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Evaluation of Federal Motor Vehicle Safety Standard 301-75, Fuel System Integrity: Passenger Cars

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EXECUTIVE SUMMARY

Motor vehicle crash fires have been a source of interest and concern within the highway safety community since the time that motor vehicle and highway safety was established as a National program in the late 1960's. Although it has generally been held that fires resulting from motor vehicle crashes occur only rarely, the fact that they do occur has been of concern because the physical effects of the fire phenomenon can significantly increase the risk to vehicle occupants involved in a crash.

Responding to this perceived hazard of fires resulting from motor vehicle crashes, the National Highway Traffic Safety Administration (NHTSA) in 1968 issued a Federal Motor Vehicle Safety Standard (FMVSS), No. 301, whose objective was to mitigate this hazard. The Standard specified certain performance criteria intended to limit the amount of fuel spilled during, and after a vehicle crash. Hence, the objective of the Standard was to reduce the occurrence of crash fires which resulted from the ignition of spilled or leaked fuel. The initial version of the Standard, which became effective in 1968, applied only to passenger cars and crashes involving only frontal impacts.

In 1975, the Standard was substantially upgraded by extending the coverage of impact types to include rollover, rearend, and side, and the vehicle coverage to include light trucks, light buses, multipurpose vehicles, and school buses. The following "Summary of Test Requirements" relates the chronological history of FMVSS 301.

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In February 1981, Executive Order 12291 (Federal Regulations) was issued which, among other requirements, directed Federal agencies to review existing regulations. This evaluation was conducted to comply both with this Order and with NHTSA's regulatory review plan published in March 1982 (Regulatory Reform - The Review Process).

This study is an evaluation, or review, of FMVSS-301, Fuel System Integrity using on-the-road data of actual motor vehicle crashes involving fire, and fuel leakage. Only that portion of the standard that was promulgated in 1975 and which applies to passenger cars is addressed by this evaluation. Insufficient data are available at this time, to adequately evaluate the effect of Standard 301-75 on light trucks.

The objectives of the evaluation are to determine or estimate:

- the extent to which crash fires and fuel leakage have been reduced by the Standard (herein referred to as effectiveness).
- (2) the magnitude of the savings of fatalities, injuries, and crash fires due to reduced crash fire rates (herein referred to as benefits).
- (3) the nature of the vehicle modifications made in response to the requirements of the Standard.
- (4) the costs incurred in order to meet the requirements as set forth in the Standard.

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The analyses of effectiveness are based on Statewide police-reported accident data from five States (Michigan, Illinois, North Carolina, Maryland, and Pennsylvania). Primary emphasis is placed on the data from Michigan due to the nature and extent of the accident information available, and the fact that data on fuel leakage in addition to crash fires, were available from this State.

Estimates of standard benefits have been derived using the results of the effectiveness analyses together with data from NHTSA's Fatal Accident Reporting and National Accident Sampling Systems.

Cost estimates of standard implementation are derived by NHTSA on the basis of information obtained from the motor vehicle manufacturers.

Findings and Conclusions

Following are the principal findings and conclusions reached in this evaluation:

1. The magnitude of this national problem for passenger cars is estimated at 20,600 crash fires annually. These fires are associated with 1,100 fatalities, 3,200 serious injuries, and more than 3,300 moderate to minor injuries. These fatalities and injuries are to occupants of passenger cars and do not consider occupants of other vehicles such as light, medium, and heavy trucks.

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- 2. The presence of post-crash fires is estimated to markedly increase the chances of occupant fatality or serious injury for passenger car crashes of similar impact force levels.
- 3. Standard 301 has been effective in significantly reducing the post-crash fire rate and post-crash fuel leakage rates for passenger cars.
 - a. The greatest reductions have occurred in the more severe crashes as defined by the extent of crash-force deformation sustained by the vehicle.
 - b. Reductions in fire and fuel leakage rates have occurred for most of the major types of impacts addressed by the Standard.
- 4. The reduction in crash fire rates is estimated to result in the following annual savings, or benefits:
 - a. 400 fewer fatalities
 - b. 520 fewer serious injuries
 - c. 110 fewer moderate injuries
 - d. 6,500 fewer passenger car crash fires

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- 5. The total cost required to implement Standard 301 is estimated at \$8.50 per vehicle, or a total of \$85 million annually. The types of vehicle modifications made in response to the Standard varied widely, and for the most part were specific to individual vehicle models or body styles. The basic objective of these modifications was to provide a "friendlier" environment for fuel system components, given the event of a vehicle crash.
- 6. In terms of comparing benefits and costs resulting from Standard 301, it can be stated that for each \$10 million expended to comply with the Standard, the following benefits are expected to accrue:
 - a. 47 fatalities avoided
 - b. 61 serious injuries avoided
 - c. 13 moderate injuries avoided
 - d. 762 crash fires avoided
- 7. Although significantly lower crash fire rates have been found for Post-Standard vehicles, there is some indication that the fire rate may be increasing slightly for newer vehicles. This is a preliminary finding and reasons for it are not clear. It does suggest, however, that the Agency continue to monitor the phenomenon of motor vehicle crash fires.

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CHAPTER 1

INTRODUCTION

This is the sixth report in a continuing series of evaluation studies being conducted by the National Highway Traffic Safety Administration (NHTSA) to review the effectiveness of its existing regulations in the motor vehicle safety area. Pursuant to the issuance of Executive Order 12291 on February 17, 1981, NHTSA developed and published a regulatory review plan [1] together with a schedule and description of those regulations selected for review. Federal Motor Vehicle Safety Standard-301 (FMVSS-301) was listed in this review plan under the category of "moderate to high" priority.

The purpose of FMVSS-301 is to reduce the number of deaths and injuries occurring from fires that result from fuel spillage during and after motor vehicle crashes. The Standard was originally promulgated in January 1968, and applied to all passenger cars produced after that date. This initial version of the Standard addressed fuel spillage as a result of impacts from a frontal direction only.

A second version, or upgrade, of Standard 301 (FMVSS-301-75) became effective in September of 1975. This upgrade extended the impact coverage to rollover, rearend, and side, as well as frontal crashes; and vehicle coverage was expanded to include light trucks and

buses, and school buses, in addition to passenger cars. Table A summarizes the chronological history [2,3] FMVSS-301:

TABLE A - CHRONOLOGICAL HISTORY OF FMVSS-301, FUEL SYSTEM INTEGRITY

/ehicle odel Year	Vehicle Type(s):	Impact Velocity	Impact Mode	With Static Rollover
1968 thru 1975	Passenger Cars	30 mph	Frontal	No
1976	Passenger Cars	30 mph	Frontal	Yes
1977	Passenger Cars	30 mph 30 mph 30 mph 20 mph	Frontal Oblique Rear Lateral	Yes Yes Yes Yes
1977	Trucks, MPVs, and Buses (6000# GVWR<10000#)	30 mph	Frontal	No
1977	Light Trucks, MPVs, and Buses (GVWR ^{\$6000} 1bs.)	30 mph 30 mph	Frontal Rear	Yes Yes
1978	Light Trucks, MPVs, and Buses (GVWR ¹ 6000 lbs.)	30 mph 30 mph 30 mph 20 mph	Frontal Oblique Rear Lateral	Yes Yes Yes Yes
1978	Trucks, MPVs, and Buses (6000#>GVWR<10000#)	30 mph 30 mph 30 mph 20 mph	Frontal Oblique Rear Lateral	Yes Yes Yes Yes
1978	School Buses (GVWR>10000 lbs.)	30 mph	Location of Fuel Tank	n No

This study addresses the effectiveness of Standard 301-75 (hereafter referred to as Standard 301-76/77) for passenger cars only. Insufficient data are available at this time to adequately assess the effect of Standard 301-75 for light trucks, multi-purpose vehicles, and school buses.

The original version of Standard 301 (301-68, passenger cars, frontal impacts) has been studied under two support contracts sponsored by NHTSA as part of the overall process of evaluation of the Standard. Within the constraints of limited data due to the small number of pre-1968 Model Year vehicles still on the road, reports [4, 5] from these two contracts found no significant difference between the crash fire rate for vehicles produced prior to the Standard and the crash fire rate for vehicles produced after the effective date of the Standard. Limited data [6] concerning the implementation costs of this initial version of Standard 301 indicated that negligible costs were incurred and the general conclusion is that most passenger car designs existing in 1967-1968 already met the requirements of this first version of the Standard.

The objective of the study reported herein is to estimate the effectiveness of 301-76/77 in reducing passenger car crash fires and the benefits, in terms of fatalities and injuries avoided, due to any such reductions.

Accident data from five States, in addition to data from NHTSA's Fatal Accident Reporting System and National Accident Sampling System

are analyzed or otherwise employed to arrive at the effectiveness and benefits estimates. Primary emphasis is placed upon the data from the State of Michigan. The nature and extent of the information available from this State, both in terms of crash fires and fuel leakage, make it the best data source available.

Costs of Standard 301-76/77 are also estimated on the basis of information obtained from the motor vehicle manufacturers.

This evaluation project is also supported by two contractual efforts which acquired the majority of the State accident data on crash fires used in this evaluation, and which performed separate analyses of the data obtained.

The report is presented in the four chapters which follow. Chapter 2 contains the analyses of the accident data on crash fires and fuel leakage to arrive at estimates of standard effectiveness in terms of reducing the rate of occurrence of these crash hazards. Chapter 3 translates the effectiveness estimates into estimates of the benefits (fatalities, injuries, and crash fires avoided). It concludes with an analysis of cost and cost effectiveness. The final chapter, Chapter 4 summarizes the overall findings and conclusions of the evaluation.

Appendix A contains a description of the primary data sources employed in the study. Appendix B contains copies of the various accident report forms for these data sources.

CHAPTER 2

The Effectiveness of Standard 301-75/76

2.0 Introduction

This Chapter contains the results of the statistical analyses conducted to estimate the effectiveness of Standard 301-75. Effectiveness, as used herein, is defined in terms of the magnitude of reduction in crash fire rates, per vehicle crash, and in terms of the magnitude of reduction of crash-induced fuel leakage per vehicle crash. Crash fire reduction is the principal measure of effectiveness as this is considered most closely associated with the ultimate objective of the Standard, which is to reduce the number of deaths and injuries attributable to crash fires. Also available data are restricted primarily to fires vis-a-vis fuel leakage. The estimate of the reductions in fire-related deaths and injuries are covered in Chapter 3.0 on Benefits.

Perhaps the greatest obstacle to be overcome in carrying out the evaluation of FMVSS-301 has been that of acquiring satisfactory data, both with which to estimate effectiveness and to estimate the costs of implementing the Standard.

Early in the evaluation process, a contract [7] was let to the Highway Safety Research Institute (HSRI), University of Michigan, for the purpose of searching out and acquiring data sources on vehicle crash fires, and performing analysis of the data obtained. An exhaustive search of State accident data sources, State Fire Department data sources, and the National Fire Administration's National Fire Incident Reporting System (NFIRS) revealed very few sources that could supply satisfactory

data on vehicle crash fires. Preliminary information had indicated that fire departments might be a usable source. However, this possibility did not prove fruitful as the data contained insufficient information to adequately determine whether a vehicle fire resulted from a crash or from other factors, and vehicle model year (a "must" variable) was inconsistently reported. State accident data was determined to offer the best potential for vehicle crash fire data, but even here the availability was severely limited as very few States were found to record vehicle fires as part of their motor vehicle accident reporting systems. Fire data from this source consisted of two basic types: (1) fire occurrence recorded as a specific and independent element to be reported on each motor vehicle accident report, and (2) fire occurrence recorded as a secondary or auxiliary item of information, usually in a narrative portion of the accident report form or as a "second adverse or harmful event." Of a total of seven States where some type of fire data was reported, only two. Michigan and Illinois, were concluded to be potentially satisfactory for use in evaluating the effects of Standard 301.

It was later determined that three additional States, North Carolina, Pennsylvania, and Maryland offered some potential for the analysis of crash fire data from motor vehicle accident files. A second support contract was let to the Highway Safety Research Center, University of North Carolina to access and analyze the data from the data from the States of North Carolina and Maryland [8] and a follow-on effort [5] was awarded to HSRI to analyze the data from Pennsylvania as well as more current data from Michigan and Illinois. Appendix A contains a more detailed discussion of the data sources.

This study analyzes fire data from five States, Michigan, Illinois, North Carolina, Maryland, and Pennsylvania along with fuel leakage data from one State, Michigan. The Michigan data are considered the best source of information on crash fires and fuel leaks, and therefore the primary analysis is carried out on this set.

Throughout the analyses, vehicles are grouped into two categories, Pre-standard vehicles, comprised of Model Years 1972 through 1975, and Post-Standard vehicles, comprised of Model Years 1976 through 1980. This grouping assumes that effectively a single, or combined standard was introduced and no attempt is made to assess the individual effectiveness of the two Standard upgrades, for reasons given in the subsequent analyses.

In addition to the effect of the standard, the analyses also considers the effects of other factors such as vehicle age, impact direction, and impact severity, which may influence crash fire rates and crash-induced fuel leakage.

2.1 Analysis of Michigan Crash Fire Data

Michigan Data on Crash Fires encompasses three calendar years (1978, 1979, 1980) of Statewide, police-reported accidents. Beginning in 1978, the Michigan Accident Report Form was revised to include a specific check-box element for denoting presence of crash fires and/or fuel leakage (see Appendix B for a copy of the report form).

For purposes of analysis, the data were grouped into two categories corresponding to those vehicles produced before, and after, Standard 301 became effective. These two groups are referred to as "Pre-Standard" and "Post-Standard," respectively, throughout this report. The Pre-Standard Group contains vehicles of Model Years 1972 through 1975, while the Post-Standard Group contains vehicles of Model Years 1976 through 1980. This choice of restricting the Pre-Standard Group to four years creates a more balanced sample size for comparison and also minimizes any potential, extraneous variation (due to vehicle model year change, traffic exposure changes, aging effects, reporting biases, etc.) which might exist. This restriction essentially provides for a "cleaner" and more conservative analysis of the effects of Standard 301.

Also in the analysis, Standard 301-75, which became fully effective over two Model Years, 1976 and 1977, is considered as a single, combined standard, or effect, in a statistical sense, and attempts are not made to estimate the effect of these two standard upgrades separately. The reasoning here is that rollover accidents, to which the 1976 version of

the standard was directed, occur <u>very</u> rarely as compared to other types such as frontal impacts or rear impacts and the resultant small sample size would likely be insufficient to provide a very sensitive or precise test, especially since fires themselves are such rare events. This small

sample size constraint is further compounded in that only one Model Year, 1976, existed before the standard was upgraded to include side, and rear, as well as strengthened frontal impact requirements. Therefore, the two standard upgrades are considered as a "single" standard for purposes of analysis of their impact.

Table 1 displays the fire data as described above for each of the three calendar years. The data refer to all crash fires reported by the State of Michigan. Individual table entries are the ratios of fire frequency to that of vehicle crash frequency and the corresponding relative frequency, or proportion of vehicle crashes resulting in fire.

The overall fire rate is approximately two (2.0) fires per 1,000 vehicle crashes. Inspection of the column totals does not reveal any evidence of an increase in fire rate, due to possible aging or degradation of vehicle/fuel system components. In fact, the overall rates for the three calendar years are amazingly close. Similarly, inspection of row totals, within each Pre- and Post-Standard grouping, indicates little evidence of a trend of higher fire rates for older vehicles. Of course this latter comparison also contains a potential effect of model year as distinct from any age effect. Within standard groups, however, the rates for model years are reasonably homogeneous.

TABLE 1 - MICHIGAN CRASH FIRE RATES

No. of Crash Fires/No. of Crash-Involved Vehicles and Fire Rates, Per 1,000 Vehicle Crashes, for Calendar Years Shown

MODEL	Calendar		~	TOTAL	
Year	Years 1978	1979	1980	1978 thru 1980	ĺ
1972	115/50635 = 2.271	116/40530 = 2.862	71/28543 = 2.487	302/119708 = 2.523	ſ
1973	134/57560 = 2.328	138/48529 = 2.844	106/36290 = 2.921	378/142379 = 2.655	
1974	137/49783 = 2.752	91/43199 = 2.107	95/32659 = 2.909	323/125641 = 2.571	
1975	96/40235 = 2.386	76/35497 = 2.141	71/28037 = 2.532	243/103769 = 2.342	ļ
1976	90/52393 = 1.718	86/45713 = 1.881	64/36069 = 1.774	-240/134175 = 1.789	
1977	104/65928 = 1.729	82/55664 = 1.473	67/44426 = 1.508	263/166018 = 1.584	
1978	86/47002 = 1.830	102/60281 = 1.692	69/46349 = 1.489	257/153632 = 1.673	
1979		82/41475 = 1.977	86/47791 = 1.780	168/89266 = 1.882	
1980			47/28305 = 1.660	47/28305 = 1.660	
1981				·	ļ
TOTALS	$\overline{772/363536} = \overline{2.124}$	$\overline{773/370888} = 2.084$	676/328469 = 2.058	$\overline{2221/1062893} = \overline{2.090}$	

Yet a third view of the potential effect of age can be seen in Table 2. Here fire rates for Pre- and Post-Standard vehicles are shown as a function of the (chronological) age of the vehicle at the time of the crash. Again it is seen that little evidence of an age effect (i.e., higher rates for older vehicles) appears within either the Pre- or the Post-Standard groups, but a rather distinct difference is noted between the two groups with the rates for Pre-Standard vehicles being consistently higher than the rates for Post-Standard vehicles. For the two cases where the same ages (e.g., three years and four years, denoted by the "box" in Table 2) are available, this same trend holds.

TABLE 2 - MICHIGAN CRASH FIRE RATES BY AGE OF VEHICLE (AT TIME OF CRASH) AND STANDARD STATUS

	Fires Per Vehicl	e Crash (x 10 °)
Vehicle Age,		,
Years	Pre-Standard	Post-Standard
8	2.487	
. 7	2.890	,
6	2.640	
5	2.298	
4	2.498	1.774
3	2.386	1.697
2		1.561
1		1.736
0		1.841

Tables 1 and 2 both show a rather distinct breakpoint beginning with the 1976 Model Year group, or the onset of the Post-Standard period. Figure 1 graphically illustrates this decline in fire rates between the



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1975, and earlier, model years, and the 1976, and later, model years. The mean fire rates for the two groups, computed from the data in Table 1, are:

Pre-Standard:

1246 vehicle fires 491,497 vehicle crashes = 2.535 fires per 1,000 crashes

Post-Standard:

975 vehicle fires 571,396 vehicle crashes = 1.706 fires per 1,000 crashes

The difference in these two means is 2.535 - 1.706 = 0.828 fires per 1,000 vehicle crashes, or a reduction of .828/.2535 = 32.7 percent for the Post-Standard group compared to the Pre-Standard group.

2.1.1 Overall Fire Rate

We can assess whether this difference is statistically significant using the normal distribution since the sample sizes are guite large even though the individual "p's" are guite small. We compute the value:

$$z_{calc} = \frac{P_1 - P_2}{D_{P_1} - P_2}$$

(1)

$$\frac{p_1 - p_2}{\left[p (1 - p)\left(\frac{1}{n_1} + \frac{1}{n_2}\right)^{l_2}\right]}$$

where

 p_1 , p_2 = observed sample rates for the Pre-Standard and Post-Standard groups, respectively, with corresponding sample sizes n_1 , n_2 ;

and

p = overall, or weighted average rate given by

$$\hat{\mathbf{p}} = \frac{n_1 \mathbf{p}_2 + n_2 \mathbf{p}_2}{n_1 + n_2} \tag{2}$$

 $\hat{\mathcal{O}}_{p_1-p_2}$ is the estimate of the overall population standard

deviation.

Substituting into (2), we obtain

 $\hat{\mathbf{p}} = \frac{491497 (.002535) + 571396 (.001706)}{491740 + 571396}$

Next, substituting into (1):

$$z_{calc} = \left[\frac{.002535 - .001706}{(.002089)(.997911)} \left(\frac{1}{491740} + \frac{1}{571396} \right) \right]^{\frac{1}{2}}$$

Assuming a one-tail test at a 95 confidence level, (i.e., $H_0: \mu_1 = \mu_2$ against the alternative, $H_1: \mu_1 > \mu_1; \alpha = .05$), this result is highly significant since

$$Z_{calc} = 9.325 > Z_{Table;.05} = 1.645$$

From this we reject the null hypothesis in favor of the alternative and conclude that the samples do not represent vehicles from the same population; the fire rate in the Post-Standard population is significantly lower than that for the Pre-Standard population. The estimated difference is 0.828 fires per vehicle crash less for the Post-Standard group, or a reduction of .828/2.534 = 32.8 percent.

2.1.2 Influence of Other Factors on Crash Fire Rates

In the above analysis, the effect of Pre- and Post-Standard vehicles, age, model year, and calendar (or accident) year have been considered. Of course it is possible that other factors could be influencing crash fire rates in addition to standard effects. For instance, impact speed, object impacted, type or direction of impact, and vehicle type/size are other potential factors that might affect whether or not a fire occurs as a result of a vehicle crash. Certainly, it is more reasonable to expect that the more severe the crash, in terms of damage to the vehicle, the more likely fuel system damage and fuel leakage would occur; similarly, ignition sources such as friction-generated sparks (from metal-to-metal

contact, metal-to-pavement contact, electrical shorting, etc.) would be expected to occur with greater probability in more severe crashes. Due to the nature and location of fuel system components, fuel tank, fuel lines, fuel pump, carburetor, etc.), it is also reasonable to expect that type of impact (i.e., rollover, side swipe) or the direction of impact (rear, front, etc.) could influence the likelihood of fires in vehicle crashes.

In the Michigan data, one can investigate vehicle crash severity as recorded on the accident report by a Vehicle Damage Severity (VDS) scale. For each accident involved vehicle, the investigating/ reporting officer assigns a numerical value, from 1 to 8, to denote the extent of damage sustained by each vehicle. A VDS of 1 represents very light, or minor, vehicle damage, while a VDS of 8 represents very extreme damage (See Appendix A). The Michigan data also include a variable to describe the direction, or type, of impact sustained by each accident involved vehicle.

Tables 3 and 4 contain the distribution of Vehicle Damage Severity and the distribution of impact direction, for the Pre-Standard and Post-Standard vehicle groupings, respectively. It can be postulated that if the distribution of either, or both, of these variables differs significantly between Pre- and Post-Standard groups, then the overall fire rates for these groups, as computed earlier might need to be adjusted, in order to obtain a more realistic, or "net" effect of Standard 301.

	Pre-Standard (Mod. Yrs. 1972-1975)			Post-Standard (Mod. Yrs. 1976-1980)			
Vehicle Damage Severity	Observed Frequency	Expected Frequency	Column Frequency	Observed Frequency	Expected Frequency	Column Frequency	TOTALS (Observed Frequency)
1	4721	3990	.03858	5743	6474	.02892	10464
2	31317	31711	.25595	51842	51448	.26108	83159
3	31976	32761	.26134	53936	53151	.27162	85912
4	24740	24981	.20220	40770	· 40529	.20532	65510
5	15230	15196	.12447	24619	24653	.12398	39849
6	8017	7866	.06552	12610	12761	.06350	20629
7	3814	3590	.03112	5601	5825	-02821	9415
- - 8	2540	2261	.02076	3390	3669	.01707	5930
TOTALS	122355		.999	198511		.999	320866

TABLE 3 - DISTRIBUTION OF VEHICLE DAMAGESEVERITY BY STANDARD GROUP

Based on Michigan data for Calendar Year 1980

TABLE 4 - DISTRIBUTION OF IMPACTTYPE BY STANDARD GROUP

	Pre-Standard (Mod. Yrs. 1972-1975)			Post-Standard (Mod. Yrs. 1976-1980)			TOTALS
Impact Type	Observed Frequency	Expected Frequency	Column Percentage	Observed Frequency	Expected Frequency	Column Percentage	(Observed Frequency)
Frontal	76943	75406	72.1	118511	120048	69.8	195454
Rollover	1793	1773	1.7	2802	2822	1.6	4595
Rearend	27981	29539	26.2	48584	48026	28.6	76595
TOTALS	106717		100.0	169897	``	100.0	276614

Based on Michigan data for Calendar Year 1980 To ascertain whether the Vehicle Damage Severity and impact type distributions differ between Pre- and Post-Standard groups, Chi-square tests for independence were run.

For the distribution of Vehicle Damage Severity, the test proceeds as follows; first compute:

$$\chi^{2} = \sum_{i=1}^{16} \frac{(o_{i} - e_{i})^{2}}{e_{i}}$$
 (3)

Where o_1 and e_1 represent the individual observed and expected cell frequencies, respectively, from Table 3. Substituting these individual values and performing the calculation yields a χ^2 value of 341.6. This value is significant, statistically, since it is larger than the corresponding tabled Chi-square value of 14.1 (σ_1^{\bullet} .05, df = 7). This value implies that indeed, Pre- and Post-Standard vehicles cannot be presumed to come from the same population of Vehicle Damage Severity. Closer inspection reveals that the primary contributors to a significant test statistic, are the upper and lower ends of the damage severity scale. More specifically the Post-Standard vehicles tend to have a smaller proportion of higher severity crashes, but a larger proportion of lower severity crashes than Pre-Standard vehicles. One would, of course, expect higher severity crashes to result in greater likelihood of fire.

Turning to the Impact Type Distribution, a similar test is performed using equation (3), but this time substituting the data from Table 4. This calculation yields a χ^2 value of 185.2. Again this result is
statistically significant since 185.2 is greater than the corresponding tabled Chi-square value of 5.99 (a = .05, df = 5). Inspection of Table 4 indicates that Post-Standard vehicles experience a somewhat greater proportion of rear end, but a slightly lower proportion of frontal impacts, than do Pre-Standard vehicles.

The foregoing findings of different Vehicle Damage Severity and Impact Type distributions, between Pre- and Post-Standard groups imply the need to investigate these effects on the overall decrease in fire rates for Post-Standard vehicles, as computed earlier, to determine if some adjustment is warranted.

The investigation of the Vehicle Damage and Impact Type effects takes the form of breaking the data down, according to these additional variables, and reperforming the analyses of Pre- and Post-Standard groups. Specifically, the two groups, Pre and Post, will be compared for each Vehicle Damage Severity level and Impact Type.

2.1.3 Analysis of Michigan Data by Crash Type and by Vehicle Damage Severity

In order to preserve reasonable cell sizes and since fire rates exhibited a rather distinct difference between lower and higher damage severity levels, the data were grouped into two categories, "Low to Moderate," defined by Vehicle Damage Severity = 2, 3, 4, or 5, and "Major," defined by Vehicle Damage Severity = 6, 7, 8, for purposes of analysis. Vehicle Damage Severity = 1 was not included since it represented a very minor accident severity and since very few crash fires occur at this level.

2.1.3.1 Vehicle Damage Severity: Low to Moderate (VDS = 2, 3, 4, 5)

Tables 5, 6, and 7 contain the distributions of fires, crashes, and fire rates for Pre- and Post-Standard vehicles for each of the three major impact types, frontal, rearend, and rollover. The data are from Michigan and cover years 1978, 1979, and 1980. In general, the magnitude of the fire rates for frontal and rearend impacts is similar at slightly more than one fire per 1,000 vehicle crashes. Rollover fire rates are highest, ranging from approximately three to five fires per 1,000 vehicle crashes.

 TABLE 5 - FIRE RATES, PRE- AND

 POST-STANDARD GROUPS,

 FRONTAL CRASHES, LO-MODERATE

 CRASH SEVERITY

Standard Group	No. Fires	No. Veh. Crashes	Fire Rate $(x \ 10^{-3})$
Pre-Std.	360	229,433	1.569
Post-Std.	311	261,002	1.192

First a comparison is made for frontal impacts. As before, the Pre-Standard rate is representated by p_1 and the Post-Standard rate by

P2.

Substitution of the respective values from Table 5 into (1) gives a Z-calculated value of 3.577. Since 3.577 is greater than the normal distribution value of 1.645 (α = .05, one-tailed test), the null hypothesis of equal fire rates for Pre- and Post-Standard vehicles is rejected in favor of the alternative hypothesis that the Post-Standard fire rate is lower. The estimated magniture of the reduction in fire rate is given by:

$$\frac{P_1 - P_2}{P_2} = \frac{.000377}{.001509} = 24.0\%$$

Moving to rearend crashes (Table 6), a similar comparison yields a Z-value of 1.49. The test statistic value of 1.49 is less than the tabled value of 1.645. Therefore, the conclusion for rearend impacts at a Lo to Moderal level is that no significant difference exists between the fire rate for Pre- and Post-Standard vehicles. Although the Post-Standard fire rate is numerically lower by an amount equal to $\frac{P_1 - P_2}{P_1} = \frac{.000377}{.001395} = 16.3$ percent, it is not significant at the .05 level which is the (risk) level chosen for the statistical comparison. The value 1.49 would reach significance, however, if the risk level were raised by approximately only <u>two</u> percentage points, to a level of 0.7, which would correspond to a 93 percent confidence level.

TABLE 6 - FIRE RATES, PRE- AND POST-STANDARD GROUPS, REAREND CRASHES, LO-MODERATE CRASH SEVERITY				
Standard Group	No. Fires	No. Veh. Crashes	Fire <u>Rate (x 10³)</u>	
Pre-Std.	139	99,663	1.395	
Post-Std.	139	119,141	1.167	

The final comparison in the Lo-Moderate crash severity is for rollover crashes for which the data are shown in Table 7.

TABLE	7 - FIRE RA POST-S ROLLOVI CRASH S	ATES, PRE- AND IANDARD GROUPS ER CRASHES, LO SEVERITY	, -MODERATE
Standard Group	No. <u>Fires</u>	No. Veh. Crashes	Fire <u>Rate (x 10³)</u>
Pre-Std.	14	2,946	4.752
Post-Std.	10	3,541	2.824

This time, since cell sample sizes are considerably lower, a nonparametric statistic is employed to test for difference between the Pre- and Post-Standard groups. Using the Chi-square test, as in (3) and the data from Table 7, the following calculation results

$$\chi^{2} = \frac{(14 - 10.9)^{2}}{10.9} + \frac{(3935.1 - 2932)^{2}}{2935.1}^{2}$$

$$+\frac{(10-13.1)^2}{13.1} + \frac{(3531-3527.9)^2}{3527.9}$$

= 1.63

Comparison of this value, 1.63 with the corresponding table value. of the χ^2 distribution of 3.84 ($\varkappa = .05$, df = 1), indicates a nonsignificant result. Hence the conclusion of no difference between the Pre- and Post Standard fire rates for rollover crashes of Lo-Moderate crash severity. Once again, the Post-Standard rate is numerically lower than the Pre-Standard rate--by an amount equal to: $\frac{p_1 - p_2}{p_1} = \frac{.004752 - .002824}{.004752}$

= 40.6 percent, but the small number of fires and vehicle crashes precludes this reduction as significant.

Summarily, for the Lo-Moderate crash category, only Frontal impacts showed a statistically significant reduction in fire rate for the Post-Standard vehicles. This reduction was estimated at 24 percent based on a difference of 1.57 fires per 1,000 crashes for Pre-Standard vehicles vis-a-vis

1.19 fires per 1,000 crashes for Post-Standard vehicles. Rearend and rollover crashes, although displaying numerically lower fire rates for Post-Standard vehicles did not reach statistical significance between Pre- and Post-Standard groups at the chosen significance level of 5 percent. Very sparse data were available for rollover crashes and rearend crashes which would show significance at an *equivalenter* of 7 percent (i.e., 93 percent confidence level.

2.1.3.2 Vehicle Damage Severity: Major (VDS = 6, 7, 8)

Pre- and Post-Standard fires and fire rates for frontal, rearend, and rollover impacts are shown in Tables 8 through 10, respectively, for those vehicles sustaining Major crash damage (i.e., VDS = 6,7,8). As with the Lo-Moderate crash damage level, the data are from Michigan Statewide files for Calendar Years 1978, 1979, and 1980.

The general trend of the fire rates over the three impact types is somewhat similar to that noted for the Lo-Moderate severity impacts with the rates for frontals and rearends being more nearly similar but less in magnitude than the rates for rollovers. One departure within this general trend, however, is that for Pre-Standard vehicles, rearend fire rates are higher than frontal fire rates, and in fact are as high as rollover fire rates. When contrasted with the fire rates for the Lo-Moderate crash level, the effect of higher crash forces on the liklihood of fire is clearly evident, with fire rates ranging as much

as ten times higher for the major severity crashes.

TABLE	8	-	FIRE RATES, PRE- AND
			POST-STANDARD GROUPS,
			FRONTAL CRASHES, MAJOR
			CRASH SEVERITY

Standard Group	No. Fires	No. Veh. Crashes	Fire <u>Rate (× 10⁻³)</u>
Pre-Std.	91	9,465	9.614
Post-Std.	79	14,425	5.477

Table 8 displays the fire rate data for Frontal crashes. Testing for significance between the Pre- and Post-Standard rates, as before, gives a value of 3.848. This value of 3.848 is greater than 1.645, the reference value of 1.645 (ϕ_1 = .05) and it is concluded that the Post-Standard fire rate is significantly lower than the Pre-Standard rate. The corresponding magnitude of reduction is given by $\frac{P_1 - P_2}{P_1} = \frac{.004137}{.009614} = 43.0$ percent.

Turning next to Rearend impacts, Table 9 shows the Post-Standard rate of 5.76 fires per 1,000 vehicle crashes to be considerably below the Pre-Standard rate of 14.28.

 TABLE 9 - FIRE RATES, PRE- AND

 POST-STANDARD GROUPS,

 REAREND CRASHES, MAJOR

 CRASH SEVERITY

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e 296 - 2 6	Standard Group	No. Fires	No. Veh. Crashes	Fire <u>Rate (</u> x	10 ⁻³)	4	1
	Pre-Std.	90	6,304	14.28			
	Post-Std.	40	6,944	5.76			

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To ascertain whether this difference is statistically significant, the previous computation is repeated using the data from Table 9. This results in a Z-value of 4.982 which again, is significant since it exceeds 1.645 (q = .05), the reference normal distribution point. Computing the extent of the reduction in fire rate for the Post-Standard group yields $\frac{p_1 - p_2}{p_1} = \frac{.00852}{.01428} = 66.7$ percent.

TABLE 10 - FIRE RATES, PRE- AND POST-STANDARD GROUPS, ROLLOVER CRASHES, MAJOR CRASH SEVERITY

Standard Group	No. <u>Fires</u>	No. Veh. Crashes	Fire Rate (× 10 ⁻³)
Pre-Std.	49	3,389	14.46
Post-Std.	29	3,599	8.05

The final analysis under the Major crash severity category is for Rollovers. Using the data from Table 10 and performing the calculations as before gives a Z-value of 2.504.

Hence, the third and last analysis under Major crash severity also yields a significant result, the computed value of 2,504 once again being greater than the reference value of 1.645 (e_s = .05). The corresponding reduction in fire rate for the Post-Standard group over the Pre-Standard group being $\frac{P_1 - P_2}{P_1} = \frac{.00641}{.01466}$ or 44.3 percent. In summary, analysis of the crashes involving Major crash severity (i.e., major vehicle damage) exhibited statistically significant fire rate reductions for the Post-Standard vehicles for all three impact types, Frontal, Rearend, and Rollover. The greatest reduction was noted for Rearend impacts (67 percent), followed by Rollovers and Frontal impacts with nearly identical reductions estimated at 44 percent and 43 percent, respectively.

2.1.3.3 Summary of Analysis of Other Factors

In summary, even though Post-Standard vehicles, overall, experienced a slightly lower rate of higher severity crashes, and slightly lower relative frequencies of those types of impacts most likely to be associated with fires, separate analyses of the data, controlling for these factors showed Post-Standard vehicles still had significantly lower fire rates than Pre-Standard vehicles for four of the six subgroups compared. In the remaining two subgroups where significant reductions were not found, one subgroup (Rollover Lo-Moderate) was characterized by limited sample

size; the other subgroup (Rearend, Lo-Moderate) was nearly significant, needing a relaxation of only two percentage points above the 5 percent risk level chosen for the statistical comparison to be declared significant, (i.e., at an e_{x} = .07, or a confidence level of 93 percent, the fire rate

for Rearend, Lo-Moderate severity would have been significantly lower for the the Post-Standard group).

The reductions in fire rate were concentrated in the higher crash severity range, as defined by extent of vehicle damage, and occurred for all three major impact types, Frontal, Rearend, and Rollover. Finally, the magnitude of the reduction in fire rates for these categories was greater than the reduction noted in the overall, unadjusted data and these categories accounted for approximately 80 percent of the total number of vehicle crash fires. Table 11 summarizes the results of these analyses.

Crash Type	Vehicle Damage Severity	Proportion of Total Fires	Percent Reduction for Post-Std. Group	Reduction Statistically Significant?
Frontal	Lo-Mod.	53.1	24.0	Yes
	Major	11.7	43.0	Yes
Rearend	Lo-Mod.	19.2	16.3	No
	Major	9.0	66.7	Yes
Rollover	Lo-Mod.	1.7	40.6	No
٠	Major	5.4	44.3	Yes

 TABLE 11 - SUMMARY OF ANALYSES BY CRASH TYPE

 AND VEHICLE DAMAGE SEVERITY

 MICHIGAN FIRE DATA

2.1.4 Summary of Analysis of Michigan Crash Fire Data

Collectively, the results of analysis of the Michigan fire data indicate that not only have significantly lower fire rates occurred in Post-Standard vehicles, but that the majority of these reductions have occurred in those accidents that have been more severe in terms of the extent of (crash) damage to the vehicle. Also, reductions occurred for the three major impact types investigated, Frontal, Rearend, and Rollover. This can be seen graphically in Figure 2, which plots fire rates by vehicle model year for the family of vehicle damage severity ratings (i.e., VDS) from 3 through 8. Here it is seen that at the lower crash severities (3 to 5), rather homogeneous fire rates occur over the eight to nine model years. In contrast, for the highest crash severities (6, 7, 8), rather marked decreases are noted, in fire rates, over the same model year span. Furthermore, these changes are basically consistent over each of the three highest crash severity ratings. This figure also shows that the primary point of decrease in fire rates occurs at the 1976 Model Year and, once again, this phenomenon is consistent for each of the three highest crash severities (VDS = 6, 7, 8).

From a safety standpoint, the fact that the greatest reductions in fire rates occurred at the higher crash force levels can be viewed in at least two ways. First, since more severe crash forces are more likely to produce occupant injury (due to the crash forces themselves), it may be stated that the concomitant occurrence of fire might not be considered so great a hazard. On the other hand, it can be argued that it is desirable to minimize fire in more severe (crash force) accidents, since the higher



likelihood of occupant injury (due to impact forces) would render the (victim)(s) less likely to be able to extricate themselves from the vehicle, should fire occur, and therefore less likely to escape further injury, even severe or fatal injury. Furthermore, severe crashes are more likely to result in entrapment of vehicle occupants, due to collapsed vehicle structures (jammed doors, broken/jammed window cranks, etc.). In such instances the occurrence of fire poses an extreme hazzard since the only hope for occupants would be extrication by "outside" assistance, and since critically short time would typically be available for rescue.

Finally, the results of these analyses are in general agreement with the nature of the 1976 and 1977 upgrades of Standard 301. That is, the greatest decreases in fire rates were noted for Rearend and for Rollover crashes, the primary types of impacts addressed by the 1976 and 1977 revisions of Standard 301. Significant reductions in fire rates were also noted for Frontal impacts, which also were addressed, as an upgrade by the 1976/77 Standard.

2.2 Analysis of Illinois Crash Fire Data

1- No. As

Analysis of data from the State of Illinois covers four calendar years, 1977, 1978, 1979, and 1980. Although data for six years (1975 through 1980) were available, years 1975 and 1976 were excluded from the analysis because of markedly higher incidences of unknown data, relative

to crash fires, for these two earliest years. Such differences in reporting could bias the data and possibly give misleading analytical results, particularly since the phenomenon of interest (crash fires) is such a rare occurrence relative to the differences in proportions of missing data.

The Illinois Accident Report form (see Appendix B) contains a specific element for the reporting of fires, although the method differs somewhat from that used by Michigan (see Appendix A - Data Sources).

As with the data from Michigan, vehicle model year range was restricted to 1972 through 1980, in order to obtain a more balanced set of data in terms of sample size, and to minimize the potential for extraneous effects which might contribute bias or confounding influences. Similarly, for purposes of analysis, and for reasons described previously (see Section 3.1), Standard Revisions 301-76 and 301-77 are considered as a "single" standard effect beginning with Model Year 1976.

2.2.1 Fire Rates Based on Illinois Data

Table 12 displays the data for Illinois for the four Calendar Years 1977 through 1980. The overall fire rate is approximately 1.6 fires per 1,000 vehicle crashes. Inspection of the column totals does not reveal any increase in fire rate due to possible aging, or vehicle/component degradation, up to a period of four years. As with the Michigan data, the results for the four years show little variation. Additionally,

TABLE 12 - ILLINOIS CRASH FIRE RATES

No. of Crash Fires/No. of Crash-Involved Vehicles and Fire Rates, Per 1,000 Vehicle Crashes, for Calendar Years Shown

MODEL Year	Calendar> 1977 Years>	1978	1979	1980	TOTAL 1977 thru 1980
1972	110/63101 = 1.743	95/58621 = 1.621	79/50068 = 1.578	57/33465 = 1.703	341/205,255 = 1.661
1973	144/71685 = 2.009	122/67289 = 1.813	100/58769 = 1.702	79/41178 = 1.919	445/238,921 = 1.863
1974	104/64359 = 1.616	114/60710 = 1.878	88/53936 = 1.632	67/38974 = 1.719	373/217,979 = 1.711
1975	90/42959 = 2.095	83/50609 = 1.640	73/45282 = 1.612	51/33120 = 1.540	297/171,970 = 1.727
1976	103/56615 = 1.819	104/67086 = 1.550	99/60903 = 1.626	66/44139 = 1.495	372/228,743 = 1.626
1977	72/57080 = 1.261	119/78599 = 1.514	102/71059 = 1.435	101/51205 = 1.972	394/257,943 = 1.527
1978		83/56314 = 1.474	107/77098 = 1.388	93/55683 = 1.670	283/189,095 = 1.497
1979			81/48130 = 1.683	81/57708 = 1.404	162/105,838 = 1.531
1980				57/30704 = 1.856	57/30704 = 1.856
	ł				

623/355799 = 1.751 720/43922 = 1.639 729/465236 = 1.567 652/386176 = 1.688 2724/1646448 = 1.654

TOTALS

inspection of row totals, within Pre- and Post-Standard groups shows little evidence of a higher rate for older vehicles. Figure 3. is a plot of the data from Table 12.

For an additional view of the potential for an aging effect, the reader is referred to Table 13, which lists fire rates as a function of vehicle age, at time of test, for the Pre- and Post-Standard groups. As was noted above, no age trend is apparent within either of the two groups.

TABLE 13 - ILLINOIS FIRE RATES BY AGE OF VEHICLE (AT TIME OF CRASH) AND STANDARD STATUS

Fires Per Vehicle Crash (x 10^{-3})

Vehicle Age, Years	Pre-Standard	Post-Standard
8	1.703	1
7	1.732	,
6	1.676	
5	1.706	
4	1.863	1.495
3	1.627	1.784
2	2.095	1.543
1		1.518
0	,	1,524
	· · ·	

In contrast to the Michigan data, Tables 12 and 13 do not evidence a distinct decrease in rates beginning with the 1976 Model Year, although



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a somewhat lower overall rate is shown for the Post-Standard group, 1.56 versus 1.75 fires per thousand crashes.

Substituting into (1) to test whether this overall observed difference is statistically significant produces a Z-statistic of 2.920. This value is significant since 2.92 is greater than Z_{AB} . .05 = 1.645. The magnitude of the reduction is thus

 $\frac{.000185}{.001746} = 10.6$ percent

2.2.2 Influence of Other Factors

Further analysis of the Illinois data to investigate potential influence of other factors such as type of impact or crash severity, is precluded since definitive variables for such factors are not available from the Illinois data. Some data exist on "type of crash" (fixed object, head-on, etc.) but it is not possible to reliably relate such information to the type of impact, as was the case with the data from Michigan.

2.3 Analyses of North Carolina, Maryland, and Pennsylvania Data

Analysis of North Carolina, Maryland, and Pennsylvania data are presented in this section. The data on crash fires from these three States have been obtained by an indirect method of extracting data from police accident reports. That is, the accident reports from these States

do not contain specific data elements for recording the presence.(absence) of a crash fire. Therefore, information on fires is obtained by extracting data from the narrative portion of the accident report (North Carolina), or by using a filtering algorithm, composed of a number of other accident report variables (Maryland, Pennsylvania). The data sources and the processes of fire data extraction are described in Appendix A.

In accordance with the approach for analysis of data from the two previous States, the data are grouped into two categories: Pre-Standard, denoting those vehicles of Model Years 1972 through 1975, and Post-Standard, denoting those vehicles of Model Years 1976 through 1980. Also, as before, Standards 301-76 and 301-77 are considered as a single standard for purposes of analysis. The data from North Carolina cover eleven (11)

calendar (or accident) years, 1971 through 1981; the data from Maryland cover four calendar years, 1977-1981, and Pennsylvania data represent calendar years 1977 through 1979 (three years).

Table 14, displays the fire rates for North Carolina, Maryland, and Pennsylvania, respectively. An initial point of interest here is the fact that the fire rates from each of the three States are of the same order of magnitude, ranging from approximately five (Maryland) to

approximately seven (Pennsylvania) fires per 10,000 vehicle crashes. The consistency of the rates lends some support to the contention that fire data obtained by the indirect method yields reasonably consistent results. These rates, however, are considerably lower, by a factor of three to four, than those found in the Michigan and Illinois data sets. These lower rates are to be expected since they are derived from indirect reporting methods as described earlier, as opposed to the direct data element methods used by Michigan and Illinois. Figure 4 displays graphically the data from Table 14.

Because of: (a) the similarity of the fire rates from each of these three States, (b) the fact that the fire data for each State are obtained by similar (indirect) methods, and (c) the lack of adequate sample sizes within each State to permit satisfactory, State-by-State analysis of various factors which might influence crash fire rates, it is therefore deemed most appropriate to carry out analysis of the data from North Carolina. Maryland, and Pennsylvania on a collective basis, i.e., by considering the data as a combined set.

Reference to Table 14 and Figure 4 give some indication that age may be a factor in contributing to higher fire rates for older, or for Pre-Standard Vehicles. Some evidence of this is seen in the rates within the Pre-Standard group for Pennsylvania and within both Pre-Standard and Post-Standard groups for the Maryland data. In contrast, little or no evidence of an age factor is seen for the Post-Standard group for Pennsylvania or for either group (Pre- or Post-Standard) in the North Carolina data.

TABLE 14 - CRASH FIRE RATES FOR NORTH CAROLINA, MARYLAND, AND PENNSYLVANIA.

Model Year	North Carolina	Maryland	Pennsylvania
1972	91/151,787 = .5995	49/72,824 = .6729	46/63,261 = .7746
1973	79/139,931 = .5646	51/85,020 = .5999	48/74,032 = .6484
1974	58/100,553 = .5768	38/76,994 = .4935	49/69,093 = .7092
1975	31/57,957 = .5349	33/63,881 = .5166	37/55,844 = .6621
1427 QUUD GUID QUU QUU QUU QUU QUU			
1976	36/69,947 = .5147	35/85,959 = .4072	42/68,383 = .6142
1977	24/57,015 = .4209	28/85,159 = .3288	44/77,900 = .5648
1978	12/46,200 = .2597	19/62,689 = .3031	41/61,928 = .6621
1979	9/39,222 = .2295	6/33,053 = .1815	26/30,394 = .8554
1980	11/21,259 = .5174		

No. of Crash Fires/No. of Crash-Involved Vehicles and Respective Crash Fire Rates, Per 1,000 Vehicle Crashes

Overall 351/683,871 = .5133 239/565,579 = .4579 336/500,875 = .6708



A O V A E E

TABLE 15 - CRASH FIRE RATES, PRE- AND POST-STANDARD VEHICLES BY AGE AT TIME OF CRASH FOR NORTH CAROLINA, MARYLAND, AND PENNSYLVANIA

No. of Crash Fires/No. of Crash-Involved Vehicles and Fire Rates, Per 1,000 Vehicle Crashes

	North Car	North Carolina		Maryland		Pennsylvania	
Age (Yrs.) at Time of Crash	Pre-Standard	Post-Standard	Pre-Standard	Post-Standard	Pre-Standard	Post-Standard	
7	••• ·	*-					
6	50/90746 = .5510	5/104334792			11/29119 = .6182		
5	57/96150 = .5928	14/26175 = .5349	40/67436 = .5932	7/11189 = .6256	54/69414 - .772 9	-	
4	64/103732 = .6170	19/38207 = .4973	22/45320 = .4854	13/33945 = .3830	42/64198 = .6542		
3	64/103414 = .6189	11/466112360	8/20258 = .3949	17/63062 = .2696	18/32250 = .5581	20/3201 = .6236	
2	46/90638 = .5075	17/62825 = .2706		30/69986 = .4287	9/10385 = .8667	31/59535 = .5207	
1	29/58555 = .4953	26/52694 = .4934		21/66663 = .3150		52/80511 = .6459	
0						50/66488 = .7520	

In addition to age as a potential factor here, it must be borne in mind that other factors, such as <u>model year</u> differences, could also be affecting the fire rates. Perhaps a better method of examining the effect of age is to compare the Pre- and Post-Standard vehicle groups on the basis of similar age (of vehicle) at the time of the accident, or crash. Such comparisons are made in Table 15 for North Carolina, Maryland, and Pennsylvania, individually, and in Table 16 for the three States, combined.

TABLE	16	FIRE RATES, PRE- AND POST-STANDARD
		VEHICLES, BY AGE AT TIME OF CRASH -
		NORTH CAROLINA, MARYLAND AND
		PENNSYLVANIA DATA, COMBINED

*7 . 9 . 4 . 1	Fire Rates $(x \ 10^{-3})$		
Years	Pre-Standard	Post Standard	
7	Alian Alian	titue dide	
6	.5510	.4792	
5	. 5930	. 5620	
4	.5770	.4435	
3	.5772	.4253	
2	. 5444	.3923	
1	.4953	.4934	
0	Data das	' <u></u>	

A study of Table 15 indicates that age has a minor or negligible influence while for equivalent ages, fire rates for Post-Standard vehicles are rather consistently below fire rates for Pre-Standard vehicles. In eight of eleven individual cases where vehicles of the same age could be compared, Post-Standard vehicles had lower fire rates. In one case, Pre- and Post-Standard vehicle rates were essentially the same, and in the remaining two cases, Post-Standard vehicles had higher fire rates. Figure 5 is a graphic display of the combined data from Table 16. In summary, this comparison does not support the theory that vehicle aging affects crash fire rates, at least for the range of data considered here.

To determine if the overall Pre- and Post-Standard rates as shown in Table 16 are statistically significant, a Z-statistic is calculated. The value obtained is 9.867.

Therefore, it is concluded that the difference (e.g., $22.0\% = \frac{P_1 - P_2}{P_1} = \frac{.0001248}{.0005662}$

is statistically significant, since 9.867 $Z_{TAB,.05} = 1.645$, and that the Post-Standard vehicle population exhibits a 22 percent lower fire rate than Pre-Standard vehicles.

Further analysis of other factors which might influence fire rates is precluded since common variables are not identified in the three State data sets.



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2.4 Fuel Leak Reduction (Michigan Data)

Data of fuel leakage were available from only one source--the State of Michigan. Appendix A describes the procedure for recording fuel leakage on the Michigan Accident Report Form, a copy of which is included in Appendix B.

Overall leakage rates are contained in Table 17 for the three calendar years of data and for Model Years 1972 through 1980. It is seen that the overall leak rate is approximately one per 100 vehicle crashes, which is some five times as high as the overall fire rate for the same (i.e., Michigan) set of data.

Inspection of the marginal totals in Table 17 reveals little evidence of an age trend over the three calendar years, but over model years there is considerable indication that older vehicles may have higher leak rates, particularly for the Pre-Standard or 1972-1975 group where a linear increase appears most consistent.

Of course, as was stated earlier, such differences or indications of age trends may be confounded with other factors such as the model year of the vehicle. Table 18 affords a better view of the aging phenomenon by age of vehicle at the time of the crash. Here a trend relating to age

TABLE 17 - FUEL LEAKAGE RATES, STATE OF MICHIGAN

Frequency of Fuel Leakage (Vehicles)/No. of Crash-Involved Vehicles, and Leak Rates, Per 1,000 Vehicle Crashes, for Calendar Years Shown

MODEL Year	Calendar > 1978 Years	1979	1980	TOTAL 1978 thru 1980	
1972	802/50635 = 15.84	664/40530 = 16.38	475/28543 = 16.64	1941/119708 = 16.21	
1973	800/57560 = 13.90	667/48529 = 13.74	520/36290 = 14.33	1987/142379 = 13.96	
1974	647/49783 = 13.00	501/43199 = 11.60	428/32659 = 13.11	1576/125461 = 12.54	
1975	416/40235 = 10.34	342/35497 = 9.63	282/28037 = 10.06	1040/103769 = 10.02	
1976	415/52393 = 7.92	403/45713 = 8.82	308/36069 = 8.54	1126/134175 = 8.39	
1977	496/65928 = 7.52	391/55664 = 7.02	332/44426 = 7.47	1219/166018 = 7.34	
1978	383/47002 = 8.15	411/60281 = 6.82	290/46349 = 6.26	1084/153632 = 7.06	
1979		329/41475 = 7.93	326/47791 = 6.82	655/89266 = 7 . 34	
1980			177/28305 = 6.25	177/28305 = 6.25	
TOTAL	2050/262526 - 10 90	3708/270898 - 0.008	2129/229460 - 0.55	10905 (1062902 - 10.13	
TOTALS	10.03 = 0.02	J100/J10000 = 9.990	JTJ0/ JT04/03 = 3.33	TOOD / TOO SA2 = TO'T /	

is still in evidence and is similar to that noted above in that the trend is more pronounced for the Pre-Standard group. Figures 6 and 7 are graphical illustrations of these data and trends from Tables 17 and 18, respectively.

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TABLE 18 - FUEL LEAKAGE RATES, PRE- AND
POST-STANDARD VEHICLES BY AGE
AT TIME OF CRASH (MICHIGAN DATA)

	Fuel Leakage Rate (x 10 *)		
Vehicle Age (Years)	Pre-Standard	Post-Standard	
8	16.64		
7	15.41		
6	15.39		
5	12.29	·	
4	11.60	8.539	
3	10.34	8.154	
2	-	7.098	
1		7.086	
0		7.251	



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In order to statistically evaluate the age trends appearing in the fuel leakage data, simple linear regressions were run on the data from Table 18 for the Pre-Standard and Post-Standard groups. The following results were obtained.

Pre-Standard:

 $X_1 = 8.9420(10^{-3}) + 1.28657(10^{-3}) X_2$ $s_h = 7.312(10^{-5})$

Post-Standard:

$$x_{1} = 6.5324(10^{-3}) + 3.6440(10^{-4}) x_{2}$$

s = 1.2849(10^{-4})
b

In the above equations, X_1 represents the leakage rate; X_2 represents vehicle age, at time of crash; and s_b is the standard error of the estimates, or coefficients of the X_2 variables, generally denoted by "b". From Table 18, it is seen that the Pre-Standard model is based on N = 6 observations while the Post-Standard model is based on N = 5 observations.

The positive coefficients for X₂ in both of the above equations indicates that leakage rates tend to increase with age. Testing for significance of these trends (i.e., the null hypothesis is that the coefficient is not significantly different from zero, against the alternative

hypothesis that the coefficient is greater than zero), we have:

Pre-Standard:

$$t_{s} = \frac{b_{-0}}{s_{b}} = \frac{1.28657}{7.312} \frac{(10^{-4})}{(10^{-5})}$$

Post-Standard:

$$t_{s} = \frac{b - o}{s_{h}} = \frac{3.6440(10^{-4})}{1.2849(10^{-4})}$$

= 2.836

For the Pre-Standard group, the test statistic, t_s , is significant since $t_s = 17.595$ is greater than the corresponding table value of "t"TAB,.05 = 2.776 (with N -2 = 4 df). For the Post-Standard group, the test statistic is not significant since $t_s = 2.836$ is not greater than the corresponding table value of "t"TAB,.05 = 3.182 (with N -2 = 3 df). Mence, it is concluded that there is a significant age trend for the Pre-Standard vehicle group, but not for the Post-Standard group.

2.4.1 Effect of Standard 301 on Fuel Leakage

Since age (at time of crash) has been found to have a significant influence on leakage rate, it is appropriate to use data sets of common age (e.g., denoted to "box" in Table 18 to test for any difference between Pre-Standard and Post-Standard groups. These data correspond to vehicles that were three and four years of age at the time of crash, and more specifically, represent vehicles of Model Years 1974 and 1975, for the Pre-Standard group and Model Years 1976 and 1977, for the Post-Standard group. To test for differences, we proceed as in prior analyses:

Let $p_1 = Pre-Standard$ mean rate = (989 + 416)/(85,280 + 40,235)

= 1405/125,515

= .01119

Let $p_2 = Post-Standard$ mean rate = (308 + 735)/(36,069 + 90,139)= 1043/126,208= .008264

Substituting into (1) and performing the indicated calculations gives a z-statistic = 7.491.

Thus it can be concluded that the Post-Standard group has a significantly lower leak rate since 7.491 is greater than $Z_{TAB} = 1.645$ (A = .05).

This lower rate translates to a 26.2 percent reduction $\left(\frac{p_1 - p_2}{p_1}\right)$ and is the difference after controlling for age.

It should be noted in the above analysis that age at time of crash also includes some effect of vehicle model year. It may be that model year, in addition to age, has an effect on leak rate. To the extent this effect exists, the above analytical approach will produce estimates of fuel leak reduction that are somewhat high, since the estimates of differences between Pre- and Post-Standard groups would also include the confounded effect of model year. Preliminary investigation of this possibility indicates that the greater effect of model year is for the lower severity crashes (i.e., crashes having a small likelihood of serious occupant injury). While estimates of fuel leakage reduction between Pre- and Post-Standard groups would decline, significant reductions in fuel leakage would still exist, especially for accidents of higher crash severity.

2.4.2 Influence of Vehicle Damage Severity and Impact Type

Since the earlier analysis of fire data for the State of Michigan showed some differences in distributions of crash severity as denoted by vehicle damage severity (VDS), and impact type between the Pre-Standard and Post-Standard groups, it is appropriate to examine the effect on fuel leakage of these same parameters. Even though differences in crash severity and impact type distributions were found to be statistically significant, the actual numerical magnitude of these differences was quite small and subsequent analyses of sublevels of data showed predominately

significant reductions in fire rate for the Post-Standard population of vehicles. The analyses in the following sections are based on vehicles of equal age, Pre- and Post-Standard, since age was found to have a significant effect on fuel leakage.

2.4.2.1 Vehicle Damage Severity: Lo-Moderate

Tables 19, 20, and 21 contain the fuel leakage rates for Pre- and Post-Standard vehicles for the three Impact Types, Frontal, Rearend, and Rollover, respectively. The data are from Michigan for the years 1978, 1979, and 1980. For this Lo-Moderate level of crash severity, it is seen that fuel leakage rates are lowest for Frontal impacts at 3 to 4 leaks per 1,000 vehicle crashes. Rollovers are next with 6 to 7 leaks per 1,000 vehicle crashes, and Rearend collisions have the highest rate at 6 to 10 leaks per 1,000 crashes.

To determine whether significant differences exist between the Pre- and Post-Standard groups, analyses similar to those performed on the fire data are carried out. First the rates for Frontal crashes (Table 19) are compared:

TABLE 19 - LEAKAGE RATES, PRE- AND
POST-STANDARD GROUPS,
FRONTAL CRASHES, LO-MODERATE
CRASH SEVERITY

Standard Group	No. Fuel Leaks	No. Vehicle <u>Crashes</u>	Leakage R <u>ate (x 10⁻³)</u>
Pre-Std.	276	61,951	4 455
Post-Std.	197	52,665	3.741
As with the fire analysis, p_1 and p_2 are used to denote the leak rates for the Pre- and Post-Standard groups, respectively. Calculating the test statistic from (1) and (2), as before results in a Z-value of 1.879.

is $\frac{P_1 - P_2}{P_1} = 7.14 \times 10^{-4} / 4.455 \times 10^{-3} = 16.0$ percent.

Next Rearend crashes (Table 20) are compared:

Standard Group	No. Fuel Leaks	No. Vehicle Crashes	Leakage <u>Rate (x 10⁻³)</u>
Pre-Std.	204	20,321	10.039
Post-Std.	169	26,301	6.426

POST-STANDARD GROUPS,

REAREND CRASHES, LO-MODERATE

TABLE 20 - LEAKAGE RATES, PRE- AND

CRASH SEVERITY

Substituting into equation (1), the values from Table 20, yields a Z-value of 4.342.

Comparing this value, 4.342 with the tabled value (i.e.,

 $Z_{tab} = 1.645$, A = .05) again results in statistical significance; the conclusion being that Post-Standard vehicles exhibit a lower rate of fuel leakage than do Pre-Standard vehicles. The reduction in leakage rate is given by $3.613 \times 10^{-3}/1.0039 \times 10^{-2} = 36.0$ percent.

The final comparison of Pre- and Post-Standard leakage rates at the Lo-Moderate crash severity level is for Rollovers. The corresponding data are contained in Table 21.

TABLE 21 - LEAKAGE RATES, PRE- AND

CRASH SEVERITY

Standard Group	No. Fuel Leaks	No. Vehicle Crashes	Leakage <u>Rate (× 10⁻³)</u>
Pre-Std.	62	704	8.807
Post-Std.	60	781	7.682

POST-STANDARD GROUPS,

ROLLOVER CRASHES, LO-MODERATE

To determine whether the above numerical difference is significant, a statistical test of hypothesis is performed as before. Calculations produce a Z-value of .788, which is non-significant.

The conclusion is that no significant difference exists between the fuel leakage rates of Pre-Standard vehicles and Post-Standard vehicles for Rollover crashes with vehicle damage in the Lo-Moderate level.

2.4.2.2 Vehicle Damage Severity: Major

Tables 22, 23, and 24 list the fuel leakage rates for crashes of Major impact severity; Pre- and Post-Standard rates are given for Frontal, Rollover, and Rearend impacts, respectively. In general, it is seen that Frontal impacts have lower rates of fuel leakage, ranging from 25 to 40 per 1,000 vehicle crashes, while rates for Rollovers and Rearend impacts are much higher at 60 to 130 leaks per 1,000 vehicle crashes. The effect of higher crash severity on leakage rate is clearly seen here as the leakage rates are markedly higher than those for Lo-Moderate severity crashes as given in the previous section.

To determine whether the Pre- and Post-Standard leakage rates given in Tables 22-24 are significantly different, statistical analyses similar to those for the Lo-Moderate crashes are performed.

TABLE	22	-	LEAKAGE RATES, PRE- AND
			POST-STANDARD GROUPS,
			FRONTAL CRASHES, MAJOR
			CRASH SEVERITY

Standard Group	No. Fuel Leaks	No. Vehicle Crashes	Leakage Rates (x 10 ⁻³)
Pre-Std.	354	8,798	40.24
Post-Std.	213	8,402	25.35

First, for Frontal crashes, the data from Table 22 are substituted into equation (1) and calculations carried out as for the Lo-Moderate severity impacts. This gives a Z-statistic of 5.384, which is greater than the reference value of 1.645 (d = .05), and therefore it is concluded that the leakage rate for the Post-Standard vehicle is significantly lower than for Pre-Standard vehicles. The amount of the reduction in leakage rate for Post-Standard vehicles is 1.4866 x $10^{-2}/4.024 \times 10^{-2} = 37$ percent.

TABLE 23 - LEAKAGE RATES, PRE- AND POST-STANDARD GROUPS, REAREND IMPACTS, MAJOR CRASH SEVERITY

Standard Group	No. Fuel <u>Leaks</u>	No. Vehicle Crashes	Leakage <u>Rate (x 10-3)</u>
Pre-Std.	177	1,398	126.61
Post-Std.	172	2,795	61.54

Secondly, a comparison is made for Rearend Impacts. Using the data from Table 23 and performing the computations as before. For this comparison, Z = 7.191.

As before our reference value is Z = 1.645 (< < = .05). Since the calculated Z is greater than 1.645, the conclusion again is that Post-Standard vehicles have a significantly lower fuel leak rate. The magnitude of the reduction is $\frac{P_1 - P_2}{P_1} = 6.507 \times 10^{-2}/.12661$ or 51.4 percent.

TABLE 24 - LEAKAGE RATE, PRE- AND
POST-STANDARD GROUPS,
ROLLOVER IMPACTS, MAJOR
CRASH SEVERITY

Standard Group	No. Fuel Leaks	No. Vehicle Crashes	Leakage <u>Rate (x 10⁻³)</u>
Pre-Std.	96	′ 733	130.97
Post-Std.	50	725	68.97

The third and last comparison in the Major crash severity category is for Rollovers. Using the data from Table 24 and performing the computations as before gives a Z-value = 3.741.

Once again the conclusion is that the fuel leakage rate is significantly lower for the Post-Standard vehicles since the computed value of 3.741is greater than the tabled value of 1.645 (= .05). The percent reduction in leakage rate for the Post-Standard group is .0620/.13097 or 47.3.

2.4.3 Summary of Analysis of Fuel Leakage Data

Figure 8 is a plot of fuel leakage rate as a function of vehicle damage severity (VDS). These VDS levels are the same as those described in the section on fires. The data for the plot come from Table 18 and hence account for the effect of vehicle age. The graph is similar to earlier findings on fire rates, with the fuel leakage rates exhibiting marked tendencies to rise with higher vehicle damage severity or crash levels. The figure also depicts a consistently lower leak rate for the Post-Standard group.



Table 25 summarizes the results of the analyses of fuel leakage by Impact Type and Vehicle Damage Severity. Although age was found to have a significant effect on fuel leakage following a crash (i.e., older vehicles had significantly higher leakage rates), analyses controlling for this factor gave results which are in general agreement with the earlier results for crash fire data.

TABLE 25 - SUMMARY OF STATISTICAL COMPARISONS OF LEAK RATES FOR PRE- VS. POST-STANDARD VEHICLES: IMPACT TYPE X VEHICLE DAMAGE SEVERITY

Impact Type	Vehicle Damage Severity	Percent Reduction For Post-Std.	Reduction Statistically Significant?
Frontal	Lo-Mod.	16.0	Yes
	Major	37.0	Yes
Rearend	Lo-Mod.	36.0	Yes
	Major	51.4	Yes
Rollover	Lo-Mod.	12.8	No
	Major	47.3	Yes

Leakage rates for Post-Standard vehicles showed significant reductions for five of the six subgroups, with the magnitude of the reduction ranging from 16.0 percent (Frontal-Lo-Moderate) to 51.4 percent (Rearend-Major). Again, as with the earlier results on fire, the largest reductions are noted for Rearend and Rollover impacts (which is in general agreement with the intent of Standard 301-76 and 301-77 upgrades), and for the more severe crashes, as denoted by the extent vehicle damage (VDS). Figures 9, 10, and 11 graphically illustrate the results.



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2.5 Summary of Effectiveness Analyses

The preceding analyses indicate that significantly lower rates of both crash-induced fire and crash-induced fuel leakage have occurred coincident with passenger cars manufactured after the effective dates of 301-76/77, as compared with cars produced prior to the standard. The greatest reductions have occurred at the higher crash severities, where crash severity is defined as the extent of crash deformation sustained by the vehicle. The reductions in fire and fuel leakage rates have occurred at three of the major types of impacts addressed by the standard: rollovers, rearend impacts, and frontal impacts. Side impacts could not specifically be evaluated with the available data. Age was found to have a significant effect on fuel leakage, but not on crash fires. A possible explanation here is the degradation, with time, of metal fuel system components due to rust, corrosion, and the hardening, cracking of rubberbased/neoprene connecting hoses or lines, and clamps.

Both fire and fuel leakage increase markedly at the higher severity crashes, which coincides with engineering judgment.

The findings of a significant reduction in fire rate for Post-Standard vehicles, and the factors which affect five rates are in general agreement with two other contractual studies, [5], and [8], performed for NHTSA in support of its overall evaluation of Standard 301. The first study was done by the Highway Safety Research Institute, (HSRI), University of Michigan, and analyzed data from the States of Michigan, Illinois, and Pennsylvania. The second study, performed by the Highway Safety Research Center, University of North Carolina, analyzed data from North Carolina, and Maryland. The latter study covered only fires while the former study

covered both fires and fuel leakage. As stated earlier, fuel leakage data was available only from one State, Michigan. The findings of the latter study with respect to fuel leakage are also in general agreement with the findings given in this report.

All data sources analyzed herein showed significantly lower fire rates for vehicles produced after Standard 301 became effective. As is not unexpected, however, not all data sources showed the same degree of fire reduction. It is believed that most of these differences relate to the manner in which the fire event is recorded in the various accident report systems and that the data from the State of Michigan represents the best source from which to infer about the extent and nature of the crash fire problem, and hence the best source with which to evaluate the effects of Standard 301.

Data sources where fire is accorded a specific reporting element (as in the States of Michigan and Illinois) provide considerably higher estimates of crash fire rates than do sources where fire is not designated as an independent element, but can be investigated through secondary methods such as accident narratives or Vehicle damage contributing factors. This difference is to be expected since some crash fires will no doubt go unreported on accident forms where explicit provision is not made to record such events. It is considered likely that fires reported via nonspecific element methods will tend to represent the more serious or catastrophic fires. On the other hand, since fires are relatively rare

events compared to the "average" accident, it is reasonable to expect less than complete reporting even for systems which list fire as an explicit element. On balance, it is believed that systems which embody specific reporting elements for fire provide the more accurate picture of the crash fire problem and hence the better basis for evaluation of the effectiveness of Standard 301.

A few concluding comments are offered concerning the potential influence or confounding effect that various factors might have on the analyses of the effect of Standard 301 in reducing passenger car crash fires. Certainly there are several factors which could reasonably be expected to influence the occurrence of crash fires, other than the standard itself. Perhaps the most obvious factors would be: (1) the severity of the crash experienced by the vehicle in terms of crash speed, extent of vehicle damage, or other similar measure; (2) the direction of impact sustained by the vehicle; and (3) the age of the vehicle. These factors have been evaluated in this study. Perhaps the factor having the greatest influence on the occurrence of crash fires (and fuel leakage) is the crash severity, with fire rates markedly higher for the crashes of high vehicle damage levels. Fire rates also vary by the type of impact. Although slight differences in the distributions of crash severity and impact type were noted between Pre- and Post-Standard vehicles, these differences did not appreciably alter the estimated effect of Standard 301. Age was found to significantly affect fuel leakage, but did not exhibit a significant effect on fire rates. Other factors such as the

number of vehicles in the crash or the time of the accident (day versus night) were investigated by the HSRI study, but these were found to be correlated with and adequately explained by crash severity.

Other potential factors which might affect the likelihood of crash fires are the size of the vehicle and other vehicle modifications such as emission control devices (e.g., catalytic converters and fuel evaporation control systems--cannisters, lines). As for vehicle size, the Post-301 Standard vehicles comprise a population of increasingly smaller-sized vehicles as compared with the Pre-Standard vehicle population. Beginning in 1977, the first major wave of vehicle downsizing began with General Motors' completely new design of its standard-sized vehicle line; 1978 and subsequent years have seen a steadily increasing proportion of smaller vehicles being introduced into the Nation's fleet, with further downsizing by domestic manufacturers and with an increased penetration of import vehicles. To the extent that smaller vehicles are more vulnerable in a crash, including any increased tendency to experience a crash fire, it would appear that the analyses categories used in this study would serve to provide a more conservative estimate of Standard 301. A similar situation would hold with respect to emission control devices.

Evaporation control systems saw general application in the early 1970's so that both Pre-301 and Post-301 vehicle populations should be equipped with similar proportions of this equipment; catalytic converters saw general introduction with the 1975 Model Year so that a greater proportion of the Post-301 vehicle population should contain these devices. Again, this

would argue for a conservative estimate of the effect of 301, as given herein, to the extent that such emission control devices might increase the likelihood of a crash fire.

Another factor of general concern in most "before-after" analyses such as this (where experimental control or randomization of extraneous sources of variation is not possible) is that older vehicles may be subject to greater underreporting of accidents as compared with newer vehicles. Such a phenomenon could serve to artificially increase fire rates for older vehicles. It is believed that the restriction on the age of the vehicles permitted in the Pre-Standard population as used herein and the analysis on "equal age vehicles" where such is indicated, serve to minimize any confounding due to any "artifactual" effect of age.

Summarily, with available data, complete elimination of all potential confounding effects is not possible. Additionally, the rare event characteristic of crash fires and limited sample size preclude investigation of all possible factors of interest. However, the results obtained, which are based on the factors deemed most important, and which show general agreement, both between the data sources analyzed in this evaluation and with other separate analyses [5], and [8], are collectively believed sufficient to demonstrate that a statistically significant and substantial effect has resulted from the promulgation of FMVSS-301-76/77.

One final observation from the effectiveness analyses is noted. Although there are significant reductions in crash fire rates for the Post-Standard vehicles, there is some indication that rates may be

increasing slightly for the newer vehicles (see Figures 1, 3, 4). This is considered a preliminary finding and reasons for it are not clear at this juncture. It may be only a statistical aberration or it may portend an actual increase. Additional data over the next one to two years should be sufficient to determine the answer.

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CHAPTER 3

THE BENEFITS, COST, AND COST-EFFECTIVENESS OF STANDARD 301-76/77

3.0 Introduction

The benefits, cost, and cost-effectiveness of Standard 301-76/77 are developed and discussed in this chapter.

The benefits are defined in terms of the fatalities, injuries and vehicle crash fires avoided as a result of the standard. These benefits are derived by applying the effectiveness estimates from the preceding chapter to the estimated magnitude of the problem of fire-related fatalities, injuries, and crashes, and adjusting the results by estimates of the hazard attributable to a crash fire (i.e., the degree to which fatalities and injuries result from the physical hazards of fire itself apart from the hazards of impact forces). Accident data from Michigan, together with data from the Fatal Accident Reporting System and the National Accident Sampling System are used to derive the benefits.

The cost of Standard 301-76/77 is given in Section 3.2. The costs are based on detailed information solicited from the manufacturers as to the vehicle modifications made in order to comply with the standard requirements. Individual cost and modification weight estimates are developed and extrapolated to national totals on a sales-weighted basis. The cost estimates include both the final (i.e., consumer) cost of the manufacturing changes and the lifetime cost of the increased fuel penalty due to the added increment of vehicle weight.

Finally in Section 3.3, a brief discussion of the cost-effectiveness of the standard is presented.

3.1 Benefits

In order to estimate the magnitude of benefit due to Standard 301, it is necessary to translate the effectiveness estimates from the preceding chapter into estimates of the number of fatalities and injuries, and vehicle crash fires avoided. The additional factors needed for these benefit estimates are:

- (1) National estimates of the total number of "fire-related" fatalities and injuries occurring annually in passenger car crashes. Here, "fire-related" is interpreted to mean that a crash fire accompanied a fatal crash but the degree of contribution of the fire to occupant fatality or injury is not ascertainable, or unknown. However, the assumption is made that the fatalities are a result of both crash force injuries and burn injuries, in some combination.
- (2) A national estimate of the total number of passenger car crash fires occurring annually.
- (3) An estimate of the increased likelihood of a passenger car occupant fatality, or injury, due to the presence of fire resulting from a vehicle crash. This factor is herein referred to as the "fire-lethality" factor.

Only one of the above needed estimates, national fire-related fatalities, is available from existing sources. The remaining estimates, therefore, have been derived and are explained throughout the following analyses sections. The Fatal Accident Reporting System (FARS), operated by NHTSA

is the source for the national estimate of fire-related fatalities. FARS is an automated data system containing information on all (i.e., a census) fatal motor vehicle accidents occurring annually in the united states, and has been in continuous operation since 1975. FARS reporting forms (see Appendix A) have a specific data element for recording the presence of crash fires which accompany fatal accidents.

The effectiveness estimates derived in this report, for reasons given in Appendix A and Section 2.5 are based on the results of the analyses of the data from Michigan. Michigan data are also used to estimate the fire lethality factor, and are considered the best source for such estimates. Ideally, if autopsy information were available from a representative sample of fire-related passenger car occupant fatalities, it would be the preferable basis for estimating a firelethality factor. However, no known source of autopsies of firerelated crash deaths is available.

The benefits of Standard 301-75/76, in terms of fatality reduction, injury reduction, and crash fire reduction, are derived in the following sections.

3.1.1 Fatality Reduction

The estimated benefit of Standard 301-75/76 in terms of fatality reduction, is calculated from the following basic formula:

$$B_{fat} = (N - NL) E = N(1 - L)E$$
 (3)

where,

B_{fat} = estimated number of fatalities avoided,

- N = national estimate of the number of fire-related fatalities (i.e., fatalities in crashes accompanied by post-crash fires),
- L = fire-lethality factor = ratio of P [fatality/no fire] to
 P [fatility/fire] for crashes of similar levels of crash
 force severity,

and,

E = effectiveness estimate for standard at given crash force level.

The quantity NL, in the above equation, is seen to be an estimate of the number of fatalities that would be expected to occur if fires were completely eliminated as a post-crash phenomenon. The fatalities saved would thus be the difference between N and NL, or N(1 - L).

The product of this number and E, the effectiveness estimate, or the proportion of total crash fires estimated to be eliminated by the standard thus provides an estimate of the total fire-fatalities saved.

The fire-lethality factors are derived from the data contained in Tables 26 and 27 which show the distribution of vehicle occupant injury, in police-reported K (fatal), A-B-C levels' for vehicles in which fire occurred versus vehicles in which no fire occurred. The data represent total accident statistics for calendar years, 1978, 1979, and 1980 from the State of Michigan and the injury distribution is based on the "worst

TABLE 26 - DISTRIBUTION OF OCCUPANT INJURY FOR
FIRE VERSUS NO-FIRE (PASSENGER CAR) CRASHES.INJURY = WORST INJURY IN VEHICLE, VEHICLE DAMAGE
SEVERITY = 6,7,8 (MAJOR), MICHIGAN DATA FOR
1978, 1979, 1980 (TOTALS)

FATAL No. 148 2590 2738 Row% 5.41 94.59 100.00 Col% 11.31 1.61 1.69	INJURY	FIRE	NO FIRE	TOTALS
No. 148 2590 2738 Row% 5.41 94.59 100.00 Col% 11.31 1.61 1.69 A-INJURY	FATAL			
Row% 5.41 94.59 100.00 Co1% 11.31 1.61 1.69 A-INJURY No. 318 24068 24386 Row% 1.30 98.70 100.00 Co1% 24.29 14.97 15.05 B-INJURY No. 266 38057 38323 Row% .69 99.31 100.00 23.65 C-INJURY No. 153 32122 32275 Row% 0.47 99.53 100.00 100.00 Co1% 11.69 19.98 19.91 19.91 No No. 424 63929 64353 Row% 0.66 99.34 100.00 Co1% 1309 160766 162075 Row% 0.81 99.19 100.00 Co1% 100.00 100.00 0	No.	148	2590	2738
Col% 11.31 1.61 1.69 A-INJURY No. 318 24068 24386 Row% 1.30 98.70 100.00 Col% 24.29 14.97 15.05 B-INJURY No. 266 38057 38323 Row% .69 99.31 100.00 Col% 20.32 23.67 23 65 C-INJURY No. 153 32122 32275 Row% 0.47 99.53 100.00 Col% 0.47 99.53 100.00 Col% 0.66 99.34 19.91 No. 1309 160766 162075 Row% 0.81 99.19 100.00 Col% 0.81 99.19 100.00	Row%	5.41	94.59	100.00
A-INJURY No. 318 24068 24386 Row% 1.30 98.70 100.00 Co1% 24.29 14.97 15.05 B-INJURY	Co1%	11.31	1.61	1.69
No. 318 24068 24386 Row% 1.30 98.70 100.00 Co1% 24.29 14.97 15.05 B-INJURY No. 266 38057 38323 Row% .69 99.31 100.00 Co1% 20.32 23.67 23 65 C-INJURY No. 153 32122 32275 Row% 0.47 99.53 100.00 Co1% 11.69 19.98 19.91 NO INJURY 32.39 39.77 39.71 TOTAL No. 1309 160766 162075 Row% 0.81 99.19 100.00 100.00	A-TN.IURY		ى يەرىپىيە بىر بىلىلىكى ئەرىپىلىكى بىلىكى بىلىك بىلىكى بىلىكى	
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Coliz 24.29 14.97 15.05 B-INJURY No. 266 38057 38323 Row% .69 99.31 100.00 Coliz 20.32 23.67 23.65 C-INJURY No. 153 32122 32275 Row% 0.47 99.53 100.00 Coliz 11.69 19.98 19.91 No INJURY No. 424 63929 64353 Row% 0.66 99.34 100.00 00.00 Coliz 32.39 39.77 39.71 39.71 TOTAL No. 1309 160766 162075 Row% 0.81 99.19 100.00 00.00	Row%	1.30	98.70	100.00
B-INJURY No. 266 38057 38323 Row% .69 99.31 100.00 Co1% 20.32 23.67 23.65 C-INJURY No. 153 32122 32275 Row% 0.47 99.53 100.00 Co1% 11.69 19.98 19.91 NO <injury< td=""> No. 424 63929 64353 Row% 0.66 99.34 100.00 Co1% 32.39 39.77 39.71</injury<>	Co1%	24.29	14.97	15.05
No. 266 38057 38323 Row% .69 99.31 100.00 Co1% 20.32 23.67 23.65 C-INJURY No. 153 32122 32275 Row% 0.47 99.53 100.00 Co1% 11.69 19.98 19.91 NO INJURY No. 424 63929 64353 Row% 0.66 99.34 100.00 Co1% 32.39 39.77 39.71 TOTAL No. 1309 160766 162075 Row% 0.81 99.19 100.00 Co1% 100.00 100.00 100.00	R-TN HIPY	an a fan a fan skrief f		
NO. 100 100.00 Col% 20.32 23.67 23.65 C-INJURY 0.47 99.53 100.00 Col% 0.47 99.53 100.00 Col% 11.69 19.98 19.91 NO <injury< td=""> 0.66 99.34 100.00 NO INJURY 0.66 99.34 100.00 Col% 0.66 99.34 100.00 TOTAL 0.61 99.19 100.00 No. 1309 160766 162075 Row% 0.81 99.19 100.00 Col% 100.00 100.00</injury<>	No.	266	38057	38323
No. 153 32122 32275 No. 153 32122 32275 Row% 0.47 99.53 100.00 Co1% 11.69 19.98 19.91 NO INJURY	Row%	.69	99.31	100.00
C-INJURY 32122 32275 No. 153 32122 32275 Row% 0.47 99.53 100.00 Co1% 11.69 19.98 19.91 NO INJURY 64353 100.00 No. 424 63929 64353 Row% 0.66 99.34 100.00 Co1% 32.39 39.77 39.71 TOTAL No. 1309 160766 162075 Row% 0.81 99.19 100.00 Co1% 100.00 100.00 100.00	Co1%	20.32	23.67	23 65
No. 153 32122 32275 Row% 0.47 99.53 100.00 Co1% 11.69 19.98 19.91				
NO NO <th< td=""><td>No.</td><td>153</td><td>32122</td><td>32275</td></th<>	No.	153	32122	32275
Col% 11.69 19.98 19.91 NO INJURY	Row%	0.47	99.53	100.00
NO INJURY 63929 64353 Row% 0.66 99.34 100.00 Co1% 32.39 39.77 39.71 TOTAL 1309 160766 162075 Row% 0.81 99.19 100.00 Co1% 100.00 100.00 100.00	Co1%	11.69	19.98	19.91
No. 424 63929 64353 Row% 0.66 99.34 100.00 Co1% 32.39 39.77 39.71				
Row% 0.66 99.34 100.00 Co1% 32.39 39.77 39.71 TOTAL	No.	424	63929	64353
Col% 32.39 39.77 39.71 TOTAL	Row%	0.66	99.34	100.00
TOTAL No. 1309 160766 162075 Row% 0.81 99.19 100.00 Co1% 100.00 100.00 100.00	Col%	32.39	39.77	39.71
No. 1309 160766 162075 Row% 0.81 99.19 100.00 Co1% 100.00 100.00 100.00	TOTAL			
Row% 0.81 99.19 100.00 Co1% 100.00 100.00 100.00	No.	1309	160766	162075
Co1% 100.00 100.00 100.00 /	Row%	0.81	99.19	100.00
	Co1%	100.00	100.00	100.00 /

TABLE27 - DISTRIBUTION OF OCCUPANT INJURY FOR
FIRE VERSUS NO-FIRE PASSENGER CAR CRASHES.INJURY = WORST INJURY IN VEHICLE, VEHICLE
DAMAGE SEVERITY = 2,3,4,5 (LO-MODERATE).MICHIGAN DATA FOR 1978, 1979, 1980 (TOTALS)

INJURY	FIRE	NO FIRE	TOTALS	
FATAL No. Row% Col%	7 3.37 0.40	201 96.63 0.02	208 100.00 0.02	
A-INJURY No. Row% Col%	43 0.37 2.47	11593 99.63 0.97	11636 100.00 0.97	-
B-INJURY No. Row% Col%	131 0.26 7.54	51117 99.74 4.27	51248 100.00 4.27	
C-INJURY No. Row% Col%	205 0.16 11.80	125264 99.87 84.28	125469 100.00 10.47	
NO INJURY No. Row% Col%	1352 0.13 77.79	100825 99.87 84.28	1010177 100.00 84.27	
TOTAL No. Row7 Col7	1738 0.14 100.00	1197000 99.86 100.00	1198738 100.00 100.00	

injury in the vehicle." As would be expected, this injury distribution, particularly the proportion of fatal or serious injuries, varies markedly with the crash severity level, or Vehicle Damage Severity (VDS) discussed in the previous chapter as does the probability of crash fire, as was also noted previously. Therefore, two tables were produced which show the injury distribution, fire versus no fire, for Lo-Moderate (VDS = 2, 3, 4, 5) and for Major (VDS = 6, 7, 8) crash severity levels. Fatality reduction estimates are made for each severity level. In order to retain resonable cell sizes, the data were not further subdivided by impact type as was done in the effectiveness analysis. Therefore slightly revised effectiveness estimates from these derived in the previous section have been made to conform to the two VDS levels, Lo-Moderate, and Major used here. Table 28 contains the data for these estimates.

TABLE 28 - CRASH FIRE RATES, PRE-STANDARD VERSUS POST-STANDARD VEHICLES, LO-MODERATE AND MAJOR CRASH SEVERITIES. MICHIGAN DATA, 1978-1980

	CRASH SEVERITY						
	L (o-Moderat VDS=2,3,4	e ,5)	Ma (VDS	jor =6,7,8)		
STANDARD		TOTAL			TOTAL		
GROUP	FIRES	CRASHES	RATE	FIRES	CRASHES	RATE	
PRE-STANDARD	625	406,933	.001536	562	55,564	.010114	,
POST-STANDARD	569	480,796	.001835	<i>,</i> 346	59,558	.005810	

Reductions in crash fire rates for the Post-Standard group are 22.95% and 42.56% for the Lo-Moderate and Major crash severities, respectively. Both of these are statistically significant at $\alpha = .05$ level.

For major crash severity (VDS = 6, 7, 8), the estimated fatality reduction is given by

$$B_{fat} = N (L -1) f E$$
(4)

which is the same as (3) except for the addition of the factor, f, which represents the proportion of total fire-fatalities occurring at the given crash severity (i.e., VDS = 6, 7, 8) level and computed from the data in Table 26. The following values are used to estimate the fatality savings:

N = 1099 = four-year average (1978-1981) of passenger car occupant fatalities in crashes with post-crash fires (i.e., fire-fatalities) per FARS,

 $L = \frac{1.6110 \times 10^{-2}}{11.3063 \times 10^{-2}} = .1425 = ratio of proportion of fatal crashes$ for all non-fire crashes at VDS = 6,7,8and the proportion of fatal crashes forall fire crashes at VDS = 6,7,8 (computedfrom Table 26),

f = .95 = proportion of total fire fatalities occurring at VDS = 6,7,8
 (computed from Tables 26, 27)

E = .426 = effectiveness estimate for standard at VDS = 6,7,8 (computed from the data in Table 28).

Substituting these values into equation (4), we obtain:

 $B_{fat} = 1099 (1 - .1425) (.95) (.426)$

= 1099 (.8575) (.95) (.426)

= 381.38 2 381 fatalities

Next, the benefit at Lo-Moderate crash severity (VDS = 2,3,4,5) is computed. For this computation, the values for the factors are:

N = 1099, as before,

$$\frac{1.679 \times 10^{-4}}{4.028 \times 10^{-3}} = .0417 \text{ (computed from Table 27)}$$

f = .05 = 1 - f (VDS = 6,7,8) = 1 -.95

E = .2295 = effectiveness estimate for standard at VDS = 2,3,4,5 (computed from the data in Table 28)

Again substituting these values into (4), we have:

 $B_{fat} = 1099 (1 - .0417) (.05) (.2295)$

= 1099 (.9583) (.05) (.2295)

= 12.09 = 12 fatalities

Therefore, the total estimate of fatalities saved annually is:

381 + 12 = 393 **⁴** 400 fatalities

3.1.2 Injury Reduction

The estimated benefit for 301-76/77 in terms of injury reduction is calculated in the same manner as the fatality reduction benefit, except that a national estimate of the total number of fire-related injuries must be estimated since no National estimate for fire-related injuries is available as in the case of fatalities. Injury reduction is estimated in terms of standard K-A-B-C police-reported inuries since again this is the best known type of information available and is taken from the Michigan data.

Appendix B contains the definition of the K-A-B-C injury scale as used by the State of Michigan. General definitions are:

- K Fatal Injury: any injury that results in death within 12 months of the crash.
- A Incapacitating Injuries: any injury that prevents the person from performing his/her normal activities; hospitalization normally required.
- B Non-incapacitating Injury: any injury other than fatal or incapacitating.
- C Possible Injury any injury reported or claimed, other than fatal, incapacitating, or non-incapacitating.

3.1.2.1 A-Injury Reduction

First, a national estimate of the number of A-injuries that are fire-related is needed. Two methods are used to derive this figure, both based on ratio estimation methods. The first method uses the ratio of the number of fire-related A-injuries to all passenger cars in (police-reported) accidents in Michigan and the national total of police-reported passenger car accidents as estimated by the National Accident Sampling System (NASS) being operated by NHTSA's National Center for Statistics and Analysis.

The NASS estimate used here is taken from the "Report on Traffic Accidents and Injuries for 1979-1980," which is based on the NASS System (Reference 8). The following equivalency is used:

> No. Fire-Related "A" Injuries, Mich. _ X No. Passenger Cars No. Passenger Cars (5) in Police-Related in Police-Reported Accidents, Mich. Accidents, U.S.

where x is the national estimate of the number of A-injuries.

From Tables 26 and 27, the ratio on the left side is found to be 361/1,368,813 which is the total of fire-related A-injuries and the total passenger cars in accidents, over both VDS levels, Lo-Moderate and Major.

The denominator on the right side is set equal to 9.247×10^6 , the national estimate of passenger cars in accidents annually, from [8]. Substituting these values into (5), we have

$$x = 9.247 \times 10^{6} \frac{361}{1,368,813}$$
$$= 2439$$

as the national estimate of fire-related A-injuries. Actually, this number is somewhat conservative since it only considers one fire-related A-injury per passenger car crash (recall that Tables 26 and 27 are based on the "worst" injury in the vehicle). Therefore, the number is adjusted by the average number of fire-related A-injuries per crash from Michigan which is 1.543, for calendar years 1978-1980.

This gives:

x' = 2439 (1.543) = 3763 fire-related A-injuries

A second method, similar to the first, for estimating the national number of fire-related A-injuries is the ratio:

> No. Fire-Related <u>A-Injuries, Mich.</u> No. Fire-Related Fatalities, Mich.

x No. National Fire- (6) Related Fatalities, FARS

Again, from Tables 26 and 27, the left side is set equal to 361/155. From the previous section, the denominator on the right side is 1099, the average number of "fire-fatalities" from FARS for 1978-1981. Substituting into (6), we obtain:

 $x = 1099 \frac{361}{155}$

= 2650 fire-related A-injuries

Thus, the two estimation methods, one based on the national total of annual fire-fatalities, from FARS, and the other based on the national total of annual, police-reported passenger car accidents from NASS, give reasonably close estimates for the national number of fire-related A-injuries annually. For purposes of the analysis, the mean of these two numbers is taken as the best estimate, which is:

 $\frac{3763 + 2560}{2} = 3161 \cong 3160 \text{ fire-related A-injuries}$

Returning to Equation (4), the following values can be inserted to estimate the reduction in fire-related A-injuries due to Standard 301-76/77, for major crash severity:

N = 3160
L = .1497/.2429 = .616, from Table 26
f = 318/361 = .881, from Tables 26 and 27
E = .426, from Table 28

Therefore,

Next, for Lo-Moderate crash severity:

N = 3160 L = .0097/.0247 = .393, from Table 27 f - 1 -(318/361) = .119 E = .2295, from Table 28

Substituting,

B = 3160 (1 -.393) (.119) (.2295) A-inj.

= 52.4 = 52 fire-related A-injuries

Therefore, the total fire-related A-injuries saved annually by 301-76/77 is estimated to be

467 + 52 = 519 ≈ 520

3.1.2.2 B-Injury Reduction

As with the A-injuries, a national estimate of the total number of fire-related "B"-injuries must be derived in order to estimate the injury reduction at this level due to Standard 301-76/77. Methods of estimation similar to those above are used. Rewriting (5) for the case of B-injury gives:

> No. Fire-Related "B"-Injuries, Mich. No. Passenger Cars in Police-reported Accidents, Mich.

x No. Passenger Cars in Police-reported Accidents, U.S.

From Tables 26 and 27, the numerator on the left side is found to be 397.

The denominators have the same values as before, 1,368,813 and 9.247 x 10^6 , respectively. Solving for x gives:

 $x = 9.247 \times 10^6 \frac{397}{1,368,813}$

= 2682 fire-related B-injuries

Adjusting for average number of fire-related B-injuries per crash injuries as before gives:

x' = 2682 (1.392) = 3733 fire-related B-injuries

Next the estimate based on FARS fire-related fatalities is computed. Rewriting (6) for the case of B-injury:

No. Fire-Related	
B-Injuries, Mich.	x
No. Fire-Related	No. National Fire-
Fatalities, Mich.	Related Fatalities,
	FARS

Using the values determined previously gives:

$$x = \frac{397}{155}$$
 (1099)

Taking the mean of these two estimates, as before, for the National total of fire-related B-injuries:

$$\frac{3733 + 2814}{2} = 3274$$
 fire-related B-injuries

Equation (4) can now be used with the following values to estimate the reduction in fire-related B-injuries, for major crash severity:

N = 3274

L = .2367/.2032 = 1.16, from Table 26

f = 266/397 = .67, from Tables 26 and 27

E = .426, from Table 28

Since the fire-lethality factor, L, is >1, it is not necessary to proceed with the computation for B-injury reduction at this crash severity - there will be none. (Actually, there will be an increase). The explanation here is that the increased injury severity for fire occurrence versus no fire is concentrated entirely in the fatal and "A" or serious injury categories. The excess of injuries at these upper levels occurs at a tradeoff of lower proportions of injuries at the "B" and lesser injury levels, as opposed to non-fire crashes. Therefore, the next step is to compute the B-injury savings of the Lo-Moderate crash severity level.

The following values are used:

N = 3274, as computed above
L = .0427/.0754 = .566, from Table 26
f = 1 -(266/397) = .33
E = .2295, from Table 27

Substituting into (4),

 $B_{B-inj} = 2954 (1 - .566) (.33) (.2295)$

= 108.4 **~** 110

Therefore, the total fire-related B-injuries saved annually by 301-76/77 is estimated to be 110.

The analyses of injury reduction concludes at this juncture. Although the data in Table 27 indicate a slightly lower chance of

C-injury for no-fire versus fire crashes (Lo-Moderate severity), this difference is very small and the severity of police-reported C-injuries is minor.

3.1.3 Crash Fire Reduction

In order to estimate the number of passenger car crash fires saved annually, the national total of such fires must be estimated. Two methods are again used to derive this estimate. The first method applies the overall Michigan crash fire rate of .002090, from Table 1 to the total annual number of police-reported passenger car crashes from NASS, 9.247×10^6 . This yields:

 $9.247 \times 10^{6} (2.09 \times 10^{-3}) = 19,326$ crash fires

The second method is based on the Michigan data and the total number of fire-related fatalities from FARS. The following equality is defined:

Average Annual		Average Annual
Fire-Related		Fire-Related
Fatalities from		Passenger Car
<u>Michigan (1978-1980)</u>	-	Crashes from Michigan (1978-1980)
Average Annual Fire-Related Fatalities		x

From Tables 26, 27 and from the previous work, this equation takes on the

$$\frac{52.7}{1099} = \frac{1055.3}{x} , \text{ or}$$
$$x = \frac{1055.3}{52.7} (1099)$$
$$= 22.007$$

Once again, the two methods of estimation give reasonably close results. Taking the mean of the two as the best estimate gives:

$$\frac{19,326+22,007}{2} = 20,667$$
 fire-related crashes annually

Using a modified version of equation (4), the number of crash fire reductions for each crash severity level (Lo-Moderate and Major), and the total can be estimated. The equation is:

 $B_{crash fires} = N f E$, where N, f, and E are defined as before (7)

For Lo-Moderate crash severity, N = 20,667; f = 1738/(1738 + 1309) = .57 (from Tables 26 and 27); E = .2295, from Table 28. Substituting these values gives:

B_{crash fires} = 20,667 (.57) (.2295)

= 2,703 fire-related crashes, annually

For Major crash severity, the same procedure yields:

B_{crash fires} = N (1 -f) E

- = 20,667 (.43) (.426)
- = 3,786 fire-related crashes, annually

The total number of passenger car crash fires estimated to be reduced annually due to the standard is thus

 $2,703 + 3,786 = 6,489 \cong 6,500$

To the extent that fire damage increases the property damage loss in passenger car crashes, above that which is a result of crash incurred damage, the above figure represents an indication of the magnitude of such loss that would be reduced by Standard 301-76/77. Property damage dollar estimates of these phenomena are not available.

3.1.4 Summary of Benefits

The following table summarizes the total benefits estimated for Standard 301-75/76:

Table 29 - Summary of Benefits, Standard 301-75/76

Benefit Category	Estimated	
	<u>Annual</u>	Benefit
Fatalities avoided		400
Serious ("A") injuries avoided		520
Noderate ("B") injuries avoided		110
Post-Crash Fires avoided*	6	,500

[&]quot;Property damage reduction savings to the extent that crash fire increases the loss, over and above that sustained as a result of crash/impact forces. Such losses would typically be to the accidentinvolved vehicles.
These benefit estimates are those which would be expected to accrue annually when the entire passenger car fleet is brought into compliance with Standard 301, an estimated five-to-seven years hence or approximately 1987-1989. Also, it should be noted that the estimate of 6,500 post-crash fires avoided is not mutually exclusive of the estimated number of fatalities and injuries avoided, but is inclusive of these latter two numbers.

Note in Table 29 that "A"-injuries have been redefined by the term "serious" injuries and "B"-injuries have been redefined using the term "moderate" injuries. This places the injury categories on a more generic and readily understood scale. As previously noted in this report, fatal injuries are defined by the State of Michigan (see Appendix B) to be any injury that results in death within 12 months of the crash. A-injuries are termed incapacitating in nature and typically require hospitalization. B-injuries are defined as non-incapacitating. To these general definitions should be added the fact that the fatality and injury savings given in Table 29 would be those that would otherwise occur due to burn or asphyxiation.

As the estimates clearly show, the primary impact of Standard 301 is at the severe end of the accident consequence spectrum, or the reduction of fatalities and serious injuries. Although the actual numbers are not large relative to the overall toll of motor vehicle accident fatalities and injuries, they nonetheless constitute a sizable proportion relative to the magnitude of the problem of fire-related fatalities, injuries and fires that occur as a result of passenger car crashes.

One of the key factors in the estimation of the benefits of Standard 301 is the extent to which the likelihood of occupant fatality or serious injury is increased by the occurrence of crash fire, or the fire-lethality factor. For crashes of major accident severity, which account for an estimated 95 percent of the total fire-related fatalities, the fire-lethality factor estimated in this study indicates that fire is the cause of some 85 percent of the total fire-related fatalities. A second estimate of this fire-lethality factor is given by Cooley [10] in a study done in 1974. This study analyzed a relatively small sample of fire-related fatal accidents and assigned cause of death using information from auxiliary sources such as certificate of death, police officer's confidential reports,

witness statements, and pathologists' reports in addition to microfilm files of hard-copy police accident reports. The study estimated that 70 percent of the fire-related deaths were due to fire where death was judged to be either the result of fire or ensured by fire. The study noted that "deaths associated with crash fires are actually distributed along a causal continuum on which deaths solely due to burns or asphyxiation are located at one pole and deaths due solely to impact trauma are located at the opposite pole." The Cooley study also quoted an earlier study by the National Safety Council which estimated that a total of 17,000 fires resulted annually from motor vehicle crashes; presumably, this figure included all motor vehicles, not just passenger cars as covered in this study.

Yet two additional estimates of the fire-lethality factor can be derived from NHTSA's Fatal Accident Reporting System (FARS). The first

estimate is based on the occupant fatality rate for passenger car fatal crashes in which fire occurs versus the occupant fatality rate for passenger car fatal crashes in which no fire occurs. FARS data show that the occupant fatality rate is 67 percent higher for fatal crashes in which fire occurs compared to fatal crashes in which no fire occurs.

The second estimate from FARS concerns the "most harmful event" in the fatal accident. For passenger car fatal crashes in which fire occurred, 38 percent listed fire as the most harmful event. The interpretation of the most harmful event is that event which is judged the one which contributed most to the occurrence of fatality, injury, or the accident, in that order of precedence, and is assigned by the FARS analysts in the various States based on the information available to them which includes coroner's reports, and death certificates as well as police accident forms.

Collectively, these various estimates of the lethality effect of crash fires indicate that the occurrence of fire has a major impact on increasing the liklihood of fatality or serious injury. The estimate of lethality derived in this report is somewhat higher than the other estimates given, but this is to be expected since the basis for this estimate is a lower severity threshold (i.e., accidents of major and severity as defined by VDS levels of 6, 7, 8) while the basis for the other estimates is fatal accidents, a more severe threshold. The higher the severity of the accident, in terms of the impact or crash forces, the greater the likelihood that these forces will contribute to injury, or fatality, relative to the likelihood of fire contributing to the injury or fatality, should fire occur.

3.2 Costs

The nature of the requirements of FMVSS-301 have made it difficult to arrive at a consumer cost estimate of the standard. NHTSA's normal procedure of estimating the cost of vehicle changes necessary to comply with its Federal Standards has been to disassemble affected vehicle structures and estimate the consumer costs of the affected components. This methodology, generally referred to as "vehicle tear-down studies", uses weight differentials of affected component parts, for vehicles produced prior to and after a standard is promulgated, as the primary basis for estimation of the costs incurred. Individual cost estimates are then projected to overall fleet costs based on sales-weighted data for the various vehicle lines represented by the tear-down cost studies. While some weight changes (generally increases) have occurred as a result of 301, many of the changes made to meet the standard requirements required no or negligible weight changes. In certain few instances, no changes of any nature were made since the manufacturer determined that the then existing vehicle design was such that the 301 requirements were (already) met.

An additional factor which complicates cost estimation of 301 is that the type of changes made to comply with the standard not only varied widely among the different vehicle manufacturers (both domestic and foreign), but also these changes varied widely among vehicle lines, different make-models, and even by body style (2-door, 4-door, station wagon, hatchback, etc.).

The unique situation of 301, described above, contrasts with other standards, such as 214 (Side Door Strength), and Part 581 (Bumpers), and

makes difficult not only the actual estimation of costs of various changes, but also the selection of a representative sample of véhicles on which to estimate costs. For these reasons, the primary basis for estimating costs of FMVSS-301 has been to solicit from various manufacturers the nature and cost of the changes they made to their vehicles to meet the requirements of 301. The actual information received from the manufacturers was accompanied by a request of confidentiality on the basis of being deemed proprietary in nature. Therefore the information contained in this report is of a general, or generic nature, and specific data relating to specific manufacturers have been omitted.

Only the changes made to meet the 301-77 version of the standard are covered in this report. Available information does not provide an estimate of the cost of 301-76, the rollover requirement. However, due to the basic differences between the requirements for 301-76 and 301-77, it is considered likely that the cost of 301-76 is considerably less than the cost herein estimated for 301-77, and resulted in no significant increase in vehicle weight.

3.2.1 Nature of Vehicle Modifications Made

In general, the vehicle modifications instituted to comply with 301-77 consisted of those things necessary to provide a "friendlier" and more secure environment for the fuel system components when the vehicle was subjected to a 30 MPH rear, perpendicular, barrier impact, a 20 MPH side (lateral) barrier impact, or a 30 MPH offset (\pm 30° from vehicle longitudinal axis) frontal, barrier impact. The primary fuel system components are listed in Table 30.

TABLE 30 - FUEL SYSTEM COMPONENTS

1. Fuel Tank

Tank Filler Neck

Tank Filler Cap (Gas Cap)

Tank Mounting Straps

Tank Mounting Bolts, Anchors

2. Fuel Gauge Sensor/Sending Units

3. Fuel Lines

Connecting Hoses, Clamps

4. Fuel Vapor Lines

Connecting Hoses, Clamps

5. Fuel Pump

Pump Mounting Bolts

6. Evaporation Control Cannister

7. Carburetor

8. Fuel Filter

Based on the information provided by the manufacturers, changes made to meet 301 requirements related to the first five fuel system components listed. Table 31 summarizes the various types of changes made to improve the integrity of these components. As can be seen, these changes ranged from very minor items such as revising mounting bolts or clips, or reversing the mounting procedure for these items to more major changes such as recontouring the fuel tank or adding reinforcements to the rear floor pan structure to provide a more crashworthy environment for the fuel tank. The vast majority of the modifications made involved components 1 through 4 of Table 30 . As stated previously, the actual modifications made to individual vehicle models and body types varied widely.

3.2.2 Cost of Vehicle Modifications

Based on the information submitted to NHTSA by the manufacturers, as noted in the above Sections, overall industry, or fleet estimates, have been derived for the cost and weight increase of the vehicle modifications made in response to FMVSS 301-77. These estimates are the average (i.e., sales or production-weighted) incremental increases, per vehicle, for model year 1977 vehicles versus 1976 vehicles. These estimates are:

Average cost increase: \$4.60 per vehicle Average weight increase: 3.07 lb. per vehicle

In order to estimate the total cost increase to the consumer, an estimate

TABLE 31 - SUMMARY OF VEHICLE MODIFICATIONS IN RESPONSE TO 301-77

Vehicle Components

Fuel System Components

Fuel Tank

Modification(s) to Improve Crashworthiness

- Increase gauge of tank material
- Add protective shield
- Recontour to minimize contact/puncture by other adjacent vehicle components.
- Strengthen/shield filler neck
- Increase strength of solder/weld seams
- Strengthen mounting by adding brackets, revising mounting bolts, increasing torque of mounting straps
- Strengthen filler cap seal, improve impact resistance

Fuel Gauge Sensor

Fuel Lines

Fuel Vapor Lines

Fuel Pump

Other Vehicle Components Changed to Improve Fuel System Integrity

Rear Floor Pan/Support Rails/Wheel Housing

Rear Suspension (Springs, Shock Absorbers)

Rear Axle Assembly

Tailgate (S.W.)

Seat Belt Brackets

Engine Mount

Power Steering Pump Bracket

- Strengthen mounting

- Recontour

- Recontour, revise, revise clamps

- Provide shield
- Revise, add supports
- Change support brackets, Revise mounting bolts, Revise mounting procedure, and shield
- Minor changes in contour of lines, screw heads, mounting clips, recontour vent cover
- Revise hinge assembly
- Revise anchorage
- Slight revision
- Slight revision

of the increased fuel necessary to transport the additional vehicle weight is also made. Prior study [11] has estimated that an additional 1.0 gallons of fuel will be needed, over the life of the vehicle to compensate for each additional pound of vehicle weight. The average price for fuel in 1982 [12] is estimated at \$1.28 per gallon. Therefore the fuel cost estimate is:

3.07 lb. (1.0 gal./lb.) (\$1.28/gal.) = \$3.93 per vehicle

The total cost estimate is hence:

\$4.60 + 3.93 = \$8.53 per vehicle 🕊 \$8.50 per vehicle These cost estimates are in terms of 1982 dollars.

3.2.3 Discussion of Cost Estimates

Ideally, the cost estimate should cover both the 301-76 (rollover) and 301-77 (rear, side, offset frontal) upgrades of the standard, since benefits are estimated for both versions. However, as stated previously, no data were available to estimate the cost of 301-76; hence the total per vehicle cost of \$8.50 from the preceding section must be considered conservative. Also as discussed previously, it is believed that the (manufacturing) cost for the 301-76 version would be considerably lower than the manufacturing cost of the 301-77 version, due to the differing nature of the requirements for the two versions. Also, it is believed that no significant increase in vehicle weight resulted from 301-76. This implies that the cost of 301-77 would have to be increased by some

(small) fraction of \$4.60 (the 301-77 consumer cost of vehicle modification) in order to arrive at a total cost figure for both 301-76 and 301-77.

On the other hand, the cost estimate for 301-77 may be somewhat high in that the assumptions are made that: (1) the average new car sells for the full amount of the sticker, or manufacturer's suggested retail price, (2) it costs as much to incorporate 301-related component changes to a vehicle when that vehicle represents a totally newly designed vehicle as it costs when 301-related component changes are made to an existing vehicle design (i.e., retrofit changes). While no known national data are available on which to estimate the magnitude of the "average dealer discount" given to purchasers of new vehicles, it is generally accepted that some discount from the full sticker amount is typically given. Similarly, no known information is available on which to estimate the general effect of vehicle modifications made to existing vehicle designs as opposed to incorporating such changes when a vehicle is undergoing an entirely new design, but it is generally held that less effort is required to incorporate changes in the latter case.

Finally, the estimated fuel penalty cost resulting from Standard 301 may be somewhat high. The value of the extra fuel that is estimated to be consumed over the life of the vehicle is projected over that life in terms of the estimated 1982 cost of gasoline. If the present value approach for the future fuel consumed is used, as in other recent NHTSA studies [11], indications are that the additional consumer cost due to 301 would be somewhat lower than the value of \$3.93 per vehicle estimated above.

Certain other assumptions were necessary in arriving at a cost and weight estimate for 301-77, since all manufacturers did not furnish similar types of data and furthermore acknowledged the difficulty of being able to obtain the required data from existing company records.

One final comment is made concerning the point at which the 301-related changes were actually made to the vehicles. Experience has shown that manufacturers may elect to incorporate standard-related modifications in advance of the actual effective date set by a given standard, if the manufacturer finds that it is more efficient (less costly) to do so. Such instances typically occur when other modifications or design changes are being made by the manufacturer, in addition to those required by the standard. Incorporation of such standard-related modifications in advance of their required date is generally referred to as "anticipating the standard." Based on information available to NHTSA, it is concluded that changes for both 301-76 and 301-77 were made at points coincident with the effective dates of the requirements (i.e., 1976 and 1977 Model Years, respectively).

3.3 Cost Effectiveness of Standard 301

In the preceding sections, it was estimated that the average consumer cost resulting from 301 was \$8.50 per vehicle. If it is assumed that the average annual production of passenger cars sold in the U.S. is 10 million, then the total estimated cost to the vehicle buying public is:

8.50/vehicle x 10^6 vehicles = 85 million

The corresponding benefits of 301, as estimated in Section 3.1.4 are:

No. fatalities avoided = 400 No. serious injuries avoided = 520 No. moderate injuries avoided = 110 No. post-crash fires avoided = 6,500

From these two sets of estimates, the following comparison may be developed:

"For each \$10 million expended, Standard 301-76/77 is estimated to prevent:

47 fatalities,
61 serious injuries,
13 moderate injuries,
762 total crash fires"

The fatalities prevented are those that would otherwise occur due to fire (i.e., from burn injuries or from asphyxiation). It is possible that non-fatal (i.e., serious, moderate) injuries caused by, or contributed to by fire would be more severe than non-related injuries, due to the nature

of the injury and the medical treatment required for burn injuries. However, no empirical data are available on such costs nor are data available on the property damage costs of crash fires.

Given the rare-event nature of motor vehicle crash fires, the effectiveness estimates indicate that Standard 301-76/77 has had a substantial impact relative to the magnitude of the problem of crash fires. With respect to the cost-effectiveness of the standard, no specific conclusion is drawn, but it would seem that the costs of the standard do not represent an undue investment when weighed against the estimated benefits. The vehicle modifications made to comply with Standard 301-76/77, have been comprised of a number of small and varied changes which collectively are intended to provide a "friendlier," and "more forgiving" environment for fuel system components when subjected to a vehicle crash environment. Indications are that these vehicle modifications have substantially achieved their intended purpose.

CHAPTER 4

FINDINGS AND CONCLUSIONS

Based on the results of this study, the following findings and conclusions are made:

- Passenger car crash fires are relatively rare events compared with the total number of passenger car accidents occurring annually. Crash fires are estimated to occur at the rate of approximately two fires per 1,000 police reported passenger car crashes.
- 2. In terms of the magnitude of the national problem of passenger car crash fires, it is estimated that 20,600 vehicle crash fires occur each year. These crash fires are associated with 1,100 fatalities, 3,200 serious injuries and more than 3,300 moderate to minor injuries, all of which occur to occupants of the crash-fire involved vehicles.
- 3. Crash fire and fuel leakage rates vary by impact severity and impact type, with rates being markedly higher for crashes of higher impact severity as measured by the extent of vehicle deformation caused by impact forces.
- 4. Compared with non-fire crashes of similar crash force levels, passenger car crashes involving fire show a marked increase in the probability of occupant fatality and serious injury.

The primary factor contributing to this increase in lethality is concluded to be the presence of fire.

- Standard 301-76/77 has significantly reduced the post-crash fire rate and fuel leakage rate for passenger cars.
 - a. The greatest reductions have occurred in the more severe accidents as defined by the extent of crash-force damage sustained by the vehicle. These crashes are those most likely to result in serious injury or death. The standard is estimated to have reduced the fire rate by 43 percent in crashes of major crash force levels, and by 23 percent in crashes of low-to-moderate crash force levels.
 - Reductions have occurred for most of the major types of impacts (rollover, rearend, frontal) addressed by the standard.
- 6. When all vehicles in the U.S. fleer comply with Standard 301-76/77, the benefits of the reduction in crash fire rates are estimated to consist of annual reductions of:
 - a. 400 fatalities
 - b. 520 police-reported serious injuries
 - c. 110 police-reported moderate injuries
 - d. 6,500 vehicle crash fires

- 7. The consumer cost of the standard is estimated at \$8.50 per vehicle, or a total cost of \$85 million annually.
- 8. In a type of cost-effectiveness comparison, it may be stated that for each \$10 million spent to comply with Standard 301, the following total benefits are expected to accrue:

a. 47 fatalities avoided, plus

b. 61 serious injuries avoided, plus

c. 13 moderate injuries avoided, plus

d. 762 vehicle crash fires avoided

The 762 crash fires avoided would represent a savings in property damage costs to the extent that damage from fire exceeded the damage resulting from impact forces.

- 9. The type of vehicle modifications made in response to Standard 301-76/77 varied widely among vehicle manufacturers and, for the most part were individual vehicle model/body style specific. The basic objective of these modifications was to provide a "friendlier" and more "forgiving" environment for the various fuel system components (i.e., fuel tank, fuel lines, fuel pump, etc.) when subjected to vehicle crash forces.
- 10. In view of the fact that crash fires are quite rare events relative to the frequency of total crashes, the various vehicle modifications made in response to the standard appear to have substantially achieved their goal of reducing the problem of crash fires and the attendant fatalities and injuries resulting therefrom.

11. Although signifcantly lower crash fire rates have been found for Post-Standard vehicles, there is some indication that the fire rate may be increasing slightly for newer vehicles. This is a preliminary finding and reasons for it are not clear. It does suggest, however, that the Agency continue to monitor the phenomenon of motor vehicle crash fires.

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APPENDIX A

DATA SOURCES

1.0 Crash Fire Data

Data on motor vehicle crash fires were obtained from five States as described below.

1.1 Michigan Data

Beginning in 1978, the State of Michigan revised its motor-vehicle accident report form to contain specific elements relating to the occurrence of vehicle fires and fuel leakage. The following two questions were added to the report form:

"Did fire occur?" Yes____ No____ "Did vehicle leak fuel?" Yes No

Four code values are used when these data are automated at the State level. A value of "1" indicates a "yes" code for fire, and a "no" code for fuel leakage. A value of "2" indicates that the fire variable was coded "no" and the fuel leakage variable was coded "yes." A value of "3" is used if both fire and fuel leakage are checked "yes" by the investigating officer. Finally, a value of "4" is used for all remaining cases, which includes a "no" check for both events and also cases where either variable, fire or leak, or both, are left blank. In automating the data at the State level, it is assumed that missing data correspond to a "no" check for either variable. Therefore computation of fire and leak rates in the Michigan data treats missing information as no fires or no leaks and the actual rate of missing data cannot be determined.

The calculation and analyses of fire and fuel leak rates from the State of Michigan excluded crashes which were coded as "non-collision"

or "zero damage" in order to exclude fires that may not have resulted from vehicle crashes. Finally, discussions with reporting officers resulted in the following conventions for computing fire and leakage rates: (1) fire cases are those where fire was coded yes and where both fire and leak were coded yes; (2) leak cases are those where either fire, leak, or both fire and leak, are coded yes. The rationale for this convention is that the investigating officers indicated that when a fire occurred, it was often not possible to determine whether it was fuel-fed, due to the fire damage. In general, however, it was felt that such fires were fuel-fed.

1.2 <u>Illinois Data</u>

Since 1975, the State of Illinois' accident report form (see Appendix B) has contained an explicit variable to denote the occurrence of fire. The variable reads: "Did fire occur?", and the question is to be answered yes or no for each accident-involved vehicle. The State of Illinois requires two accident reports to be completed following an accident, one by the investigating officer and a second by the driver(s) involved. Both forms contain the fire variable, and in automating the accident data at the State level, both are used in the coding of the fire variable. If either the officer or the driver's reports indicate "yes" for fire, the fire variable is coded yes. If either or both reports indicate "no" for fire, the fire variable is coded no. In cases

where neither of the two reports completed the fire variable question (i.e., no answer, either yes or no, is given), the fire variable is coded as unknown.

One problem with the Illinois data is the relatively large proportion of missing data on the fire-variable. Over the six calendar years of data (1975 through 1980) made available for this study, the missing data rate for the fire variable ranged from a high of 39 percent in 1975 to a low of 18 percent in 1980.

The following summarizes the missing data rate:

Cal. Year	<u>Missing Data Rate</u>
1975	39%
1976	33%
1977	22%
1978	20%
1979	19%
1980	18%

Because of the differences in the missing data rates and the potential for these differences to confound the analyses of fire rates, the data analyzed in this report is restricted to the four most current years 1977-1980, among which the missing rates are reasonably close.

Once again, fire cases where accident type is coded "non-collision" are excluded in order to eliminate potential non-crash fires.

1.3 North Carolina, Maryland, and Pennsylvania Data

Fire data from the States of North Carolina, Maryland, and Pennsylvania are obtained via secondary, or indirect methods rather than from explicit accident report variables, as in the cases of Michigan and Illinois, preceding.

North Carolina data on fires come from computerized files of accident report narratives. Retrieval of items of interest from these automated narratives is based on a "key word" search routine developed and maintained by the Highway Safety Research Center. Accident case narratives involving fire were selected from the file, filtered to remove non-crash fire cases, and then matched with the respective full accident report in order to obtain other needed information such as vehicle model year. Denominator data for the calculation of accident rates consisted of all police-reported crashes in North Carolina occurring in the period comparable to that from which the fire cases were extracted.

Fire data from Maryland were obtained via a filtering algorithm which is intended to select those crashes in which post-crash fires occur. The screening algorithm was specifically oriented toward screening out cases where the accident type was given as "non-collision," the listed primary or secondary cause of the crash was fire, and selecting cases where" fire damage" was indicated to have occurred.

Fire data from Pennsylvania is also based on an indirect selection method since fire is not reported as a specific element on

the accident form. Fire is one of several codes that can be assigned at the automation of data at the State level. Fire is one of three sequential events which may be assigned by the analyst responsible for coding the accident reports. The sequential nature of the events is intended to represent the order in which the accident events happened. Therefore, if fire is coded first, it is assumed to be a non-crash fire. The cases selected as crash fires were those in which fire was not listed as the first sequential event, but where fire was listed together with reported crash damage.

1.4 Other Accident Data Sources

Two other accident data sources, in addition to those described above, were used in this study.

The first is the Fatal Accident Reporting System (FARS) maintained by NHTSA's National Center for Statistics and Analysis. FARS is an automated data system of all the fatal motor vehicle accidents occurring annually in the United States and has been in continuous operation since 1975. FARS is used to assist in defining the magnitude of the crash fire problem and in estimating the increased probability of fatality or injury due to the presence of a crash fire.

The second source is the National Accident Sampling System (NASS) also operated by NHTSA's National Center for Statistics and Analysis. NASS is a probability-based sample of all police-reported accidents occurring in the United States and is intended to provide a number of

general and specific characteristics relating to the nature and magnitude of the Nation's motor vehicle accident problem. NASS has also been used to assist in defining the magnitude of the national problem of crash fires.

1.5 Cost Data

Data on the costs of implementing Standard 301 are based on confidential information solicited by NHTSA from various motor vehicle manufacturers, both domestic and foreign. Typically, NHTSA conducts its own cost studies based on vehicle tear-down and consumer cost estimating methodologies. Due to the singular nature of the vehicle modifications made in response to Standard 301, however, this methodology was deemed inappropriate.

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APPENDIX B

State of Michigan - Accident Report Form
State of Illinois - Accident Report Form
State of North Carolina - Accident Report Form
State of Maryland - Accident Report Form
State of Pennsylvania - Accident Report Form
State of Michigan - Vehicle Damage Severity Scale for
Michigan Traffic Accident Investigators
State of Michigan - Definition of Police-Reported
K-A-B-C Injury Scale
Fatal Accident Reporting System - Accident Report Forms

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STATE OF MICHIGAN - ACCIDENT REPORT FORM

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STATE OF ILLINOIS - ACCIDENT REPORT FORM

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	ACCIDENT REPORT			LD.D.T. USE ONLY	
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When any person sustains property damage in excess of \$250, or personal in-juries, the names of uninsured motoriats are sent to the Secretary of State with a lagal notice of posable security deposit. The notice names all potential property damage and bodily injury claimants, and will be closed; otherwise, a Hearing will be held. If the Hearing officer concludes, after considering all written and oral evidence, that there is a reasonable possibility of legal fault, the uninsured driver will have the following options: 1. (Security deposits, releases, or install-ment agreements are to be submitted to the Secretary of State) roniability. If the uninsured motorist fails to comply with any of the above options, higher driver's license (if driver) and vehicie registration privileges (if owner) would None of the above affects any person's (See Sections 7-100 through 7-216 of the Iilincis Vehicle Code for complete statute). be required to prove financial responsibili-ty, usually by presenting evidence of complete and accurate descriptions of property damage and bodily injuries be shown in the spaces provided on the named on the security deposit notice. 3 (or signed agreements to pay for demages in in staliments) from all potential claiments Show evidence of a final adjudication of in certain cases drivers and owners may Deposit security. 2. Present evidence o releases from liability (or signed lists the evaluated amounts of those potential claims. The evaluations at The accident file, which usually contains the uninsured driver was legally at fault. xased on information shown in the repor iled by drivers or owners. It is importate that reports be filled promptly and th office will review the reports to ascertain will be sent to the Secretary of State. The police report and a report from each driv (he Sefety Responsibility Law For general information only right to sue to recover damages) automobile liability insurance. be suspended. report form. M. P.W. Wers You Femilies With Boad on Which Auddent Osturned? 1 - Yos 2 - No 1/10 z NORVING IN OF obomette ikading RENCARK AND **BID FIRE OCCURE** POSTED 1-Yos 3-Ne SPEED LINUT II WHAT PEDESTRIAN WAS DOING - Creating at Interaction With Signal Creating at Interaction Applied Sig. Creating at Interaction No Signal Coming From Bohind Perhod Yohid Weiking in Roedway - With Treffic Crossing Not at Internetion B. Cotting off or an School But 9. Costing off or an Other Vol 3 18 - Maying in Roadway 11 - Hihding an Vohido 12 - Working in Roads 12 - Kei in Roadway w CURCLE NUMBER OF ITEM OR ITEMS IN EACH BOX PERTAINING TO A CUDENT - Welking in Read 1 - Step Sign 2 - Step and Ge Light 3 - Officer of Playmas 4 - Enimod Creating Lights 5 - Enimod Franking Lights 1-Was Tradik Sign Vinkind 1-Yes 2-Ho 15 TRAFFIC CONTROL z 2-Combol Poncioning? 1-Yes 2-No 14 - Other Direction of Trovel Your Vahicle 1 Other Vehicle 2 1903486888888888 · Geing Straight Almond 18 VISION OBSCURED 10 YOUR ACTION AT Mehing Right Torn Making Left Turs Chimping Lance Mailing U Tota - Starting in Tre 3 - Rain, Saow, Ise on 9 - Treon, Craps, Butto alot 17 Roading Marine 17 South Slotting or St 1 the Kabida ing Vehicial - Net Obscored - Shuffee Korrie Strend and Robines In Radie on Northin 1 - Sign Barris - Stence 12 - Offer **Milings** 17 TOTAL ROADWAY DESCRIBE WHAR HAPPENED (Refer to vehicles by number): Aveiding Fraction Acid Skiciling Botore Brukleg Skiciling After Brukleg 5 - Store 1 - Risering Ded Amiding Other Vations 14 WEATHER 6 - Briverious Mering Vehi - Feer Same ch Becken i - One Wer - Arolding Fadodrine F MAMEUVER Asical 0.00 į wert.T Avelding 14 ROAD DERCTS 13 LIGHT 1 - Lees Sheeder Foliow doiled lines to drue outhing of modiway at place of accession.
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STATE OF MICHIGAN - VEHICLE DAMAGE SEVERITY SCALE FOR MICHIGAN TRAFFIC ACCIDENT INVESTIGATORS

Achicle Damage Severity Scale for Michigan Traffic Accident Investigators

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FOREWORD

Since the Michigan Department of State Police has not previously had a specific published guide for use by investigators in evaluating vehicle damage in traffic accidents, the Department is attempting to fill this need with the printing of this booklet in the hope that it will prove to be a valuable tool for all law enforcement officers in Michigan.

Information as presented in this booklet is based on a brochure, "Vehicle Damage Scale for Traffic Accident Investigators", published by the National Safety Council and is produced by the Safety and Traffic Division of the Michigan Department of State Police, with the written approval of the Council, in a format applicable to Michigan.

The Michigan Department of State Police gratefully acknowledges this assistance from the Council and hopes that this booklet will help the investigator prepare a more accurate and comprehensive vehicle damage report in Michigan.

COL. GEORGE L. HALVERSON Director

PURPOSE

Purpose of this manual is to aid investigators in assessing damage sustained by motor vehicles in traffic accidents. By means of a relatively simple procedure, most common types of damage can be rated in terms of a 7-point scale.

Basically, the vehicle damage scale consists of several pages of photographs of automobiles damaged in accidents. There is a separate page for each of the common impacts that investigators are likely to encounter. In order to rate damage on a vehicle, the user must select the proper page of photographs, and then attempt to match the damage on the subject vehicle with one of the photographs appearing on the page.

In the upper left corner of each page facing a photo page, there is a small diagram of a car and an arrow, or series of arrows, showing direction of the principal impact force. In addition to the diagram, there is a number which indicates the part of the vehicle damaged and type of impact. The number is repeated in the upper right corner of the photo page.

On each of the pages in the damage rating section of this appendix, there are 3 photographs, or 3 two-view sets of photographs, showing automobiles damaged in traffic accidents. Numerals on the left page opposite the photographs and intervening spaces are used for indicating severity of damage.

Damage in the top photographs, or sets of photographs, is minor and is generally limited to dents and gouges in body sheet metal and trim. The damage rating corresponding to these photographs is "2".

The second photographs, or sets of photographs, show automobiles that have been moderately damaged, with considerable crumpling of body sheet metal, but little or no distortion of the basic structure or frame. The damage rating in this case is "4".

In the photographs at the bottom of each sheet, vehicles are severely, but not totally damaged. Sheet metal is <u>severely distorted</u>, torn, or crumpled; the basic structure of the car is distorted somewhat; and there is usually some penetration of the passenger compartment. The damage rating is "6".

The reason for the "2, 4 and 6" rating is that an investigator may not be able to match damage on the vehicle on which he is reporting with any of the photographs. In that case, he may use "1, 3, 5 or 7" ratings for damage less or greater than shown in the photographs. Thus with the 3 photographs, he should be able to select any one of seven degrees of severity to describe how badly a car was damaged.

HOW TO USE SCALE

In order to make a damage rating, the investigator must first select the proper page of pictures. The selection will be determined by the type of collision. For example, if he is reporting a broadside collision which occurred at an intersection, and the front end of a vehicle struck another vehicle on its left side, he must refer to the Index to Damage Scale and find the diagram that most nearly describes the impact on the first vehicle. In this case, it may be the diagram which shows impact on the front end (1). For convenlence, the pages are arranged in the same order as their designators appear in the index.

The next step is to compare the damage on the vehicle with the photograph in the selected page. If the front end damage of the first vehicle appears to match that of the bottom photograph on page 1 the damage rating would be "6". The entry in the accident report form would then be 1-6. However, if the damage were more severe, the rating would be 1-7; and, if less severe, 1-5.

The procedure for rating the damage on the car that was struck on its left side is similar. The entry in the accident report would be 7--6 if the vehicle damage appears to match that of the bottomphotograph on page 3 or 7.

Dual designations such as 3/7, 2/8 and 4/6 mean that the pages so labeled may be used for either left or right sides of vehicle to be rated. The investigator should exercise care in writing the rating so that there will be no question as to what side or corner was damaged.

In cases in which vehicles are damaged in more than one area, the investigator should enter the rating of the total damage after vehicle comes to rest. If a vehicle sustained no discernable damage, a "0" (zero) rating with appropriate prefix should be used; e.g., 1-0, 5-0, etc. Such ratings are usually applicable to collisions of motor vehicles with pedestrians and collisions of heavy trucks with light passenger cars.

In the case of trucks and buses, the investigator should be able to make satisfactory ratings on damage to the front end, front quarter, and side impacts in the vicinity of the driver compartment. However, in the case of impacts in other parts of the vehicle, he may rate the damage without pictures to help if he applies the principles established for passenger cars.

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This scale is applicable to damage to front of subject vehicle due to distributed impact resulting from contact with other vehicle or object. ŵ

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Damage Rating









SEVERITY SCALE

Impact 4 or 6 Rear Corner Damage



This scale is applicable to damage resulting from contact with left rear corner of right rear corner of subject vehicle with another vehicle or object. T. Part



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This scale is applicable to damage to side of subject vehicle resulting from an impact by another vehicle or object. ŝ

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SEVERITY SCALE

impact () Top Damage



This scale is applicable to roll-over damage.

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STATE OF MICHIGAN

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POLICE-REPORTED K-A-B-C INJURY SCALE

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THE K, A, B, C INJURY SCALE

= This definition is taken from the 'Manual On =

= Classification Of Motor Vehicle Traffic -

- Accidents, second edition.

Fatal injuries - K

A fatal injury is any injury that results in death within twelve months of the crash.

Incapacitating injuries - A

An incapacitating injury is any injury, other than fatal, which prevents the injured person from walking, driving, or normally continuing the activities which he was capable of performing prior to the crash. Incapacitating injuries include the following: severe lacerations, broken or distorted limbs, skull fracture, crushed chest, internal injuries, unconscious when taken from the scene, and unable to leave scene without assistance.

Hospitalization normally will be required for incapacitating injuries.

Non-incapacitating injuries - B

A non-incapacitating injury is any injury, other than fatal or incapacitating, which is evident to any observer at the scene of the crash. Non-incapacitating injuries include the following: lumps on head, abrasions, and minor lacerations.

Possible injuries - C

A possible injury is any injury reported or claimed, other than fatal, incapacitating, or non-incapacitating evident injuries. Possible injuries include the following: monentary unconsciousness, limping, complaints of pain, nausea, hysteria, and claims of injuries not evident. (Whiplash frequently falls into this catagory.)

No injury

A person is not injured when there is no reason to believe that the person received any bodily injury from the crash. No injury includes the following: confusion, excitement, and anger. FATAL ACCIDENT REPORTING SYSTEM - ACCIDENT REPORT FORMS

US.Department of Transportation

National Highway Traffic Salety Administration

1612 Fetal Accident Reporting System (FAJLE) ACCIDENT LEVEL

O.M.S. No. 2127-6005 STATE CASE NO.

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Hill Form 214 (Rov. 12/01)

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US Department of Transportation

National Highway Traffic Salety Administration

1982 Fetal Accident Reporting System (FARS) VEHICLE/DRIVER LEVEL

Form Approved thru 12/31/83 O.M.B. No. 2127-0006

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1982 Fetal Accident Reporting System (FARS)

Form Approved thru 12/31/83 O.M.B. No. 2127-6006

LLS. Deportment of Tionaportation

National Hiphway Traffic Salety Administration PERSON LEVEL STATE CASE NO. This report is authorized by the Highway Balety Act of 1988, P.L. 89-894. While the law does not require you to respond, the State is obligated under the terms of a grant of funds to defray the expanse of report. ing this information to coop srate in or to make the results of this survey comprehe neive, accurate and timely. 10 11 CONSECU-. CASE NUMBER 1 2 3 . TRANSACTION CODE 7 . CARD NO. PERSON 12 13 MI BARES TIVE NUMBER Munner (Assigned by Analyst) STATE 31—Original Submissio 32—Update or Change 3 1 MARINE PR AGEA CODES) 60 (Assigned by Analyst) NON-MOTORIST STRIKING AGE 16 17 95X 18 14 16 VEHICLE NUMBER Actual Value Amigned Vehicle Humber Except: 2-- Per 60-- Up to One Year 97 -- Ninety-Seven Years or Older B-Linksone -Unic www.weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/weiter.com/ SEATING POSITION 21 20 19 PERSON TYPE 00 - Non-Mouse 11 - Front Sout - Left Side (Driver's Side) - Middle 1- Driver of a Motor Vehicle in Transport 42-2-Passanger of a Motor Vehicle in Transport 12---- Middle - Right Side - Other 4-4-- Right Side - Other 3-Occupant of a Motor Vehicle Not in Transpo ~ Unkno -- Uniu **40**---4-Occupant of a Non-Motor Vehicle Transport Device 18-net -- Left Side -- Middle 80-Siesper Section of Cab (Truck) 21-2 \$1-Other Passanger in Enclosed Non-Occupent --- Pedentris 22-- Right Side - Other - Unknown - Left Side Personger or Cargo Area 82-Other Passanger in Unanci 21_ 8-Non-Occupant -- Bicvolist 7-Non-Occupant - Other Cyclin 28_ Passenger or Cargo Area 83 – Other Passenger in Passenger or Cargo Area, Unknown Whether or E-Non-Occupent - Other or Unknown 21 - Third Seet ----22---8-Unknown Occupant Type in a Motor Vehicle in Ymnepert - Night Side 21.... Not Enclose 64-Trailing Unit - Other **x**-55 - Riding on Vehicle Exterior 2ġ... - Unknow 41-Fourth Sent - Left Side 99-Unknown MANUAL (ACTIVE) RESTRAINT SYSTEM-USE AUTOMATIC (PASSIVE) RESTRAINT SYSTEM -- FUNCTION 22 23 0-Not Equipped or Non-Motorist 1-Automatic Belt in Use 2-Automatic Belt Not in Use 0-- None Uzed - Vehicle Occupant/Not Applicable - Non-Motoriet 1-Stoubler Belt 2-Los Belt 3-Lop and Shoulder Belt 4--Child Safety Sent 3-- Deployed Air Beg 4-- Non-deployed Air Beg 6 -- Motorcycle Haim 8-Unknown 8 - Rastraint Used - Type Unknown or Other including Other Haimet 8-Unknown NON-MOTORIST LOCATION EJECTION EXTRICATION 34 25 28 27 0—Not Extricate 1—Extricated 8—Unknown 60 - Net Applicable -- Vehicle Occurrent 0-Not Ex 1-Totally Sjected 2-Partially Sjected 01 - Intersection - In Crosswell 02-Instruction - On Roadway, Not in Crosswelk 2 03 -- Intersection -- On Roschwey, Crossweik Not Aveilable 04 -- Intersection -- On Roschwey, Crossweik Aveilability Unknown 05 -- Intersection -- Not on Roadway 09 -- Intersection -- Unknown 09 - Hismaction - Unknown 10 - Non-Interaction - In Crosswalk 11 - Non-Intersection - On Roschway, Not in Crosswalk 12 - Non-Intersection - On Roschway, Crosswalk Not Available 13 - Non-Intersection - On Roschway, Crosswalk Available 13 - Non-Intersection - On Roschway, Crosswalk Available 14-Non-Intersection - In Parking Lane 15-Non-Intersection - On Road Shoulder 16-Non-Intersection - Bills Path 17-Non-Intersection - Outside Treffice 18 - Non-Intersection - Other, Not on Reading 19-Non-Interauction - Unknown 99 --- Unknown POLICE REPORTED ALCOHOL INVOLVEMENT ALCOHOL TEST RESULT 28 20 30 . 0-No (Alcohol Not Involved) Actual Value (Decimal Implied before First Digit) (0.xx) 1-Yes (Alcohol Involved) 15-Test Refused 95-None Given 8-Net Reported 8--Unknown (Police Reported) 87-AC Test Performed, Results Unknown 00-Linkness DEATH DATE TAKEN TO HOSPITAL OR BLIUNY SEVERITY 22 23 38 31 TREATMENT FACILITY 0-wio solary (0) 1-- Possible Injury (C) 2-- Nonincepectating Evident Injury (B) 800000 - Not Appli 0-Unknown 0--No 1-- Yes MONTH DAY YEAR 3-Incepacitating Injury (A) 8-Unio 4-Fatal Injury (K) 5-Injured, Severity Union 8-Died Prior to Accident 9-Unknown DEATH TIME 42 **RELATED FACTORS** -43 ø . Allikery Time Except: See Instn ction Menuel "Related Factors-PERSON LEVEL" 0000 -- Not Application 1050 - Linkonsen

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QU.S. G.P.O. 1881- 22-850/71