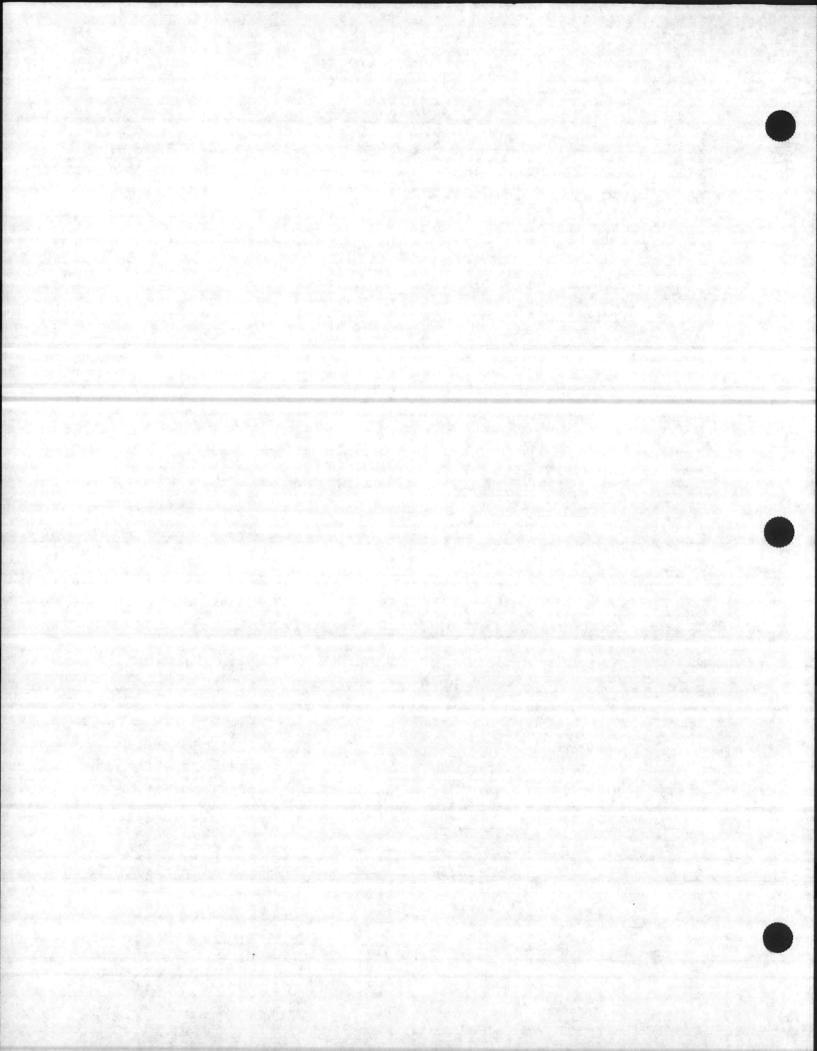


en Size ing Size ing Size ologist ate Start contractor		Slot_ Mat'l Mat'l Finis	Development  Static Water Level  Top of Well Elevation		
riller		Sketch	Lithology, Color	USCS	SF (BL/
(feet)	Sample	SKELLI	Silly Soudy - time Sandy silt. with clay + small skells		
55-60			Clayer Silty fine sund mostly fine sund some web, - Coarse sund with small Clastics (shells)		
60-65	46.75		same as about 55-60 more shells		
9,10		haid layer	Coarse-Sand and uncemented Clastics + Cemen Vots of Shells)	He T	
70-75		Semi lithofice Limes form	Coorst-sand and uncerented Clastics + Ceren (ots of Shells)  Same as about 70-75	Rale	
大の大変の大変の大変の大変の大変の大変の大変の大変の大変の大変の大変の大変の大変			Comments:  Rock layer is not very hard, driller went through pass	1/4	

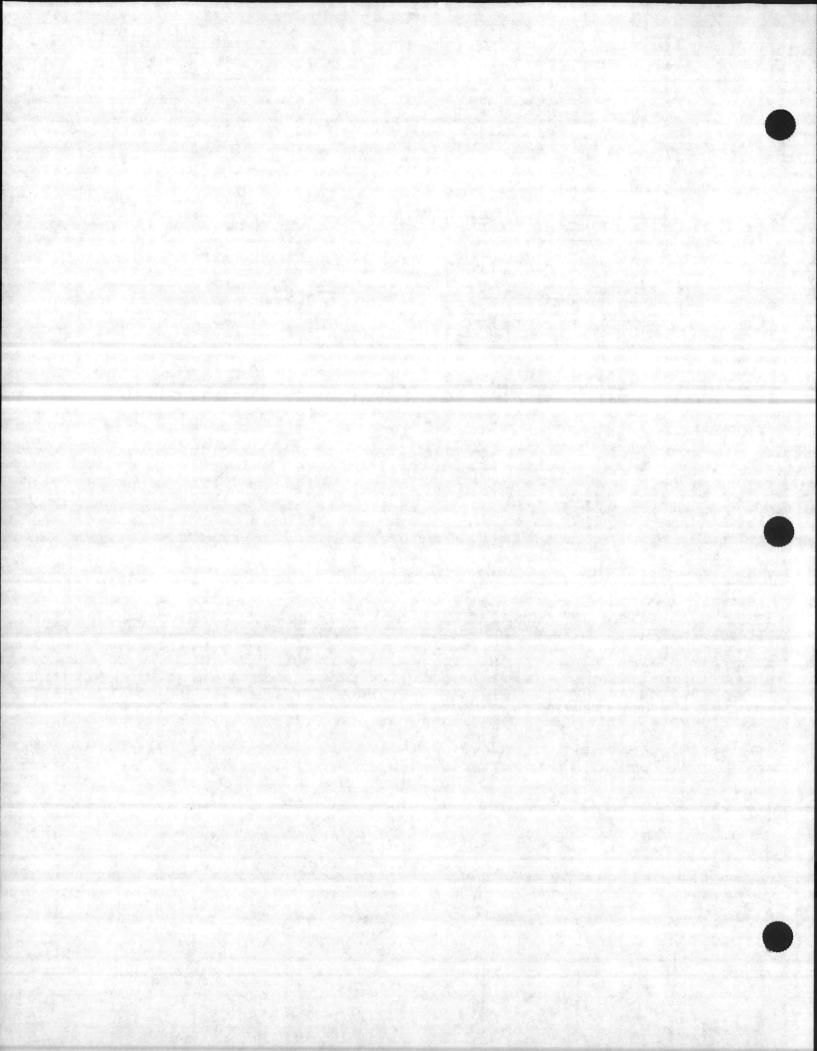


On-site and Ready 6/8/87) Dr. Ming Stops 300 PM	1 , hole closen		Pump
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well Drilling Compi	6A - 103		nch 1130 - 100
Casing + Scrup 1	7 - 103	선생님들은 그리고 하는데 그리는 그 그리는데 그 때문에 되었다.	
Well Complete	- 2:3	0	
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(OMMEAD ! CM	ained open	during	casing install
(Soft	fine sand	most al 1	sole)"
		1	
:11 Profile 3.25			7
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3'chy 25' sand 20' Screen		904	903 902 Sneeds Ring Rd
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3'chy 25' sand 20' Screen		904	903 902 Sneeds Ring Rd

SOURCE: Environmental Science and Engineering, Inc., 1

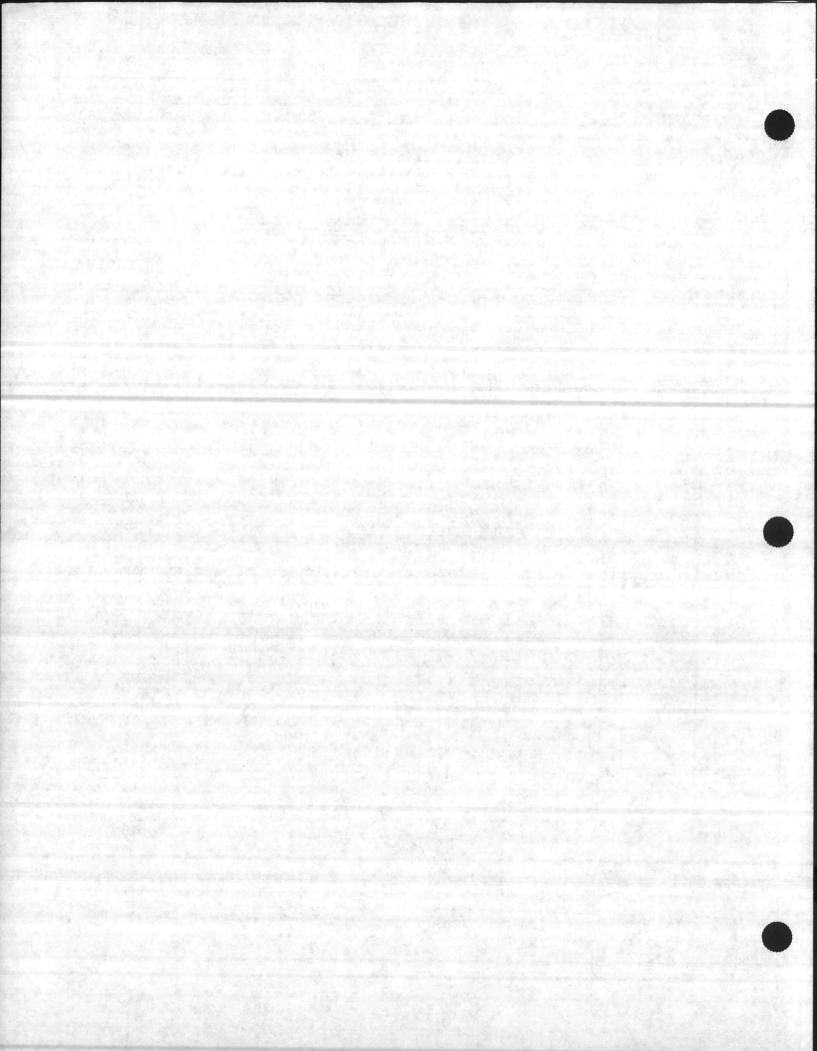


logist_	2 " David 6/10/87 ESE DON Sweet	Fin	Top of Well Elevation /. 8/	; 15	2007
Depth (feet)	Sample	Sketch	Lithology, Color	uscs	(BI
5-10			top 51, some clay layers		346
0-15		•	silty fine sond and organic clap throughout.		
15-20			Sill fin - med. Sond with course sond + peblies bo Hom 3'		
v -30			Coarse and TOP 5', Silty Clayer Gresond		
30-35		·	Sitty Fire Sond		
35-40			silty med Sond with clay logis (clay brown with coalse sond)		
40-50			(35-40) 1. Hle/no		
50-60	3		Rock at 58' (cemented clastics + Stells).		



/Size	Slot	<u> </u>
en Size	Mat'1	Filter Materials.
ing Size	Hat'l_	Grout Type
logist		Development
ate Start	Finish	Static Water Level Top of Well Elevation
Contractor		<del></del>
Driller		Drill Type

Depth (feet)	Sample	Sketch	Lithology, Color	uscs	SPT (BL/F)
60-70	Sun d Silt		V. IItle clay course soud well counded + small shells		
	Rock	68-70	Communed (lastics timestone + stells	very	Hard
70 - 75			Rock (uncommed thistics) shells, and coarse soud (well rounded).  Fine silky sand (74-75)' with less kock and shells		
75-80			gellsus clay peds, less. 10%		
1-85	50	25nd- + Rock (1:2') Suno			
» –		•	Silts very fine sand with small shells and rounded v. coarse sand pebbles		
40 - 95			silty med. Sand with mine shells and loavse sand + pebbles		
			(0. 05)	a Pos	
15-100			Same as abre (90-95)		
0- 105	The same	100-103	Silly find sond		
		. 103-104	sold comeded Lager		



en Size Mat'l Filter Materials.

Ing Size Mat'l Grout Type

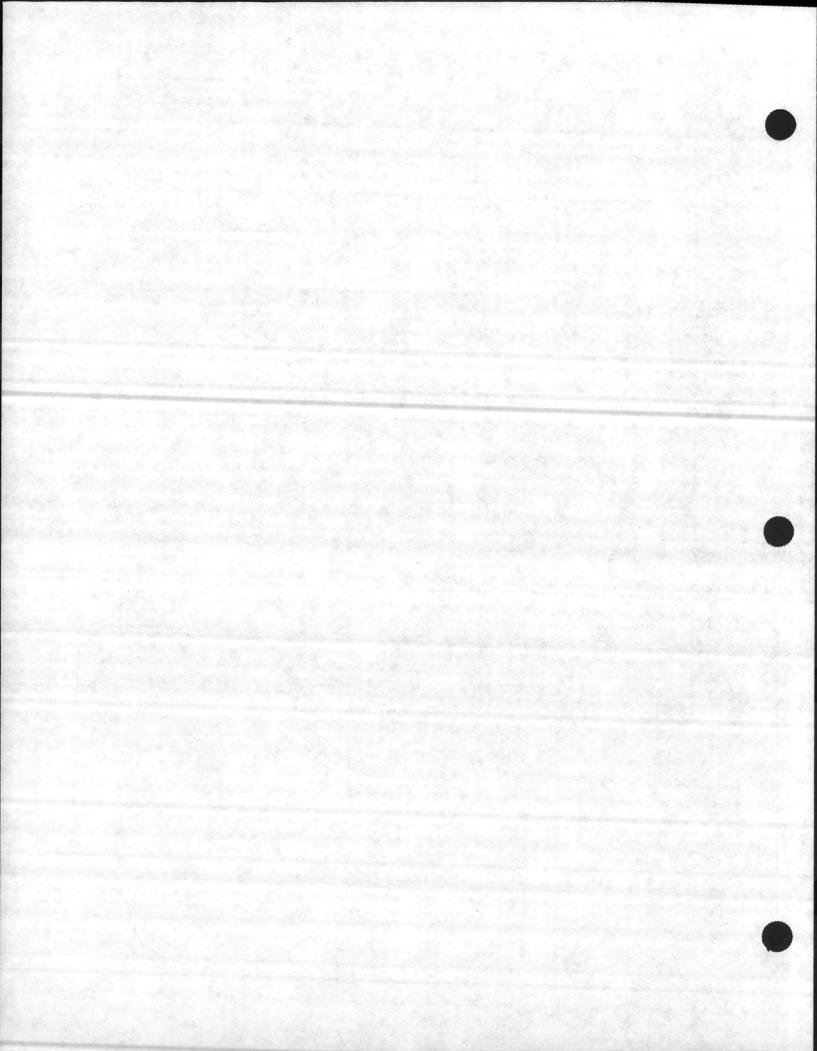
logist Development

Ate Start Finish Static Water Level

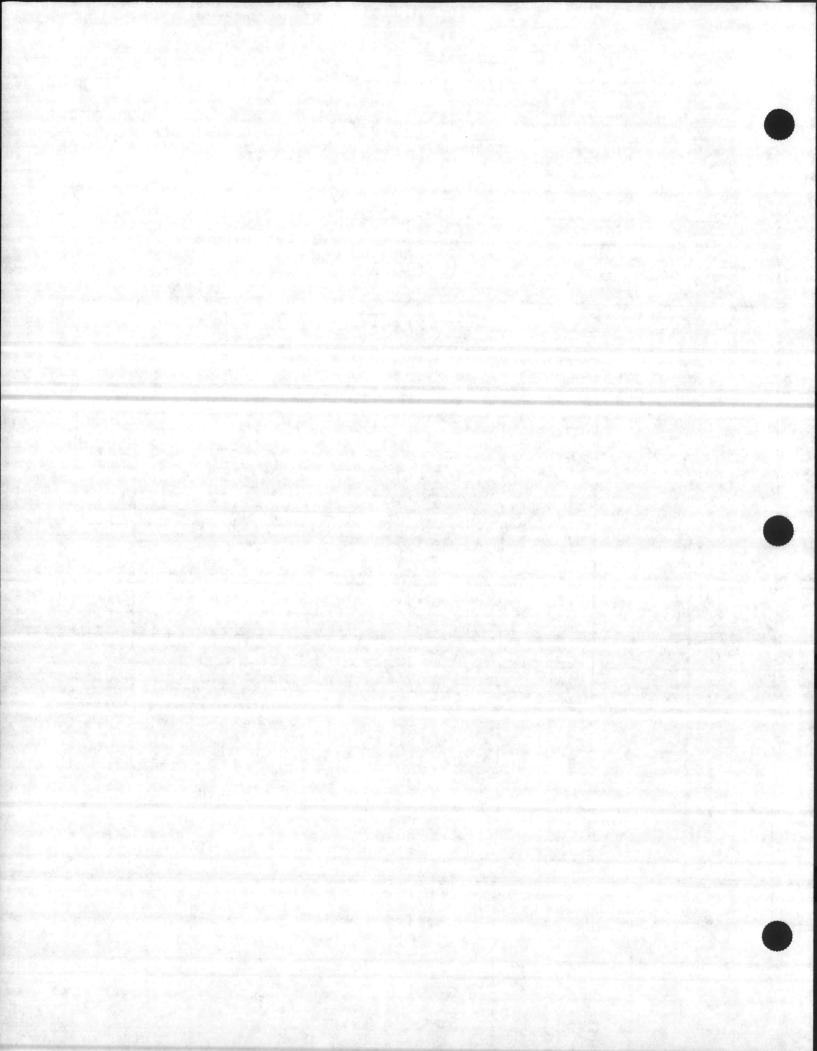
Contractor Top of Well Elevation

Driller Drill Type

Depth (feet)	Sample	Sketch	Lithology, Color	USCS	SP1
10			Sitty fine - Ve fine sand with shells + rock Fragmats		
110-115			silly fixesand and coarse sand with comented clastics shells Coarse sand angulor, clear		
115 - 170			med sond, 50% semi completed clustics (944) and Gossils, shells		
<b>5</b>	1. ·		/ (15 (26)		
150-155			Same as above (115-120)	-	
125-130			silly fine Sand with lots of shells + fossils, loarse rounded sond	ī	
130-135			Same as Above (125-130)		
135-140			with commented chisting to loosely fill of shire		

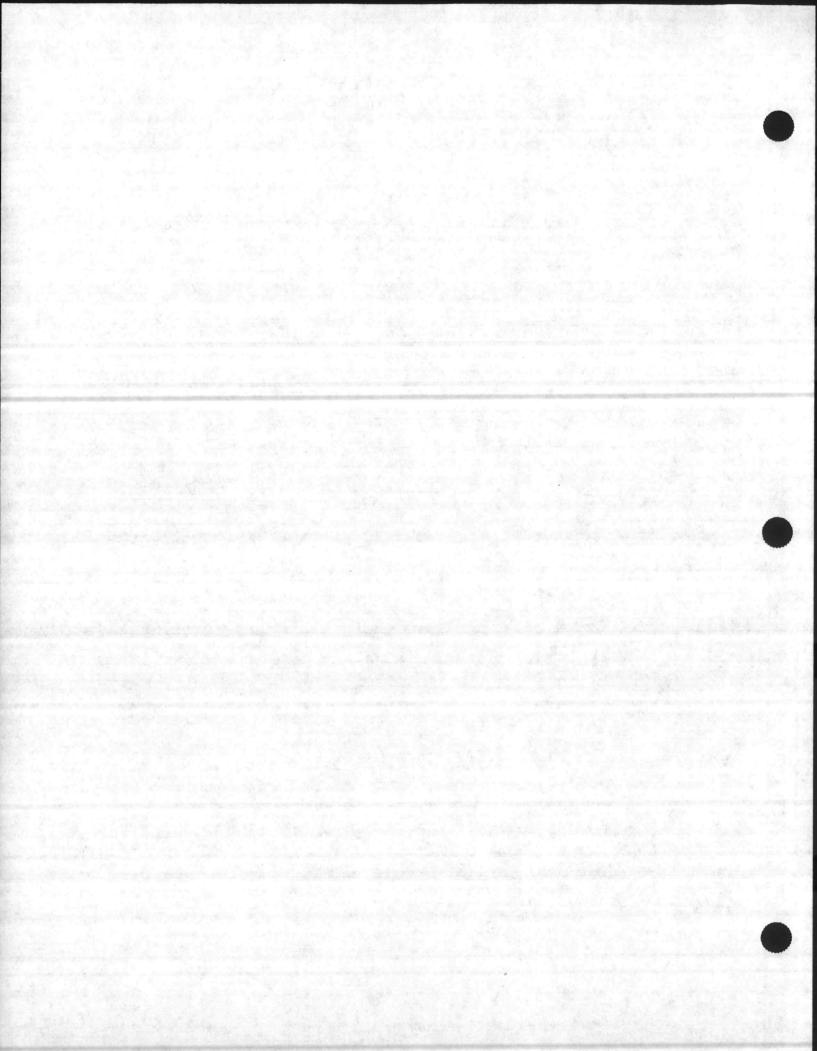


		Mat'	(2018) 1985년 1일		
ractor_		Finis			
Depth (feet)	Sample	Sketch	Lithology, Color	uscs	SI (BL,
40-145			silts fine- Mod. Sand with.  1:55 shells + Rocks, not  much coarse sand		
45-150			Some as about (140-145)  Sits fine - Med. Sand little stell + rock		
50-155		18.4	little stell + rock		ef e
				)- 	
9					



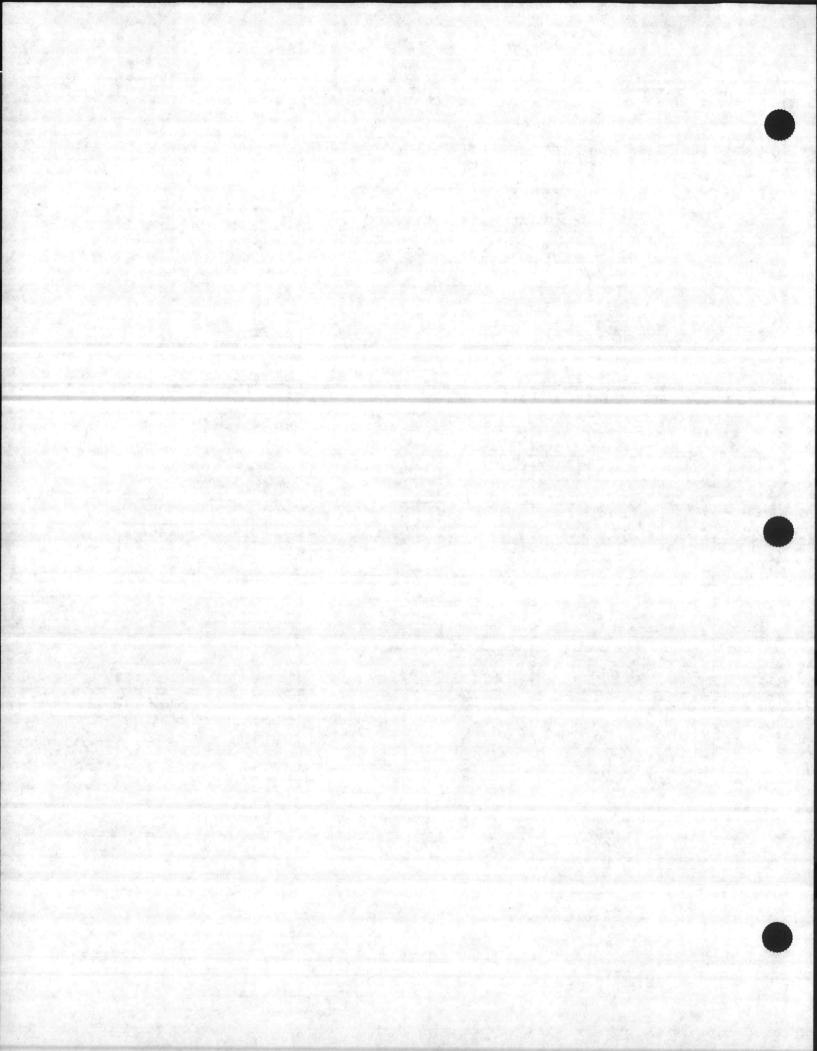
Boring No. HPGW 74-3	_ A72C	SHEET	OF_
6/18/87			
onsité 700 Am; drilling	begins 715		
Dishlows		. (	- <u> </u>
1030 Am Pomp Braice down	1 1616 60		91, 945, 97
6/15/87 B(HPGWZ4-3)			4.535
Rig set up and drillin	Drilles	(40 hole	closed
0930 - Rigis Rols cloage	d, Helper	gets a	ater
- 1030 - Mailling Rocume	(		The second secon
1130 - Dill bregts do	me aet	frim Ra	leigh
neen neur pur start up tuts	Jay 21.	<u> </u>	
6/16/87 (4PGW ZH-3) On site 08:	30 duit	42 91114	
	1.	11. R	
1200 pm 1430 dulling stops	1- 1.1	begin pulling	Rads.
(130 21500) 1300 Simen Flasing	alke	1. hour d	rille
1200 pm 1430 drilling stops (130'21500) 1500 Sinun + Casing Closes, Casing stock Pulls (asing + sinun out	1630	off pos 7	<del>/</del> :
6/17/87			
Casife 6700 D	cilling begins	0800	the
Closed badly overnight	1200 pm	after the	break
diller sets 75' casing (	temporary)	casing in	Place
1350; driller begins de	rilling past	casing an	2
64 1600 bores down to	casing in	haly 16.	30:
Thanky 1700			
	DATE	SIGN	ED

SOURCE: Environmental Science and Engineering, Inc.,\_1



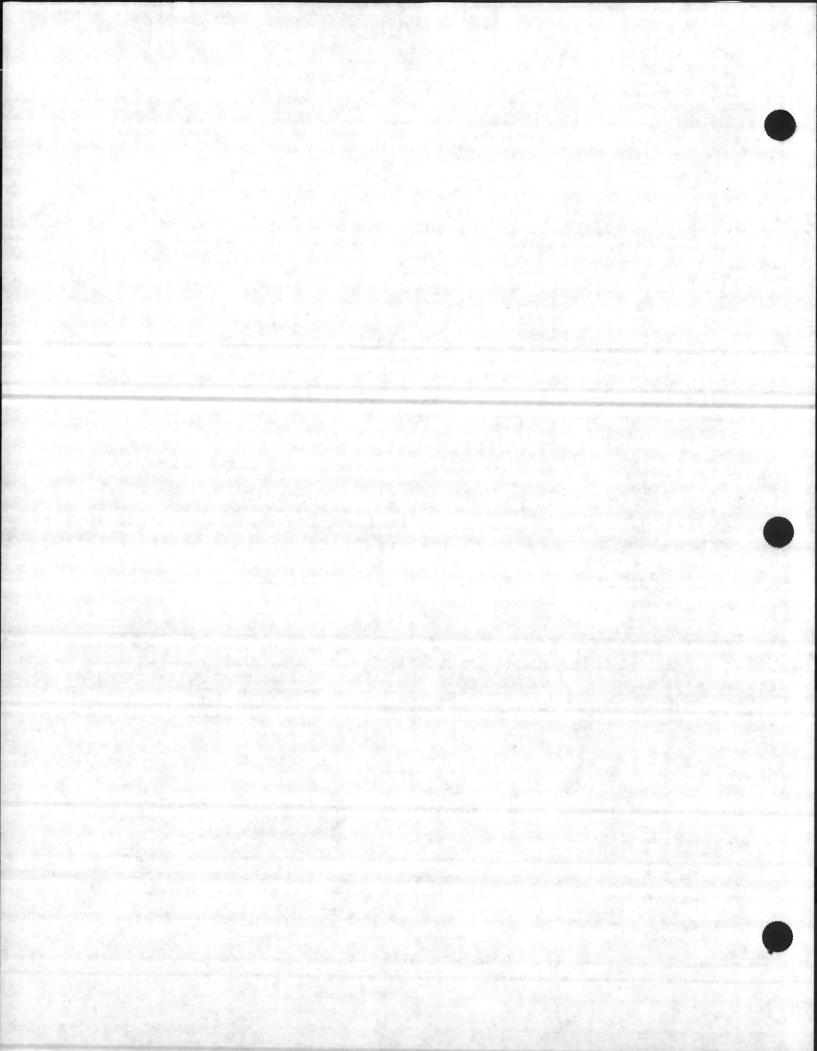
6/18/	87 H	P6W24-3	ATEC		
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1.83 stick 0	P 	Comments:	Strong (her Broke do	mudsmall swn cons	at 50'
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to Suan				MAR (	y 74-3
	) astual d 148.17		sneed ferry Rd	Bldg	Bldg # 902
			mon Rd	¥903	# YUZ

SOURCE: Environmental Science and Engineering, Inc., 19

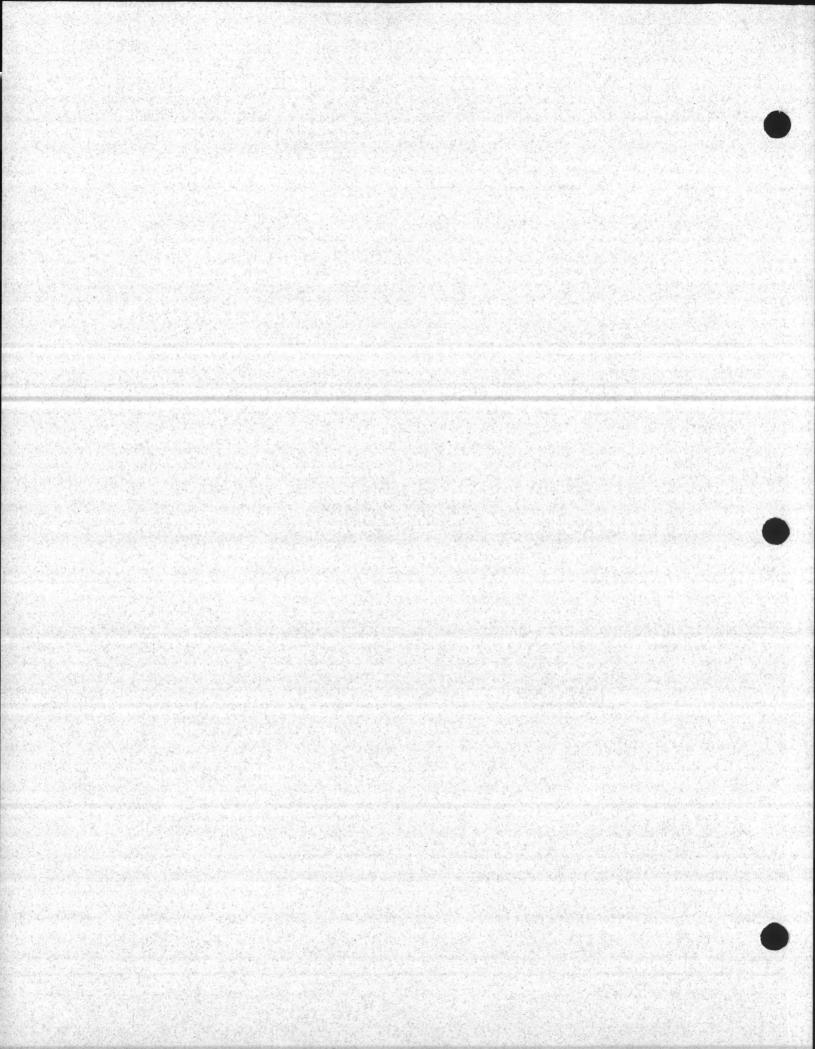


1.83 stick 0.0 1418.17 Screen + Rises (BGL, clay 128,17' RISE/ Riser (90-05) 128.17! Screen 20' Screen 150.00

21.83



APPENDIX M SEWER CAPACITY STUDY



# FINAL

# SEWER CAPACITY STUDY

HADNOT POINT INDUSTRIAL AREA MARINE CORPS BASE CAMP LEJEUNE ONSLOW COUNTY, NORTH CAROLINA

**CONTRACT TASK ORDER 0017** 

Prepared For:

DEPARTMENT OF THE NAVY
ATLANTIC DIVISION
NAVAL FACILITIES
ENGINEERING COMMAND
Norfolk, Virginia

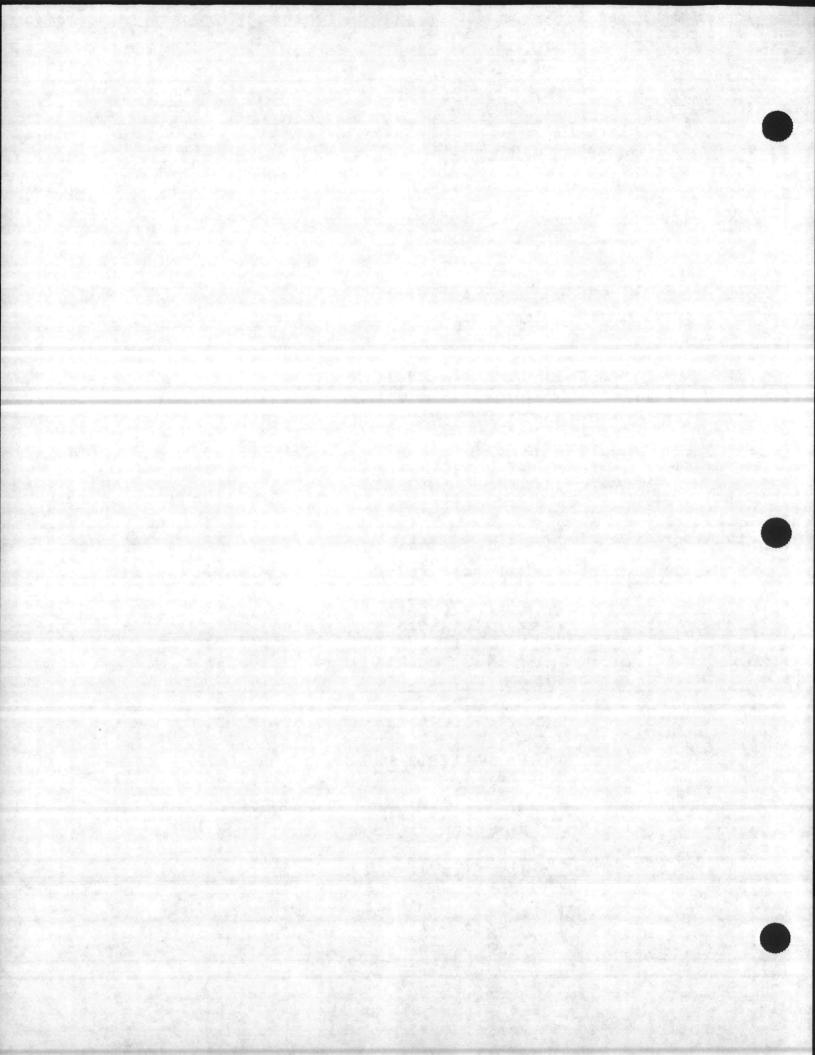
Under the:

LANTDIV CLEAN Program Contract N62470-89-D-4814

Prepared By:

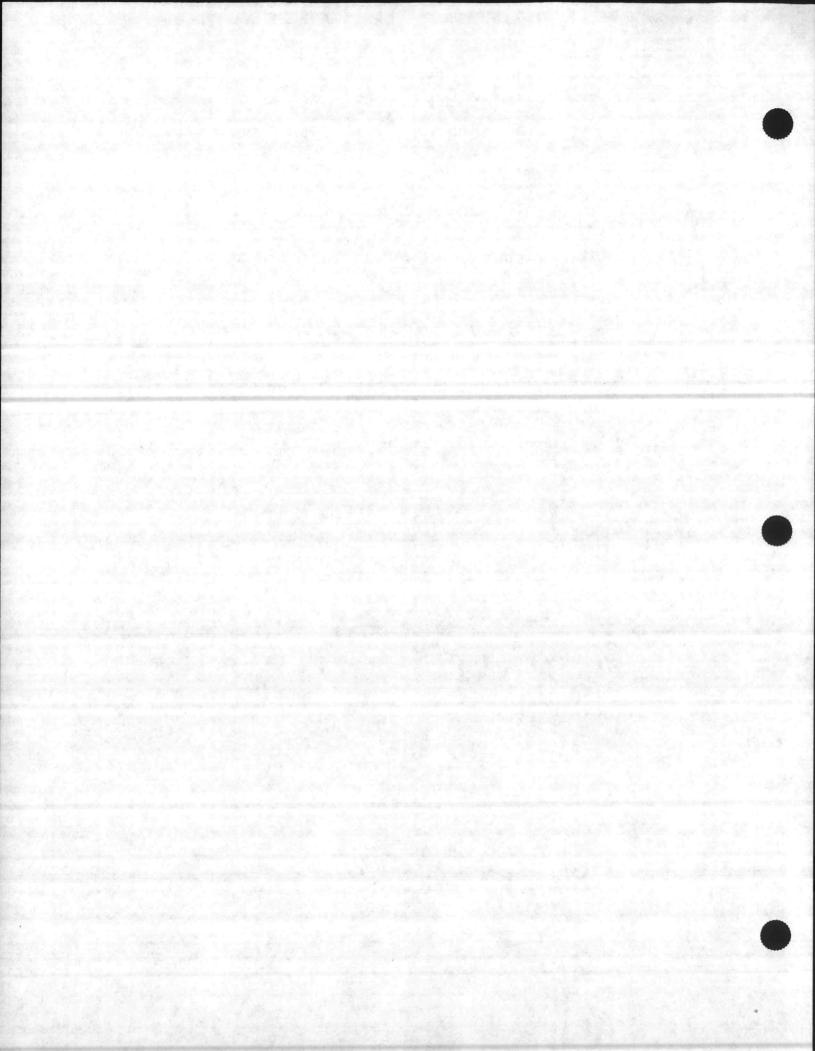
BAKER ENVIRONMENTAL, INC. Coraopolis, Pennsylvania

MARCH 11, 1993



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### 1.0 INTRODUCTION

This report documents the Sewer Capacity Study for the Hadnot Point Industrial Area (HPIA) at Marine Corps Base (MCB) Camp Lejeune located in Onslow County, North Carolina. This study is based on the Remedial Design Project Plans for the Interim Remedial Action (IRA) of the Shallow Aquifer at the HPIA, as documented in the Final Record of Decision (ROD) for the HPIA Operable Unit (Baker, September 17, 1992).

This study was completed pursuant to the Revised Implementation Plan and Fee Proposal for Remedial Design Support Studies for the IRA of the Shallow Aquifer at the HPIA, MCB Camp Lejeune, Contract Task Order 001703 under the LANTDIV Clean Program, Contract N62470-89-D-4814.

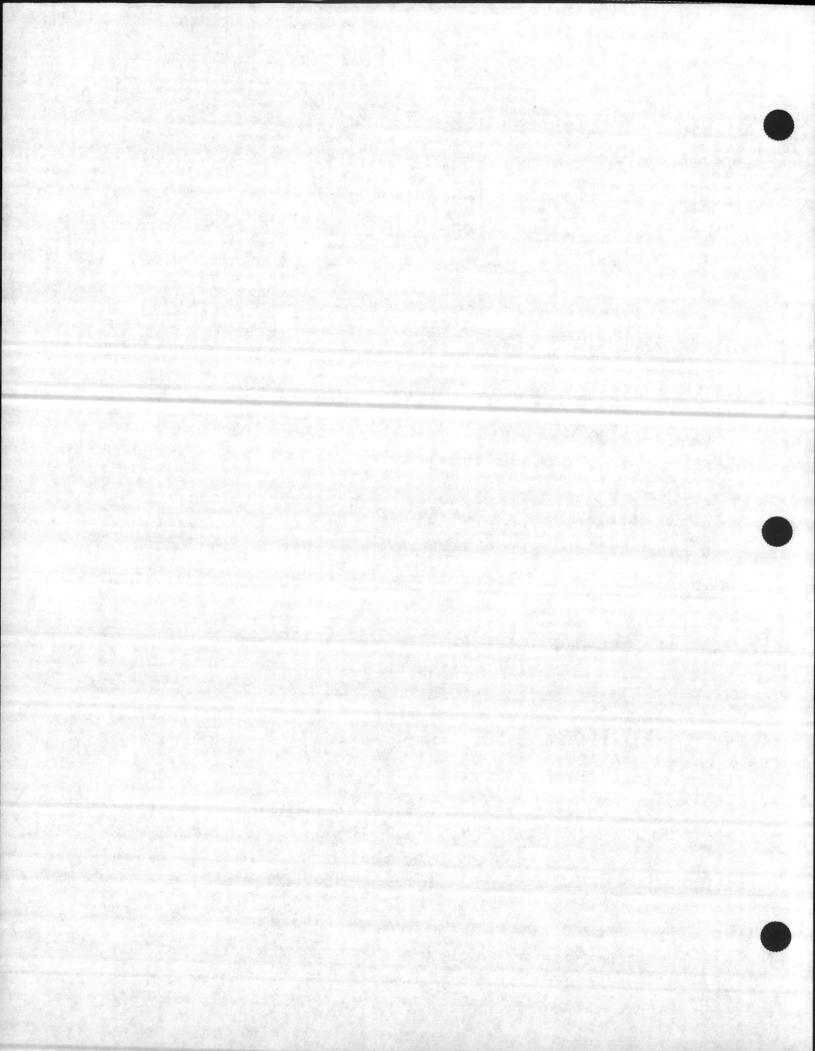
## 1.1 Objective of the Study

The objective of this study is to collect and evaluate information to determine the capacity and current usage of the sewer lines proposed for transporting treated groundwater from the two planned groundwater treatment systems located within the HPIA to the HPIA Sewage Treatment Plant (STP). This study will provide accurate sewer line usage rates in order to evaluate whether the sewer lines can handle the proposed groundwater pumping rate of between 40 gpm to 160 gpm.

#### 1.2 Site Description

The HPIA, constructed in the late 1930s, was the first facility at MCB Camp Lejeune. It was comprised of approximately 75 buildings and facilities including maintenance shops, gas stations, administrative offices, commissaries, warehouses, storage yards, and a dry cleaning facility.

Baker Environmental, Inc. (Baker) conducted an IRA Remedial Investigation (RI) and Feasibility Study (FS) for the HPIA during 1991-1992. These studies focused on the shallow groundwater aquifer beneath the HPIA and were based solely on data generated during previous field investigations. The investigations identified two contaminated groundwater plumes in the shallow aquifer at the HPIA, as shown on Figure 1-1. The FS identified seven alternatives for limiting the migration of the contamination in the shallow aquifer and reducing the concentrations of contaminants in the groundwater.

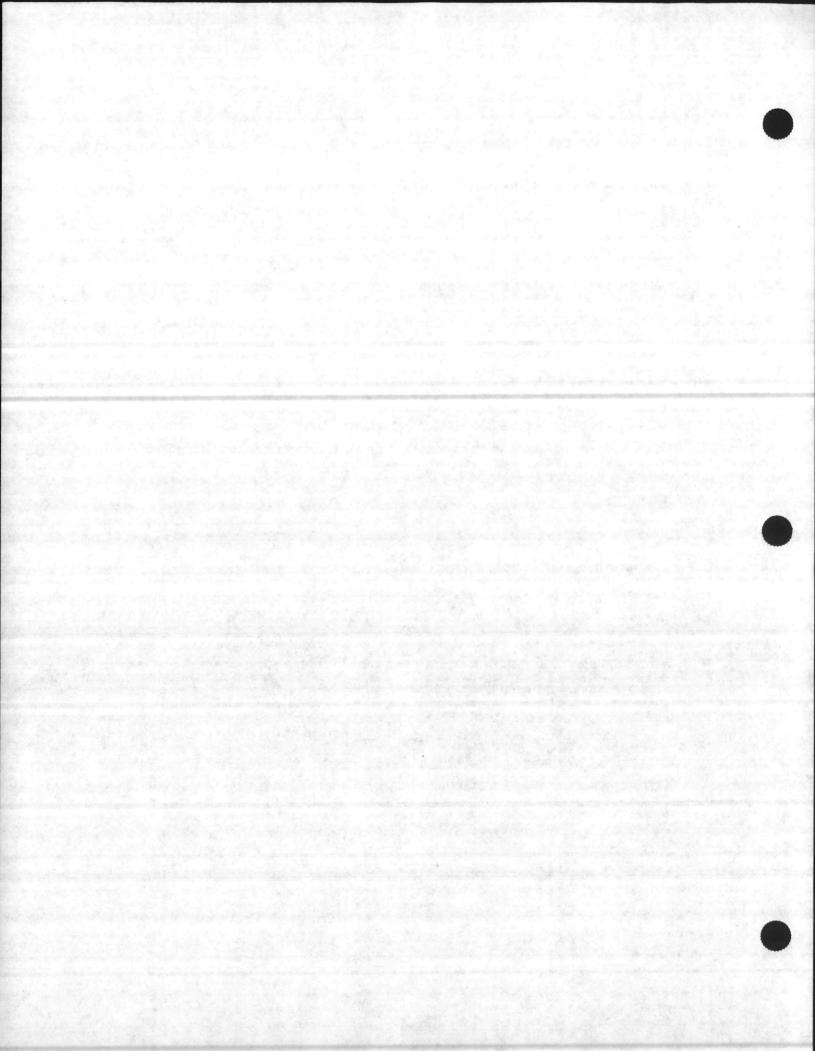


The selected interim remedial action for the shallow aquifer, as documented in the ROD, is groundwater pump-and-treat systems located at the HPIA near each contaminated plume. This IRA will be part of an overall remedy for the HPIA site which will attain protectiveness for the entire operable unit. Each treatment system will employ on-site treatment via air stripping and discharge of the treated groundwater to the sanitary sewer system for final discharge from the HPIA STP. The proposed locations of the treatment systems, as well as the proposed sewer lines to be used to convey groundwater to the STP and the flow meter locations for this study, are also shown on Figure 1-1.

The estimated flow to be added to the sanitary sewer system will come initially from four 4-inch wells installed at each of the two groundwater plumes and pumped at a rate of two to five gpm. These initial wells may contribute up to 20 gpm of groundwater flow to the sanitary sewer system from each contaminated plume. Additional wells may be added to the system as dictated by groundwater monitoring results. The maximum groundwater flow to be added to the sanitary sewer system is estimated to be 80 gpm from each contaminant plume, or a total of 160 gpm.

The sanitary sewer system conveys sanitary wastewater from both residential and industrial areas to the HPIA STP. The sewer lines are constructed of vitrified clay pipe and range in size from 8-inch at the northernmost (and upstream) portion of the sewer system to 36-inch at the inlet to the STP. The HPIA STP, located south of the HPIA area, has an operating capacity of 8 million gallons per day (MGD). The STP is a biological treatment system consisting of an aerated equalization lagoon, primary clarifiers, trickling filters, secondary clarifiers, chlorine contact chamber, anaerobic digesters, and sludge drying beds.

Final discharge of the treated groundwater from the HPIA STP is into the New River. The Environmental Protection Agency and the State of North Carolina Department of Environment, Health and Natural Resources (DEHNR) have concurred with the selection of this interim remedial alternative.



#### 2.0 FLOW MONITORING

### 2.1 Meter Installation and Monitoring

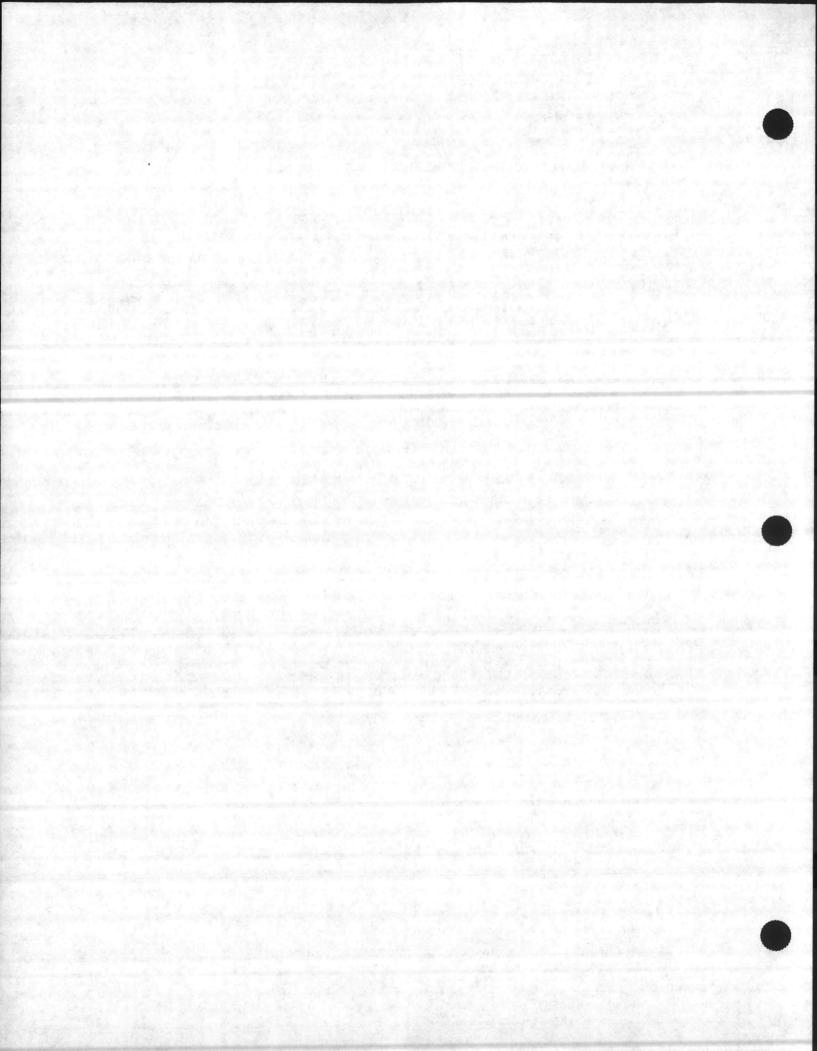
Flow monitoring was accomplished by installing a "Marsh-McBirney" Model 260 open channel flow meter in three key manholes. The flow meter was linked to a sensing device that monitored velocity and fluid level in the open channel pipe entering the manhole at predetermined time intervals. The meter recorded velocities and fluid levels and calculated flow. This data was then averaged and recorded by the meter at 30 minute intervals. Flow monitoring began on December 8, 1992 and continued through December 29, 1992.

The manholes selected for flow monitoring are shown on Figure 1-1. These manholes were selected because of their location near the point of greatest existing flow in the smallest diameter line which could service the probable tie-in location for the groundwater treatment systems. Flow meter No.1 (FM-1) was installed in the 12-inch line entering the unmarked manhole between MH 806 and MH 807, just north of Birch Street. The tie-in to the sanitary sewer system from the treatment system for the northernmost contaminated plume will most likely be at an upstream point along this 12-inch line. Flow meter No. 2 (FM-2) was installed in the 15-inch line entering MH 115, which is downstream of the probable tie-in location for the treatment system for the southernmost contaminated plume. Although possible metering locations further downstream along this line carry more flow from contributing residential areas, an increase in pipe diameter and slope compensates for this additional flow. Flow meter No. 3 (FM-3) was installed in the 8-inch line entering MH 881 in the alley south of the 900 series buildings. This location was selected to provide flow information in the event that the remedial design process relocates the proposed northernmost treatment area north towards Sneads Ferry Road or determines that a more appropriate tie-in location for the northernmost treatment system is into this 8-inch line to avoid trenching across Michael Road.

## 2.2 Rainfall Monitoring

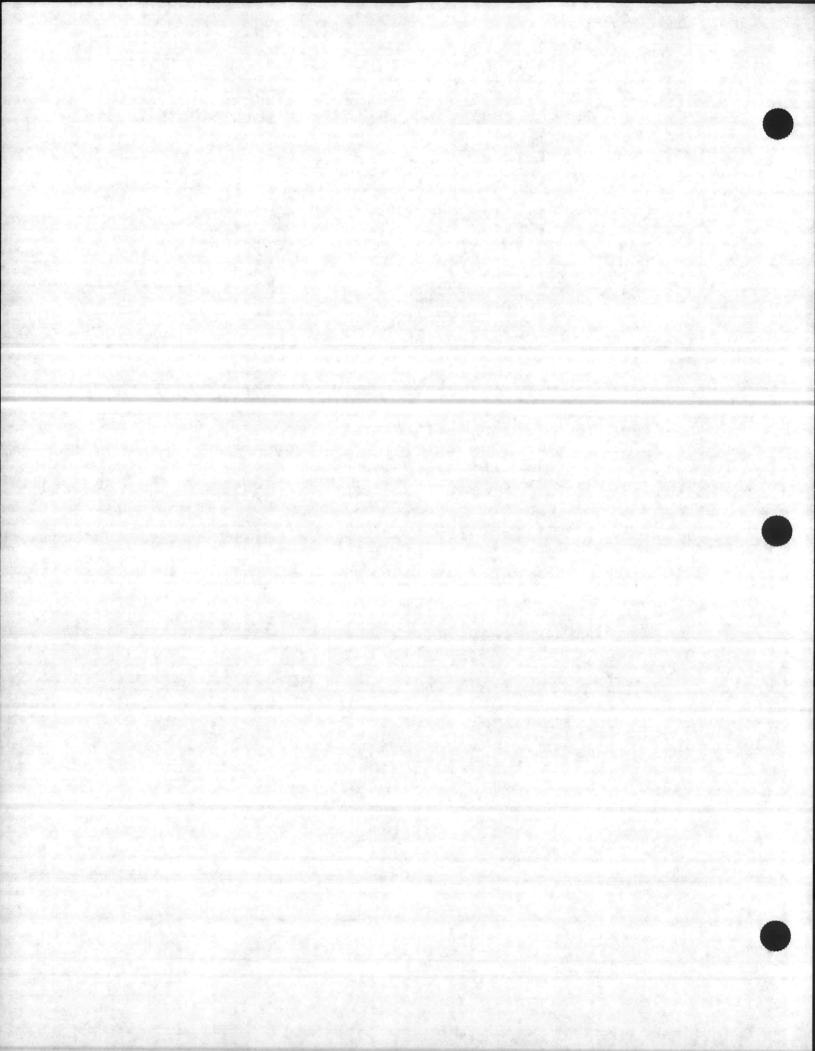
Camp Lejeune is influenced by mild winters and humid summers with elevated temperatures. Rainfall averages more than 50 inches per year. The winter and summer months are typically the wet seasons.

Cumulative rainfall totals were monitored during the flow monitoring activities at the base using a self emptying, remote indicator, rain gauge mounted to the roof of the Baker office



trailer. To supplement this effort, daily rainfall data was obtained from the Marine Air Station in Jacksonville.

Total rainfall during the period recorded, December 8 through December 29, 1992, averaged 3.75 inches, with the majority of it falling during one rainfall event on December 10, 1992.



#### 3.0 CAPACITY REPORT

# 3.1 Line Capacities

Table 3-1 presents the calculated line capacities for the three line segments of the HPIA sewer system which were monitored during this study. The calculations for flow are based on Manning's equation for maximum flow in open pipes, using a depth to diameter at 93.8 percent and the specific n value for the identified type of pipe (vitrified clay).

## 3.2 Observations

During the installation of the flow meters, a large amount of sediment build-up was observed, particularly in the 8-inch line running along the alley behind the 900 series buildings. This sediment extended upstream into the pipes as far as could be observed. The depth of sediment in the 15-inch pipe at MH 115 and the 12-inch pipe at the manhole between MH 806 and MH 807 was approximately 2 inches. The depth of sediment in the 8-inch pipe at MH 881 was 4 inches. The only useful data acquired from the meters are flow level readings, perhaps as a result of irregular hydraulic conditions resulting from this sediment buildup or other undefinable conditions. The level data have been converted by equation to produce estimated flow quantities, as shown in Table 3-1.

#### 3.3 Monitoring Results

Table 3-1 provides selected data acquired during the flow monitoring period. For each day of monitoring, the maximum depth of flow for the AM period and the PM period is shown, along with the time of occurrence. Using Manning's equation, depth of flow has been converted to flow in cfs, and subtracted from the calculated line capacity to determine the excess capacity remaining in the pipe to accommodate the addition of flow from the groundwater pump-and-treat system. Excess capacity is presented in cubic feet per minute and gallons per minute.

As shown in the table, under normal operating conditions there is on average 25 GPM of excess capacity in the 8-inch line at MH 881, 270 GPM of excess capacity in the 12-inch line at MH 806.5, and 327 GPM of excess capacity in the 15-inch line at MH 115. Under normal operating conditions the sewer system is flowing at a maximum of 86 percent of capacity at MH 881, 50 percent of capacity at MH 806.5, and 53 percent of capacity at MH 115.

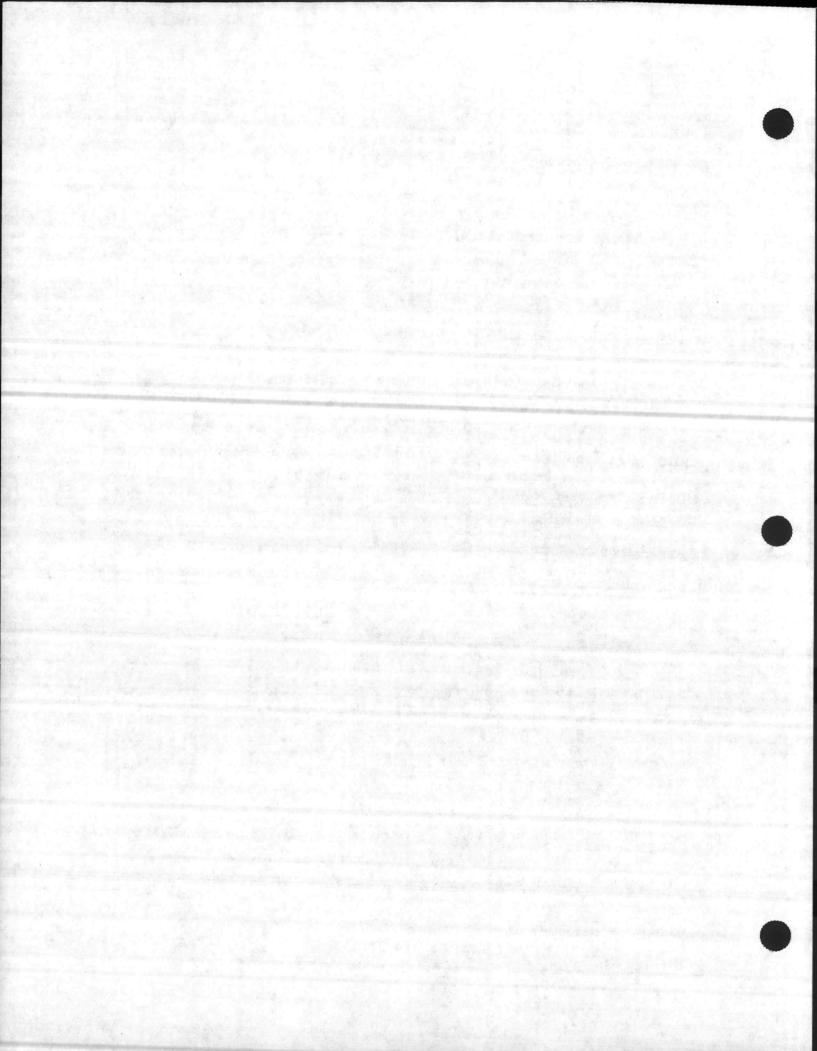


Table 3-1 Flow Monitoring Results MH 881 - 8 Inch Diameter Pipe

DATE	PEAK TIME	DEPTH	FLOW	LINE CAPCITY	EXCESS CAPACITY	EXCESS CAPACITY
		(IN)	(CFS)	(CFS)	(CFS)	(GPM)
08-Dec	05:24 PM	5.80	0.30	0.36	0.07	30.4
09-Dec	09:54 AM	5.90	0.30	0.36	0.06	27.6
09-Dec	10:24 PM	6.40	0.33	0.36	0.03	14.9
10-Dec	11:54 AM	surcharge	n/a	n/a	n/a	n/a
10-Dec	02:54 PM	surcharge	n/a	n/a	n/a	n/a
11-Dec	10:54 AM	6.00	0.31	0.36	0.06	24.9
11-Dec	09:24 PM	6.60	0.34	0.36	0.02	10.6
12-Dec	12:54 AM	6.00	0.31	0.36	0.06	24.9
12-Dec	12:54 PM	5.70	0.29	0.36	0.07	33.2
13-Dec	01:24 AM	5.60	0.28	0.36	0.08	36.2
13-Dec	06:54 PM	5.60	0.28	0.36	0.08	36.2
14-Dec	01:24 AM	6.10	0.31	0.36	0.05	22.2
14-Dec	11:54 PM	6.80	0.35	0.36	0.02	6.9
15-Dec	07:24 AM	6.20	0.32	0.36	0.04	19.7
15-Dec	04:54 PM	5.90	0.30	0.36	0.06	27.6
16-Dec	01:54 AM	6.60	0.34	0.36	0.02	10.6
16-Dec	12:24 PM	6.00	0.31	0.36	0.06	24.9
17-Dec	11:54 AM	6.20	0.32	0.36	0.04	19.7
17-Dec	01:24 PM	5.80	0.30	0.36	0.07	30.4
18-Dec	11:24 AM	6.00	0.31	0.36	0.06	24.9
18-Dec	03:54 PM	6.40	0.33	0.36	0.03	14.9
19-Dec	11:54 AM	6.40	0.33	0.36	0.03	14.9
19-Dec	12:24 PM	6.00	0.31	0.36	0.06	24.9
20-Dec	01:54 AM	5.90	0.30	0.36	0.06	27.6
20-Dec	05:54 PM	5.90	0.30	0.36	0.06	27.6
21-Dec	10:54 AM	6.00	0.31	0.36	0.06	24.9
21-Dec	12:54 PM	5.80	0.30	0.36	0.07	30.4
22-Dec	11:54 AM	6.30	0.33	0.36	0.04	17.2
22-Dec	01:24 PM	5.90	0.30	0.36	0.06	27.6
23-Dec	03:54 AM	6.10	0.31	0.36	0.05	22.2
23-Dec 23-Dec	09:24 PM	6.30	0.33	0.36	0.04	17.2
24-Dec	09:24 AM	6.20	0.32	0.36	0.04	19.7
24-Dec 24-Dec	08:24 PM	5.70	0.32	0.36	0.07	33.2
25-Dec	09:54 AM	5.70	0.29	0.36	0.07	33.2
25-Dec 25-Dec	04:24 PM	5.80	0.29	0.36	0.07	30.4
26-Dec	12:24 AM	6.30	0.33	0.36	0.04	17.2
26-Dec 26-Dec	02:54 PM	5.70	0.33	0.36	0.07	33.2
27-Dec	04:24 AM	5.90	0.29	0.36	0.06	27.6
	06:24 PM	5.70	0.30	0.36	0.07	33.2
27-Dec	06:24 PM 07:54 AM	5.80	0.29	0.36	0.07	30.4
28-Dec		5.90	0.30	0.36	0.07	27.6
28-Dec	07:24 PM 10:54 AM		0.30	0.36	0.00	19.7
29-Dec	10:34 AM	6.20	0.32	0.30	AVG	25

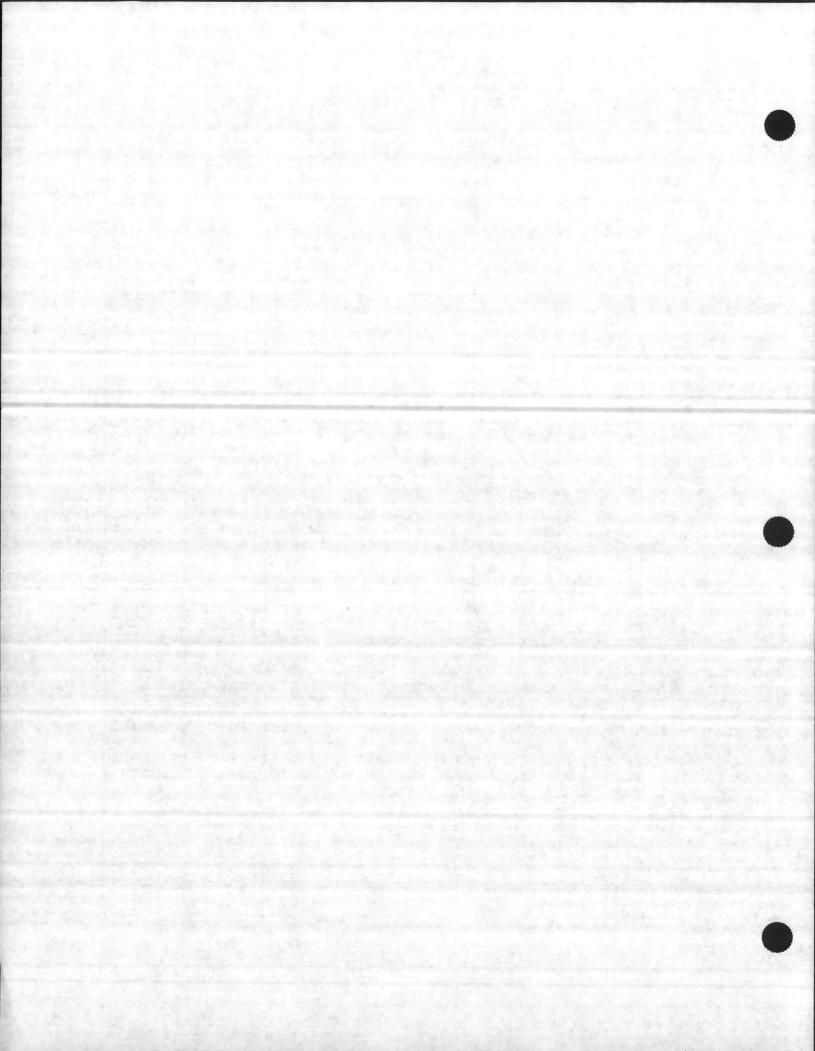


Table 3-1 (continued)
Flow Monitoring Results
MH 806.5 - 12 Inch Diameter Pipe

	PEAK			LINE	EXCESS	EXCESS
DATE	TIME	DEPTH	FLOW	CAPACITY	CAPACITY	CAPACIT
		(IN)	(CFS)	(CFS)	(CFS)	(GPM)
08-Dec	09:49 AM	7.63	0.83	1.22	0.39	189.4
08-Dec	12:19 PM	4.93	0.61	1.22	0.61	295.9
09-Dec	05:49 AM	6.63	0.67	1.22	0.55	268.2
09-Dec	12:49 PM	5.63	0.58	1.22	0.64	310.5
10-Dec	06:19 AM	surcharge	n/a	n/a	n/a	n/a
10-Dec	12:19 PM	surcharge	n/a	n/a	n/a	n/a
11-Dec	11:49 AM	6.63	0.67	1.22	0.55	268.2
11-Dec	10:49 PM	5.93	0.57	1.22	0.65	316.6
12-Dec	05:49 AM	5.93	0.57	1.22	0.65	316.6
12-Dec	03:49 PM	5.73	0.58	1.22	0.64	312.6
13-Dec	03:19 AM	5.73	0.58	1.22	0.64	312.6
13-Dec	02:49 PM	6.13	0.59	1.22	0.63	307.8
14-Dec	02:19 AM	6.33	0.62	1.22	0.60	292.0
14-Dec	01:19 PM	6.33	0.62	1.22	0.60	292.0
15-Dec	09:19 AM	6.83	0.70	1.22	0.52	252.4
15-Dec	12:19 PM	5.63	0.58	1.22	0.64	310.5
16-Dec	08:49 AM	7.03	0.73	1.22	0.48	236.5
16-Dec	11:49 PM	5.33	0.59	1.22	0.62	304.3
17-Dec	05:49 AM	6.63	0.67	1.22	0.55	268.2
17-Dec	08:49 PM	5.83	0.57	1.22	0.64	314.6
18-Dec	04:49 AM	7.23	0.76	1.22	0.45	220.7
18-Dec	12:49 PM	6.23	0.60	1.22	0.61	299.9
19-Dec	06:19 AM	6.23	0.60	1.22	0.61	299.9
19-Dec	05:49 PM	5.83	0.57	1.22	0.64	314.6
20-Dec	03:49 AM	5.73	0.58	1.22	0.64	312.6
20-Dec	03:49 PM	5.73	0.58	1.22	0.64	312.6
21-Dec	07:19 AM	5.93	0.57	1.22	0.65	316.6
21-Dec	01:49 PM	5.93	0.57	1.22	0.65	316.6
22-Dec	07:19 AM	6.93	0.72	1.22	0.50	244.4
22-Dec	05:19 PM	6.33	0.62	1.22	0.60	292.0
23-Dec	03:49 AM	7.23	0.76	1.22	0.45	220.7
23-Dec	09:19 PM	5.33	0.59	1.22	0.62	304.3
24-Dec	02:49 AM	5.83	0.57	1.22	0.64	314.6
24-Dec	09:19 PM	5.33	0.59	1.22	0.62	304.3
25-Dec	03:19 AM	5.63	0.58	1.22	0.64	310.5
25-Dec	03:19 PM	5.63	0.58	1.22	0.64	310.5
26-Dec	03:19 AM	5.53	0.58	1.22	0.63	308.5
26-Dec	08:19 PM	5.03	0.61	1.22	0.61	298.0
27-Dec	12:19 AM	5.13	0.60	1.22	0.61	300.1
27-Dec	07:19 PM	5.53	0.58	1.22	0.63	308.5
28-Dec	04:49 AM	6.23	0.60	1.22	0.61	299.9
28-Dec	12:49 PM	5.43	0.59	1.22	0.63	306.4
29-Dec	02:49 AM	5.63	0.58	1.22	0.64	310.5
		V St. in 1999			AVG	293

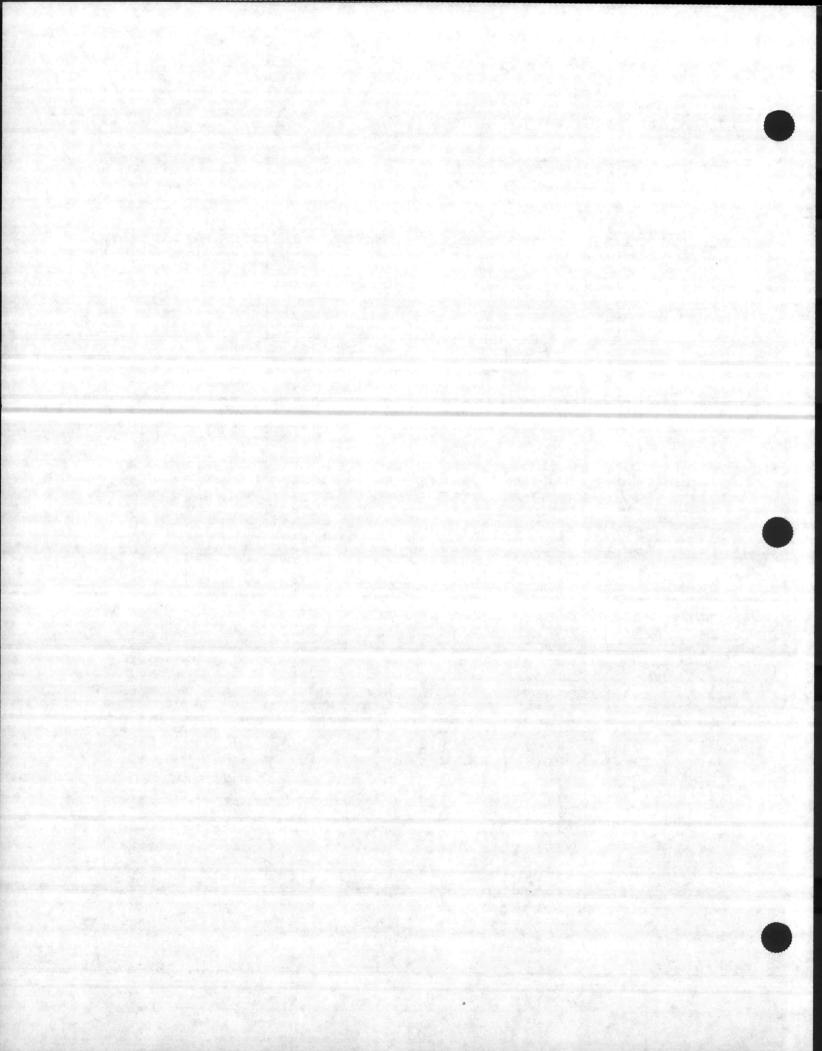
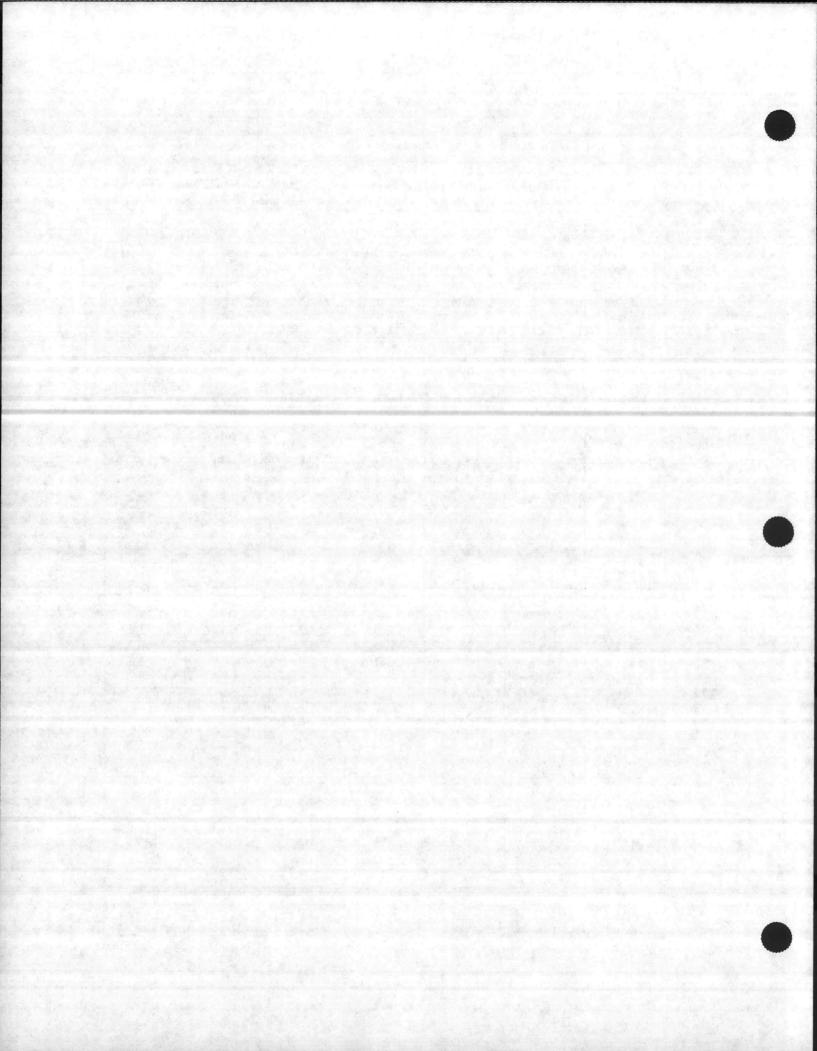
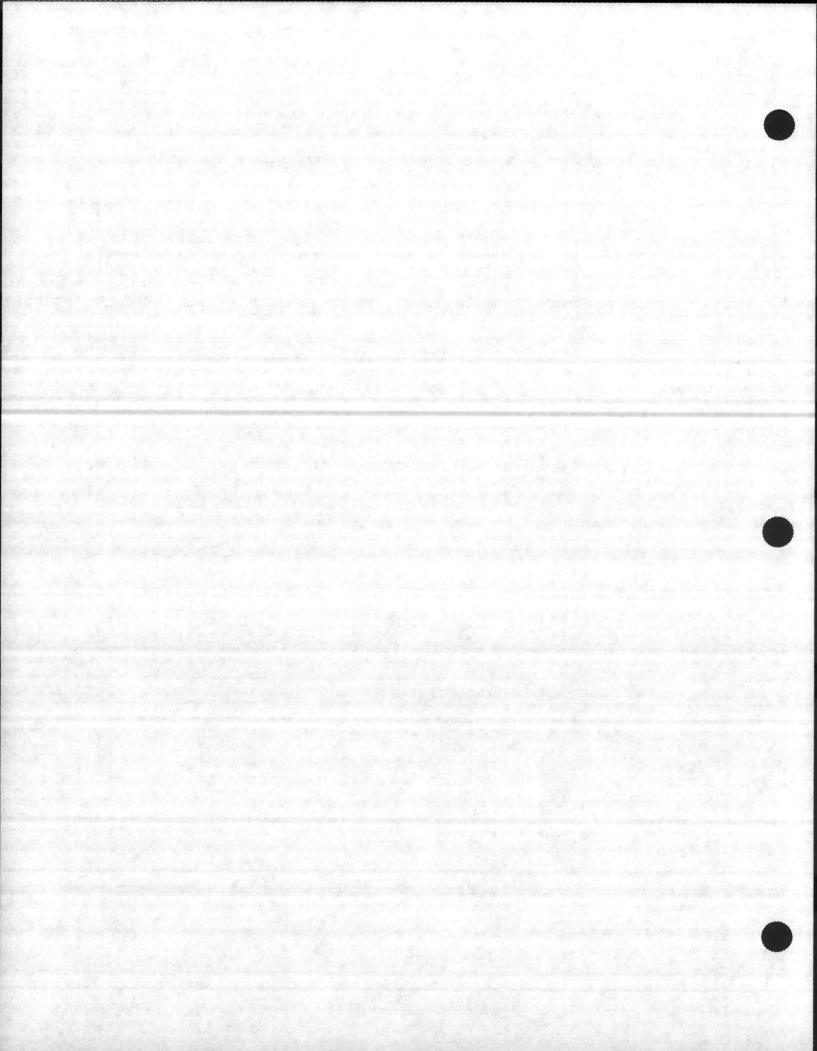


Table 3-1 (continued)
Flow Monitoring Results
MH 115 - 15 Inch Diameter Pipe

77	PEAK	act level		LINE	EXCESS	EXCESS
DATE	TIME	DEPTH	FLOW	CAPACITY	CAPACITY	CAPACITY
		(IN)	(CFS)	(CFS)	(CFS)	(GPM)
08-Dec	10:02 AM	7.70	0.75	1.54	0.79	387.2
08-Dec	12:02 PM	7.10	0.73	1.54	0.81	395.0
09-Dec	11:02 AM	7.90	0.78	1.54	0.76	371.2
09-Dec	12:02 PM	7.50	0.72	1.54	0.82	403.1
10-Dec	09:02 AM	surcharge	n/a	n/a	n/a	n/a
10-Dec	12:02 PM	surcharge	n/a	n/a	n/a	n/a
11-Dec	12:02 AM	11.80	1.38	1.54	0.16	80.3
11-Dec	12:02 PM	10.80	1.24	1.54	0.30	145.4
12-Dec	12:02 AM	7.90	0.78	1.54	0.76	371.2
12-Dec	12:32 PM	6.20	0.77	1.54	0.77	376.0
13-Dec	01:32 AM	5.60	0.80	1.54	0.74	363.6
13-Dec	04:02 PM	6.50	0.76	1.54	0.78	382.3
14-Dec	07:02 AM	7.70	0.75	1.54	0.79	387.2
14-Dec	12:02 PM	7.10	0.73	1.54	0.81	395.0
15-Dec	10:02 AM	6.60	0.75	1.54	0.79	384.5
15-Dec	12:02 PM	6.40	0.76	1.54	0.78	380.2
16-Dec	10:02 AM	6.40	0.76	1.54	0.78	380.2
16-Dec	12:02 PM	6.30	0.77	1.54	0.77	378.1
17-Dec	06:32 AM	8.20	0.83	1.54	0.71	347.1
17-Dec	12:02 PM	6.20	0.77	1.54	0.77	376.0
18-Dec	08:02 AM	6.10	0.78	1.54	0.76	373.9
18-Dec	12:02 PM	6.00	0.78	1.54	0.76	371.8
19-Dec	06:32 AM	5.30	0.81	1.54	0.73	357.8
19-Dec	12:02 PM	4.90	0.82	1.54	0.72	350.7
20-Dec	08:32 AM	5.30	0.81	1.54	0.73	357.8
20-Dec	12:32 PM	5.40	0.81	1.54	0.74	359.7
21-Dec	05:02 AM	6.70	0.75	1.54	0.79	386.6
21-Dec	01:02 PM	7.30	0.72	1.54	0.82	399.1
22-Dec	08:32 AM	6.50	0.76	1.54	0.78	382.3
22-Dec	12:02 PM	5.60	0.80	1.54	0.74	363.6
23-Dec	05:02 AM	5.80	0.79	1.54	0.75	367.6
23-Dec	12:32 PM	4.40	0.84	1.54	0.70	343.4
24-Dec	06:02 AM	5.80	0.79	1.54	0.75	367.6
24-Dec	05:02 PM	5.00	0.82	1.54	0.72	352.4
25-Dec	07:32 AM	5.70	0.79	1.54	0.75	365.6
25-Dec	04:02 PM	5.20	0.81	1.54	0.73	356.0
26-Dec	04:32 AM	6.30	0.77	1.54	0.77	378.1
26-Dec	08:32 PM	6.50	0.76	1.54	0.78	382.3
27-Dec	10:02 AM	7.30	0.72	1.54	0.82	399.1
27-Dec	06:02 PM	9.00	0.96	1.54	0.58	282.8
28-Dec	05:02 AM	9.90	1.11	1.54	0.43	212.0
28-Dec	02:02 PM	7.20	0.73	1.54	0.81	397.0
29-Dec	05:02 AM	8.10	0.81	1.54	0.73	355.2
					AVG	355



During the significant rainfall event of December 10 which measured 3.67 at the Marine Air Station in Jacksonville, all of the monitored manholes experienced surcharge conditions. This means that due to inflow and/or infiltration, the flow of water exceeded the capacity of the sewer system, and as a result water backed up in the monitored manholes. Inflow is water discharged into sewer pipes from sources such as foundation drains, roof drains, cellars or from other commercial or industrial establishments. Infiltration is groundwater entering sewers through defective joints and broken or cracked pipe or manholes. The height of surcharge in MH 881 (FM-3) was recorded at 17 inches. More severe surcharges were measured by FM-1 at MH 806.5 (62 inches) and by FM-2 at MH 115 (46 inches).



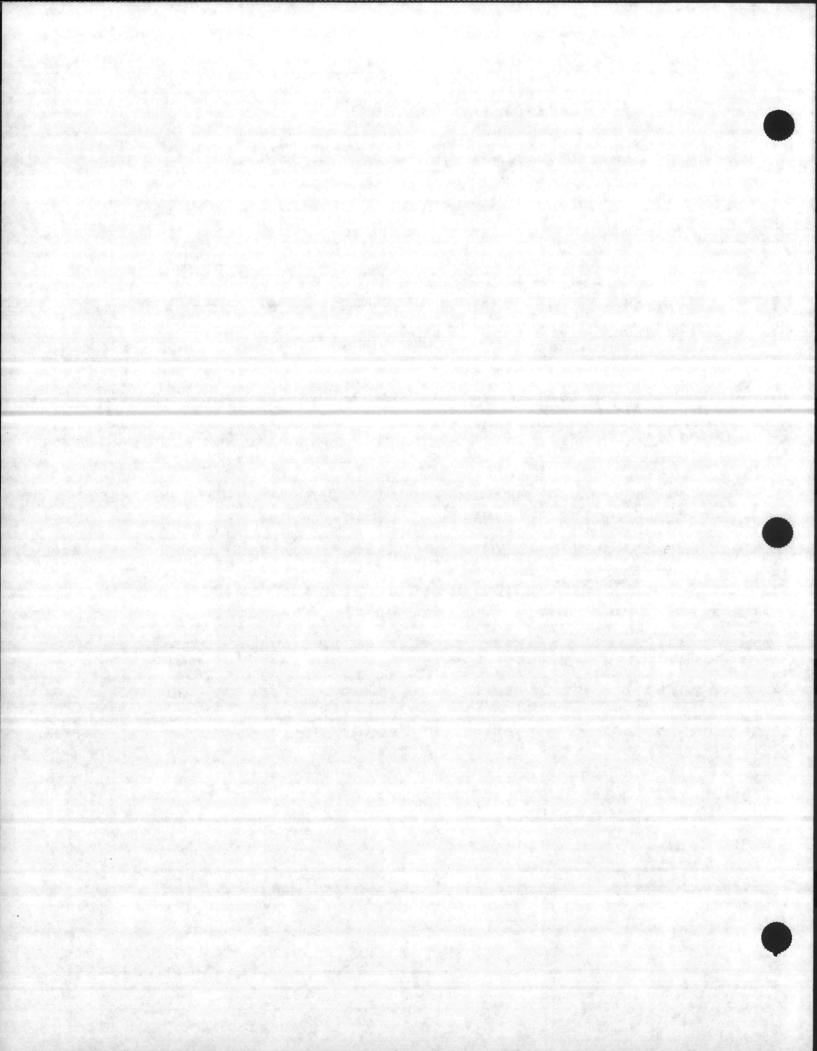
#### 4.0 SUMMARY AND RECOMMENDATIONS

This sewer capacity study involved the flow monitoring of three key manholes within the HPIA sanitary sewer system. Information was obtained which will assist in the design of the proposed groundwater pump-and-treat for the Interim Remedial Action of the Shallow Aquifer at the HPIA.

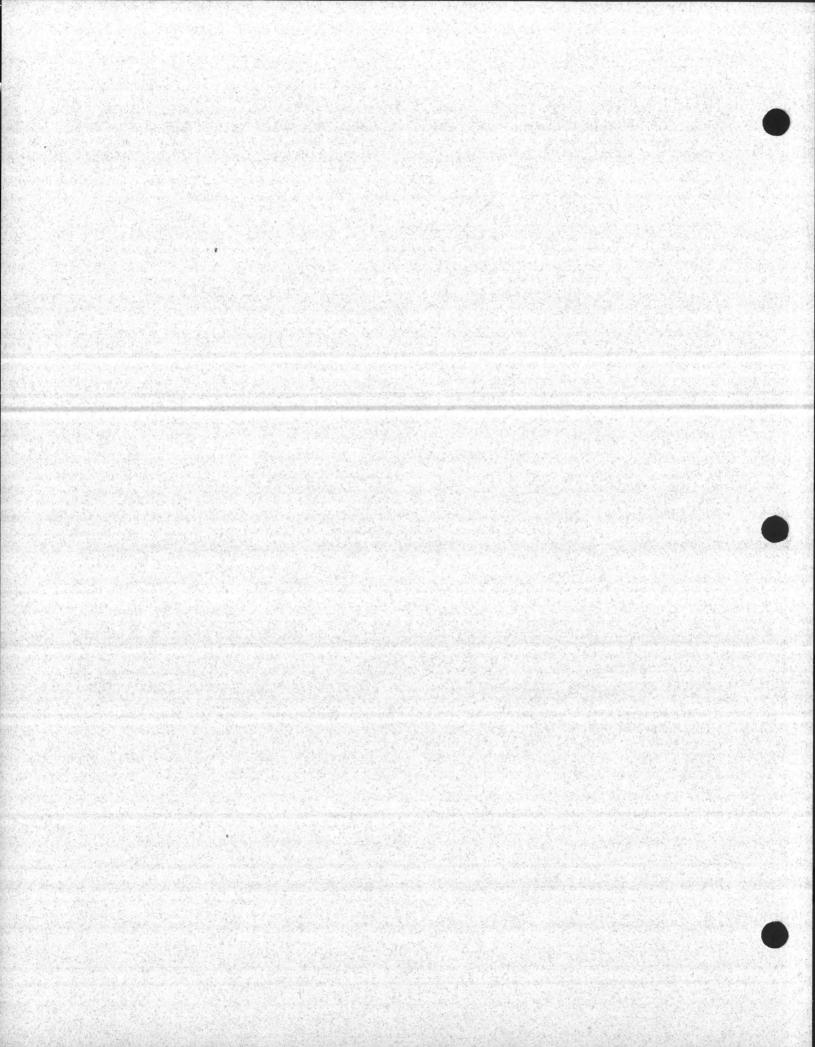
Under normal operating conditions, there is sufficient excess capacity in the 12-inch and larger sewer lines to accept the anticipated additional flow of 40 GPM to 160 GPM of treated groundwater. Based on the monitoring results, it is recommended that the 8-inch line not be used as a tie-in location for the system.

During severe rainfall events, inflow and infiltration result in excessive flows in the sewer system causing surcharges at the manholes. Design details should be incorporated into the pump-and-treat system to protect against extreme surcharges. These include a check valve in the clean water discharge line to prevent backflow, and a level switch at the clean water sump to stop groundwater pumping when excessive hydraulic head due to surcharging is encountered.

As a secondary, long-term recommendation, cleaning of the sewer lines, particularly the 8inch lines, and grouting of the lines based on closed circuit television inspection would be beneficial to the cost-effective operation of the HPIA Sewage Treatment Plant.



APPENDIX N AIR STRIPPER EMISSIONS REPORT



#### Introduction

The purpose of this document is to review the air quality impact of an air stripper that is being considered as part of a groundwater treatment system for remediating a former fuel tank farm located at the United States Marine Corps Base Camp Lejeune in Onslow County, North Carolina.

Previous studies indicate that the shallow groundwater is contaminated with benzene, 1,2-dichloroethene (1,2-DCE), trichloroethene (TCE), and vinyl chloride (VC). These volatile organic compounds (VOCs) will be stripped from the groundwater to a gaseous stream that will be exhausted to the atmosphere.

#### Emissions Estimation

The maximum concentrations of the VOCs emitted from the air stripper are shown below:

benzene	7,900	ug/l
1,2-DCE	42,000	ug/l
TCE	14,000	ug/l
VC	360	ug/l

Assuming worst-case conditions, the maximum concentration of each VOC will be emitted continuously during the operation of the air stripper. Hourly VOC emissions may be estimated as follows:

Hourly Max VOC Stripper 
$$60 \text{ min} \times 100 \text$$

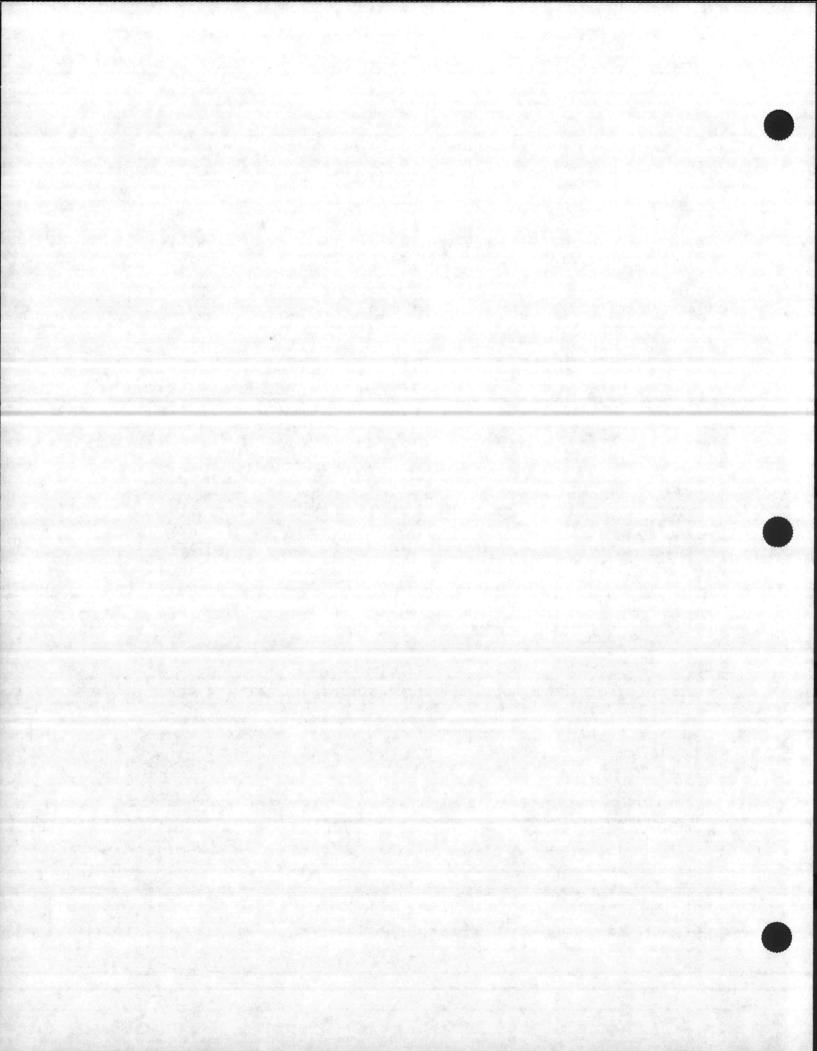
The stripper exhaust flowrate is assumed to be 80 gal/min. Combining all constants in the equation above yields the following equation:

Hourly  
Emissions = 
$$4x10^{-5}$$
 (Max VOC Concentration, ug/l)  
(lb/hr)

Daily VOC emissions may be estimated based on an assumed air stripper operation of 24 hours per day.

Annual VOC emissions may be estimated based on an assumed air stripper operation of 365 days per year.

15-minute VOC emissions may be estimated from the hourly emissions be assuming that 1/4 of the hourly emissions are emitted during each 15-minute interval.



Benzene, 1,2-DCE, TCE, and VC airborne emissions from the air stripper are shown in Table 1.

#### Regulatory Review

The following North Carolina air regulations are applicable to the air stripper.

15A NCAC 2D.0518 - Miscellaneous Volatile Organic Compound Emissions

This rule states the following:

"A person shall not discharge from all sources at any one plant site more than a total of 40 pounds of photochemically reactive solvent into the atmosphere in any one day, from any article, machine, equipment, or other contrivance used for employing, applying, evaporating, or drying any photochemically reactive solvent or substance containing such solvent unless the discharge has been reduced by at least 85 percent by weight."

This rule implies that the 85 percent VOC emission reduction must be achieved site-wide but not necessarily by each emission source. Thus, some emission sources may achieve greater than 85 percent reduction, while others may be controlled to a less stringent level as long as the overall 85 percent reduction is achieved.

It is unclear whether of not MCB Camp Lejeune is currently complying with this rule. If the base currently is complying, then an evaluation must be performed to determine if it would be most cost-effective to install an 85 percent efficient control device onto the exhaust of the air stripper or to offset the increased emissions from an uncontrolled air stripper by reducing emissions from another source or to employ some intermediate strategy.

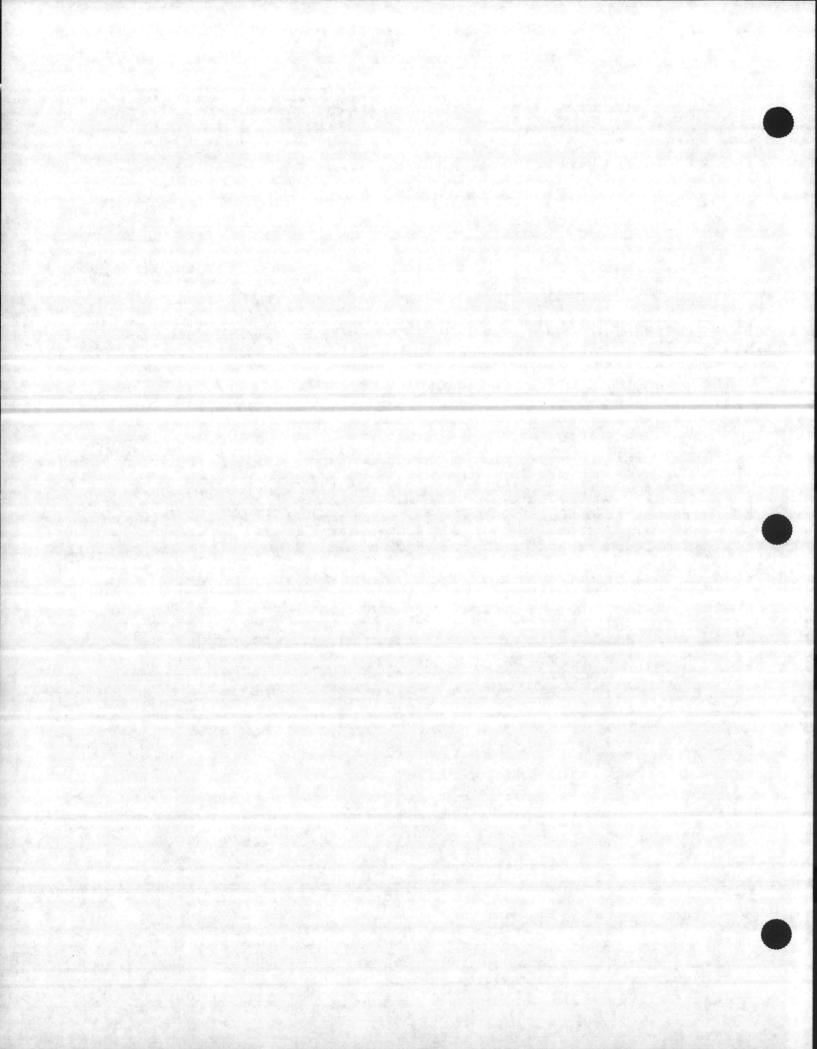
If the base currently is not complying, then a site-wide evaluation must be performed to determine the most cost-effective strategy to meet the rule.

15A NCAC 2H.0600 - Air Quality Permits

This rule requires that a permit to emit toxic air pollutants be obtained from any facility whose actual emissions from all sources exceed <u>de minimis</u> emission rates for any of 105 listed air toxic compounds.

The <u>de minimis</u> emission rates for benzene, 1,2-DCE, TCE, and VC are shown in Table 2.

MCB Camp Lejeune is already in the process of obtaining an air permit per this rule. An air emissions inventory



performed by Baker Environmental, Inc. revealed that the site exceeds several of the <u>de minimis</u> air toxic emission rates listed in this rule.

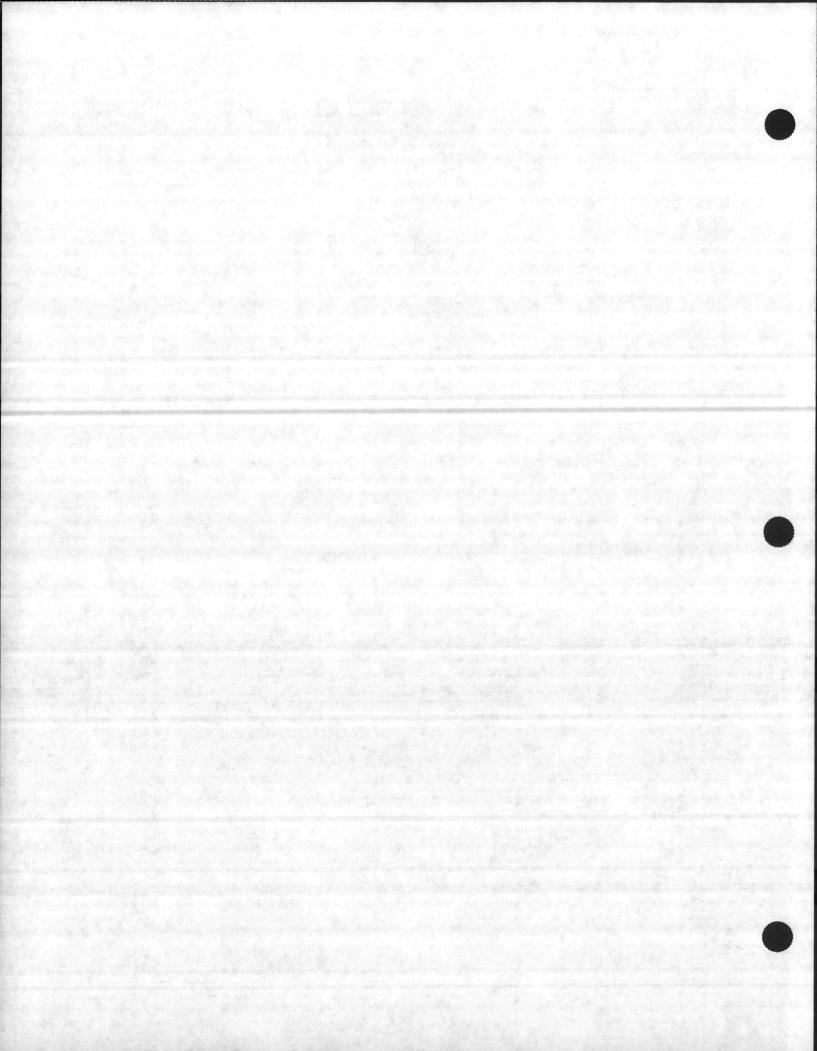


TABLE 1
AIR STRIPPER AIRBORNE EMISSIONS

Pollutant		Emission Rate		
	lb/15-min	lb/hr	lb/day	lb/yr
Benzene	0.079	0.32	7.6	2,770
1,2-DCE	0.42	1.7	40	14,720
TCE	0.14	0.56	14	4,906
VC	0.0036	0.014	0.35	130

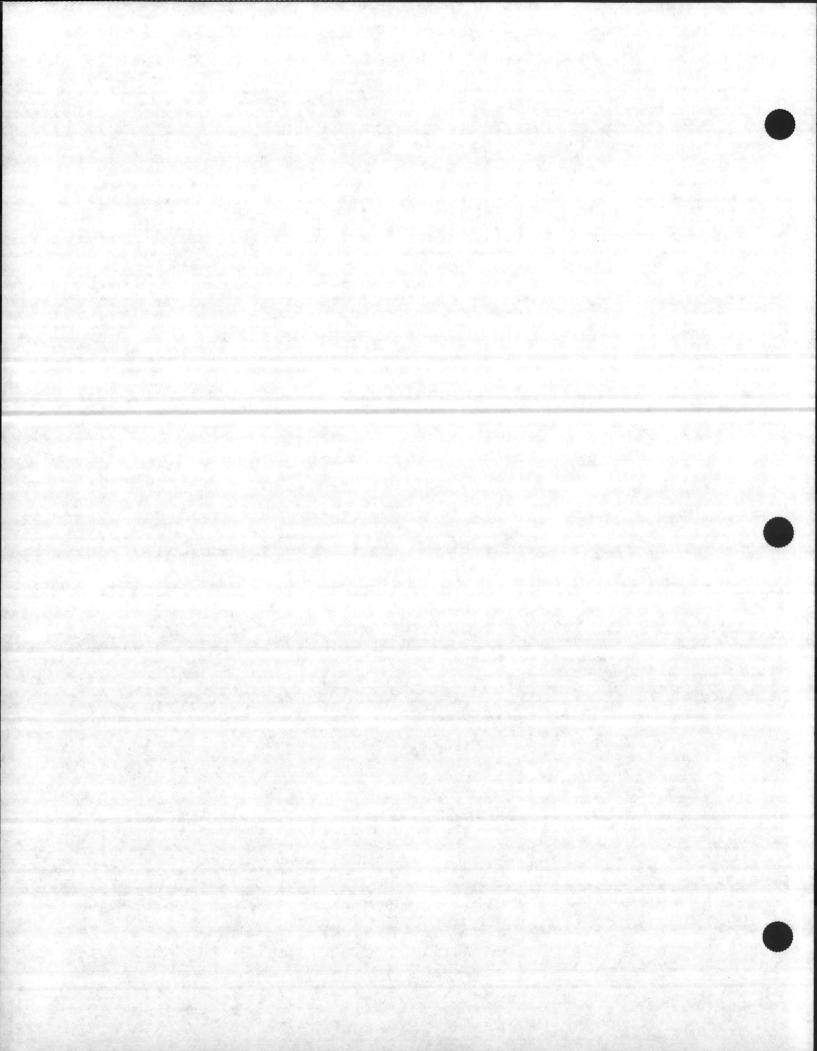
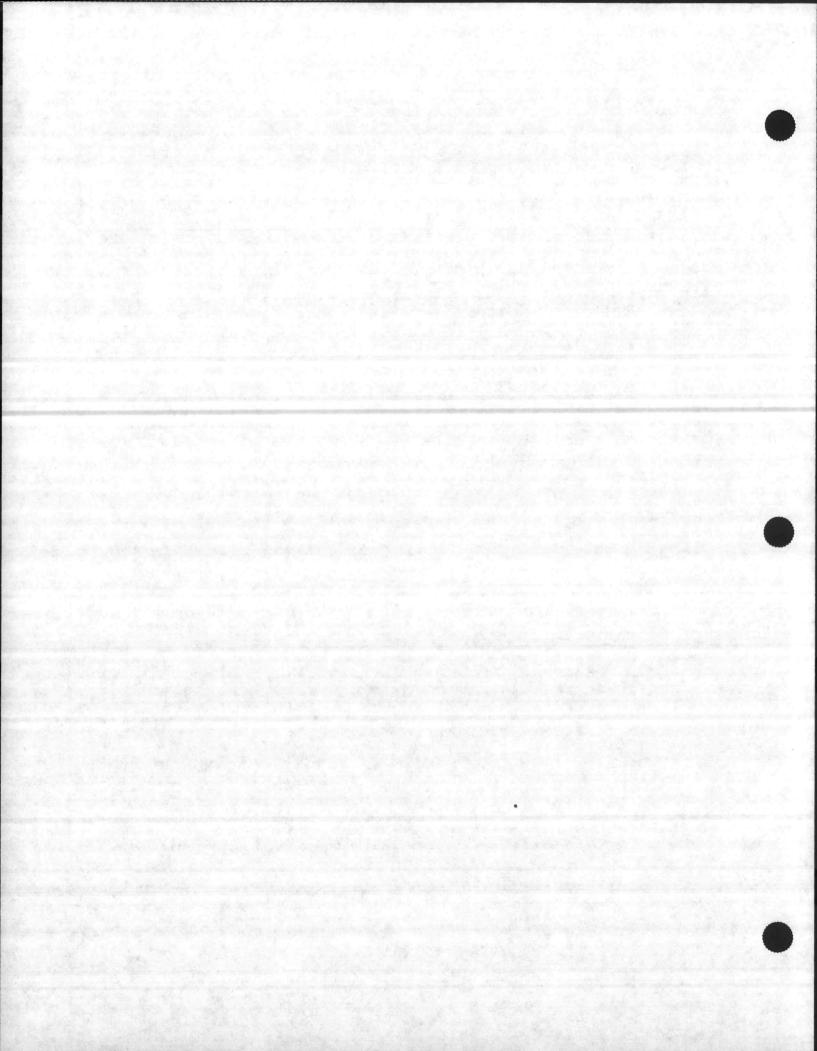
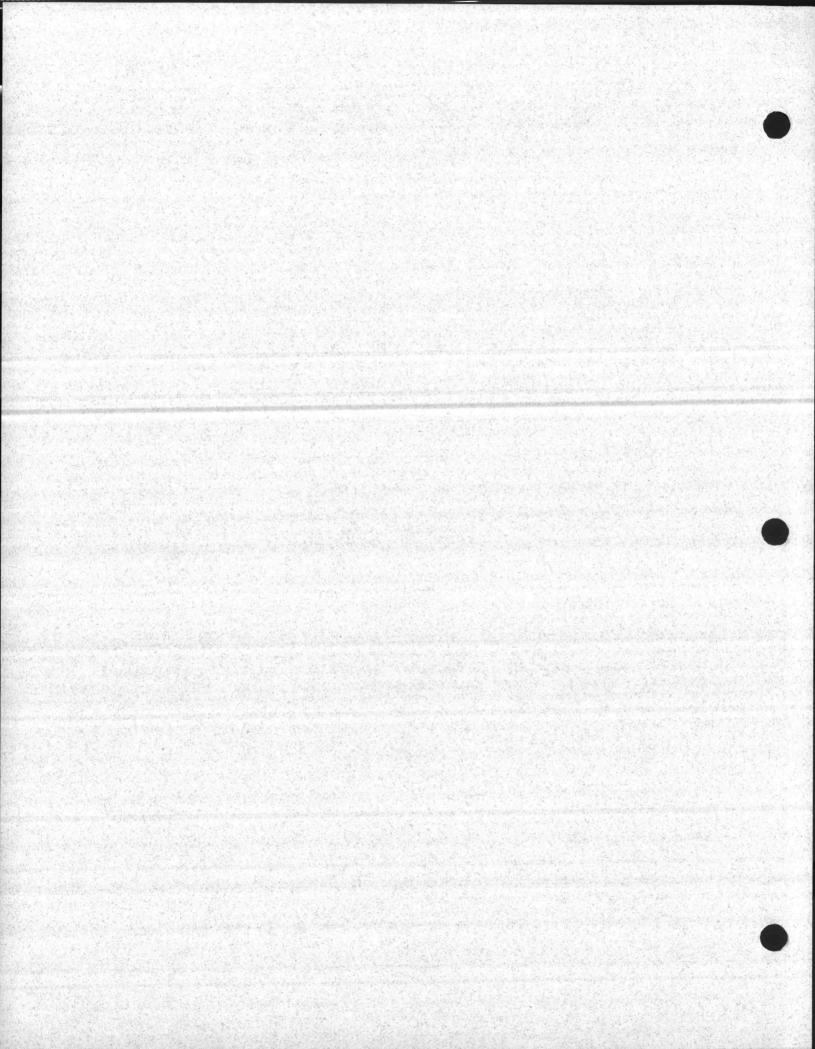


TABLE 2
DE MINIMIS EMISSION RATES

Pollutant	<u>De Minimis</u> Emission Rate	Actual Emission Rate	Emission Limit Exceeded?
Benzene	8.1 lb/yr	2,770 lb/yr	YES
1,2-DCE	NONE		N/A
TCE	4,000 lb/yr	4,906 lb/yr	YES
VC	26 lb/yr	130 lb/yr	YES



APPENDIX O O'BRIEN & GERE PRELIMINARY ENGINEERING REPORT



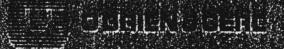
Preliminary Engineering Report

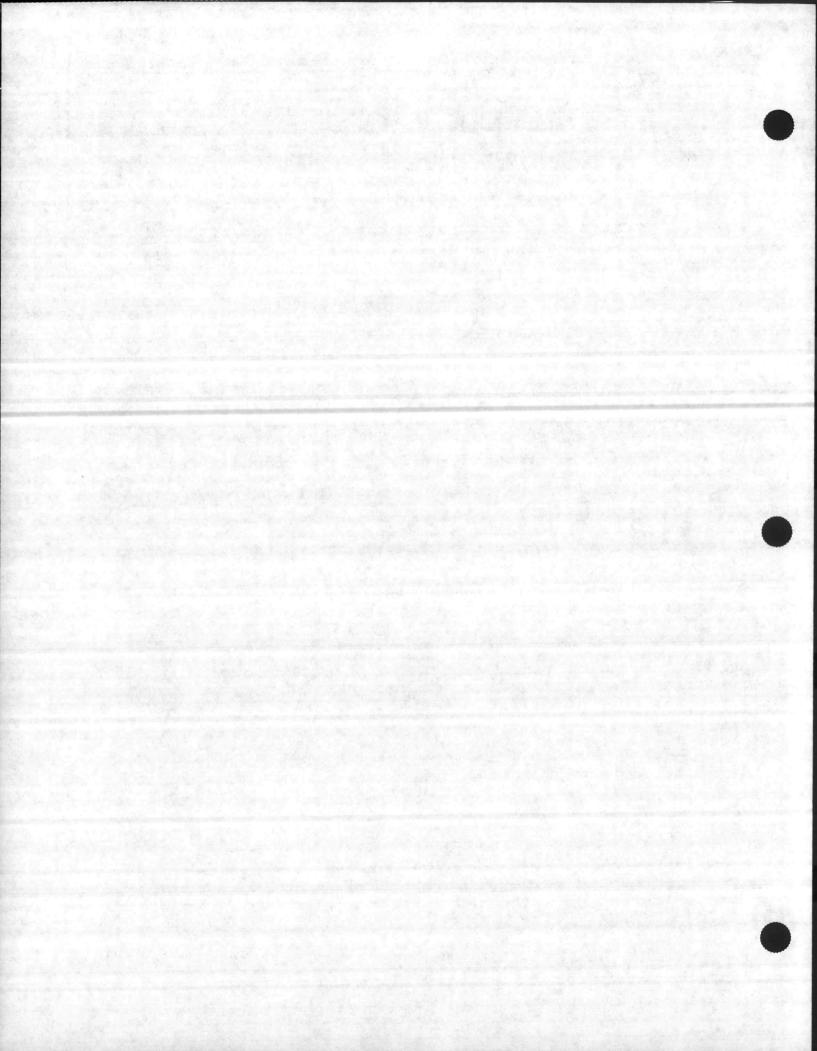
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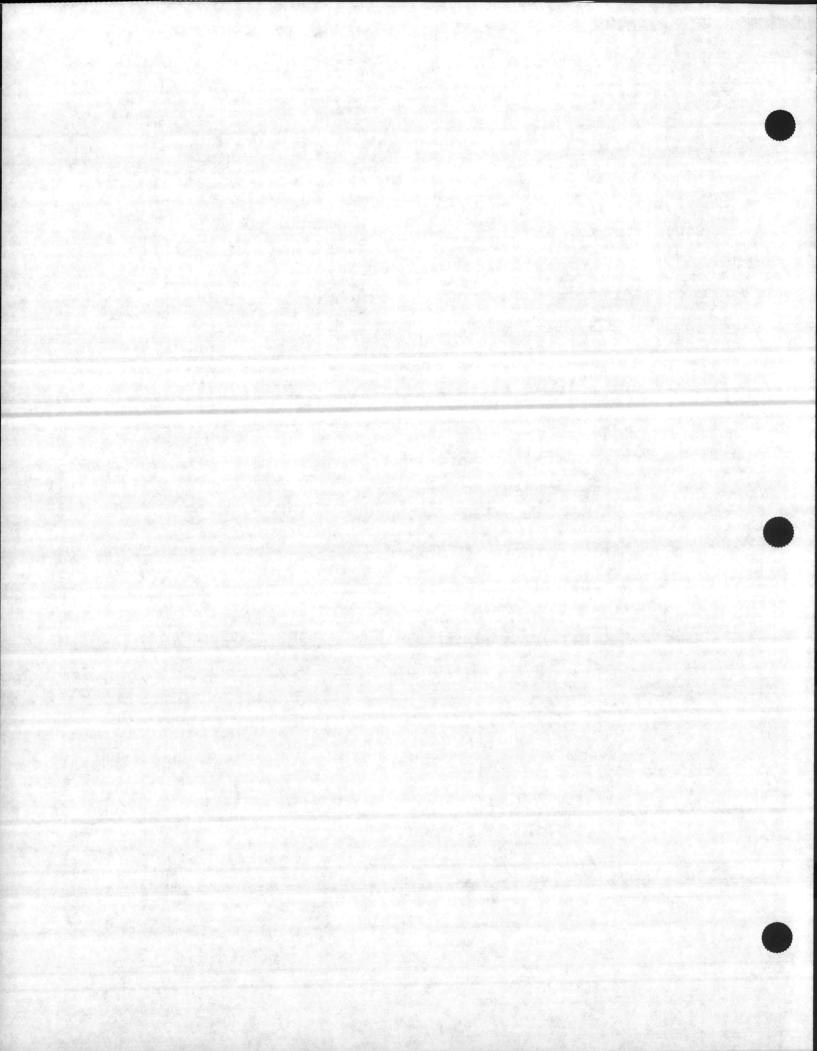
# SECTION 2 - FIELD INVESTIGATIONS

#### 2.01 General

The following investigations were conducted during the field study: monitoring well installation; grain size analysis; groundwater elevation and product thickness monitoring; aquifer analysis; groundwater sampling and analysis; and an engineering survey. These investigations were required to gather information to assist in the design of a recovery system that will efficiently remove the free product that exists at the HPFF. The field investigations are detailed below.

## 2.02 Well Installation

The locations of the groundwater monitoring wells were based upon consideration of the hydrogeologic conditions and the assessment of petroleum leakage in the study area. The placement of the wells, as illustrated in Figure 4, was selected to provide a more precise delineation of the extent of the product plume and to assist in evaluating the aquifer conditions during the pump test of the aquifer. Five (5) 2-inch PVC monitoring wells and two (2) 6-inch PVC test/recovery wells were installed at the HPFF. The 2-inch monitoring wells were constructed of Schedule 40 flush joint threaded PVC well screen (0.020 slot) and riser to a depth of 15 feet with 10 feet of screen. The 6-inch wells were constructed of Schedule 40 PVC with the screen constructed of continuous slot wire wrapped PVC (0.020 slot size). Recovery well

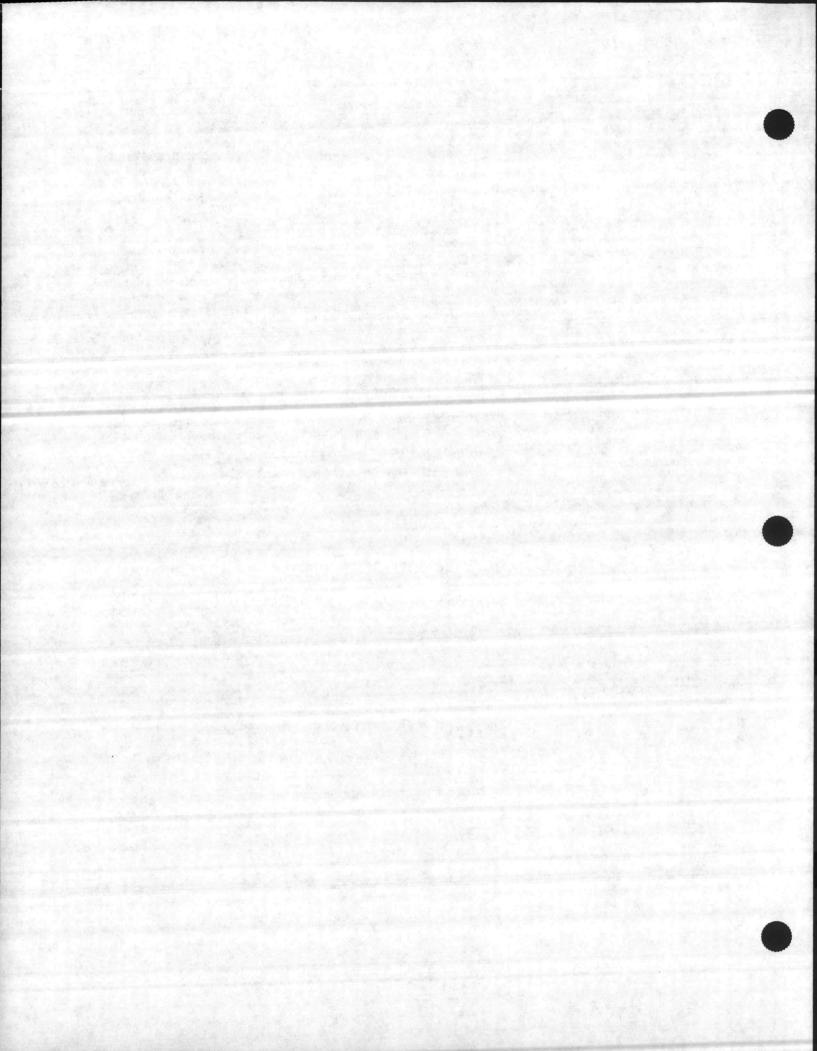


#1 was installed to a depth of 34 feet while recovery well #2 was installed to a depth of 33 feet below grade. Well construction diagrams and bore logs are included as Appendix A.

All wells were installed and constructed in accordance with NAVFAC guidelines and specifications, included in Appendix B. During the drilling program, boreholes were advanced using hollow stem auger. All wells were developed following installation to remove fine-grained materials that may have entered the well during construction. This was accomplished by a combination of the continuous low yield pumping; and air-lift pumping. Equipment used for well installation was decontaminated with a high pressure steam cleaner. Fluid generated from well development and equipment decontamination was discharged to the ground.

### 2.03 Grain Size Analysis

Grain size analysis was conducted on five (5) samples representative of the subsurface soils. Samples were initially obtained from split spoon samples; however, the split spoon did not provide enough of a sample. The augers were spun at the depth interval for 2-5 minutes to allow representative material to reach the surface and then a sediment sample was collected. The samples were obtained from each of the product recovery wells and from monitoring well #22. Each one kilogram sample of subsurface material was shipped to McCallum Testing Laboratories, Inc., located in Chesapeake, Virignia, for sieve analysis per ASTM D-422. The results of the grain size analysis are included as Appendix C,



and will be used to specify the well screen and sand pack for the proposed recovery well during the design of the recovery system.

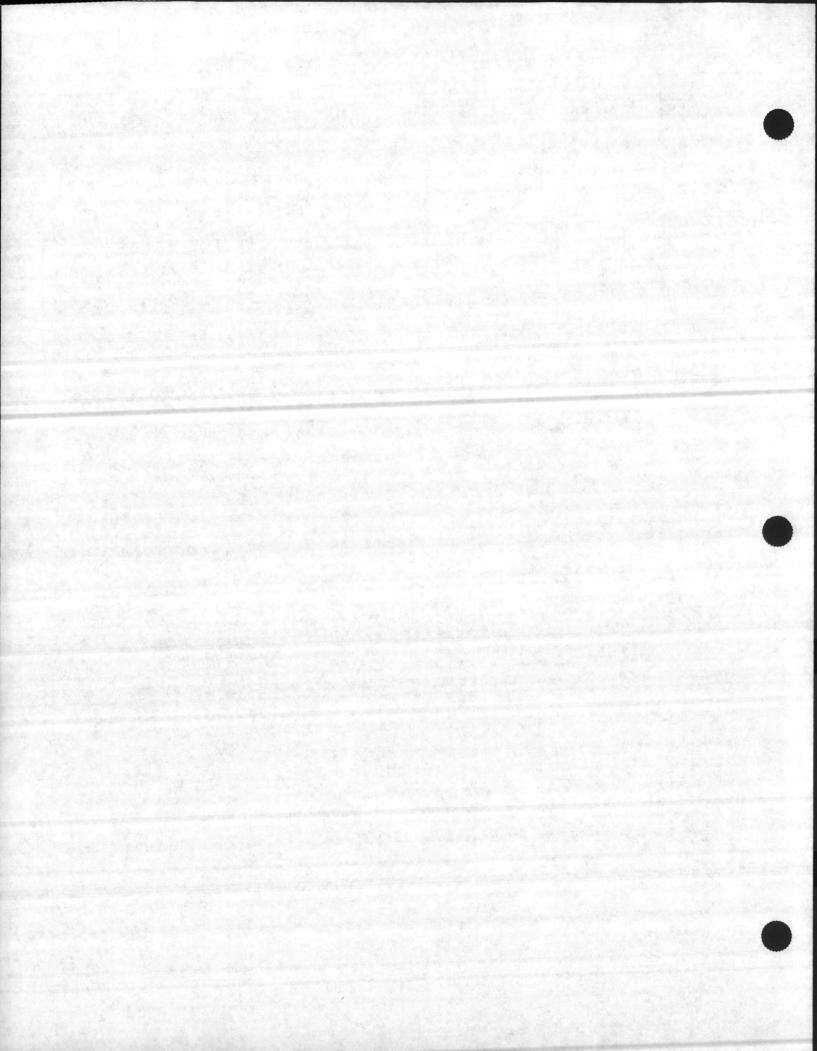
2.04 Groundwater Elevation and Product Thickness Monitoring

Groundwater elevations and product thickness measurements were collected from all of the HPFF monitoring wells before any work was performed at the site and upon completion of well installation. An oil/water interface probe was used to measure product thickness and groundwater elevation to the nearest 0.01 ft. These measurements, as well as measurements conducted during 1988, are summarized on Tables 2 and 3. These measurements are used in Section 3 to determine the hydraulic gradient, direction of groundwater flow, and assess the extent of free-phased product currently at the HPFF.

# 2.05 Aguifer Analysis

A short term pump test was performed on each of the 6-inch wells. This test was conducted to estimate design flow rates, and determine the site specific aquifer transmissivity, hydraulic conductivity, and the pumping wells radius of influence.

The test was conducted over an 8 hour period under the surervision of a hydrogeologist from O'Brien & Gere. Each well was pumped with a submersible pump at a constant rate for the duration of the test. The pumping rate was measured every 15 minutes during the aquifer testing. Water levels in the pumping and neighboring monitoring wells were recorded for the duration of the aquifer



test. Following the pump test, the residual-drawdown (recovery) rate was measured until the aquifer had reached 95% recovery.

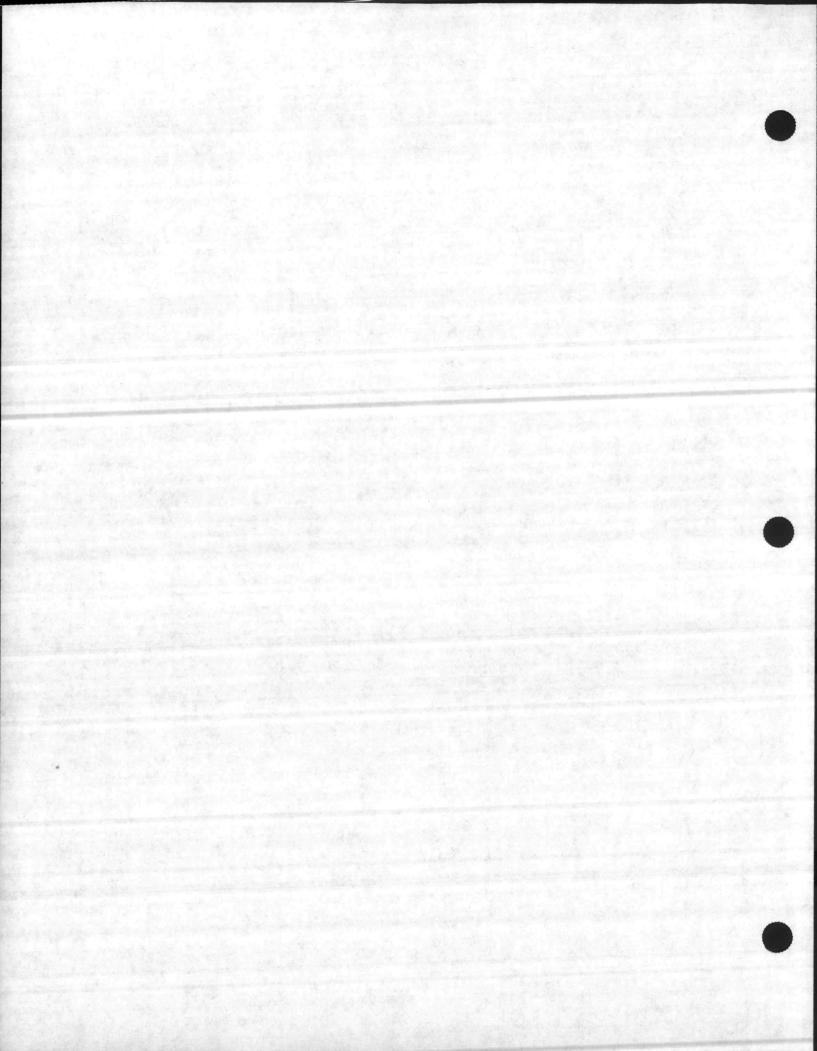
Pump test data was tabulated and analyzed using Theis type curves, the Cooper and Jacob modification of the Theis equation, and the pump test well recovery curves. Each evaluation of the data produced a slightly different value for the various aquifer parameters. This results in a range of values being presented for each parameter (Appendix D). Using the Theis nonequilibrium well equation, a radius of influence was calculated to extend 300-400 feet after 60 days of pumping. The boundary of the radius of influence for this calculation is defined at a 0.1 foot drawdown of the aquifer.

Evaluating the various coefficients that were determined using the three methods allows an estimate of aquifer characteristics for final design. For the purposes of final design the assumed aquifer characteristics are as follows:

Transmissivity: = 500 gpd/ft
Well Yield = 3 gpm
Saturated Thickness = 19-22 ft
Radius of influence = 300-400 ft

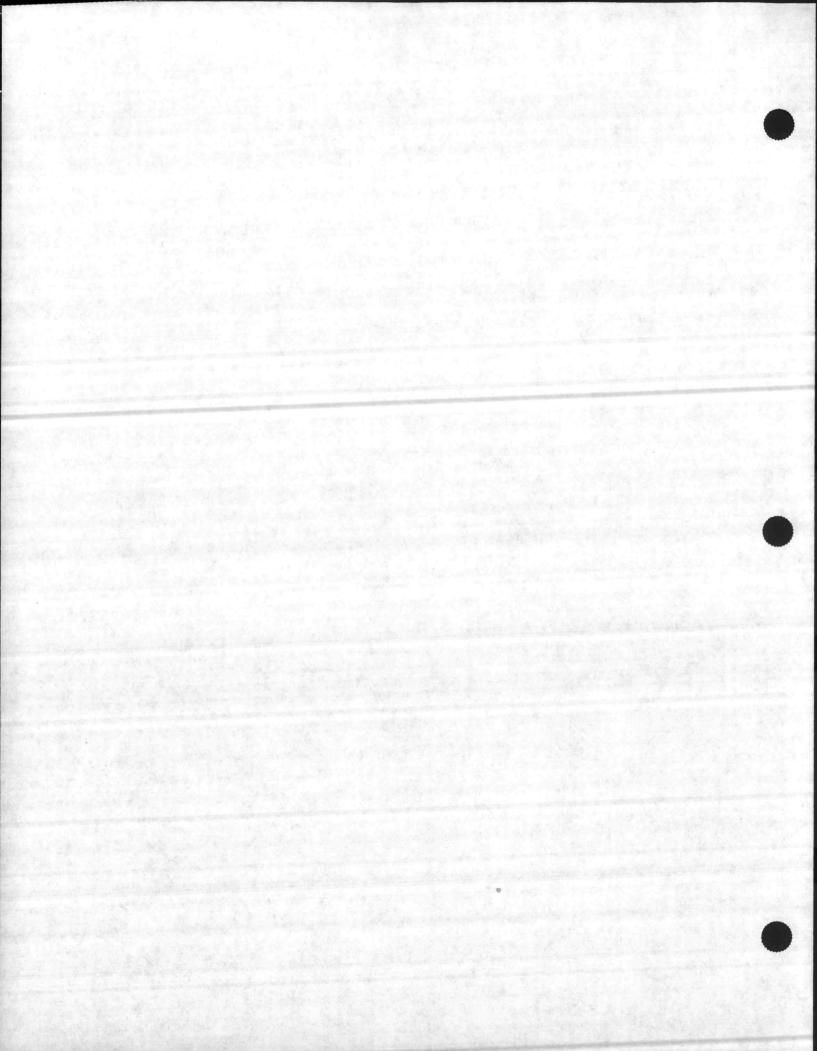
# 2.06 Groundwater Sampling and Analysis

Groundwater samples were collected from each of the newly installed monitoring wells on a single occasion. A total of seven (7) samples were analyzed for volatile organic compounds and lead in accordance with the procedures outlined in the sampling and analysis plan included as Appendix E. The results will be forwarded as a separate submission.

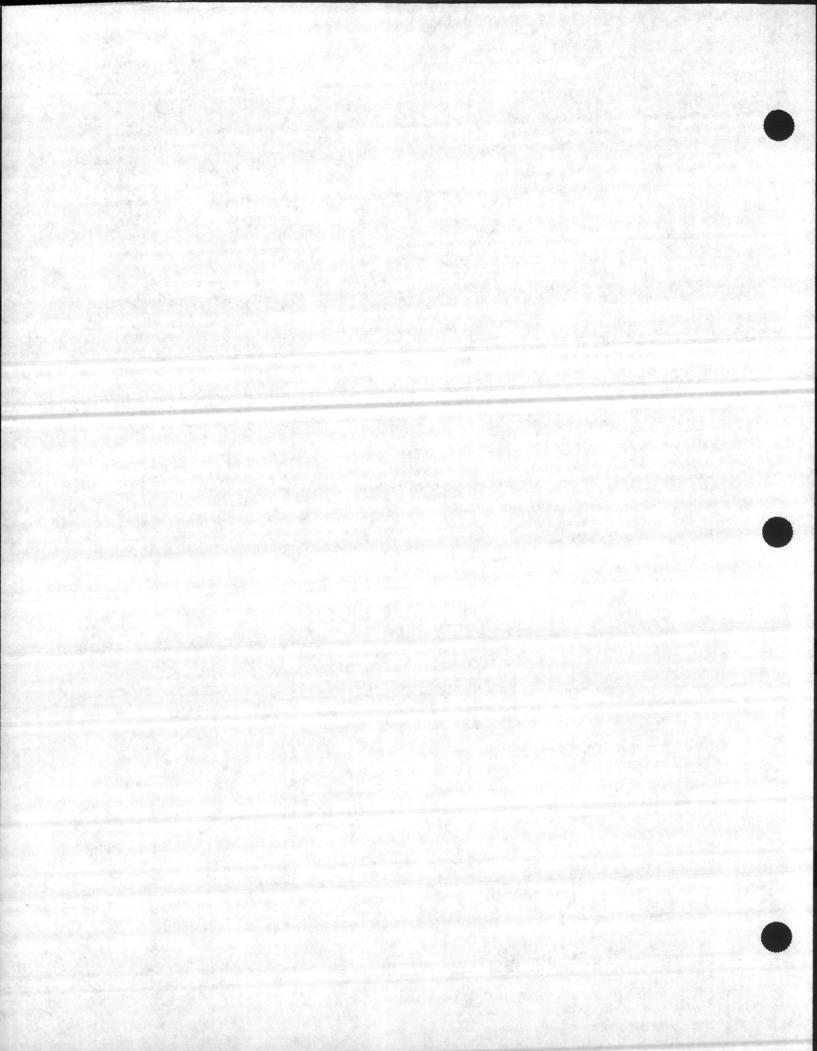


## 2.07 Engineering Survey

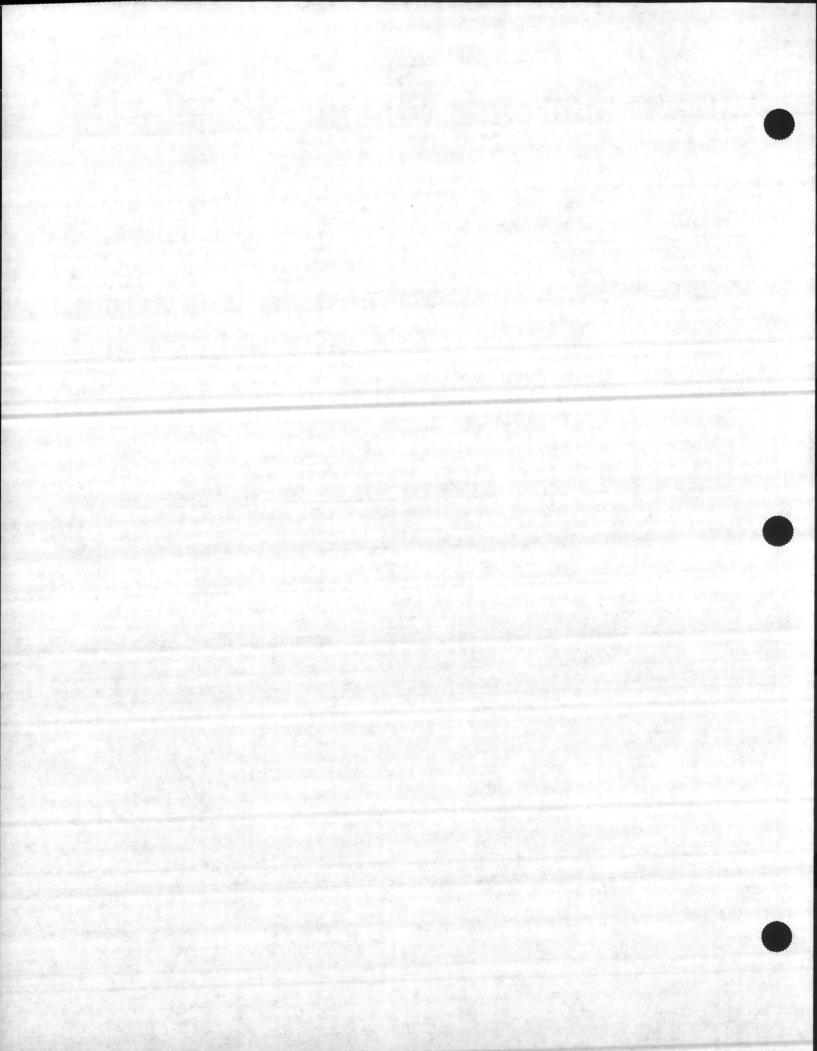
A topographic survey was conducted at the site to establish the horizontal location and elevation of above-grade features at the site. The topographic survey included the locations of catch basins, hydrants, power poles, manholes, roadways, buildings, tanks, fencing, monitoring wells, and any other indicators of subgrade utilities. Each monitoring well had the following points surveyed: top of PVC inner casing and ground elevation.



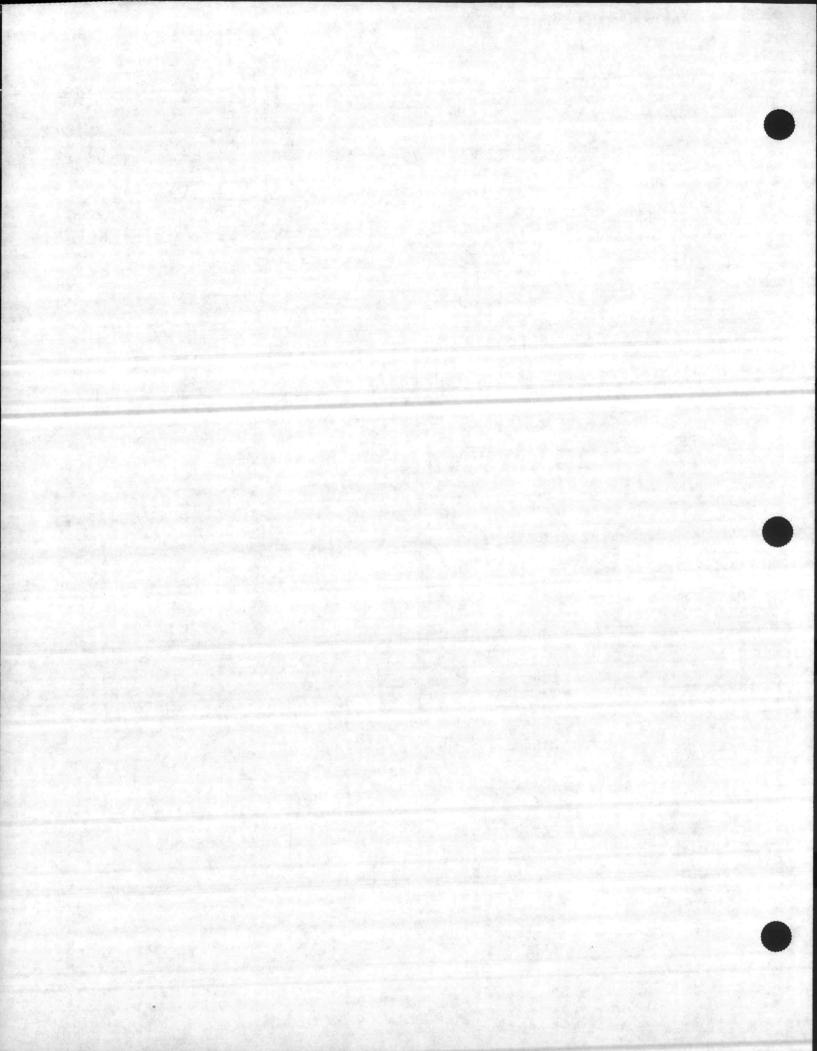
Aquifer '	e: RW#1 Thickness (b):	22.000 feet	Date of Te	25t: 12/15/09_
Fumped We	ell Discharge (O	) = 3.000		
Reditte O.	Fumping Mes 11	0		
Distance	of Observation	Well from Pu	mping boll	
			whrud merr =	0.500 feet
Cal	· ***/		9	
Entry	· Time(t)	Drawdown (s)	t / d	
No.	(min.)	(ft.)	(min./sq.ft.)	
*****	*****	********	**********	
1	0.000	12.350	***************************************	
3	0.780	0.450	3.12E+00	
3 ****	0.830	.0.550	3.32E+00	
4	0.980	0.650	3.92E+00	
5 6	1.120	0.850	4. 48E+00	
0	1.250	1.050	5.00E+00	
0.75	1.410	1.250	5.64E+00	
0	2.280	2.250	912E+00	
10	2.910	2.850	1.16E+01	
	. 3.670	4.150	1.47E+01	
11	4.380	4.650	1.75E+01	
1.6 83-7013##8-48	5.380	5.150	2.15E+01	
14	6.630 ·	5.650	2.65E+01	
24. W. A. S. C.	9.083	6.420	3.63E+01	
15 (	10.083	6.650	4.03E+01	
	15.670	7.850	6.27E+01	
17	23.330	7.770	9.33E+01	
18	26.000	7.550	1.04E+02	
19	28.000	7.500	1.12E+02	
50	29.000	8.950	1.16E+02	
21*.	34.000	10.150	1.36E+02	
22	54.000	9.150	2.16E+02	
23	84.000	9.080	3.36E+05	
24 ·	114.000	8.870	4.56E+02	
25	144.000	8.550	5.76E+02	
26	174.000	8.060	6.96E+02	
27	204.000	7.950		
28	234.000	7.850	8.16E+08 9.36E+08	
. 53	264.000	10.830	1.06E+03	
30	294.000	10.810		
~~ 31 k	324.000	10.850	1.18E+03	
A CONTRACTOR	AND A STORY OF THE STORY	" " WE WAY	1.30E+03	



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Unconfined Elastic: beta = 0.10  SUCUTION  Transmissivity = 6.255E+01 gal/day/ft Aquirer Thick. = 2.200E+01 rt Hydraulic Cond. = 2.843E+00 gal/day/sq ft Storativity = 1.112E-01	
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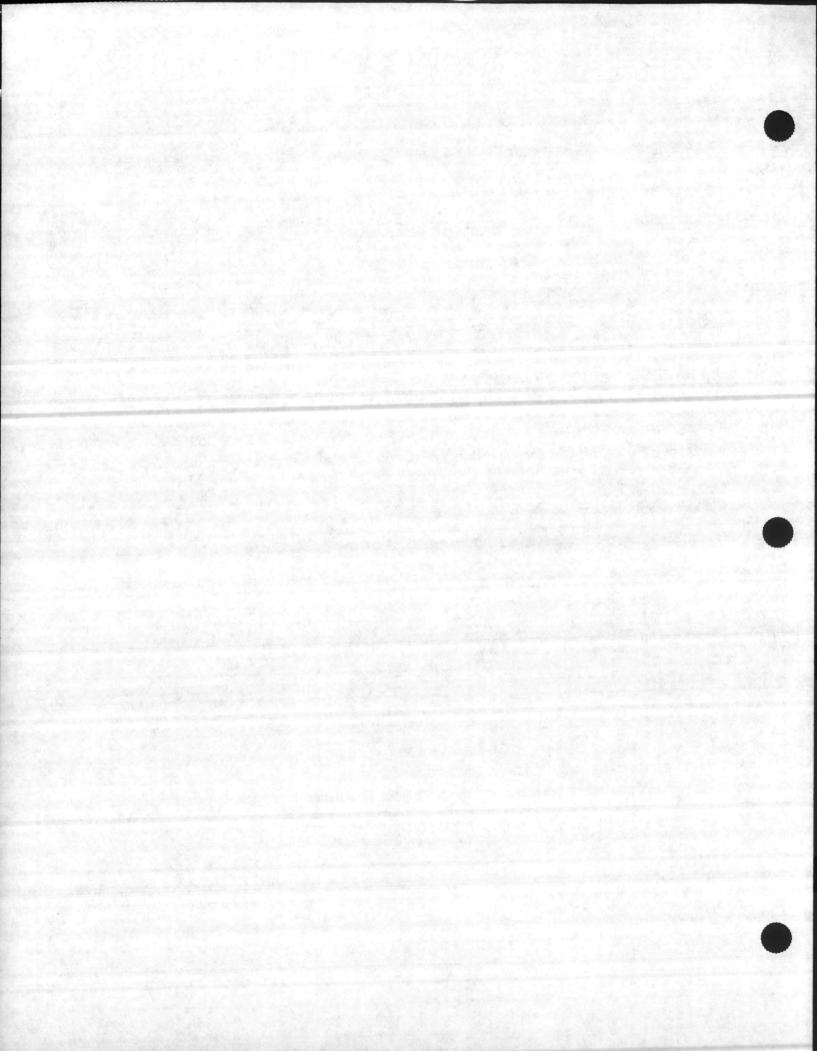


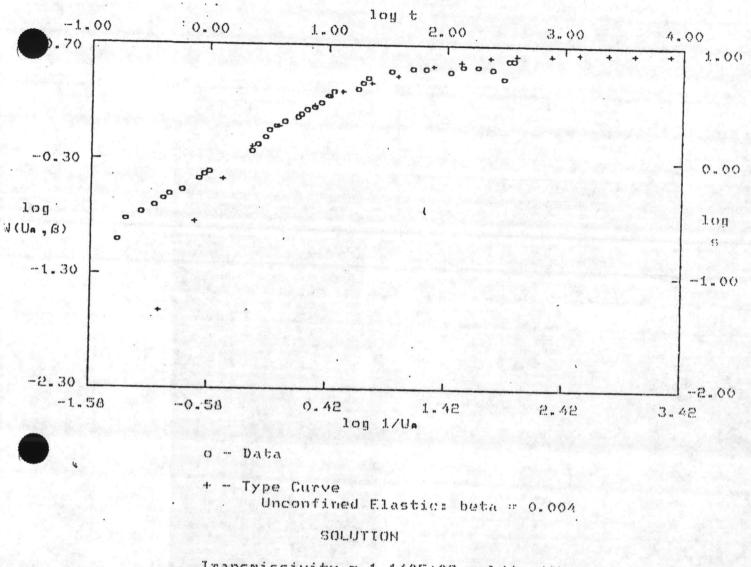
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	o - Data	
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	log 1/Ua  o - Data  + Type Curve Unconfined Elastic: beta = 0.20  SOLUTION  Transmissivity = 4.531E+01 gal/day/ft	
	log 1/Ua  o - Data  + Type Curve	
	log 1/Ua  o - Data  + Type Curve Unconfined Elastic: beta = 0.20  SOLUTION  Transmissivity = 4.531E+01 gal/day/ft	
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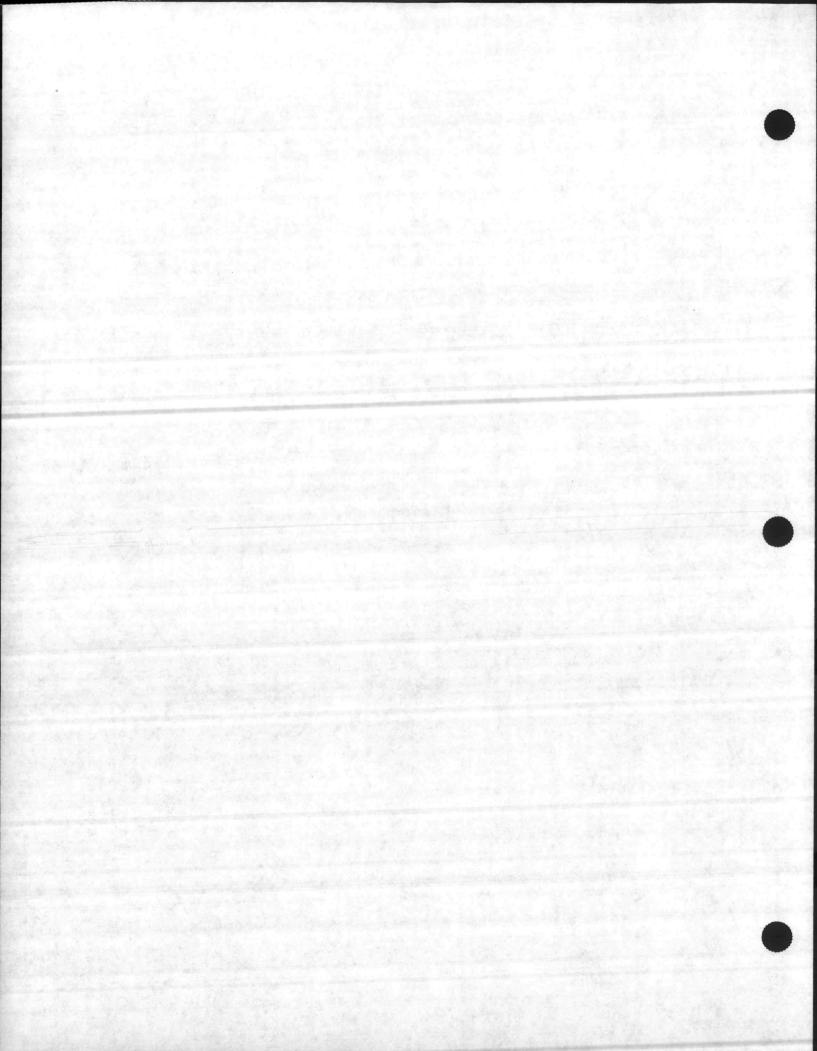
Well Name: rw2 Date of Test: 12/15/89 Aquifer Thickness (b): 19.000 feet Pumped Well Discharge(Q) = 2.000 gpm Radius of Pumping Well = 0.500 feet Distance of Observation Well from Pumping Well = 0.100 feet

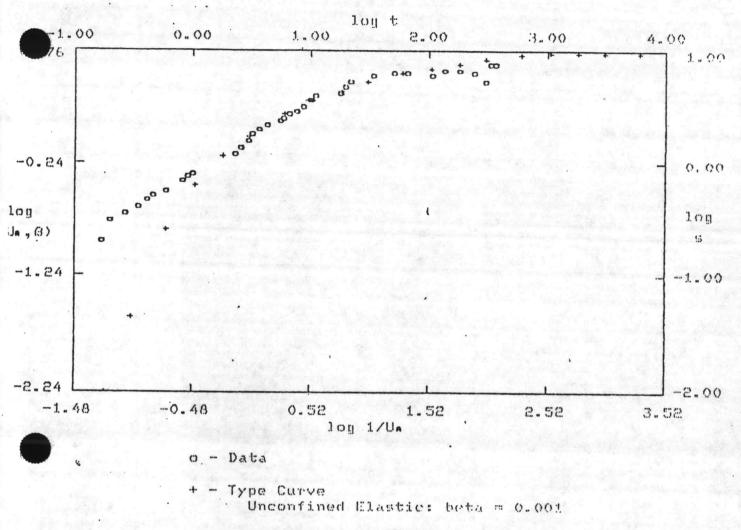
Entry	Time(t)	Drawdown (	2
No.	(min.)	(ft.)	
*****	* *********	*******	(win./sq.ft.)
1	0.000	14.400	* *********
5	0.170	0.200	1 705.44
3	0.200	0.300	1.70E+01
4	0.270	0.350	2.00E+01
5	0.350	0.400	2.70E+01
6	0.420	0.450	3.50E+01
7	0.470	0.490	4.20E+01
8	0.600	0.550	4-70E+01
. 3	0.830	0.700	6.00E+01
10	0.920	0.760	8:30E+01
11	1.000	0.800	9.20E+01
12	2.300	1.200	1.00E+02
13	2.570	1.400	2.30E+02
14	2.920	1.600	2.57E+02
15	3.250	1.800	2.92E+02
16	3.600	2.000	3.25E+02
17	4.270	2.200	3.60E+02
18	5.500	2.400	4.27E+02
19	5.930	2.500	5.50E+02
20	6.670	2.700	5.930+02
21	7.670	2.900	6.67E+02
55	8.730	3.100	7.67E+02
. 23	9.670	3.600	8.73E+02
24	10.350	3.700	9.67E+02
25	11.000	3.900	1.03E+03
26	17.630	4.250	1.10E+03
27	19.630	4.700	1.76E+03
85	21.480		1.96E+03
29	33.930	5.150	2.15E+0J
30 .	50.700	6.100	3.39E+03
31	65.650	8.260	5.07E+03
32	108.000	6.250	6.56E+03
33	134.000	5.950	1.08E+04
34 .	180.000		1.34E+04
35	240.000		1.80E+04
36 :	300.000		2.40E+04
37	330.000	5.150	3.00E+04
38 .	360.000		-30E+04
All the seal of	000.000	7.580	. 60E+04





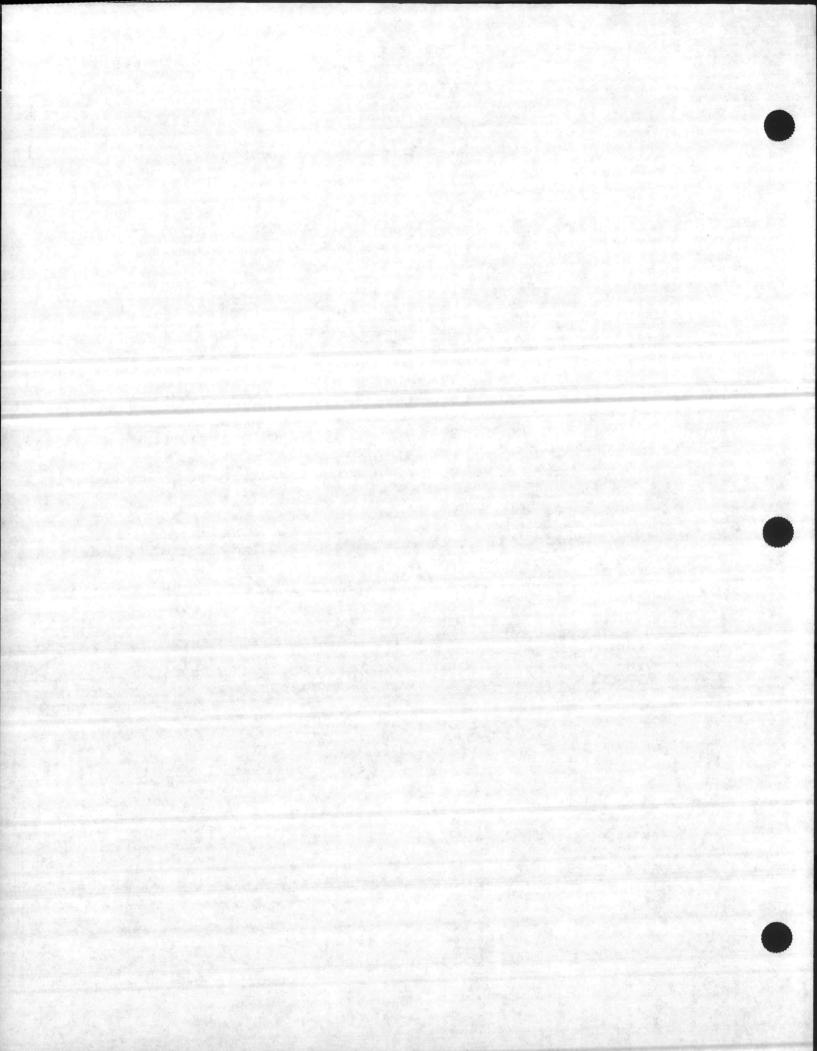
Transmissivity = 1.148E+02 gal/day/ft Aquifer Thick. = 1.900E+01 ft Hydraulic Cond. = 6.044E+00 gal/day/sq ft Storativity = 4.054E+00

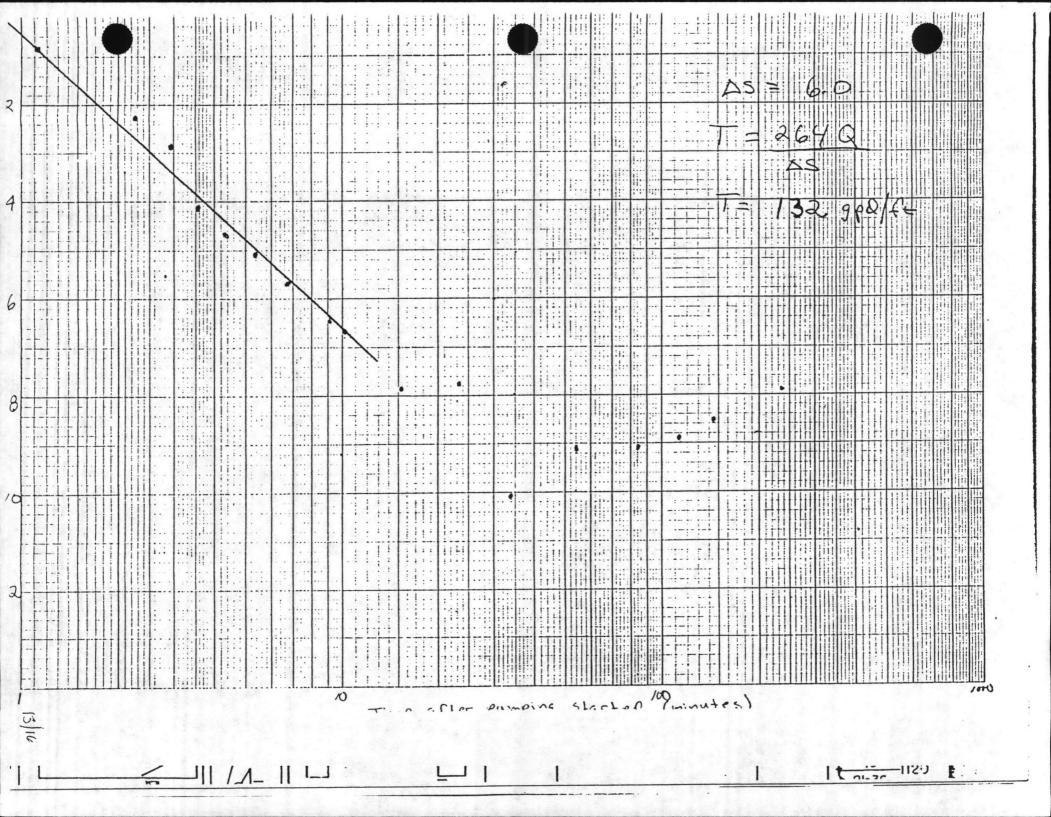


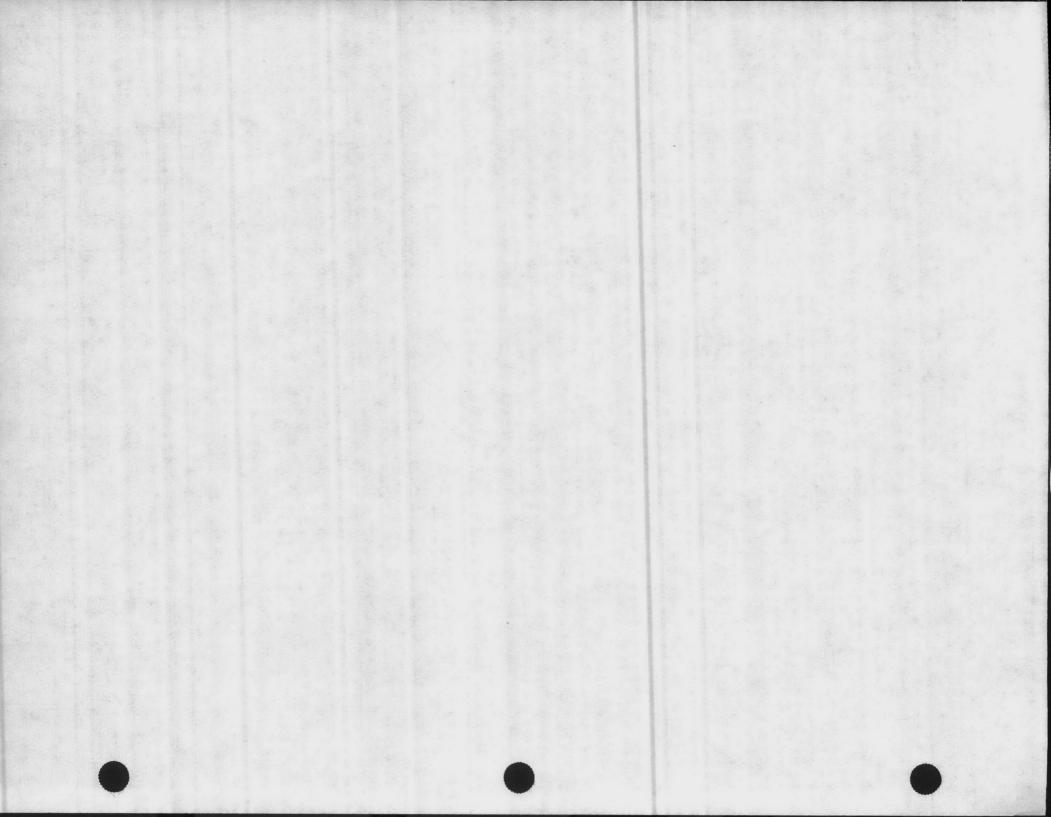


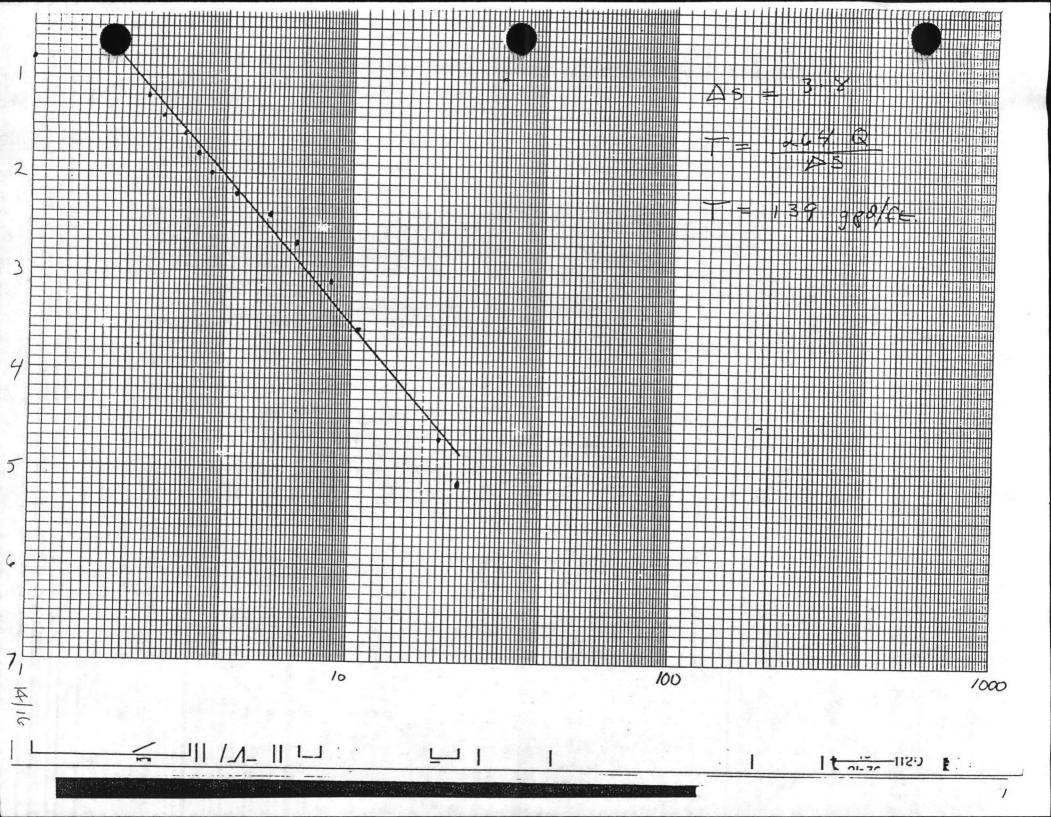
SOLUTION

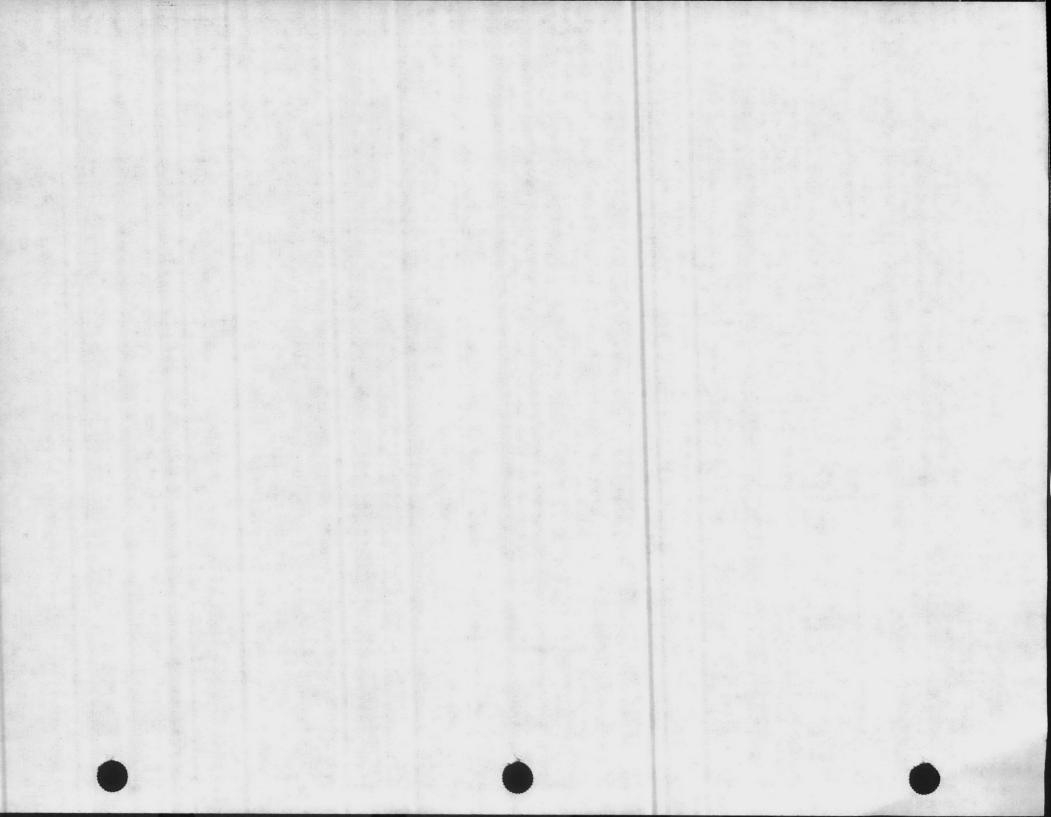
Transmissivity = 1.319E+02 gal/day/ft
Aquifer Thick. = 1.900E+01 ft
Hydraulic Cond. = 6.940E+00 gal/day/sq ft
Storativity = 3.697E+00





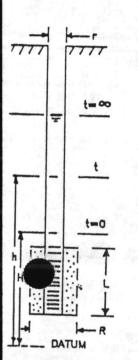






PROJECT 3543.002 WELL NUMBER KW41

LOCATION Camphejeune ELEVATION \_\_\_\_



STATIC HEAD (H) 12.35

PIPE RADIUS (r) .5

SCREEN RADIUS (R) 1.0

SCREEN LENGTH (L) 25.3

INITIAL HEAD (Ho)

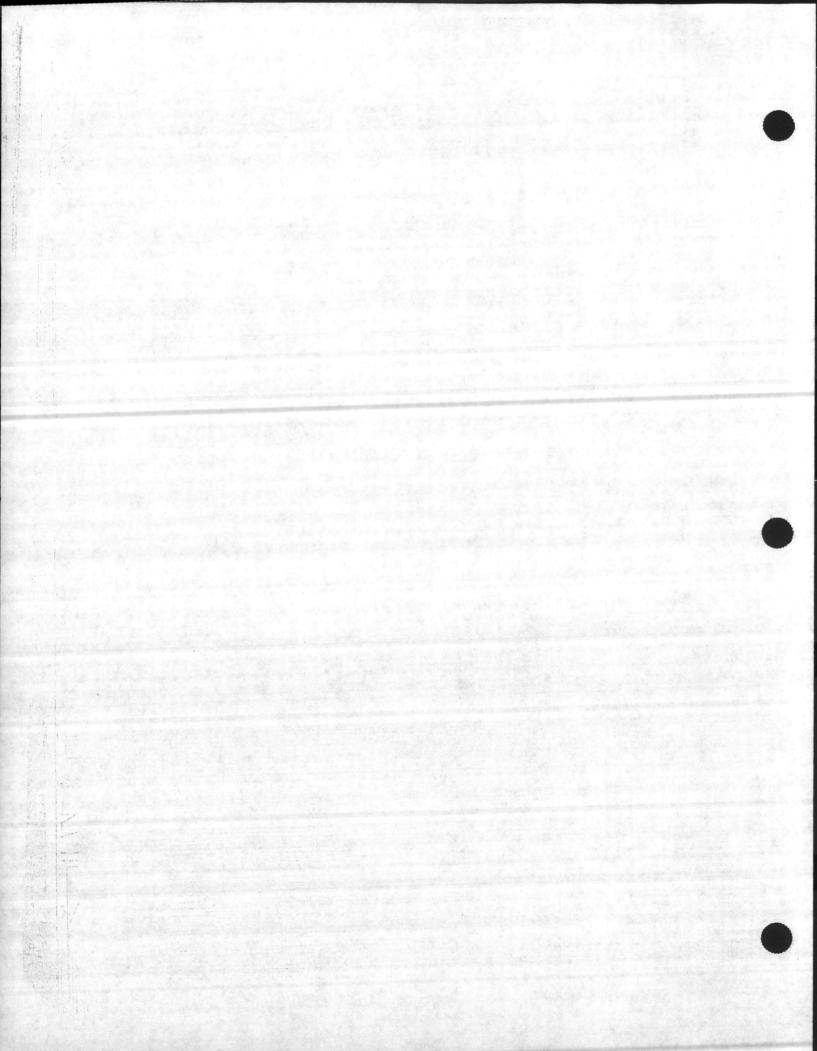
HYDRAULIC CONDUCTIVITY:

 $K=r^2ln(L/R)$ 

TIME	WATER DEPTH		h	H-h H-Ho	10,9
0	Action of the	0	23.3		1
28		.47	22.7	.94	
1:09		1.15	21.6	.84	
2:21		2.15	20.0	.70	
3: 35		3.65	19.0	.61	
5:04		5.04	17.5	.47	
9:41		9.68	15.0	124	
11:15		11.27	4.5		
		and the second			

-	le-R	2LTo			4 - 2 -		
DA	TUM	V 65	1 (25/	(1)			
		K= 100	111(-)		3.9'X10-5	f+1 = 2	5500NC3
		2	(25) (40)	8)		175- 0	2.2 dbalter
· · · · · ·					T= K5	= 561 900	elte ,
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A				+			
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	* BA	DATUM	DATUM K= (+5)	K= (5) \( \lambda \) (25) \( \lambda \) (25) \( \lambda \) (25) \( \lambda \) (35) \( \la	CATUM K = (-5) \( \lambda \) \	DATUM $K = \frac{(5)}{2} \frac{1}{(25)} \frac{25}{(408)} = 3.9' \times 10^{-5}$ $T = kb$	DATUM $K = \frac{(5)}{2} \frac{\ln(25/1)}{2(25)(408)} = 3.9' \times 10^{-5} \text{ fe/s} = 2$ $T = Kb = 561990$

6 TIME



# IN-SITU PERMEABILITY TEST FIELD LOG

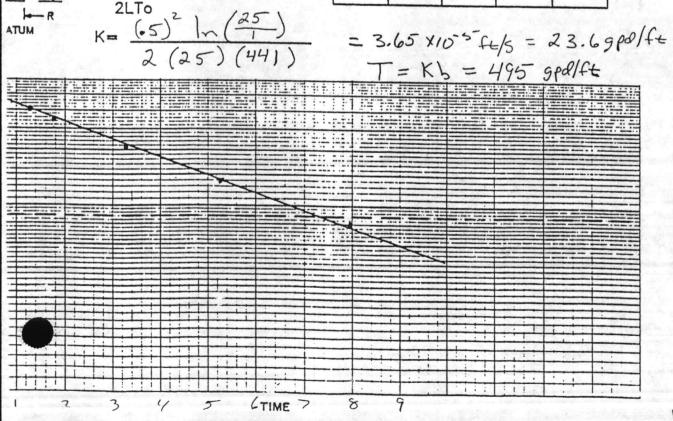
T 3543.012 BER RW#2 12/15/89 UMBER

LOCATION <u>Camps</u> Lejuen ELEVATION

STATIC HEAD (H) 14.40 PIPE RADIUS (r) .5. SCREEN RADIUS (R) 1.0 SCREEN LENGTH (L) 25 INITIAL HEAD (Ho) 21.9 HYDRAULIC CONDUCTIVITY:

 $K=r^2ln(L/R)$ 

TIME	WATER DEPTH		h	H-h H-Ho	7-6
40		167	21.0	.88	
1:13	100	1.27	20.5	.81	
1:45	Part of	1.75	20	.75-	
3:15		3.72	19.0	.61	
5:14		5.23	18.0	.48	
7:56		7.93	17.0	.35	
7:58		9.97	16.0	021	
			4 7 75		
	10000				
					11



16/16

